

# Investigations on one-way coupling effects of particle-laden decaying isotropic turbulent flows

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# 1 Nomenclature

$\eta$	Kolomogorov scale
$\boldsymbol{\tau}$	Stress tensor
$\boldsymbol{I}$	Identity tensor
$\boldsymbol{S}$	Rate-of-strain-tensor
$\mu$	Dynamic viscosity
$\rho$	Density
$\rho_p$	Particle density
$\tau_{m\text{athrm}p}$	Particle response time
$\boldsymbol{\nabla}$	Nabla-operator
$\boldsymbol{u}$	Three-dimensional velocity
$\boldsymbol{a}$	particle acceleration
$\boldsymbol{H}^i$	Stores the inviscid variables in the flux-vector included in the Navier-Stokes equations
$\boldsymbol{H}^v$	Stores the viscous variables in the flux-vector included in the Navier-Stokes equations
$\boldsymbol{H}$	Container for fluctuating variables in the Navier-Stokes equations
$\boldsymbol{Q}$	Container for conserved variables in the Navier-Stokes equations
$\boldsymbol{q}$	Heat conduction
$\boldsymbol{v}_p$	Particle velocity
$\boldsymbol{v}$	particle velocity
$\boldsymbol{x}_p$	Particle position
$\boldsymbol{x}$	particle position
$c_p$	Specific isobaric heat capacity
$c_v$	Specific isochoric heat capacity
$E$	Specific inner energy
$e$	Specific internal energy
$f_{m\text{athrm}D}$	Drag correction
$k_t$	thermal conductivity
$m_c$	number of clustered particles

$p$	Pressure
$Pr$	Prandtl number
$R$	Universal gas constant
$r_p$	Particle radius
$Re$	Reynolds number
$S$	Sutherland temperature
$T$	Temperature

## 2 Introduction

in Computational Methods for Multiphase Flow ist auf den Seiten 3-9 ein interessantes Beispiel. Sollen wir hier außerdem noch ein Bild von einer turbulenten Strömung einfügen?

### 3 Mathematical models

Zusammenfassung mathematische Modelle

#### 3.1 Single-phase flow

In this section the mathematical basics for understanding and simulating turbulent flows are discussed. However, it should be pointed out that this is no complete treatise of the mathematical and physical basics. The reader can achieve further insight on this topic by looking at different books and papers, e.g. [7].

##### 3.1.1 The Navier-Stokes equations

The Navier-Stokes-Equations are of great importance for understanding turbulent phenomena. This set of equations exists in forms for compressible and incompressible fluids. For an infinitesimal small volume element  $d\tau$  and using the cartesian coordinate system, they can be written in the so-called 'divergence form':

$$\frac{\partial \mathbf{Q}}{\partial t} + \nabla \mathbf{H} = 0 \quad (3.1)$$

It should be noted by the reader that this work only contains investigations about chemically inert fluids and particles, and that the simulation results only fit under this condition. The vector  $\mathbf{Q}$  contains all the variables which are conserved, i.e. the density  $\rho$ , the velocity  $\mathbf{u}$  and the specific inner energy  $E$ :

$$\mathbf{Q} = \begin{pmatrix} \rho \\ \rho \mathbf{u} \\ \rho E \end{pmatrix} \quad (3.2)$$

$\mathbf{H}$  is the flux vector which stores all the floating variables and may be split up into two parts:

$$\mathbf{H} = \mathbf{H}^i + \mathbf{H}^v \quad (3.3)$$

The contents of the two vectors are displayed below:

$$\mathbf{H}^i = \begin{pmatrix} \rho \mathbf{u} \\ \rho \mathbf{u} \mathbf{u} + p \\ \mathbf{u}(\rho E + p) \end{pmatrix} \quad (3.4)$$

$$\mathbf{H}^v = -\frac{1}{Re} \begin{pmatrix} 0 \\ \boldsymbol{\tau} \\ \boldsymbol{\tau} \mathbf{u} + \mathbf{q} \end{pmatrix} \quad (3.5)$$

$\mathbf{H}^i$  is called inviscid flux and contains only the variables that are independent of the fluids viscosity, it describes the way a fluid with zero viscosity would behave. In contrast, the viscous flux  $\mathbf{H}^v$  represents the effects of viscosity. The Reynolds number  $Re = \frac{\rho v d}{\eta}$  is defined to be the ratio of inertia to tenacity, which makes it very valuable for understanding turbulent flows. This is also due to the fact that two familiar objects with the same Reynolds number behave similar in turbulence. One can assume that flows with  $Re \ll 1$  are laminar and

flows with  $Re \gg 1$  are turbulent. To solve the Navier-Stokes-Equations, more information regarding some variables is required. For Calculating the specific inner Energy  $E$  and the heat conduction  $\mathbf{q}$ , the following equations are used:

$$E = e \frac{1}{2} |\mathbf{u}|^2 \quad (3.6)$$

$$\mathbf{q} = -\frac{\mu}{Pr(\gamma - 1)} \nabla T \quad (3.7)$$

with

$$\gamma = \frac{c_p}{c_v} \quad (3.8)$$

and the Prandtl number

$$Pr = \frac{\mu_\infty c_p}{k_t} \quad (3.9)$$

using the specific heat capacities of the fluid  $c_v$  and  $c_p$ . If one could assume that the fluid is a newtonian fluid, the linear correlation between stress and the rate of strain results in:

$$\boldsymbol{\tau} = 2\mu \mathbf{S} - \frac{2}{3}\mu(\nabla \cdot \mathbf{u})\mathbf{I} \quad (3.10)$$

in which  $\mathbf{S} = \frac{(\nabla \mathbf{u})(\nabla \mathbf{u})^T}{2}$  denotes the rate-of-strain-tensor. Additionally, the viscosity  $\mu$  can be approximated through Sutherland's law, which is based on the ideal gas-theory:

$$\mu(T) = \mu_\infty \left(\frac{T}{t_\infty}\right)^{3/2} \frac{T_\infty + S}{T + S} \quad (3.11)$$

$S$  is in this case the Sutherland temperature. To achieve closure the caloric state equation  $e = c_v T$  and the state equation for an ideal gas  $p = \rho R T$  are used. The specific gas constant is determined by  $R = c_p - c_v$ . These equations form a set of partial differential equations, so for solving them starting values are needed. These are initialized at the first timestep of the simulation. To achieve physical solutions, 150 timesteps are computed before the particles are initialized, so the turbulence can evolve from the synthetic values to a natural flow field.

Christoph Siewert: -2.1 bis 2.6 Stephan Fritz: -Navier-Stokes-Gleichungen (Anhang B) Randbedingungen?

### 3.2 Particle dynamics

Siewert: -3.1a-3.14 (spherical particles) OHNE GRAVITATION Stokes Drag/Stokes Coefficient Filterung (Fritz) -; Viskosität durch numerischen Fehler, Smagorinsky nicht benutzen

Cause this work deals with particle laden fluids and the impact of these particles on the flow conditions, we need to describe the interaction between them. We deal with small and heavy, rigid particles, that have a spherical shape. Their radius  $r_p$  is even smaller than the Kolmogorov scale  $\eta$ , but also large enough to neglect the Brownian motion. Due to the small particle concentration, the best and most common way to describe these flows is the point particle approach, which means that every particle is treated as an mathematical point source of mass, momentum and energy. In this case we focus on the momentum exchange. Effects like particle-particle interactions, particle-wall interactions are also neglected. At describing the motion of the particles in the following the fact, that we deal with gas-solid flows is an advantage, since we can make several simplifications. First we look at the influence of the particles on the carrier fluid. Here we make the assumption, that the fluid is incompressible and the mass exchange over the particle surface is zero. Hence the continuity equation becomes:

$$\nabla \cdot \mathbf{u} = 0 \quad (3.12)$$

. The Navier Stokes equation, described in chapter 1, becomes:

$$\rho \frac{D\mathbf{u}}{Dt} = -\nabla p + \nabla \cdot \boldsymbol{\tau} + \mathbf{F} \quad (3.13)$$

The influence of the particles on the fluid is represented by the new term  $\mathbf{F}$ , which describes the force per unit volume on the fluid. We could approximate  $\mathbf{F}$  by a superposition of Dirac's delta functions over all particles, centered at the location  $\mathbf{x}_p^n$  of each particle:

$$\mathbf{F} = \sum_n \mathbf{f}^n \delta(\mathbf{x} - \mathbf{x}_p^n) \quad (3.14)$$

$\mathbf{x}_p^n$  is the position of the n-th particle and results from the kinematic equation

$$\frac{d\mathbf{x}_p}{dt} = \mathbf{v}_p \quad (3.15)$$

$\mathbf{v}_p$  is the velocity of the n-th particle.  $\mathbf{f}^n$  is the sum of forces acting between fluid and particles. Hence it plays also an important role in the equation of motion of the particles:

$$v_p \frac{d\mathbf{v}_p^n}{dt} = v_p \frac{d\mathbf{v}_p^n}{dt} = \mathbf{g} + \mathbf{f}^n(\mathbf{x}_p^n) \quad (3.16)$$

As already mentioned  $\mathbf{f}^n(\mathbf{x}_p^n)$  could be divided in several forces. Then the equation of motion looks like:

$$v_p \frac{d\mathbf{v}_p^n}{dt} = \mathbf{g} + \mathbf{f}_d + \mathbf{f}_l + \mathbf{f}_a + \mathbf{f}_h + \mathbf{f}_{\text{additional}} \quad (3.17)$$

Here  $\mathbf{f}_d$  represents the hydrodynamical drag force that is parallel to the undisturbed streamlines, which depends on an empirical drag coefficient  $C_d$ :

$$\mathbf{f}_d = -\frac{3}{4} \rho v_p \frac{C_d}{d} |\mathbf{v}_p - \mathbf{u}| (\mathbf{v}_p - \mathbf{u}) \quad (3.18)$$



$\mathbf{u}$  is the velocity of the uniform stream, which is enough away from the particle that it is undisturbed from the particle. The other partial hydrodynamical force, the lift force  $\mathbf{f}_l$  is perpendicular to the undisturbed streamlines. Furthermore the added mass force  $\mathbf{f}_a$  represents the influence of the inertia of the fluid that has an impact on the particle, if it has a different acceleration than the mean flow. Hence it could be determined by:

$$\mathbf{f}_a = \frac{1}{2} * \rho * v_v * \left( \frac{D * \mathbf{u}}{D * t} - \frac{d * \mathbf{v}_p}{d * t} \right) \quad (3.19)$$

—nie  $\mathbf{v}$  sondern immer  $\mathbf{v}_p$  benutzen— The history force  $\mathbf{f}_h$  takes diffusion and convection, that results out of the vortices behind the particles, into account. We look at Basselt's result, neglecting the finite size correction that is proportional to  $\nabla^2 * \mathbf{u}$ :

$$\mathbf{f}_h = \frac{3}{2} * d^2 * \rho * \sqrt{\pi * \nu} * \int_t^0 \frac{dt'}{(t - t')^{1/2}} \left( \frac{D\mathbf{u}}{Dt'} - \frac{d\mathbf{v}_p}{dt'} \right) \quad (3.20)$$

In our case of gas-solid suspensions we can make several simplifications. In the following we show with an rough approximation that the added mass and history forces are negligible compared with the drag force. We use the approach that the relative velocity is of the same order as the terminal velocity  $v_t$ . The terminal velocity is the velocity of a particle in a resting fluid, when gravitation and drag force are in equilibrium. Then if the added mass and the drag force are compared, we get the following equation:

$$\frac{|\mathbf{f}_a|}{|\mathbf{f}_d|} \simeq \frac{\frac{1}{2} * \rho * v_v * g}{\frac{3}{4} * \rho * v_v * (C_d/d) * v_t^2} \frac{a_r}{g} = \frac{1}{2} * \frac{\rho}{\rho_p} * \frac{a_r}{g} \quad (3.21)$$

with

$$a_r = \left( \frac{D\mathbf{u}}{Dt} - \frac{d\mathbf{v}_p}{dt} \right) \quad (3.22)$$

Since in gas-solid suspensions the particle density is of an factor of 1000 higher than the fluid density, it shows that, if it's not the unlikely case that the relative acceleration is of the same order higher than the gravity, the added mass force is negligible compared to the drag force. The effect that fluid and particle influence each other is called two-way-coupling.  $\mathbf{f}_d$  and lift forces,  $\mathbf{f}_a$  the added mass and  $\mathbf{f}_h$  the history forces. The last term  $\mathbf{f}_{\text{additional}}$  is attached for the case that we have to take other forces like electrostatic interactions into account.

-coupling Zahl

The relaxation time  $\tau_p$  physically represents the time scale over which the drag force decreases the particle relative velocity to zero and is determined by the following equation:

$$\tau_p = \frac{\rho_p}{\rho} * \frac{2 * r_p^2}{9 * \nu} \quad (3.23)$$

Since we consider gas-solid flows, wich means we can use a point particle approach make some simplifcantions in the following To get a usefull equation of motion for the particles in the flow, we use the Euler Lagrangian approach, as it is common in Direct Numerical Simulations (DNS) and Large Eddy Simulations (LES). The density of the particles  $\rho_p$  is much higher than that of the fluid  $\rho_f$ . In addition due to the very low particle concentration we can neglect the

influence of the particles on each other. That means that they cross each other without any effect. That means particle collision is neglected. After all these simplifications we obtain a simplified version of the Maxey-Riley equations.

$$\frac{\partial \mathbf{x}_p}{\partial t} = \mathbf{v}_p \quad (3.24)$$

$$\frac{\partial \mathbf{v}_p}{\partial t} = \frac{f_D}{\tau_p} (\mathbf{u}(\mathbf{x}_p) - \mathbf{v}_p) \quad (3.25)$$

$\tau_p$  is the particle response time and a factor to obtain the drag force in Stokes flow conditions. To take the case of a Reynolds number  $\mathcal{R}$  of order 1 into account the correction factor  $f_D = 1 + 0.15\mathcal{R}(0.687)$  is used. The biggest simplification of this Lagrangian approach is that the interaction of particles coming close together is neglected.

## 4 Numerical methods

To simulate flows like those described above we have two options. The direct numerical simulation (DNS) is the easier one to understand, although it is numerically very expensive. The Large-eddy simulation (LES) is numerically more capable, still we must accept certain inaccuracies. These two numerical methods are now discussed in the following chapter.

### 4.1 Direct numerical simulation

The basis of the direct numerical simulation (DNS) are the Navier-Stokes equations as described above. The idea is that the computer is very good at calculating and solves these equations completely. This provides a very accurate result, as all scales of motion are being resolved. Still it requires an immense level of computational resources which increases rapidly with the Reynolds number. These computational resources were not available until the 1970s. Even though it is not advisable to resolve every scale of motion, if only the contained energy is of greatest interest. With the large-eddy simulation, as described below, the computational effort is 99.98 % less compared to DNS, which indeed is the fraction of the dissipative scale. This leaves 0.02 % of the flow, which is correlative with the fraction of the energy-containing larger-scale [7].

### 4.2 Large-eddy simulation

Due to the fact that DNS is effortful and wasting resources if a fully resolved resolution is not required, large-eddy simulation (LES) was created to save time and resources. This is especially efficient if mainly the temporal energy trend is considered, because the energy containing larger-scale motion is completely resolved and the indeed small effects of the expensive smaller-scale motion are just modelled. Otherwise in DNS resolving the small dissipative scale would require most of the computational resources.

Simulating only the larger-scale motions is also called filtering, which means that the smaller-scale motions are filtered out. To model the filtered smaller-scale motions usually a subgrid-scale (SGS) model is used. According to Hickel (2007) the interference between explicit SGS and the truncation error can be exploited, i.e. the truncation error can serve as model of the effects of unresolved scales, which is therefore an implicit SGS model. Thus we call it implicit LES (ILES) [5].

### 4.3 Discretisation

To integrate the Lagrangian particle tracking equations, discussed above, a predictor-corrector scheme based on the trapezoidal rule for numerical integration

$$f(t + \delta t) \approx f(t) + \frac{\delta t}{2} \left[ \frac{\partial f(t)}{\partial t} + \frac{\partial f(t + \delta t)}{\partial t} \right] \quad (4.1)$$

is used.

The first step is the prediction of the new particle position  $\mathbf{x}_{n+1}^{(p)}$  using a Taylor

expansion for a small time step  $\delta t$

$$\mathbf{x}_{n+1}^{(p)} = \mathbf{x}_n + \delta t \mathbf{v}_n + \frac{1}{2} \delta t^2 \mathbf{a}_n. \quad (4.2)$$

Due to the computational effort we will put  $\mathbf{u}_{n+1}^{(p)}$  on the level of the nearest cell fluid velocity.

The updated velocity and acceleration are calculated as

$$\mathbf{v}_{n+1} = \frac{\mathbf{v}_n + \frac{1}{2} \delta t \left( \mathbf{a}_n + \frac{f_D}{\tau_p} \mathbf{u}_{n+1}^{(p)} + \mathbf{g} \right)}{1 + \frac{1}{2} \frac{f_D}{\tau_p} \delta t}, \quad (4.3)$$

$$\mathbf{a}_{n+1} = \frac{\frac{f_D}{\tau_p} \left( \mathbf{u}_{n+1}^{(p)} - \mathbf{v}_n - \frac{1}{2} \delta t \mathbf{a}_n \right) + \mathbf{g}}{1 + \frac{1}{2} \frac{f_D}{\tau_p} \delta t}. \quad (4.4)$$

The updated particle position must be corrected by an additional term according to the trapezoidal rule

$$\mathbf{x}_{n+1} = \mathbf{x}_n + \frac{1}{2} \delta t (\mathbf{v}_{n+1} + \mathbf{v}_n) + \frac{1}{12} \delta t^2 (\mathbf{a}_{n+1} - \mathbf{a}_n). \quad (4.5)$$

#### 4.4 Particle clustering

The high number of point particles require even more computational resources for the particle-laden simulation. The main idea to reduce this requirement is to create clusters of point particles, meaning that a new variable  $m_c$  is introduced. We consider a cluster of  $m_c$  point particles as one larger point particle, i.e. the programm has less particles to simulate. To compensate this lack of particles, the coupling force is multiplied by  $m_c$ , due to the  $m_c$ -fold mass of the (cluster-)particles. In chapter 5 (results) we evaluate the legitimacy of particle clustering and the maximum acceptable value of  $m_c$ .

Projektion (noComputationalParticles), Diskretisierung implizite LES (Motivation fuer LES - Pope Chapter 9, Bild 9.4), DNS

## 5 Results

### 5.1 Boundary conditions and simulation properties

The simulations were carried out using ZFS, the simulation tool developed and implemented at the Institute of Aerodynamics at RWTH Aachen University [1] [2]. The tool is capable of simulating finite-volume flows of compressible fluids. In this case the turbulence was simulated on a cubic grid using  $64^3$ ,  $96^3$ ,  $128^3$  and  $256^3$ . The first three cases were simulated using LES, the case in which  $256^3$  cells were used is carried out as DNS. Further information can be gained by looking at [7, p.344-357 for DNS and p. 558-639 for LES]. For simplification, the special case of isotropic turbulence was used. For this idealised flow form the statistical velocities are invariant in all directions of the grid. It follows that the flows velocity are invariant for rotations and reflections. The turbulence was initialised using a seed-based random generator. To achieve physical results, the simulation was carried out to timestep 150, at which a restart file was written out. This procedure insures a fully developed turbulent flow, which has emancipated from the initialisation. In this flow field, a specific number of spherical particles were injected. The velocities of the fluid were interpolated for each particle to match the velocities of particles and fluid as accurately as possible.

Case	$Re$	$Re_\lambda$	$Re_\lambda(restart)$	$cfl$	timesteps	$m_c$	particle Diameter
64	?	?	?	?	?	?	?
96	?	?	?	?	?	?	?
128	?	?	?	?	?	?	?
264	?	?	?	?	?	?	?

Table 1: Example of a table

See table 1 on page 13 for the example table. boundary conditions, for example Reynolds number?

Graphen (particleFree rot, Laden gruen)

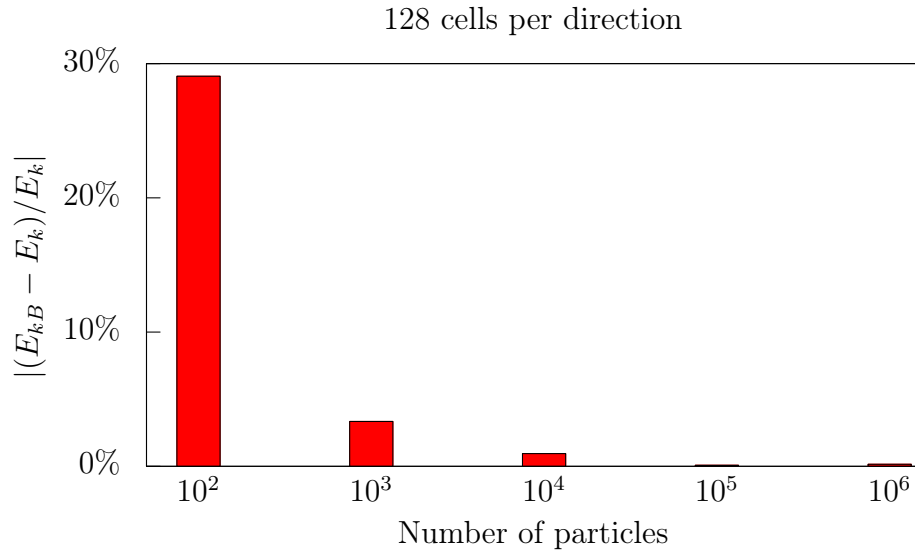


Figure 1: Include Caption

## 6 Conclusion

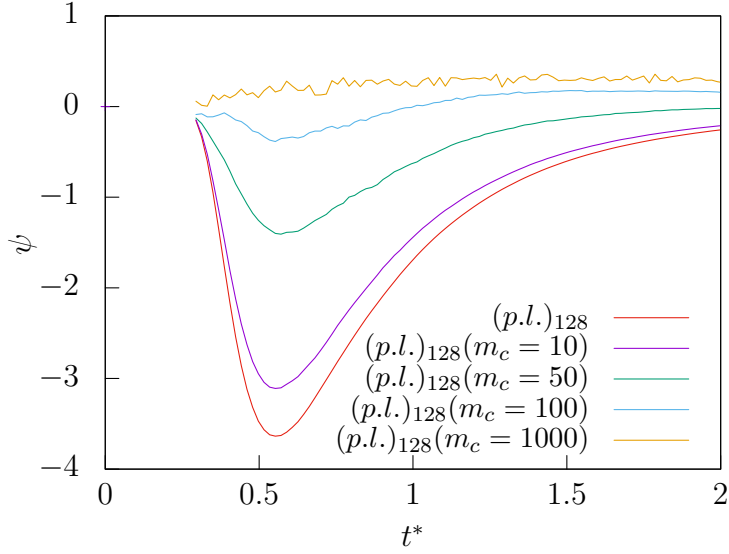


Figure 2: Include Caption

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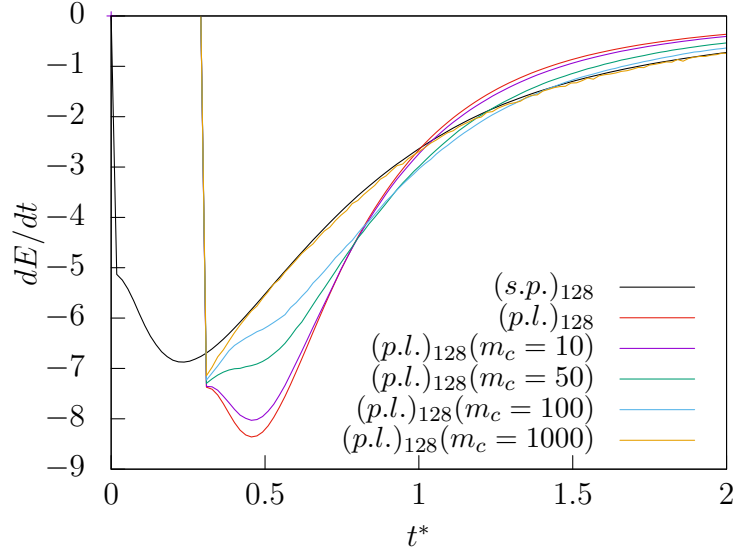


Figure 3: Include Caption

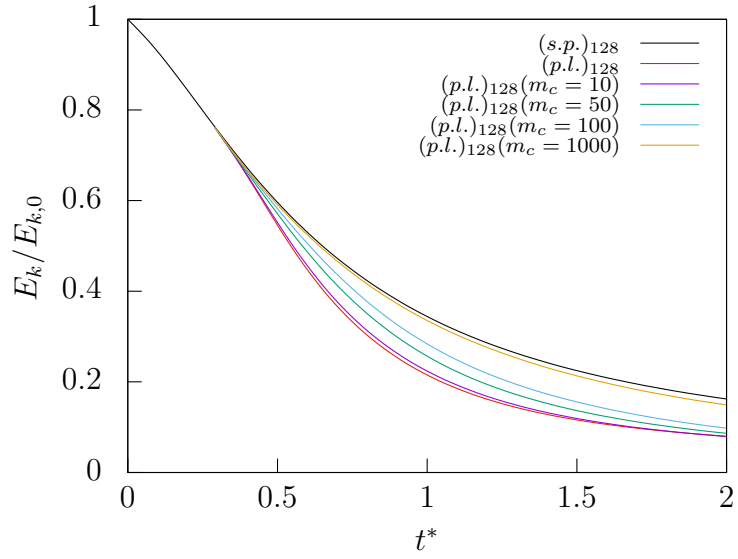


Figure 4: Include Caption