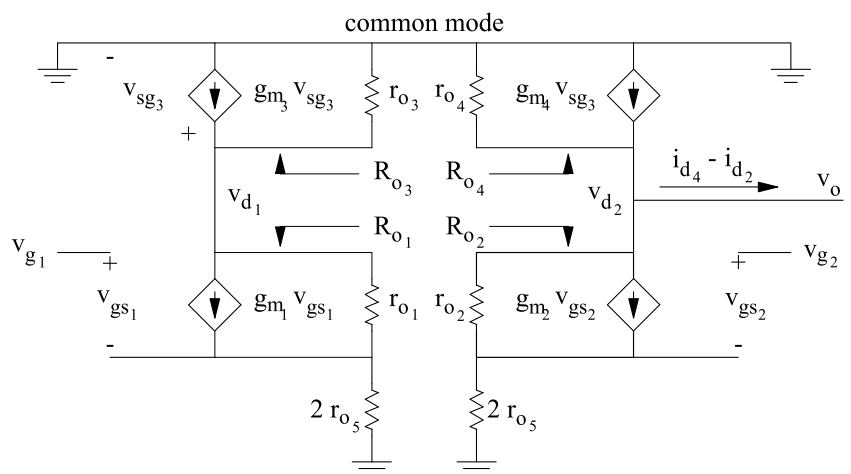
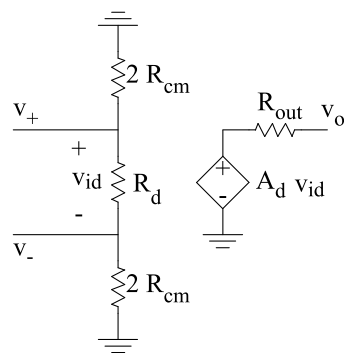
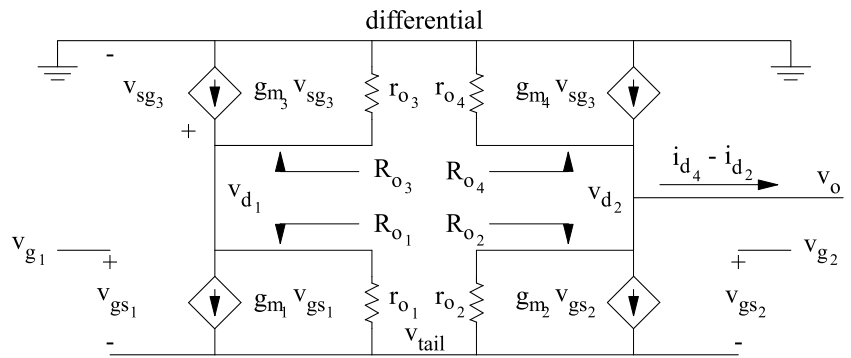
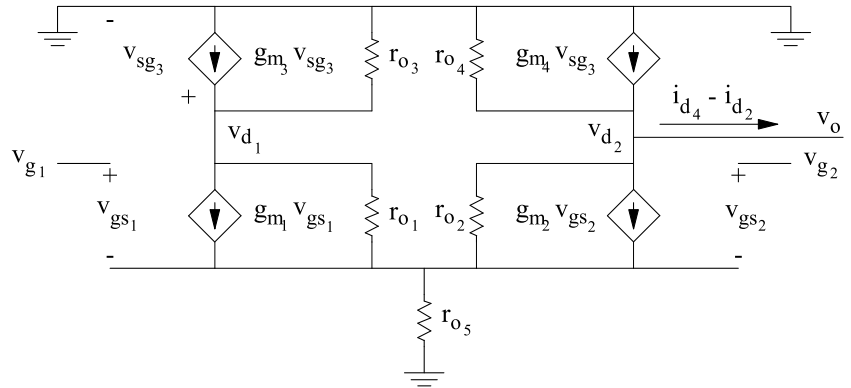
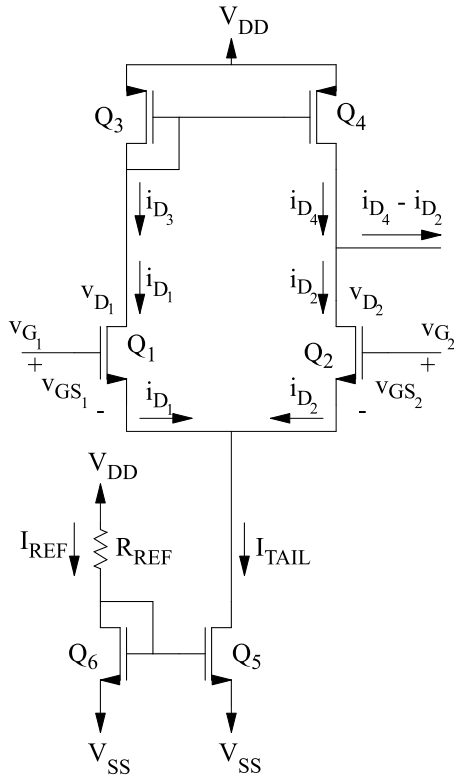


MOS transistor differential amplifiers

low frequency operation with active load



for differential operation (ignoring r_{o1} , r_{o2} , r_{o3} , r_{o4} on the current mirror action)

$$v_{id} = v_{g1} - v_{g2} \quad ; \quad v_{g1} = +\frac{v_{id}}{2} \quad ; \quad v_{g2} = -\frac{v_{id}}{2} \quad ; \quad i_{d3} = i_{d1} = g_{m1} \left(+\frac{v_{id}}{2} \right) \quad ; \quad i_{d2} = g_{m2} \left(-\frac{v_{id}}{2} \right)$$

$$v_{sg3} = \frac{i_{d3}}{g_{m3}} = \frac{g_{m1} \left(\frac{v_{id}}{2} \right)}{g_{m3}} = \frac{g_{m1}}{g_{m3}} \frac{v_{id}}{2} \quad ; \quad i_{d4} = g_{m4} v_{sg3} = g_{m4} \frac{g_{m1}}{g_{m3}} \frac{v_{id}}{2} = g_{m1} \frac{g_{m4}}{g_{m3}} \frac{v_{id}}{2} = g_{m1} \frac{v_{id}}{2}$$

$$i_o = i_{d4} - i_{d2} = \left(g_{m1} \frac{v_{id}}{2} \right) - \left(g_{m2} \left(-\frac{v_{id}}{2} \right) \right) = \left(g_{m1} \frac{v_{id}}{2} \right) + \left(g_{m2} \frac{v_{id}}{2} \right) = 2 g_{m1} \frac{v_{id}}{2} = g_{m1} v_{id}$$

$$A_d \equiv \frac{v_o}{v_{id}} = g_{m1} \left(r_{o2} \parallel r_{o4} \right)$$

for common mode operation (ignoring r_{o1} , r_{o2} , r_{o3} , r_{o4} on the current mirror action)

$$v_{icm} = \frac{v_{g1} + v_{g2}}{2} \quad ; \quad R_{o1} = r_{o1} + \left(1 + g_{m1} r_{o1} \right) 2 r_{o5} \quad ; \quad R_{o2} = r_{o2} + \left(1 + g_{m2} r_{o2} \right) 2 r_{o5} \quad ; \quad R_{o3} = \frac{1}{g_{m3}} \quad ; \quad R_{o4} = r_{o4}$$

$$R_{out} = R_{o4} \parallel R_{o2} = \left(r_{o4} \right) \parallel \left(r_{o2} + \left(1 + g_{m2} r_{o2} \right) 2 r_{o5} \right) \approx r_{o4}$$

$$i_{d3} = i_{d1} = \frac{v_{icm}}{\frac{1}{g_{m1}} + 2 r_{o5}} = \frac{g_{m1} v_{icm}}{1 + 2 g_{m1} r_{o5}} \quad ; \quad i_{d2} = \frac{v_{icm}}{\frac{1}{g_{m2}} + 2 r_{o5}} = \frac{g_{m2} v_{icm}}{1 + 2 g_{m2} r_{o5}} \quad ; \quad i_{d4} = \frac{g_{m4}}{g_{m3}} i_{d3} = \frac{g_{m4}}{g_{m3}} \frac{g_{m1} v_{icm}}{1 + 2 g_{m1} r_{o5}}$$

$$i_o = i_{d4} - i_{d2} = \left(\frac{g_{m4}}{g_{m3}} \frac{g_{m1} v_{icm}}{1 + 2 g_{m1} r_{o5}} \right) - \left(\frac{g_{m2} v_{icm}}{1 + 2 g_{m2} r_{o5}} \right) = \left(\left(\frac{g_{m4}}{g_{m3}} \frac{g_{m1}}{1 + 2 g_{m1} r_{o5}} \right) - \left(\frac{g_{m2}}{1 + 2 g_{m2} r_{o5}} \right) \right) v_{icm}$$

$$v_o = i_o R_{out} \quad ; \quad A_{cm} \equiv \frac{v_o}{v_{icm}} = \left(\left(\frac{g_{m4}}{g_{m3}} \frac{g_{m1}}{1 + 2 g_{m1} r_{o5}} \right) - \left(\frac{g_{m2}}{1 + 2 g_{m2} r_{o5}} \right) \right) r_{o4}$$

$$CMRR \equiv \frac{A_d}{A_{cm}} = \frac{\left(\frac{g_{m1} g_{m4}}{g_{m3}} \right) \left(r_{o2} \parallel r_{o4} \right)}{\left(\left(\frac{g_{m4}}{g_{m3}} \frac{g_{m1}}{1 + 2 g_{m1} r_{o5}} \right) - \left(\frac{g_{m2}}{1 + 2 g_{m2} r_{o5}} \right) \right) r_{o4}} \approx \frac{g_{m1} \left(r_{o2} \parallel r_{o4} \right)}{\left(\frac{1}{2 r_{o5}} - \frac{1}{2 r_{o5}} \right) r_{o4}} = \infty$$

for differential operation (including r_{o1} , r_{o2} , r_{o3} , r_{o4} in the current mirror action)

$$i_{d1} = g_{m1} \left(+ \frac{v_{id}}{2} \right) \quad ; \quad i_{d2} = g_{m2} \left(- \frac{v_{id}}{2} \right)$$

$$v_{sg3} = \frac{i_{d1}}{g_{m3} + \frac{1}{r_{o1}} + \frac{1}{r_{o3}}} = i_{d1} \left(\frac{r_{o1} r_{o3}}{g_{m3} r_{o1} r_{o3} + r_{o1} + r_{o3}} \right) = \left(g_{m1} \frac{v_{id}}{2} \right) \left(\frac{r_{o1} r_{o3}}{g_{m3} r_{o1} r_{o3} + r_{o1} + r_{o3}} \right)$$

$$i_{d4} = g_{m4} v_{sg3} = g_{m4} \left(\left(g_{m1} \frac{v_{id}}{2} \right) \left(\frac{r_{o1} r_{o3}}{g_{m3} r_{o1} r_{o3} + r_{o1} + r_{o3}} \right) \right) = \frac{g_{m1} g_{m4} r_{o1} r_{o3}}{g_{m3} r_{o1} r_{o3} + r_{o1} + r_{o3}} \frac{v_{id}}{2}$$

$$i_o = i_{d4} - i_{d2} = \left(\frac{g_{m1} g_{m4} r_{o1} r_{o3}}{g_{m3} r_{o1} r_{o3} + r_{o1} + r_{o3}} \frac{v_{id}}{2} \right) - \left(g_{m2} \left(- \frac{v_{id}}{2} \right) \right) = \frac{g_{m1} g_{m4} r_{o1} r_{o3}}{g_{m3} r_{o1} r_{o3} + r_{o1} + r_{o3}} \frac{v_{id}}{2} + g_{m2} \frac{v_{id}}{2}$$

$$v_o = i_o R_{out} = \left(\frac{g_{m1} g_{m4} r_{o1} r_{o3}}{g_{m3} r_{o1} r_{o3} + r_{o1} + r_{o3}} \frac{v_{id}}{2} + g_{m2} \frac{v_{id}}{2} \right) (r_{o2} \parallel r_{o4})$$

$$A_d \equiv \frac{v_o}{v_{id}} = \frac{1}{2} \left(\frac{g_{m1} g_{m4} r_{o1} r_{o3}}{g_{m3} r_{o1} r_{o3} + r_{o1} + r_{o3}} + g_{m2} \right) (r_{o2} \parallel r_{o4})$$

for common mode operation (including $r_{o1}, r_{o2}, r_{o3}, r_{o4}$ in the current mirror action)

$$\begin{aligned}
 i_{d1} &= \frac{V_{icm}}{\frac{1}{g_{m1}} + 2 r_{o5}} = \frac{g_{m1} V_{icm}}{1 + 2 g_{m1} r_{o5}} \quad ; \quad i_{d2} = \frac{V_{icm}}{\frac{1}{g_{m2}} + 2 r_{o5}} = \frac{g_{m2} V_{icm}}{1 + 2 g_{m2} r_{o5}} \\
 v_{sg3} &= \frac{i_{d1}}{g_{m3} + \frac{1}{R_{o1}} + \frac{1}{R_{o3}}} = \frac{i_{d1}}{g_{m3} + \frac{1}{r_{o1} + \left(1 + g_{m1} r_{o1}\right) 2 r_{o5}} + \frac{1}{r_{o3}}} \approx \frac{i_{d1}}{g_{m3} + \frac{1}{r_{o3}}} \\
 &= \frac{i_{d1} r_{o3}}{1 + g_{m3} r_{o3}} = \frac{\frac{g_{m1} V_{icm}}{1 + 2 g_{m1} r_{o5}} r_{o3}}{1 + g_{m3} r_{o3}} = \frac{g_{m1} r_{o3} V_{icm}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})} \\
 i_{d4} &= g_{m4} v_{sg3} = g_{m4} \frac{g_{m1} r_{o3} V_{icm}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})} = \frac{g_{m1} g_{m4} r_{o3} V_{icm}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})} \\
 i_o &= i_{d4} - i_{d2} = \left(\frac{g_{m1} g_{m4} r_{o3} V_{icm}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})} \right) - \left(\frac{g_{m2} V_{icm}}{1 + 2 g_{m2} r_{o5}} \right) \\
 &= \left(\frac{g_{m1} g_{m4} r_{o3}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})} - \frac{g_{m2}}{1 + 2 g_{m2} r_{o5}} \right) V_{icm} \\
 v_o &= i_o R_{out} \quad ; \quad A_{cm} \equiv \frac{v_o}{V_{icm}} = \frac{g_{m1} g_{m4} r_{o3}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})} - \frac{g_{m2}}{1 + 2 g_{m2} r_{o5}} \\
 CMRR &\equiv \frac{A_d}{A_{cm}} = \frac{\frac{1}{2} \left(\frac{g_{m1} g_{m4} r_{o1} r_{o3}}{g_{m3} r_{o1} r_{o3} + r_{o1} + r_{o3}} + g_{m2} \right) (r_{o2} \parallel r_{o4})}{\frac{g_{m1} g_{m4} r_{o3}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})} - \frac{g_{m2}}{1 + 2 g_{m2} r_{o5}}}
 \end{aligned}$$

for common mode operation (including r_{o1} , r_{o2} , r_{o3} , r_{o4} in the current mirror action and g_{mb1} , g_{mb2})

$$i_{d1} = \frac{v_{icm}}{\frac{1}{g_{m1}} + 2 r_{o5}} + g_{mb1} v_{icm} = \left(\frac{g_{m1}}{1 + 2 g_{m1} r_{o5}} + g_{mb1} \right) v_{icm}$$

$$i_{d2} = \frac{v_{icm}}{\frac{1}{g_{m2}} + 2 r_{o5}} + g_{mb2} v_{icm} = \left(\frac{g_{m2}}{1 + 2 g_{m2} r_{o5}} + g_{mb2} \right) v_{icm}$$

$$v_{sg3} = \frac{i_{d1}}{g_{m3} + \frac{1}{R_{o1}} + \frac{1}{R_{o3}}} = \frac{i_{d1}}{g_{m3} + \frac{1}{r_{o1} + \left(1 + g_{m1} r_{o1} \right) 2 r_{o5}} + \frac{1}{r_{o3}}} \approx \frac{i_{d1}}{g_{m3} + \frac{1}{r_{o3}}} = \frac{i_{d1} r_{o3}}{1 + g_{m3} r_{o3}}$$

$$= \frac{\left(\left(\frac{g_{m1}}{1 + 2 g_{m1} r_{o5}} + g_{mb1} \right) v_{icm} \right) r_{o3}}{1 + g_{m3} r_{o3}} = \frac{\left(g_{m1} + (1 + 2 g_{m1} r_{o5}) g_{mb1} \right) r_{o3} v_{icm}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})}$$

$$i_{d4} = g_{m4} v_{sg3} = g_{m4} \frac{\left(g_{m1} + (1 + 2 g_{m1} r_{o5}) g_{mb1} \right) r_{o3} v_{icm}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})}$$

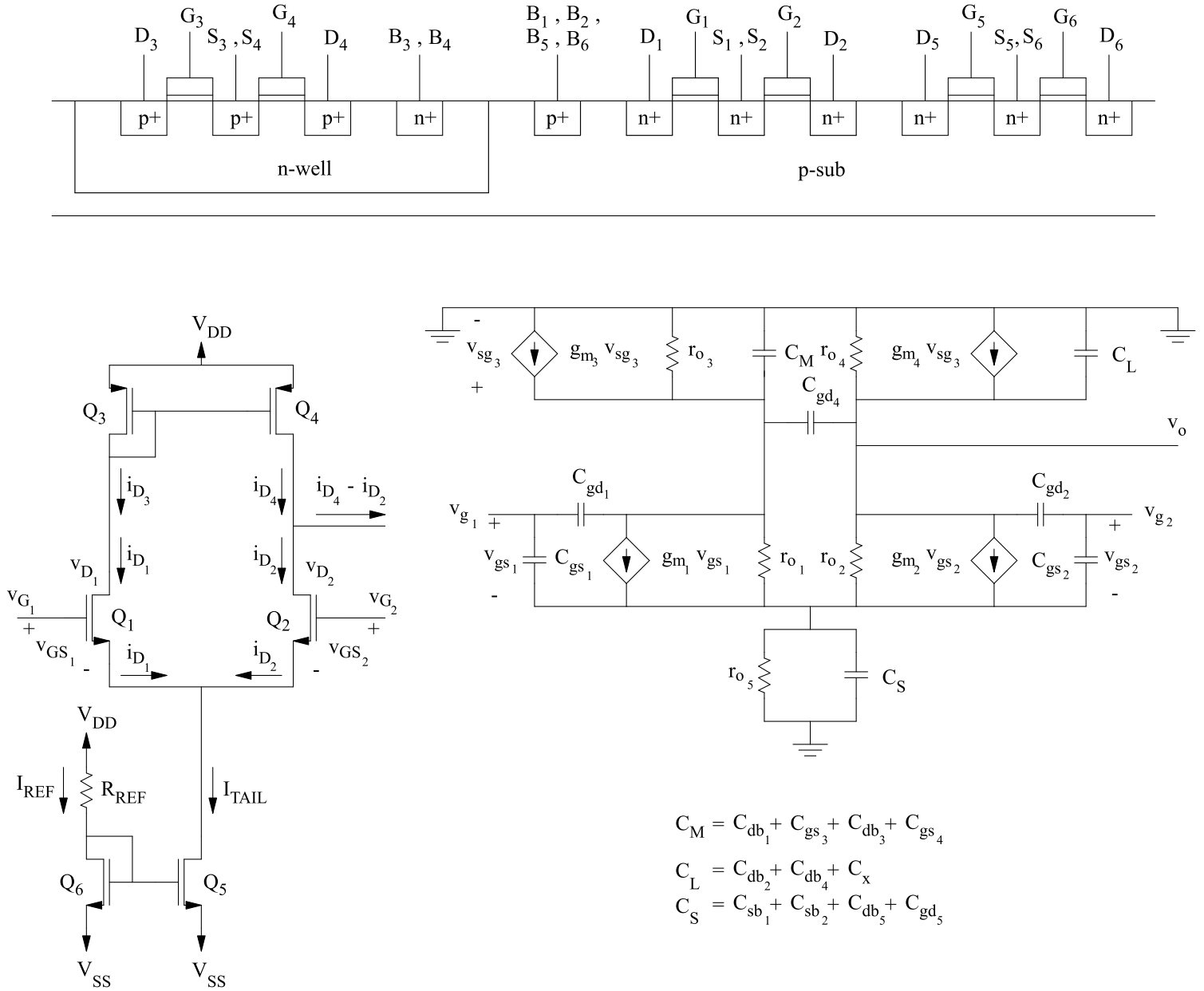
$$i_o = i_{d4} - i_{d2} = \left(g_{m4} \frac{\left(g_{m1} + (1 + 2 g_{m1} r_{o5}) g_{mb1} \right) r_{o3} v_{icm}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})} \right) - \left(\left(\frac{g_{m2}}{1 + 2 g_{m2} r_{o5}} + g_{mb2} \right) v_{icm} \right)$$

$$= \left(\frac{\left(g_{m1} + (1 + 2 g_{m1} r_{o5}) g_{mb1} \right) g_{m4} r_{o3}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})} - \frac{g_{m2}}{1 + 2 g_{m2} r_{o5}} - g_{mb2} \right) v_{icm}$$

$$v_o = i_o R_{out} \quad ; \quad A_{cm} \equiv \frac{v_o}{v_{icm}} = \frac{\left(g_{m1} + (1 + 2 g_{m1} r_{o5}) g_{mb1} \right) g_{m4} r_{o3}}{(1 + 2 g_{m1} r_{o5})(1 + g_{m3} r_{o3})} - \frac{g_{m2}}{1 + 2 g_{m2} r_{o5}} - g_{mb2}$$

$$CMRR \equiv \frac{A_d}{A_{cm}} = \frac{\frac{1}{2} \left(\frac{g_{m1} g_{m4} r_{o1} r_{o3}}{g_{m3} r_{o1} r_{o3} + r_{o1} + r_{o3}} + g_{m2} \right) (r_{o2} \parallel r_{o4})}{\left(g_{m1} + (1 + 2 g_{m1} r_{o5}) g_{mb1} \right) g_{m4} r_{o3} - \frac{g_{m2}}{1 + 2 g_{m2} r_{o5}} - g_{mb2}}$$

high frequency operation with active load

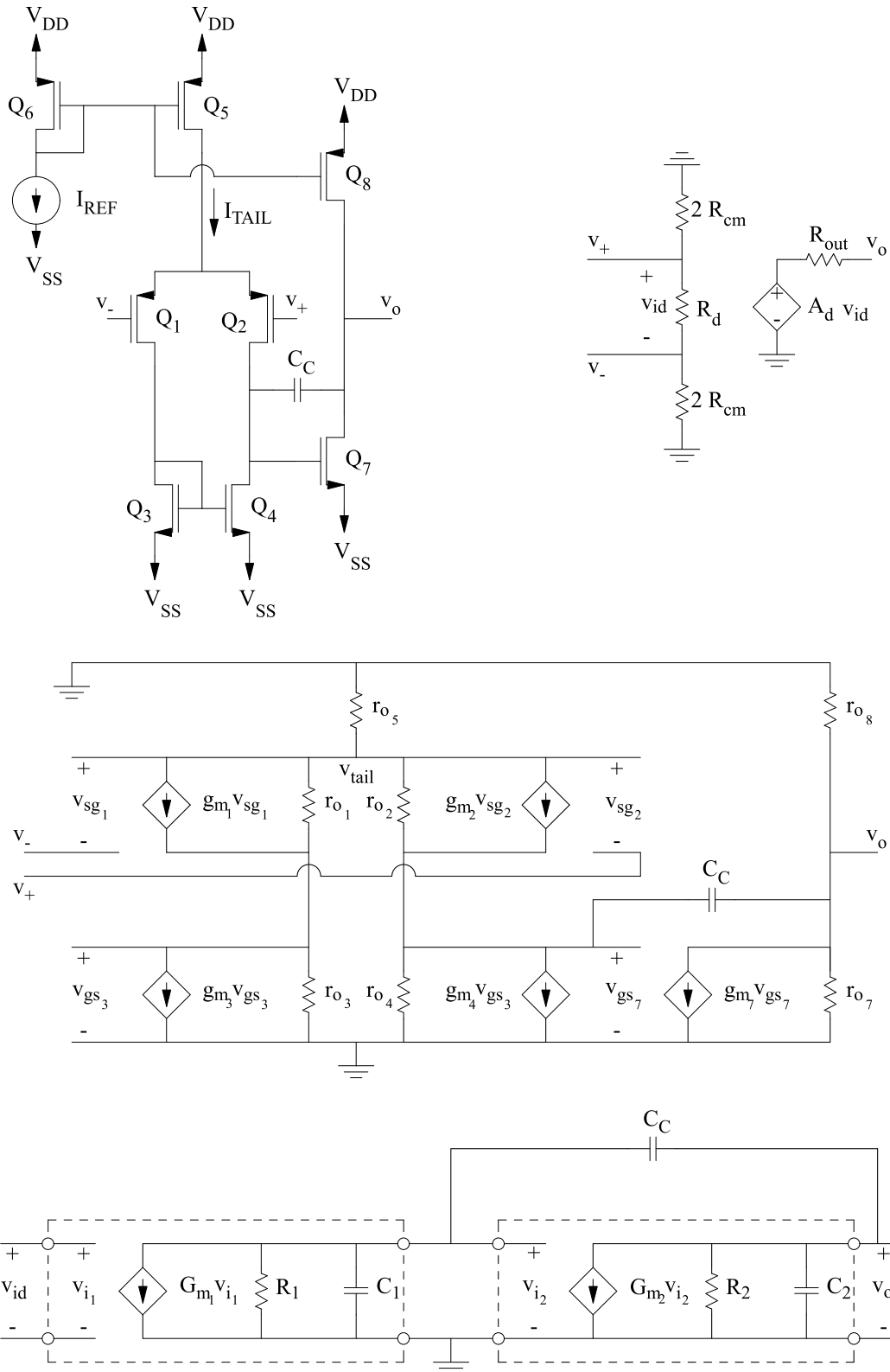


in general C_M and C_L dominate the frequency response, $f_{p1} \approx \frac{1}{2\pi C_L R_{out}}$ and $f_{p2} \approx \frac{1}{2\pi C_M \frac{1}{g_{m3}}} = \frac{g_{m3}}{2\pi C_M}$.

C_M also results in a pole-zero combination associated with the Q₃ and Q₄ current mirror $f_z \approx \frac{2g_{m3}}{2\pi C_M}$.

Recall that the transistors unity current gain frequency is $f_T \approx \frac{g_m}{2\pi(C_{gs} + C_{gd})}$ which is around f_z . This zero lift's the opamp's phase as it approaches f_T to avoid unwanted positive feedback.

multi-stage amplifiers



$$\frac{I_{D_7}}{\left(\frac{W}{L}\right)_7} = \frac{I_{TAIL}}{2} \quad ; \quad \frac{I_{D_8}}{\left(\frac{W}{L}\right)_8} = \frac{I_{TAIL}}{\left(\frac{W}{L}\right)_5} \quad ; \quad I_{D_8} = I_{D_7} \quad \rightarrow \quad \frac{\left(\frac{W}{L}\right)_7}{\left(\frac{W}{L}\right)_4} = 2 \frac{\left(\frac{W}{L}\right)_8}{\left(\frac{W}{L}\right)_5}$$

$$V_{SS} + V_{OV_4} + V_{t_2} \leq v_+ \leq V_{DD} - V_{OV_5} - V_{t_2} - V_{OV_2}$$

$$V_{SS} + V_{OV_3} + V_{t_1} \leq v_- \leq V_{DD} - V_{OV_5} - V_{t_1} - V_{OV_1}$$

$$V_{SS} + V_{OV_7} \leq v_O \leq V_{DD} - V_{OV_8}$$

cascaded transconductance amplifier

$$R_d = \infty \quad ; \quad R_{cm} = \infty \quad ; \quad R_{out} = r_{O_7} \parallel r_{O_8}$$

$$A_d = A_1 A_2 = \left(G_{m_1} R_1 \right) \left(G_{m_2} R_2 \right) = \left(g_{m_1} (r_{O_2} \parallel r_{O_4}) \right) \left(g_{m_7} (r_{O_7} \parallel r_{O_8}) \right)$$

$$C_1 \approx C_{gd_2} + C_{db_2} + C_{gd_4} + C_{db_4} + C_{gs_7} \quad ; \quad C_2 \approx C_{db_7} + C_{db_8} + C_{gd_8} + C_{load}$$

$$\omega_z \approx \frac{G_{m_2}}{C_C}$$

$$\omega_{p_1} \approx \frac{1}{R_1 \left(C_1 + C_C \left(1 + G_{m_2} R_2 \right) \right) + R_2 (C_C + C_2)} \approx \frac{1}{R_1 \left(C_1 + C_C \left(1 + G_{m_2} R_2 \right) \right)} \approx \frac{1}{R_1 C_C G_{m_2} R_2}$$

$$\omega_{p_2} \approx \frac{G_{m_2} C_C}{C_1 C_2 + C_C (C_1 + C_2)} \approx \frac{G_{m_2} C_C}{C_C (C_1 + C_2)} \approx \frac{G_{m_2}}{C_1 + C_2} \approx \frac{G_{m_2}}{C_2}$$

$$\omega_t = \left(G_{m_1} R_1 G_{m_2} R_2 \right) \omega_{p_1} = A_o \omega_{p_1}$$

Want $\omega_t < \omega_z$ and $\omega_t < \omega_{p_2}$