

# EE4C10 Analog Circuit Design Fundamentals

## Homework Assignment II

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September 24, 2021

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## Simulation Files

Each question with simulation files will have their respective subfolder. Except for **q6**, the other questions will have separate subfolders for each sub questions.

Running the simulation files should be able to directly plot the graphs used (configured in the \*.plt file). The folders for each question are arranged as follows after extracting:

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spice
q4
a
step3
step4
b
e
q5
a
b
q6

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## Problem 1

(a) Overdrive voltage,  $V_{gt}$ , for:

1. M1

$$I_{D1} = \frac{\mu_n C_{OX}}{2} \left(\frac{W}{L}\right)_1 (V_{GS1} - V_{TH1})^2 (1 + \lambda_1 V_{DS1})$$

$$I_{D1} \approx \frac{\mu_n C_{OX}}{2} \left(\frac{W}{L}\right)_1 (V_{gt1})^2$$

$$V_{gt1} \approx \sqrt{\frac{2I_{D1}}{\mu_n C_{OX}} \left(\frac{L}{W}\right)_1}$$

$$V_{gt1} \approx 109.11mV$$

2. M2

$$V_{gt_2} \approx \sqrt{\frac{2I_{D_2}}{\mu_p C_{OX}} \left(\frac{L}{W}\right)^2}$$

$$V_{gt_2} \approx 377.96mV$$

(b) Small-signal gain

$$g_{m1}V_{in} = \frac{-V_{out}}{r_{o1}/r_{o2}}$$

$$\frac{V_{out}}{V_{in}} = -g_{m1}(r_{o1}/r_{o2})$$

$$g_{m1} = \mu_n C_{OX} \left(\frac{W}{L}\right)_1 V_{gt_1}$$

$$= 4.582mS$$

$$r_{o1} = \frac{1}{I_{D1}\lambda_n}$$

$$= 20k\Omega$$

$$r_{o2} = \frac{1}{I_{D2}\lambda_p}$$

$$= 40k\Omega$$

$$\frac{V_{out}}{V_{in}} \approx -61.09$$

(c)  $V_{out}$  output swing

For  $M_1$  to be in saturation,

$$V_{DS1} \geq V_{gt1}$$

$$V_{out} \geq 0.109V$$

For  $M_2$  to be in saturation,

$$V_{DS2} \geq V_{gt2}$$

$$V_{DD} - V_{out} \geq 0.377V$$

$$V_{out} \leq 3.3V - 0.377V$$

$$V_{out} \leq 2.923V$$

Swing of  $V_{out}$ ,

$$0.109V < V_{out} < 2.923V$$

$$V_{out,pp} = 2.923V - 0.109V$$

$$= 2.814V$$

(d) The up-swing is limited by the PMOS leaving saturation, while the down swing is limited by the NMOS leaving saturation. The up-swing can be increased by connecting the base of the PMOS to the drain to form a diode connected structure, therefore  $V_{SD2}$  will always be larger than  $V_{gt2}$  by  $V_{TH2}$ . As a result,  $V_{out}$  can be increased to  $V_{DD} - V_{TH2}$  without PMOS leaving saturation.

## Problem 2

(a) For  $M1$  to be 100mV from triode,

$$V_{DS1} = V_{GS1} - V_{TH,N} + 100mV$$

$$X = V_{in} - V_{TH,N} + 100mV$$

$V_{in}$  for M1 to be in saturation with  $I_{D1}$  of 0.35 mA,

$$\begin{aligned}
I_{D1} &= \frac{\mu_n C_{OX}}{2} \left(\frac{W}{L}\right)_1 (V_{GS1} - V_{TH,N})^2 \\
I_{D1} &= \frac{\mu_n C_{OX}}{2} \left(\frac{W}{L}\right)_1 (V_{in} - V_{TH,N})^2 \\
V_{in} &= \sqrt{\frac{2I_{D1}}{\mu_n C_{OX}} \left(\frac{L}{W}\right)_1} + V_{TH,N} \\
&= 0.653V
\end{aligned}$$

$$\begin{aligned}
X &= \sqrt{\frac{2I_{D1}}{\mu_n C_{OX}} \left(\frac{L}{W}\right)_1} + 100mV \\
&\approx 0.253V
\end{aligned}$$

$V_b$  for M2 to be in saturation with  $I_{D2}$  of 0.35 mA,

$$\begin{aligned}
I_{D2} &= \frac{\mu_n C_{OX}}{2} \left(\frac{W}{L}\right)_2 (V_{GS2} - V_{TH,N})^2 \\
I_{D2} &= \frac{\mu_n C_{OX}}{2} \left(\frac{W}{L}\right)_2 (V_b - X - V_{TH,N})^2 \\
V_b &= \sqrt{\frac{2I_{D2}}{\mu_n C_{OX}} \left(\frac{L}{W}\right)_2} + X + V_{TH,N} \\
&\approx 0.906V
\end{aligned}$$

(b) Small-signal gain

$$\begin{aligned}
G_m &= \frac{g_{m1}(g_{m2}r_{o1}r_{o2} + r_{o1})}{g_{m2}r_{o1}r_{o2} + r_{o1} + r_{o2}} \\
&\approx g_{m1} \\
R_{out} &= (g_{m2}r_{o1}r_{o2} + r_{o1} + r_{o2})//R_d
\end{aligned}$$

Small-signal gain,

$$\begin{aligned}\frac{V_{out}}{V_{in}} &= -G_m R_{out} \\ &= -g_{m1}[(g_{m2}r_{o1}r_{o2} + r_{o1} + r_{o2})//R_d]\end{aligned}$$

$$\begin{aligned}g_{m1} &= \mu_n C_{OX} \left(\frac{W}{L}\right)_1 (V_{GS1} - V_{TH,N}) \\ &= \mu_n C_{OX} \left(\frac{W}{L}\right)_1 (V_{in} - V_{TH,N}) \\ &= 4.583mS\end{aligned}$$

$$\begin{aligned}g_{m2} &= \mu_n C_{OX} \left(\frac{W}{L}\right)_2 (V_{GS2} - V_{TH,N}) \\ &\approx \mu_n C_{OX} \left(\frac{W}{L}\right)_2 (V_b - X - V_{TH,N}) \\ &= 4.583mS\end{aligned}$$

$$\begin{aligned}r_{o1} &= \frac{1}{I_{D1}\lambda_n} \\ &= 28.571k\Omega\end{aligned}$$

$$\begin{aligned}r_{o2} &= \frac{1}{I_{D2}\lambda_p} \\ &= 28.571k\Omega\end{aligned}$$

$$\frac{V_{out}}{V_{in}} \approx -22.88$$

(c) Assume  $V_b$  to be 1.65V, For M2 to be in saturation,

$$\begin{aligned}V_{out} - X &\geq V_b - X - V_{TH,N} \\ V_{out} &\geq 1.15V\end{aligned}$$

When  $I_D \geq 0$ ,

$$\begin{aligned}V_{out} &\leq V_{DD} \\ 1.15V &\leq V_{out} \leq 3.3V\end{aligned}$$

$$V_{out,pp} = 2.15V$$

(d)  $X_{pp}$

Gain of X,

$$\begin{aligned}\frac{X}{V_{in}} &= \frac{-g_{m1}}{g_{m2} + \frac{1}{r_{o1}} + \frac{1}{r_{o2}}} \\ &\approx \frac{-g_{m1}}{g_{m2}} \\ &\approx -1\end{aligned}$$

$X_{pp}$

$$\begin{aligned}\frac{X}{V_{out}} &= \frac{X}{V_{in}} \frac{V_{in}}{V_{out}} \\ &= \frac{1}{22.88}\end{aligned}$$

$$X_{pp} = 54.63mV$$

### Problem 3

(a) Sketch of:

1. Output voltage [[

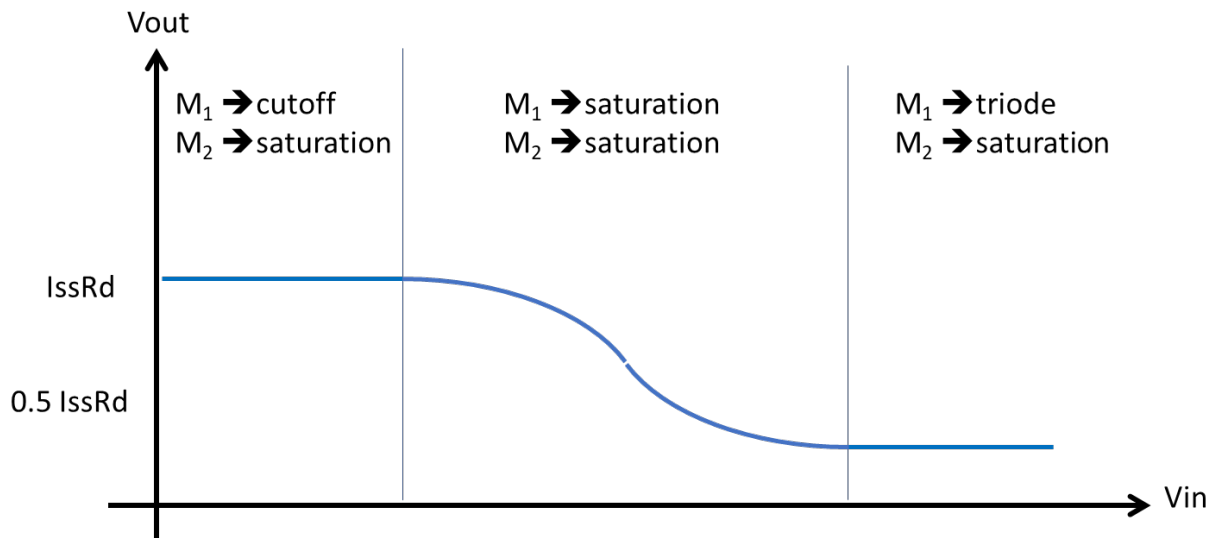


Figure 1: Output voltage sketch

2. Small-signal gain

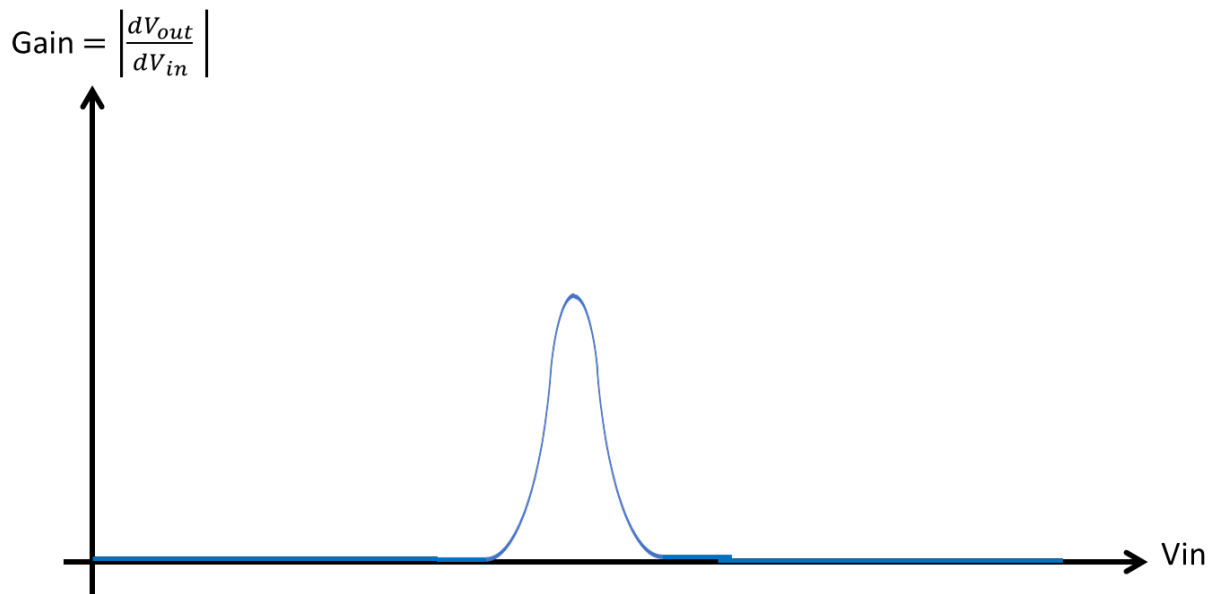


Figure 2: Small-signal gain

(b) Small-signal model

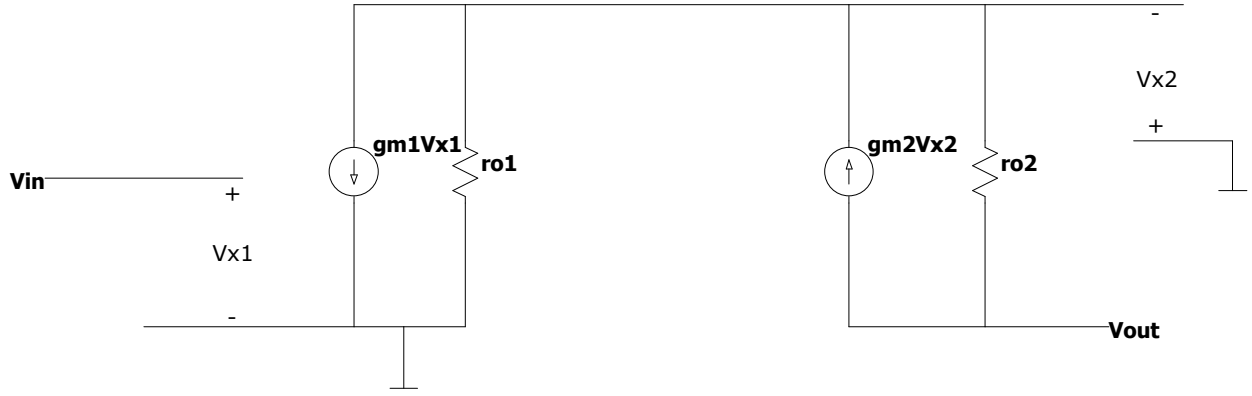


Figure 3: Small-signal model of folded-cascode stage

$$\begin{aligned}
 R_{out} &= g_{m2}r_{o1}r_{o2} + r_{o1} + r_{o2} \\
 &\approx g_{m2}r_{o1}r_{o2} \\
 G_m &= \frac{-g_{m1}(g_{m2} + \frac{1}{r_{o1}})}{g_{m2} + \frac{1}{r_{o1}} + \frac{1}{r_{o2}}} \\
 &\approx -g_{m1}
 \end{aligned}$$

$$\frac{V_{out}}{V_{in}} = g_{m1}g_{m2}r_{o1}r_{o2}$$

## Problem 4

(a) Testbench

```

.lib 'C:\Program Files\LTC\LTspiceXVII\lib\cmp\log018.l' TT
;ac dec 10 1Meg 1G
;op
;step param Vb 0.5 2.5 0.25
.dc VIN 0 3.3 10m

```

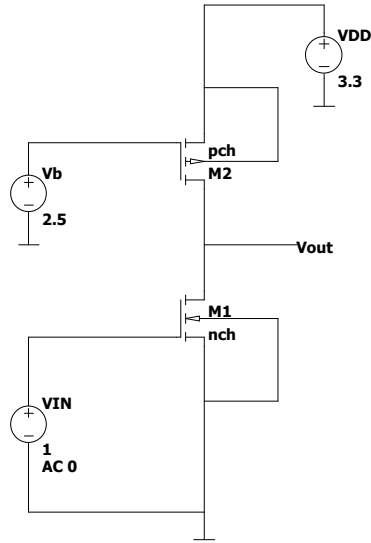


Figure 4: Testbench

$V_{out} - V_{in}$  characteristics

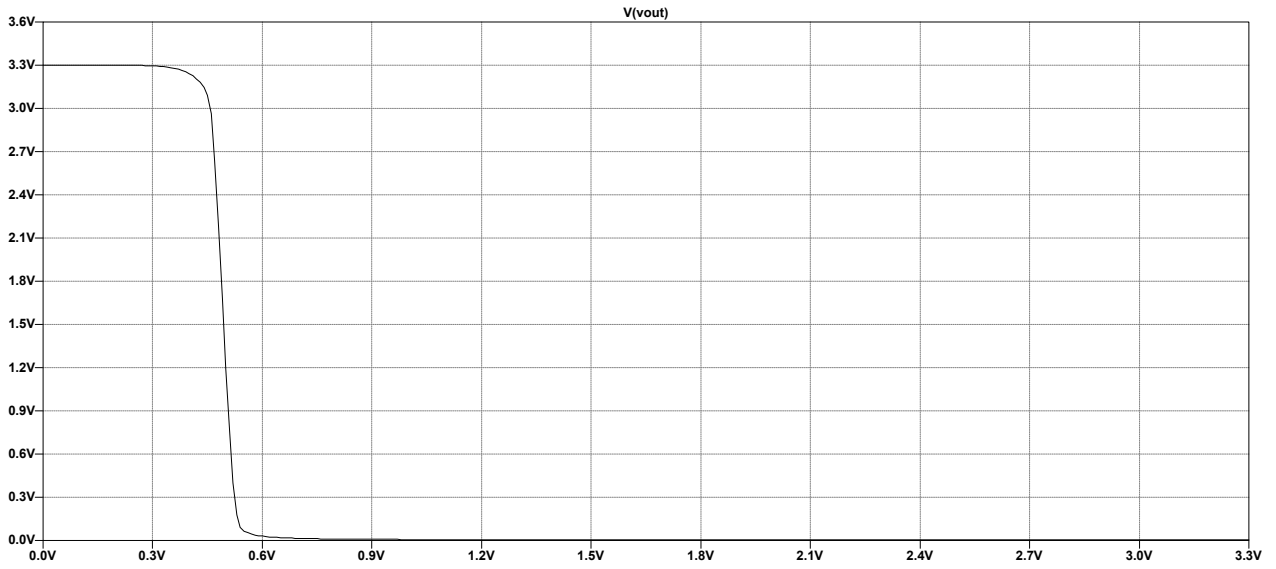


Figure 5:  $V_{out} - V_{in}$  characteristics

(b) Small-signal gain,  $\frac{dV_{out}}{dV_{in}}$

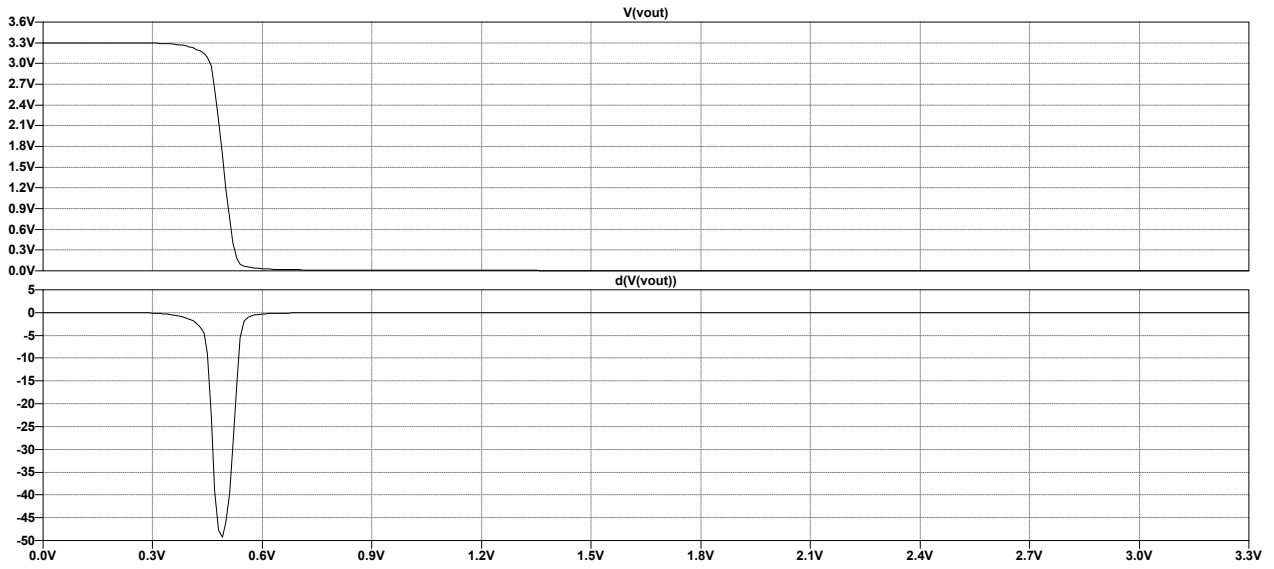


Figure 6: Small-signal gain,  $\frac{dV_{out}}{dV_{in}}$

From figure 6 the gain when:

1.  $V_{out} = 0.6 \text{ V}$   
 $\frac{dV_{out}}{dV_{in}} = -35.59$
2.  $V_{out} = 2.8 \text{ V}$   
 $\frac{dV_{out}}{dV_{in}} = -32.77$

(c) From figure 6, the input voltage,  $V_{in}$ , for maximum gain,  $\max(|\frac{dV_{out}}{dV_{in}}|)$  is given to be:

$$\max(|\frac{dV_{out}}{dV_{in}}|) = 50.07$$

$$V_{in} = 489mV$$

(d) Output voltage swing for gain of 1,

$$V_{out,max} = 3.24V$$

$$V_{out,min} = 56mV$$

$$V_{out,pp} = 3.184V$$

Output peak to peak voltage

$$V_{out,pp} = 3.184V$$

(e) Small-signal voltage gain when:

1.  $V_{out} = 0.6 \text{ V}$ ,  $V_{in} = 0.514 \text{ V}$



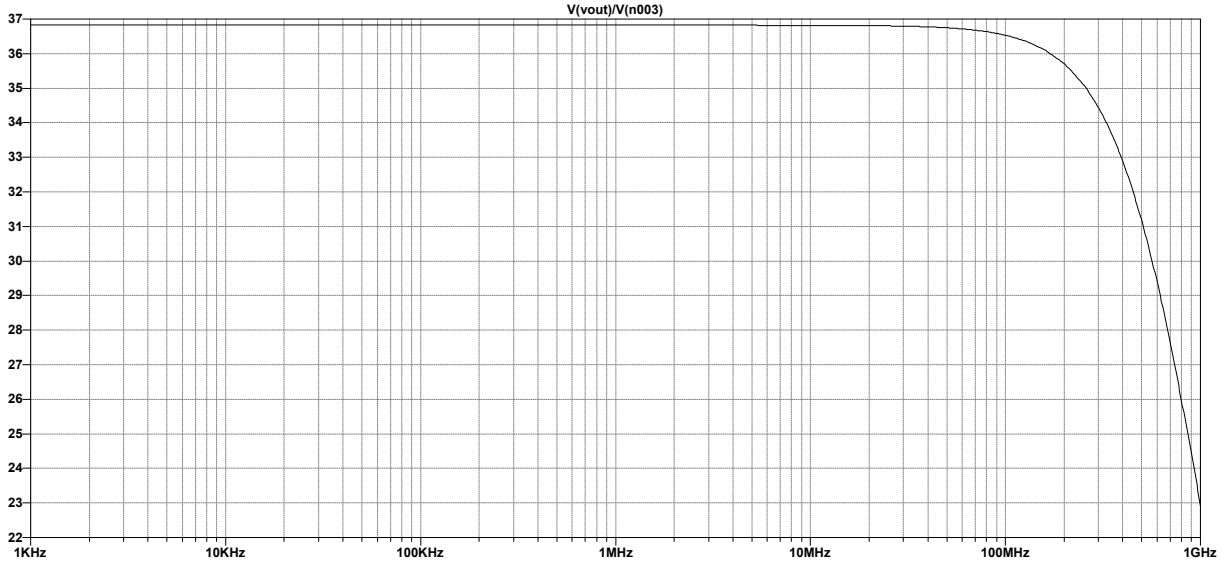


Figure 7: Small-signal gain,  $| \frac{V_{out}}{V_{in}} |$ ,  $V_{out} = 0.6$  V,  $V_{in} = 0.514$  V

Gain = 36.82

2.  $V_{out} = 2.8$  V,  $V_{in} = 0.464$  V

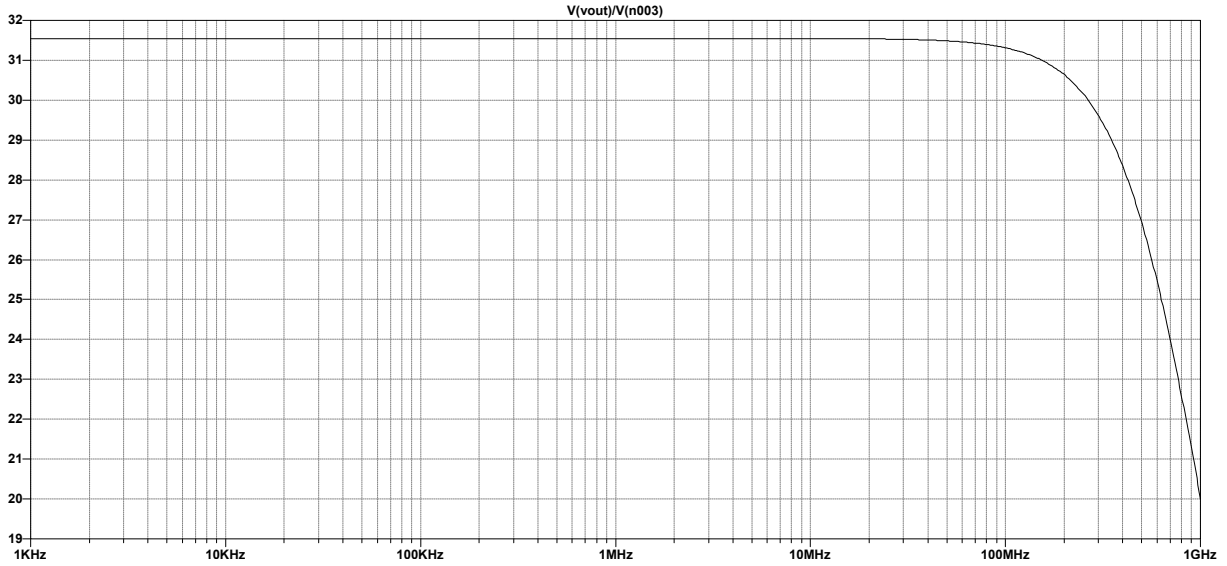


Figure 8: Small-signal gain,  $| \frac{V_{out}}{V_{in}} |$ ,  $V_{out} = 2.8$  V,  $V_{in} = 0.464$  V

Gain = 31.54

## Problem 5

(a) Procedure for designing  $V_b$  for M1 to be 100mV away from triode,  $V_b = 0.825$ V, is determined by the following:

1. Select an initial value  $V_b$  for M1 and M2 to be in saturation when  $V_{in} > V_{TH1}$ . In figure 9,  $V_b = 1.5$  V. From the error logfile 10,  $V_{DS1} > V_{GS1} - V_{TH1}$  and  $V_{DS2} > V_{GS2} - V_{TH2}$ .

```

.lib 'C:\Program Files\LTC\LTspiceXVII\lib\cmp\log018.l' TT
.ac dec 10 1k 1G
.op
.dc vin 0 3.3 0.001

```

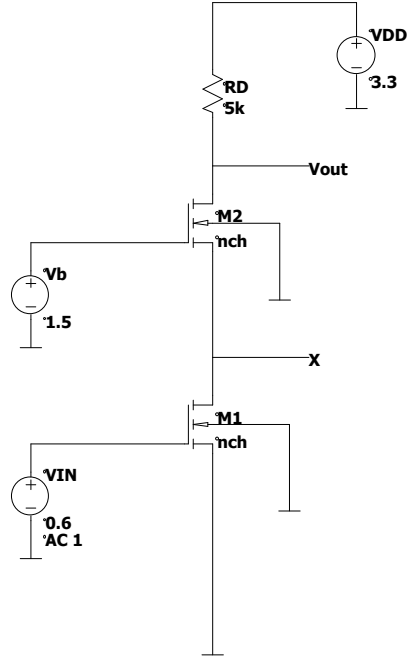


Figure 9: Testbench for Q5

```

Semiconductor Device Operating Points:
      --- BSIM3 MOSFETS ---
Name:      m2      m1
Model:     nch.3   nch.3
Id:        3.74e-04 3.74e-04
Vgs:       7.73e-01 6.00e-01
Vds:       7.05e-01 7.27e-01
Vbs:       -7.27e-01 0.00e+00
Vth:       6.78e-01 4.97e-01
Vdsat:     1.18e-01 1.35e-01
Gm:        4.21e-03 4.42e-03
Gds:       1.29e-04 4.49e-05
Gmb:       7.98e-04 1.27e-03
Cbd:       0.00e+00 0.00e+00
Cbs:       0.00e+00 0.00e+00
Cgsov:     6.59e-15 1.32e-14
Cgdov:     6.59e-15 1.32e-14
Cgbvov:    3.18e-17 6.47e-17
dQgdVgb:   3.21e-14 1.00e-13
dQgdVdb:   -6.47e-15 -1.32e-14
dQgdVsb:   -2.27e-14 -7.78e-14
dQddVgb:   -6.61e-15 -1.33e-14
dQddVdb:   6.60e-15 1.32e-14
dQddVsb:   2.09e-17 9.01e-17
dQbdVgb:   -3.63e-15 -1.24e-14
dQbdVdb:   1.50e-17 2.88e-18
dQbdVsb:   -2.22e-15 -1.44e-14

```

Figure 10: Semiconductor Device Operating Points

2. Doing a DC-sweep for  $I_{D1}$ - $V_{in}$ ,  $V_{in} \approx 0.6V$  when  $I_{D1} = 0.35mA$ .

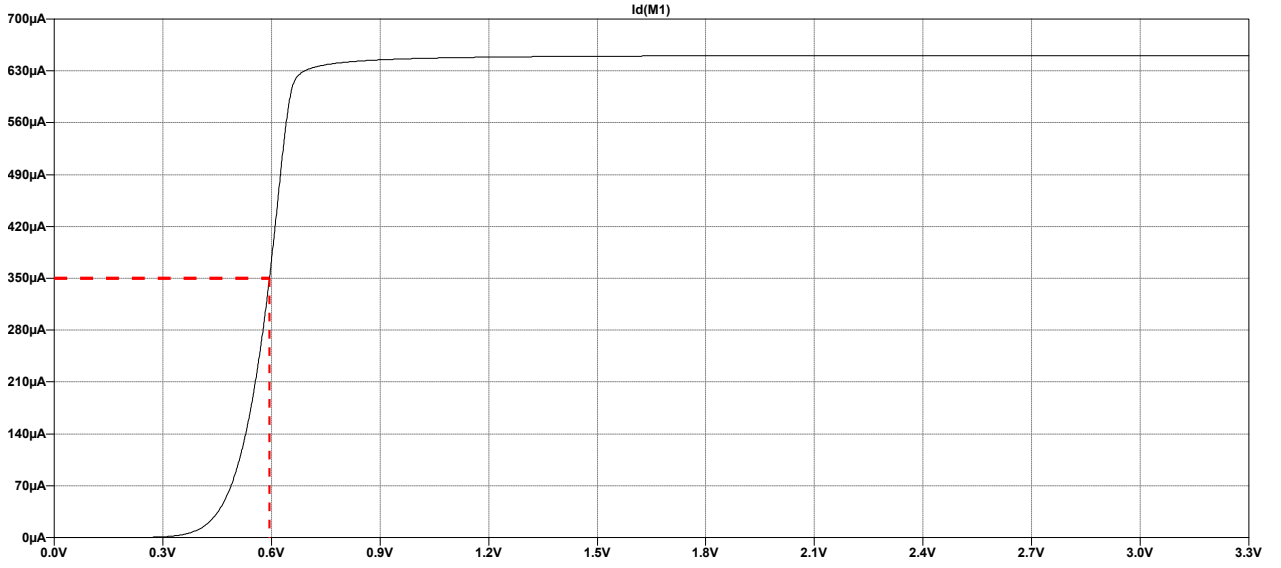


Figure 11:  $I_{D1}$ - $V_{in}$

3. From the operation point simulation in figure 10,  $V_{TH1}$  is determined to be 0.497V. For M1 to be 100mV from triode region,

$$V_x = V_{in} - V_{TH1} + 100mV$$

$$\approx 0.2V$$

4. DC-sweeping  $V_x$ - $V_b$  and determining  $V_b$  for  $V_x = 0.2V$ . From the figure 12,  $V_b = 0.825V$ .

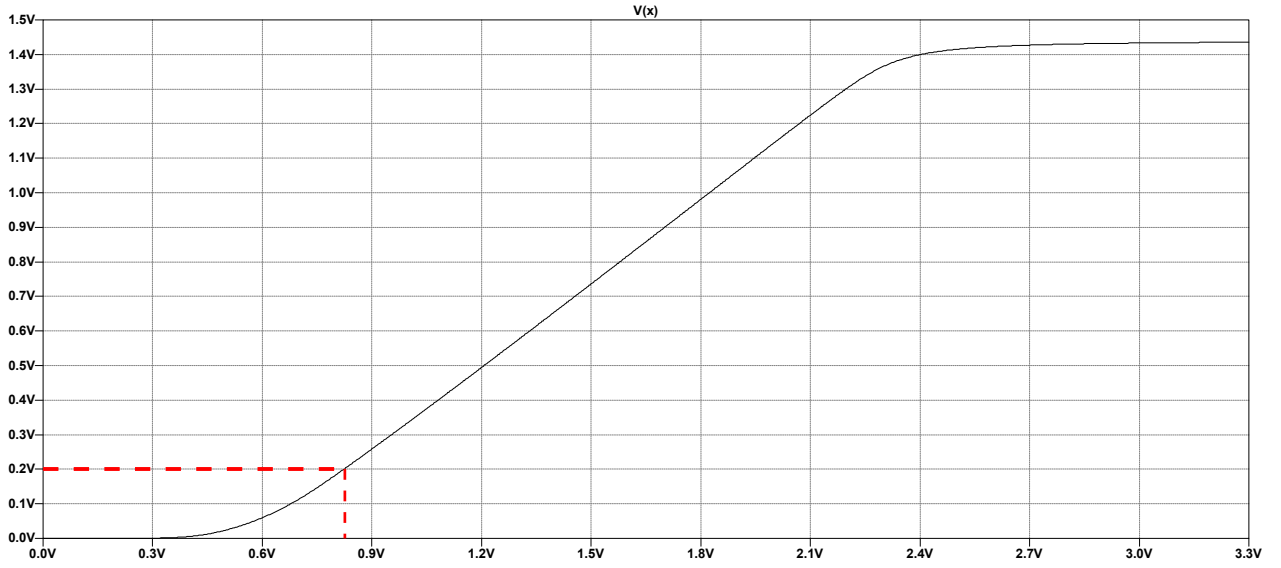


Figure 12:  $V_x$ - $V_b$

- (b)  $I_{OUT}$ - $V_{OUT}$  when  $V_{IN}$  is fixed for  $I_{D1} = 0.35$  mA

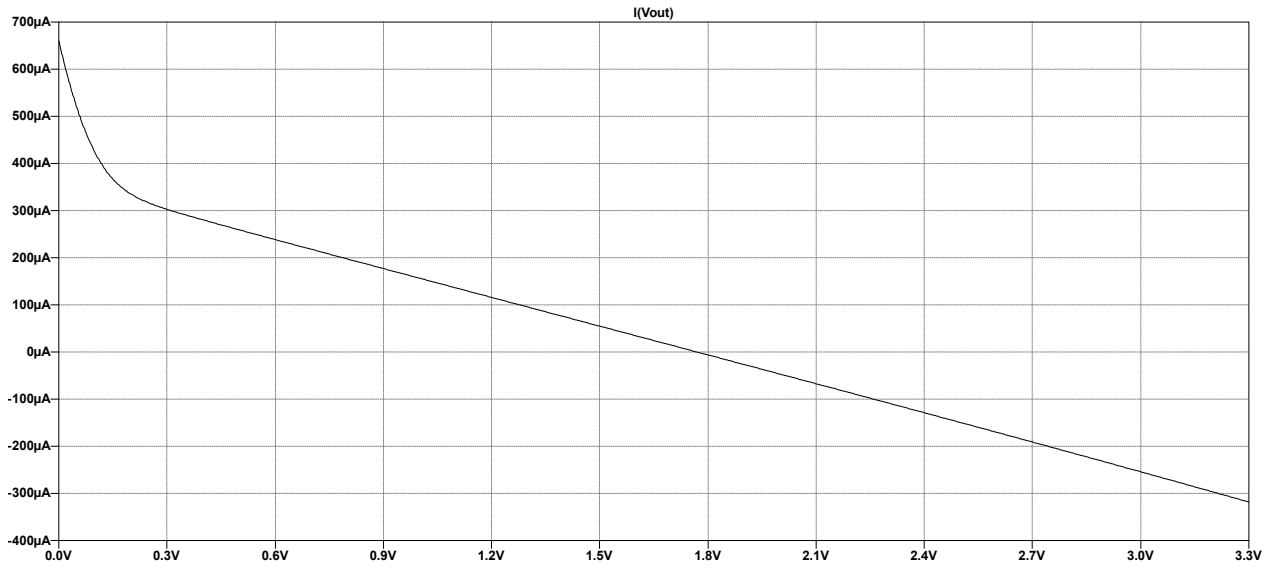


Figure 13:  $I_{OUT}$ - $V_{OUT}$

## Problem 6

The output resistance,  $R_{out}$  is the reciprocal of the slope of  $I_{OUT}$ - $V_{OUT}$ ,

$$R_{out} = \left( \frac{I_{OUT}}{V_{OUT}} \right)^{-1}$$

The results are shown in figure 14,

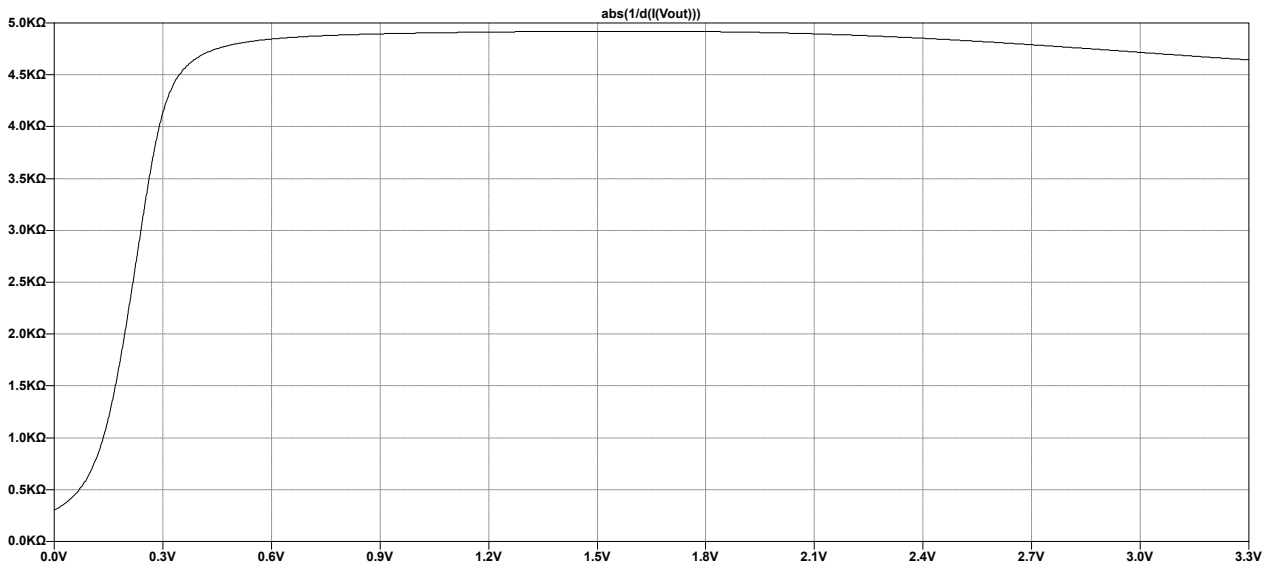


Figure 14:  $R_{OUT}$ - $V_{OUT}$

From figure 15,  
 $\max(R_{out}) = 4920 \, \Omega$   
 when,  
 $V_{out} = 1.53 \, V$

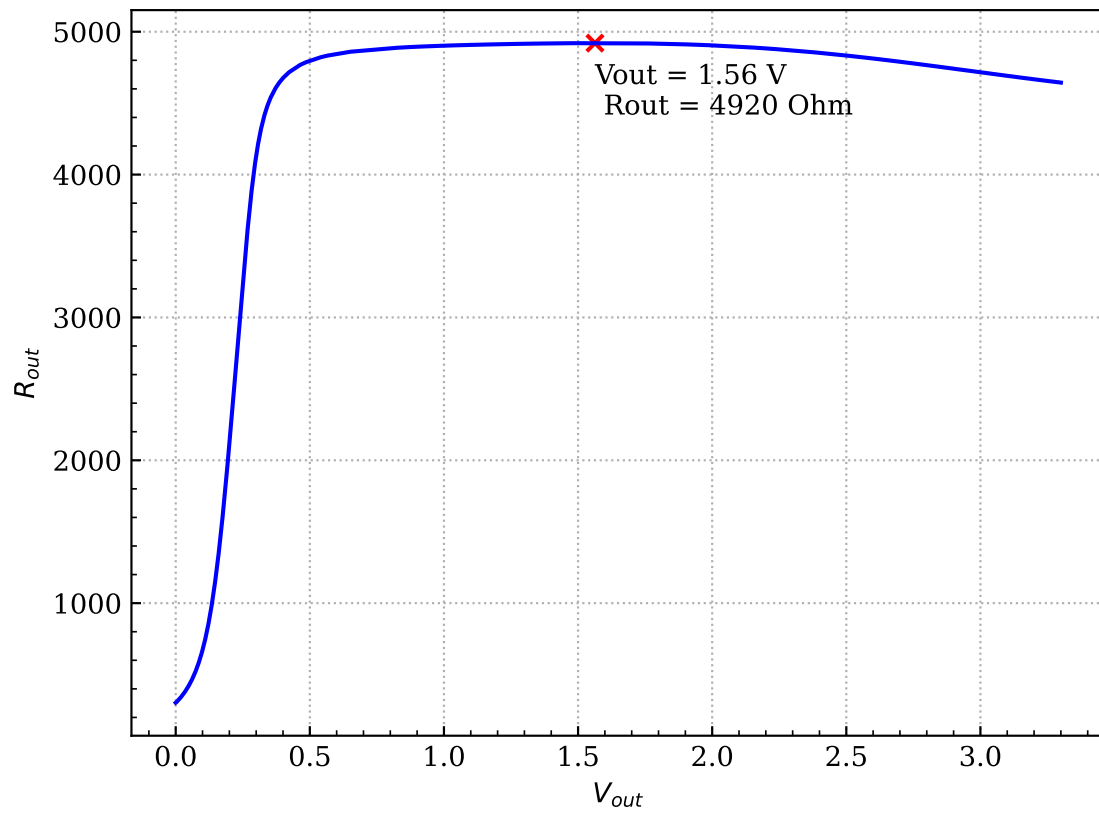


Figure 15: Maximum  $R_{out}$