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1 Equations of Motion

1.1 Reference

Gravity force in inertial frame

$$\mathbf{g} = -g\mathbf{k}$$

Rotor force in body frame

$$\mathbf{F}_{R,B} = k \left(\gamma_1 + \gamma_2 + \gamma_3 + \gamma_4 \right) \mathbf{k}$$

Rotor force in inertial frame

$$\mathbf{F}_R = \mathbf{R}(\mathbf{q})\mathbf{F}_{R,B}(\gamma)$$

Drag force in body frame

$$\mathbf{F}_{D,B}(\dot{\mathbf{x}}_B)$$

$$\dot{\mathbf{x}}_B = \mathbf{R}^{-1}\dot{\mathbf{x}}$$

Drag force in inertial frame

$$\mathbf{F}_D = \mathbf{R}(\mathbf{q})\mathbf{F}_{D,B}(\dot{\mathbf{x}}_B)$$

1.2 Translation

$$\begin{split} m\ddot{\mathbf{x}} &= m\mathbf{g} + \mathbf{F}_R + \mathbf{F}_D \\ \ddot{\mathbf{x}} &= \mathbf{g} + \frac{1}{m}\mathbf{F}_R + \frac{1}{m}\mathbf{F}_D \\ \ddot{\mathbf{x}} &= \mathbf{g} + \frac{1}{m}\mathbf{R}\mathbf{F}_{R,B} + \frac{1}{m}\mathbf{R}\mathbf{F}_{D,B} \end{split}$$

1.3 Rotation

$$\begin{split} \mathbf{I}\dot{\boldsymbol{\omega}} &= \boldsymbol{\tau} - \boldsymbol{\omega} \times (\mathbf{I}\boldsymbol{\omega}) \\ \dot{\boldsymbol{\omega}} &= \mathbf{I}^{-1} \left(\boldsymbol{\tau} - \boldsymbol{\omega} \times (\mathbf{I}\boldsymbol{\omega}) \right) \\ I &= \begin{bmatrix} I_{xx} & 0 & 0 \\ 0 & I_{yy} & 0 \\ 0 & 0 & I_{zz} \end{bmatrix} \\ \boldsymbol{\tau}_{B} &= \begin{bmatrix} Lk \left(\gamma_{1} - \gamma_{3} \right) \\ Lk \left(\gamma_{2} - \gamma_{4} \right) \\ b \left(\gamma_{1} - \gamma_{2} + \gamma_{3} - \gamma_{4} \right) \end{bmatrix} = \begin{bmatrix} Lk & 0 & -Lk & 0 \\ 0 & Lk & 0 & -Lk \\ b & -b & b & -b \end{bmatrix} \begin{bmatrix} \gamma_{1} \\ \gamma_{2} \\ \gamma_{3} \\ \gamma_{4} \end{bmatrix} \end{split}$$

1.3.1 Quaternion

$$\dot{\mathbf{q}} = \mathbf{A}_3 \boldsymbol{\omega}$$
 $\ddot{\mathbf{q}} = \dot{\mathbf{A}}_3 \boldsymbol{\omega} + \mathbf{A}_3 \dot{\boldsymbol{\omega}}$ $\ddot{\mathbf{q}} = \dot{\mathbf{A}}_3 \boldsymbol{\omega} + \mathbf{A}_3 \mathbf{I}^{-1} \left(\boldsymbol{\tau} - \boldsymbol{\omega} \times (\mathbf{I} \boldsymbol{\omega}) \right)$

1.3.2 Euler

$$\omega = \begin{bmatrix} 1 & 0 & -s_{\theta} \\ 0 & c_{\phi} & c_{\theta}s_{\phi} \\ 0 & -s_{\phi} & c_{\theta}s_{\phi} \end{bmatrix} \dot{\theta} = \mathbf{A}_{5}^{-1}\dot{\theta}$$

$$\dot{\theta} = \mathbf{A}_{5}\omega$$

$$\ddot{\theta} = \dot{\mathbf{A}}_{5}\omega + \mathbf{A}_{5}\dot{\omega}$$

$$\ddot{\theta} = \dot{\mathbf{A}}_{5}\omega + \mathbf{A}_{5}\left(\mathbf{I}^{-1}\left(\boldsymbol{\tau} - \boldsymbol{\omega} \times (\mathbf{I}\boldsymbol{\omega})\right)\right)$$

$$\ddot{\theta} = \mathbf{S}^{-1}\left(\mathbf{I}^{-1}\left(\boldsymbol{\tau} - \boldsymbol{\omega} \times (I\boldsymbol{\omega})\right) - \dot{\mathbf{S}}\dot{\theta}\right)$$
(1)

2 Control

2.1 Attitude

2.1.1 Quaternion

$$\mathbf{e}_1 = \mathbf{q}_{ref} \mathbf{q}^*$$

$$\mathbf{e}_2 = \boldsymbol{\omega}_{ref} - \boldsymbol{\omega}$$

2.2 Position

$$\mathbf{e}_5 = \mathbf{x}_{ref} - \mathbf{x}$$

$$\dot{\mathbf{e}}_5 = \dot{\mathbf{x}}_{ref} - \dot{\mathbf{x}}$$

$$\dot{\mathbf{e}}_5 = \dot{\mathbf{x}}_{ref} - \mathbf{v}$$

$$\mathbf{v}_{ref} = \mathbf{C}_5 \mathbf{e}_5 + \dot{\mathbf{x}}_{ref} + \mathbf{\Lambda}_5 \boldsymbol{\chi}_5$$

$$\dot{\mathbf{v}}_{ref} = \mathbf{C}_5 \dot{\mathbf{e}}_5 + \ddot{\mathbf{x}}_{ref} + \mathbf{\Lambda}_5 \mathbf{e}_5$$

$$\mathbf{e}_6 = \mathbf{v}_{ref} - \mathbf{v}$$

$$\mathbf{e}_6 = \mathbf{C}_5 \mathbf{e}_5 + \dot{\mathbf{x}}_{ref} + \mathbf{\Lambda}_5 \boldsymbol{\chi}_5 - \mathbf{v}$$

$$\dot{\mathbf{e}}_6 = \dot{\mathbf{v}}_{ref} - \dot{\mathbf{v}} = \dot{\mathbf{v}}_{ref} - \mathbf{a}$$

$$\dot{\mathbf{e}}_6 = \mathbf{C}_5 \dot{\mathbf{e}}_5 + \ddot{\mathbf{x}}_{ref} + \mathbf{\Lambda}_5 \mathbf{e}_5 - \ddot{\mathbf{x}}$$

$$\dot{\mathbf{x}}_{ref} = \mathbf{v}_{ref} - \mathbf{C}_5 \mathbf{e}_5 - \mathbf{\Lambda}_5 \mathbf{\chi}_5$$

$$\dot{\mathbf{x}}_{ref} = \mathbf{e}_6 + \mathbf{v} - \mathbf{C}_5 \mathbf{e}_5 - \mathbf{\Lambda}_5 \mathbf{\chi}_5$$

$$\dot{\mathbf{e}}_5 = \mathbf{e}_6 - \mathbf{C}_5 \mathbf{e}_5 - \mathbf{\Lambda}_5 \mathbf{\chi}_5$$

$$\dot{\mathbf{e}}_6 = \mathbf{f}_6(\mathbf{e}_5,\mathbf{e}_6)$$

$$\mathbf{f}_{6}(\mathbf{e}_{5},\mathbf{e}_{6}) = \mathbf{C}_{5}\left(\mathbf{e}_{6} - \mathbf{C}_{5}\mathbf{e}_{5} - \mathbf{\Lambda}_{5}\boldsymbol{\chi}_{5}\right) + \ddot{\mathbf{x}}_{ref} + \mathbf{\Lambda}_{5}\mathbf{e}_{5} - \ddot{\mathbf{x}}$$

$$\begin{split} \ddot{\mathbf{x}} &= -\mathbf{f}_{6}(\mathbf{e}_{5},\mathbf{e}_{6}) + \mathbf{C}_{5}\left(\mathbf{e}_{6} - \mathbf{C}_{5}\mathbf{e}_{5} - \mathbf{\Lambda}_{5}\boldsymbol{\chi}_{5}\right) + \ddot{\mathbf{x}}_{ref} + \mathbf{\Lambda}_{5}\mathbf{e}_{5} \\ \mathbf{F}_{R} &= m\left(-\mathbf{C}_{7}\mathbf{e}_{5} - \mathbf{C}_{8}\mathbf{e}_{6} + \mathbf{C}_{5}\left(\mathbf{e}_{6} - \mathbf{C}_{5}\mathbf{e}_{5} - \mathbf{\Lambda}_{5}\boldsymbol{\chi}_{5}\right) + \ddot{\mathbf{x}}_{ref} + \mathbf{\Lambda}_{5}\mathbf{e}_{5} - \mathbf{g} - \frac{1}{m}\mathbf{F}_{D}\right) \\ \mathbf{F}_{R} &= m\left(\left(-\mathbf{C}_{7} - \mathbf{C}_{5}^{2} + \mathbf{\Lambda}_{5}\right)\mathbf{e}_{5} + \left(\mathbf{C}_{8} + \mathbf{C}_{5}\right)\mathbf{e}_{6} - \mathbf{C}_{5}\mathbf{\Lambda}_{5}\boldsymbol{\chi}_{5} + \ddot{\mathbf{x}}_{ref} - \mathbf{g} - \frac{1}{m}\mathbf{F}_{D}\right) \\ \mathbf{F}_{R} &= m\left(\left(-\mathbf{C}_{7} - \mathbf{C}_{5}^{2} + \mathbf{\Lambda}_{5}\right)\mathbf{e}_{5} \\ &+ \left(-\mathbf{C}_{8} + \mathbf{C}_{5}\right)\left(\mathbf{C}_{5}\mathbf{e}_{5} + \dot{\mathbf{x}}_{ref} + \mathbf{\Lambda}_{5}\boldsymbol{\chi}_{5} - \mathbf{v}\right) \\ &- \mathbf{C}_{5}\mathbf{\Lambda}_{5}\boldsymbol{\chi}_{5} + \ddot{\mathbf{x}}_{ref} - \mathbf{g} - \frac{1}{m}\mathbf{F}_{D}\right) \\ \frac{1}{m}\mathbf{F}_{R} &= \left(-\mathbf{C}_{7} - \mathbf{C}_{5}^{2} + \mathbf{\Lambda}_{5} + \left(-\mathbf{C}_{8} + \mathbf{C}_{5}\right)\mathbf{C}_{5}\right)\mathbf{x}_{ref} \\ &- \left(-\mathbf{C}_{7} - \mathbf{C}_{5}^{2} + \mathbf{\Lambda}_{5} + \left(-\mathbf{C}_{8} + \mathbf{C}_{5}\right)\mathbf{C}_{5}\right)\mathbf{x}_{ref} \\ &+ \left(-\mathbf{C}_{8}\right)\mathbf{\Lambda}_{5}\boldsymbol{\chi}_{5} \\ &- \left(-\mathbf{C}_{8} + \mathbf{C}_{5}\right)\mathbf{v} \\ &+ \ddot{\mathbf{x}}_{ref} - \mathbf{g} - \frac{1}{m}\mathbf{F}_{D} \\ \\ 0 &= + \mathbf{C}_{11}\boldsymbol{\chi}_{5} \\ &+ \mathbf{C}_{9}(\mathbf{x}_{ref} - \mathbf{x}) \\ &+ \mathbf{C}_{10}(\dot{\mathbf{x}}_{ref} - \mathbf{v}) \\ \end{split}$$

2.3 Dynamics of Acceleration

Instead of assuming $\ddot{\mathbf{x}}$ is our control input, we can continue the above process. We guess that the result will be

 $+\ddot{\mathbf{x}}_{ref} - \ddot{\mathbf{x}}$

$$\begin{aligned} 0 &= + \ \mathbf{C}_9 \boldsymbol{\chi}_5 \\ &+ \ \mathbf{C}_{10} (\mathbf{x}_{ref} - \mathbf{x}) \\ &+ \ \mathbf{C}_{11} (\dot{\mathbf{x}}_{ref} - \mathbf{v}) \\ &+ \ \mathbf{C}_{12} (\ddot{\mathbf{x}}_{ref} - \mathbf{a}) \\ &+ \ \ddot{\mathbf{x}}_{ref} - \dot{\mathbf{a}} \end{aligned}$$

$$\mathbf{a} = \mathbf{a}_g + \mathbf{a}_R$$

$$\dot{\mathbf{a}} = \dot{\mathbf{a}}_R$$

$$\mathbf{a}_R = \mathbf{q}^* \mathbf{a}_{RB} \mathbf{q}$$

In general, if q rotates from y to x frame

$$y = q^*xq$$

$$\dot{\mathbf{y}} = \dot{\mathbf{q}}^* \mathbf{x} \mathbf{q} + \mathbf{q}^* \dot{\mathbf{x}} \mathbf{q} + \mathbf{q}^* \mathbf{x} \dot{\mathbf{q}}$$

$$\dot{\mathbf{y}} = \mathbf{q}^* \boldsymbol{\omega}^* \mathbf{x} \mathbf{q} + \mathbf{q}^* \dot{\mathbf{x}} \mathbf{q} + \mathbf{q}^* \mathbf{x} \boldsymbol{\omega} \mathbf{q}$$

$$\dot{\mathbf{y}} = \mathbf{q}^* \left(\boldsymbol{\omega}^* \mathbf{x} + \dot{\mathbf{x}} + \mathbf{x} \boldsymbol{\omega} \right) \mathbf{q}$$

$$\mathbf{q}\dot{\mathbf{y}}\mathbf{q}^* = \boldsymbol{\omega}^*\mathbf{x} + \dot{\mathbf{x}} + \mathbf{x}\boldsymbol{\omega}$$

In our case

$$\mathbf{a}_{RB} = \begin{bmatrix} 0 \\ 0 \\ a_{RB} \\ 0 \end{bmatrix}$$

which leads to the simple result

$$\boldsymbol{\omega}^* \mathbf{x} + \dot{\mathbf{x}} + \mathbf{x} \boldsymbol{\omega} = \begin{bmatrix} 0 \\ -\omega_y a_{RB} \\ \omega_x a_{RB} \\ \dot{a}_{RB} \end{bmatrix}$$

Notice that ω_z does not appear because it has no effect on the translation of the vehicle. In order to solve for ω_x , ω_y , and a_{RB} , we need a relationship between a_{RB} and its derivative. For example, we could use forward differencing.

2.3.1 Transfer Function

$$\ddot{x} = (c_9 y - c_9 x + c_{10} \dot{y} - c_{10} \dot{x} + c_{11} \int y - c_{11} \int x + \ddot{y} - g - \frac{F_D}{m}$$

$$s^{2}X - sx(0) - \dot{x}(0) = (c_{9}Y - c_{9}X + c_{10}sY - c_{10}y(0) - c_{10}sX + c_{10}x(0) + c_{11}\frac{Y}{s} - c_{11}\int x + \ddot{y} - g - \frac{F_{D}}{m}$$