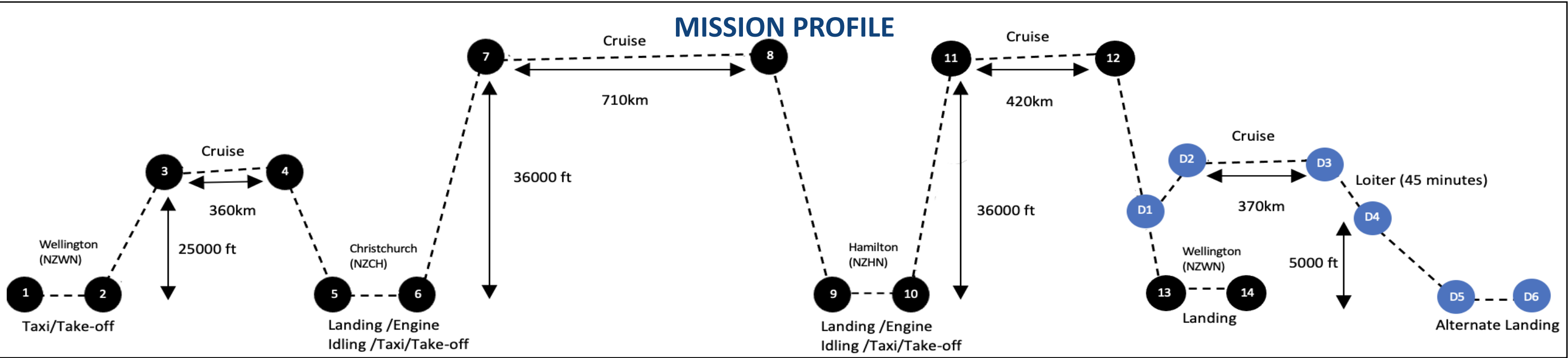


# Conceptual Design for a Regional Jet Aircraft

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## DESIGN SPECIFICATION



### DESIGN CONSTRAINTS

- 90 passengers and baggage.
- 2 pilots and 3 cabin crew.
- 30 minute turnaround at each location with powerplant idling: no refuelling.
- Diversion and 45 minute loiter at 5000 ft
- Absolute ceiling: 40,000 ft
- Maximum speed of Mach 0.75
- Compliant with FAR-25 regulations.

## BASELINE CONFIGURATION

### LOW WING

- Easy cabin access.
- Shortened take-off distance due to enhanced ground effect and softer touchdown.
- Reduced impact of downwash from wings on horizontal stabiliser.

### UNDERWING ENGINES

- High bypass turbofan engines.
- Minimise interference drag.
- Easy to service: minimal extra equipment required and faster turnaround.

### TRICYCLE UNDERCARRIAGE

- Front wheel enables steering and prevents tipping in the event of harsh braking.
- Stored underwing for better aerodynamics.



### CONVENTIONAL TAIL

- Lightweight: no additional reinforcement needed.
- Good indication when stall is near: violently vibrates when approaching stall.

### HIGH LIFT DEVICES

Fowler flaps:

- Increase  $C_{Lmax}$
- Easily maintained
- Reliable activation mechanism

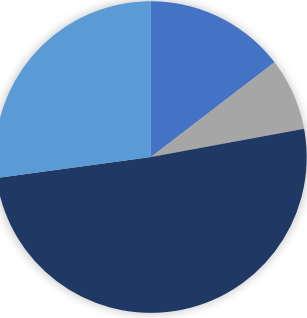
Slats:

- Increase  $C_{Lmax}$

## INITIAL SIZING

Table 1: Weight Fraction Estimations

Journey Segments	Weight Fractions
S1: Wellington – Christchurch	0.918
S2: Christchurch – Hamilton	0.834
S3: Hamilton – Wellington	0.767
D: Hamilton – Wellington (including diversion)	0.734



Fuel: 27%  
Crew and Passengers: 15%  
Payload: 7%  
Empty: 51%

Figure 1: Weight Fractions

Description	S1 Weight Fractions	S2 Weight Fractions	S3 Weight Fractions
Taxi + Take-off	0.970	0.970	0.970
Climb + Accelerate	0.985	0.985	0.985
Cruise	0.986	0.975	0.985
Descent	0.980	0.980	0.980
Landing + Taxi	0.995	0.995	0.995

Description (Diversion)	Weight Fractions
Missed Approach	0.985
Cruise	0.987
Loiter	0.985
Descent	0.980
Landing + Taxi	0.995

➤ Initial guesses of  $AR = 8$ ,  $S_{wet}/S_{ref} = 5.5$  and  $e = 0.8$  were made.

➤  $\left(\frac{L}{D}\right)_{max}$  and  $C_{D0}$  calculated using  $\left(\frac{L}{D}\right)_{max} = \frac{1}{2} \sqrt{\frac{\pi A R e}{C_{D0}}} = K_{LD} \sqrt{\frac{AR}{\frac{S_{wet}}{S_{ref}}}}$ . [4]

➤ Weight fractions for specific flight segments make use of [4]:

- Specific Fuel Consumption:  $c_{cruise} = 1.38 * 10^{-4} s^{-1}$ ,  $c_{loiter} = 1.11 * 10^{-4} s^{-1}$ .

- Range constraints:  $\frac{W_i}{W_{i-1}} = e^{\frac{V(L/D)_{cruise}}{RC}}$ .

- Endurance constraints:  $\frac{W_i}{W_{i-1}} = e^{\frac{-EC}{(L/D)_{max}}}$ .

➤ Fuel weight fraction:  $\frac{W_f}{W_0} = 1.01 \left(1 - \frac{W_n}{W_0}\right)$ , where  $\frac{W_n}{W_0} = \frac{W_i}{W_{i-1}} * \dots * \frac{W_1}{W_0}$ .

➤ Empty weight fraction:  $\frac{W_e}{W_0} = A W_0^C$ , where  $A = 0.97$  and  $C = -0.06$ . [1]

➤ Iterative equation based on initial  $W_0$  guess :  $W_0 = \frac{W_{crew} + W_{payload}}{1 - \left(\frac{W_f}{W_0}\right) - \left(\frac{W_e}{W_0}\right)}$ .

## SIZING TO CONSTRAINT

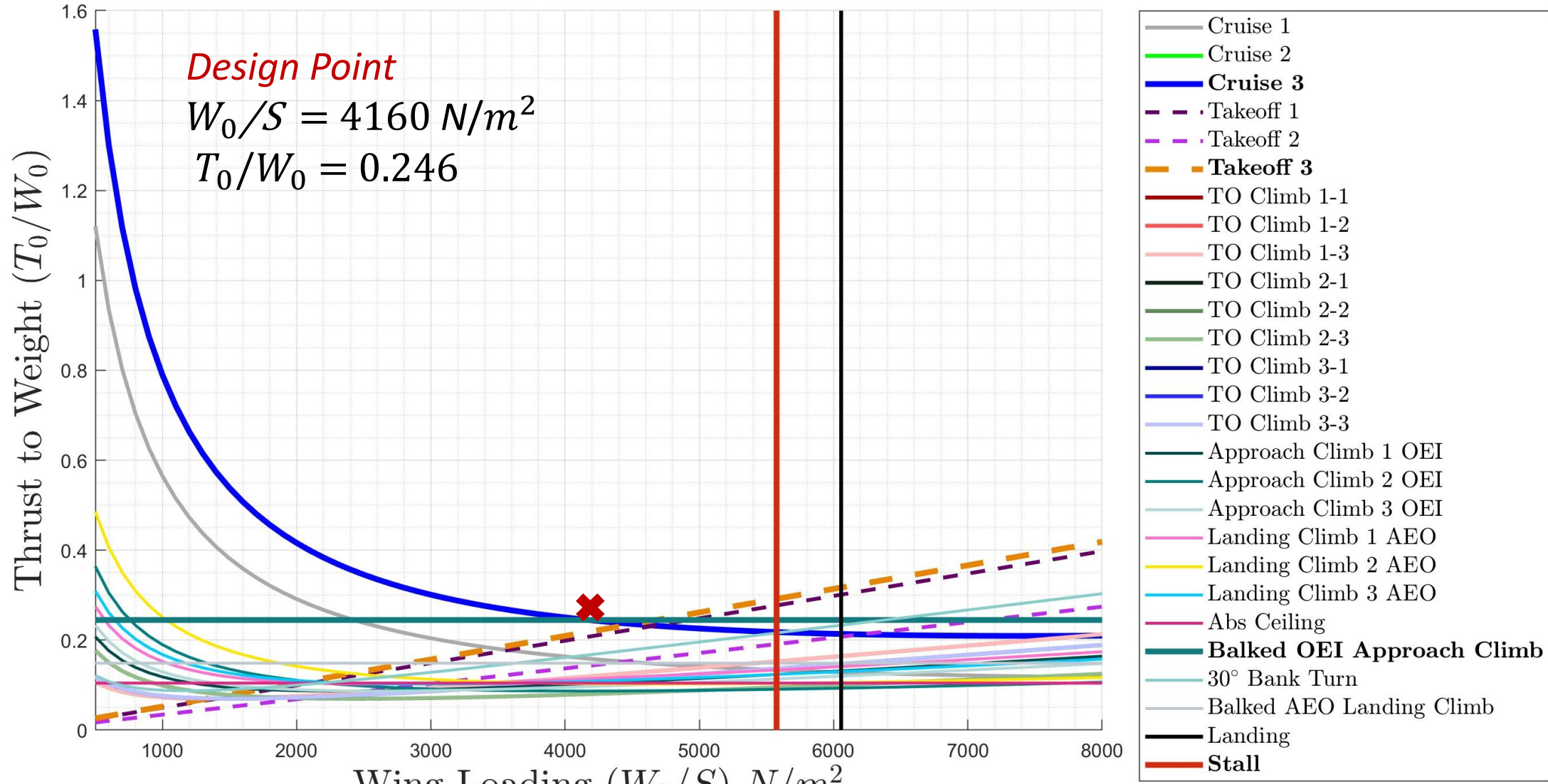


Figure 2: Final Constraint Diagram

**FIELD PERFORMANCE:** Empirical formulae shown below are used to calculate T/O & landing distances.

Table 2: Design Process for Field Performance

Segment	Formula used [3]	Constraints	$C_{Lmax}$ and $V$ [2]
Take-off	$TOP = \frac{W/S}{(T/W)\sigma C_{LmaxTO}}$	$TOP_1 = 9576 N/m^2$ $TOP_2 = 13885 N/m^2$ $TOP_3 = 9097 N/m^2$	$C_{LmaxTO} = 2.1$ $V_{TO} = 1.1V_S$
Landing / Approach	$ALD = \frac{0.51W/S}{\sigma C_{LmaxL}} K_R + S_a$	$ALD = \frac{3}{5} * LDA$	$C_{LmaxL} = 3.3$ $\Delta C_{LmaxHLD} = 1.7$ $V_A = 1.3V_S$

Table 4: Final results at chosen design point

### FINAL RESULTS AT CHOSEN DESIGN POINT

$W_0/S_{ref}$	$S_{ref}$	$T_0/W_0$	$W_0$	$AR$	$e$	$S_{wet}/S_{ref}$	$C_{D0}$	$W_e/W_0$	$W_f/W_0$	$\left(\frac{L}{D}\right)_{max}$	$K_{LD}$	MAX Range	MAX Endurance
4160 N/m <sup>2</sup>	113.87 m <sup>2</sup>	0.246	48288 kg	8	0.8	5.007	0.0262	0.508	0.269	19.6	15.5	7570 km	9.06 hrs

**POINT PERFORMANCE:** Using the Specific Excess Power [3] equation at ISA conditions, all point performances were determined except for absolute ceiling.

$$\left(\frac{T}{W}\right)_0 = \frac{\alpha}{\beta} \left( \frac{1}{V_\infty} \frac{dh}{dt} + \frac{1}{g} \frac{dV_\infty}{dt} + \frac{\frac{1}{2} \rho V_\infty^2 C_{D0}}{\alpha \frac{W_0}{S_{ref}}} + \frac{\alpha n^2 \frac{W_0}{S_{ref}}}{\frac{1}{2} \rho V_\infty^2 \pi A R e} \right) [3]$$

Table 3: Design Process for Point Performance

Mission Segment	Reasoning and Parameters	Assumptions
Take-off and Landing Climb	Take-off climb for twin-engines consists of 3 stages, subjected to minimum climb gradients, dh/dt, of 0%, 2.4% and 1.2% respectively.[5] Similarly, landing climb (AEO) and approach climb (OEI) require dh/dt of 3.2% and 2.1% respectively.[5]	<ul style="list-style-type: none"><li>Instantaneous climb assumed such that the aircraft only operates at minimum climb gradient.</li><li>Negligible ground effects.</li></ul>
Cruise	Cruise 1 performed at 25,000 ft as per requirements. Cruise 2 and 3 performed at 36,000 ft from typical values of similar aircraft. $C_{Lmax}$ (clean configuration) = 1.9	<ul style="list-style-type: none"><li>Steady level flight.</li><li>Cruise 1 performed at Mach 0.69.</li><li>Cruise 2 &amp; 3 performed at maximum speed of Mach 0.75 (to present the most constraining situation).</li></ul>
Absolute Ceiling	Absolute ceiling is at 40,000 ft. Since $T = D_{min}$ at steady level flight, using: $\frac{T_0}{W} = \frac{T}{D_{min}} \frac{1}{1.439\sigma \left(\frac{L}{D}\right)_{max}}$ , $\left(\frac{T}{W}\right)_0$ for maximum ceiling is calculated.	<ul style="list-style-type: none"><li>Max ceiling is reached during Cruise 2 and 3.</li><li><math>\left(\frac{L}{D}\right)_{maxcruise} = 0.866 \left(\frac{L}{D}\right)_{max}</math></li><li>Clean configuration for aircraft assumed.</li></ul>

[1] Daniel P. Raymer. *Aircraft Design: A Conceptual Approach*. American Institute of Aeronautics and Astronautics. 1992.  
[2] Dr. Jan Roskam. *Airplane Design Part I: Preliminary sizing of airplanes*. Roskam Aviation and Engineering Corporation. 1985.  
[3] Dr. Errikos Levis. *Sizing to Constraints Lecture Notes*. Department of Aeronautics, Imperial College London. 2022.  
[4] Dr. Robert Hewson. *Initial Sizing Lecture Notes*. Department of Aeronautics, Imperial College London. 2022.  
[5] Part 25 Airworthiness Standards: Transport Category Airplanes, Code of Federal Regulations. 2022