

FORMULÆ FOR ME 211 INTRODUCTION TO SOLID MECHANICS



Vectors, forces and moments:

$$m{F} = m{i}F_x + m{j}F_y + m{k}F_z = \{F_x, F_y, F_z\} = m{e}|m{F}| \; ; \quad |m{F}| = \sqrt{F_x^2 + F_y^2 + F_z^2}$$

$$\boldsymbol{e} = \left\{ \frac{F_x}{|\boldsymbol{F}|}, \frac{F_y}{|\boldsymbol{F}|}, \frac{F_z}{|\boldsymbol{F}|} \right\} = \left\{ \cos \theta_x, \cos \theta_y, \cos \theta_z \right\}$$

$$oldsymbol{M} = oldsymbol{r} imes oldsymbol{F} = \left| egin{array}{ccc} oldsymbol{i} & oldsymbol{j} & oldsymbol{k} \ x & y & z \ F_x & F_y & F_z \end{array}
ight| = (yF_z - zF_y) oldsymbol{i} + (zF_x - xF_z) oldsymbol{j} + (xF_y - yF_x) oldsymbol{k} \ .$$

$$\boldsymbol{p} \cdot \boldsymbol{q} = p_x q_x + p_y q_y + p_z q_z = |\boldsymbol{p}||\boldsymbol{q}|\cos\theta$$
,

where θ is the angle between the vectors \boldsymbol{p} and \boldsymbol{q} .



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Properties of areas: Coordinates of the centroid are \bar{x}, \bar{y} where

$$A = \iint dA$$
; $A\bar{x} = \iint xdA$; $A\bar{y} = \iint ydA$; $I_x = \iint y^2dA$; $I_y = \iint x^2dA$.

In Cartesian coordinates, dA = dxdy. In polar coordinates, $dA = rdrd\theta$.

$$A = \sum A_i \; ; \quad A\bar{x} = \sum A_i x_i \; ; \quad A\bar{y} = \sum A_i y_i \; ; \quad I_x = \sum I_x^i + \sum A_i (\bar{y}_i - \bar{y})^2 \; ,$$

where I_x^i is the second moment of A_i about its own centroidal axis and I_x is the centroidal second moment of the composite area. For a circular section of radius a and diameter d = 2a,

$$I = \frac{\pi d^4}{64} = \frac{\pi a^4}{4}$$
; $J = \frac{\pi d^4}{32} = \frac{\pi a^4}{2}$.

For a rectangular section of height h and width b about a horizontal axis

$$I = \frac{bh^3}{12}$$

Bending: Relations between loading w, shear force V, bending moment M, slope θ and deflection v for a beam.

$$\frac{dV}{dx} = -w(x) \; ; \quad \frac{dM}{dx} = V(x) \; ; \quad EI\frac{d\theta}{dx} = M(x) \; ; \quad \frac{dv}{dx} = \theta(x) \; .$$

$$\frac{M}{I} = -\frac{\sigma_x}{u} = \frac{E}{R} = E\frac{d\theta}{dx} \; .$$

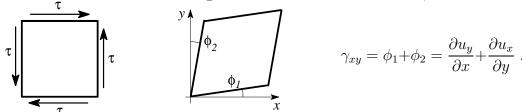
Definition of strain: Normal strain: if ϵ_x is uniform along the bar,

$$\epsilon_x = \frac{\Delta}{L} = \frac{u_B - u_A}{L_{AB}} \; ,$$

where Δ is the extension of the bar and L is its original length. If ϵ_x varies along the bar, use

$$\epsilon_x = \frac{\partial u_x}{\partial x} \ .$$

Shear strain: If the initial rectangular element deforms as shown,



Axial loading: Axial force N, cross-sectional area A.

$$\sigma_x = \frac{N}{A}$$
; $u_B - u_A = \frac{N_{AB}L_{AB}}{E_{AB}A_{AB}}$.

Torsion: (axis of the bar is along z), torque T, rotation ϕ about the axis.

$$\frac{T}{J} = \frac{\tau_{z\theta}}{r} = G\frac{d\phi}{dz} = \frac{G(\phi_B - \phi_A)}{L_{AB}}; \qquad \phi_B - \phi_A = \frac{T_{AB}L_{AB}}{G_{AB}J_{AB}}.$$

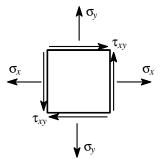
Power transmitted is $P = T\Omega$ where Ω is the angular velocity of the shaft in radians per second.

$$1 \text{ rpm } = \frac{\pi}{30} \text{ rad/s} ; 1 \text{ W} = 1 \text{ Nm/s} ; 1 \text{ hp } = 550 \text{ ft lb/s}$$

Multiaxial Hooke's law:

$$\begin{split} \epsilon_x &= \frac{\sigma_x}{E} - \frac{\nu \sigma_y}{E} - \frac{\nu \sigma_z}{E} + \alpha \Delta T \\ \epsilon_y &= \frac{\sigma_y}{E} - \frac{\nu \sigma_x}{E} - \frac{\nu \sigma_z}{E} + \alpha \Delta T \\ \epsilon_z &= \frac{\sigma_z}{E} - \frac{\nu \sigma_x}{E} - \frac{\nu \sigma_y}{E} + \alpha \Delta T \; . \\ \\ \gamma_{yz} &= \frac{\tau_{yz}}{G} \; ; \quad \gamma_{zx} = \frac{\tau_{zx}}{G} \; ; \quad \gamma_{xy} = \frac{\tau_{xy}}{G} \; ; \quad G = \frac{E}{2(1+\nu)} \; . \end{split}$$

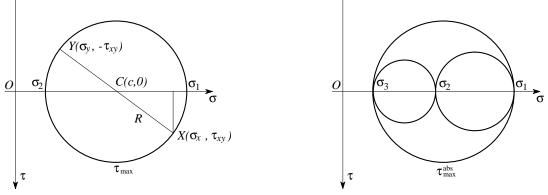
Stress transformation equations: Sign convention for stress components in two dimensions:



For stresses on a specified plane (rotated counterclockwise through θ from x) use

$$\sigma_{x'} = \sigma_x \cos^2 \theta + \sigma_y \sin^2 \theta + 2\tau_{xy} \sin \theta \cos \theta$$
$$\tau_{x'y'} = \tau_{xy} (\cos^2 \theta - \sin^2 \theta) + (\sigma_y - \sigma_x) \sin \theta \cos \theta$$

For principal stresses σ_1, σ_2 or maximum shear stress use Mohr's circle:-



where

$$R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$
; $c = \frac{\sigma_x + \sigma_y}{2}$; $\sigma_1, \sigma_2 = c \pm R$; $\tau_{\text{max}} = R$.

If the stress element is rotated through an angle θ , the points X,Y on the circle will move around the circle through an angle 2θ in the same direction. If the third principal stress σ_3 is known, sketch three Mohr's circles and the absolute maximum shear stress $\tau_{\rm max}^{\rm abs}$ is the radius of the largest circle.

Strain transformation equations: (for strain gages)

$$\epsilon_{x'} = \epsilon_x \cos^2 \theta + \epsilon_y \sin^2 \theta + \gamma_{xy} \sin \theta \cos \theta$$
$$\gamma_{x'y'} = \gamma_{xy} (\cos^2 \theta - \sin^2 \theta) + 2(\epsilon_y - \epsilon_x) \sin \theta \cos \theta$$

Discontinuity functions

$$\langle x - a \rangle^n = 0 ; x < a$$

$$= (x - a)^n ; x > a$$

$$\int \langle x - a \rangle^n dx = \frac{\langle x - a \rangle^{n+1}}{n+1} ; \int \delta(x-a) dx = H(x-a) = \langle x - a \rangle^0$$

Trigonometric identities and integrals:

$$\sin^2 x + \cos^2 x = 1 \; ; \quad \cos^2 x = \frac{1 + \cos(2x)}{2} \; ; \quad \sin^2 x = \frac{1 - \cos(2x)}{2} \; ;$$
$$\sin(2x) = 2\sin x \cos x \; ; \quad \cos(2x) = \cos^2 x - \sin^2 x \; .$$
$$\int_0^{n\pi/2} \cos^2 x dx = \int_0^{n\pi/2} \sin^2 x dx = \frac{n\pi}{4} \; , \text{ where } n \text{ is any integer } .$$