NMOS FET Equations

Triode Region

$$i_D = k'_n \left(\frac{W}{L}\right) \left(v_{OV}v_{DS} - \frac{1}{2}v_{DS}^2\right) = k'_n \left(\frac{W}{L}\right) \left((v_{GS} - V_t)v_{DS} - \frac{1}{2}v_{DS}^2\right)$$

Saturation Region

$$i_D = \frac{1}{2} k'_n \left(\frac{W}{L}\right) v_{OV}^2 = \frac{1}{2} k'_n \left(\frac{W}{L}\right) (v_{GS} - V_t)^2$$

PMOS FET Equations

Triode Region

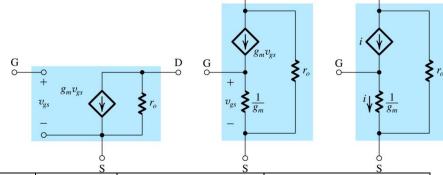
$$i_{D} = k'_{p} \left(\frac{W}{L}\right) \left(|v_{OV}|v_{SD} - \frac{1}{2}v_{SD}^{2}\right) = k'_{p} \left(\frac{W}{L}\right) \left((v_{GS} - |V_{t}|)v_{SD} - \frac{1}{2}v_{SD}^{2}\right)$$

Saturation Region

$$i_D = \frac{1}{2} k_p' \left(\frac{W}{L} \right) v_{OV}^2 = \frac{1}{2} k_p' \left(\frac{W}{L} \right) (v_{GS} - |V_t|)^2$$

$$g_m = \frac{2I_D}{V_{OV}} = k_n' \left(\frac{W}{L}\right) (V_{GS} - V_t)$$

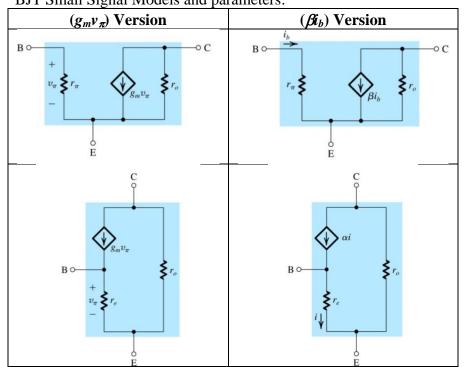
$$r_o = \frac{1}{\lambda I_D} = \frac{V_A}{I_D}$$



Characteristics of MOSFET Amplifiers

| | | | S | S | S |
|---------------------------------------|----------------|--|---|---|---|
| Amplifier type | R_{in} | A_{vo} | R_o | $A_{ u}$ | $G_{ u}$ |
| Common source | ∞ | $-g_{m}R_{o}$ | R_D or $(R_D \parallel r_o)$ | $-g_{m}\left(R_{o} R_{L}\right)$ | $-g_{m}\left(R_{o} \parallel R_{L}\right)$ |
| Common source with R_S | ∞ | $-\frac{g_m R_o}{1 + g_m R_s}$ | R_{D} or $\left(R_{D} \parallel r_{o}\right)$ | $-\frac{g_m(R_o R_L)}{1 + g_m R_s}$ | $-\frac{g_m(R_o R_L)}{1+g_m R_s}$ |
| Common gate | $1/g_m R_s$ | $g_m R_o$ | R_D or $(R_D \parallel r_o)$ | $g_{m}\left(R_{o} R_{L}\right)$ | $\left(\frac{R_{in}}{R_{in} + R_{sig}}\right) g_m \left(R_o \parallel R_L\right)$ |
| Common drain or source follower | ∞ | $ \begin{array}{c} 1 \text{ w/o } r_o \\ \text{or} \\ \frac{r_o}{r_0 + \left(1/g_m\right)} \end{array} $ | $1/g_m R_s$ | $\frac{R_L \parallel r_o}{\left(R_L \parallel r_o\right) + \left(1/g_m\right)}$ | $\frac{R_L \parallel r_o}{\left(R_L \parallel r_o\right) + \left(1/g_m\right)}$ |

BJT Small Signal Models and parameters:



$$g_m = \frac{I_C}{V_T}$$

$$r_\pi \equiv \frac{v_{be}}{i_b} = \frac{\beta}{g_m} = \frac{V_T}{I_b}$$

$$r_e \equiv \frac{v_{be}}{i_e} = \frac{V_T}{I_E} = \frac{\alpha}{g_m}$$

$$r_o = \frac{|V_A|}{I_C}$$

Characteristics of BJT Amplifiers (with and without r_o):

| Amplifier type | R_{in} | A_{vo} | R_o | $A_{ u}$ | $G_{ u}$ |
|---|-------------------------------|--|---|--|--|
| Common emitter | $(\beta+1)r_e$ or r_π | $-g_{m}R_{o}$ | R_C or $\left(R_C \parallel r_o\right)$ | $-g_m(R_o R_L)$ | $-\left(\frac{R_{in}}{R_{in}+R_{sig}}\right)g_{m}\left(R_{o} R_{L}\right)$ |
| Common emitter with R_e | $(\beta+1)(r_e+R_e)$ | $-\frac{g_m R_o}{1+g_m R_e}$ | R_C or $(R_C \parallel r_o)$ | $-\frac{g_m\left(R_o \parallel R_L\right)}{1+g_m R_e}$ | $-\left(\frac{R_{in}}{R_{in}+R_{sig}}\right)\frac{g_m(R_o \parallel R_L)}{1+g_mR_e}$ |
| Common base | $r_{e} \parallel R_{E}$ | $g_m R_o$ | R_C or $(R_C \parallel r_o)$ | $g_m\left(R_o \mid\mid R_L\right)$ | $\left(\frac{R_{in}}{R_{in}+R_{sig}}\right)g_m\left(R_o \parallel R_L\right)$ |
| Common collector or emitter follower | $(\beta+1)(r_e+(R_L R_o))$ | $ \begin{array}{c} 1 \text{ w/o } r_o \\ \text{or} \\ \hline \frac{r_o}{r_0 + r_e} \end{array} $ | $r_o \parallel R_{\scriptscriptstyle E}$ | $\frac{R_L \parallel r_o}{\left(R_L \parallel r_o\right) + r_e}$ | $\left(\frac{R_{in}}{R_{in} + R_{ig}}\right) \frac{R_L \parallel R_o}{\left(R_L \parallel R_o\right) + r_e}$ $R_{out} = r_o \parallel R_E \parallel \left(r_e + \frac{R_B \parallel R_{sig}}{\left(\beta + 1\right)}\right)$ |

Quadratic Equation:

Roots of
$$ax^2 + bx + c = 0$$
 are $\frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$