A large, light blue watermark of the University of Delaware seal is centered in the background. The seal is circular with the text "SIGILLUM UNIVERSITATIS DELAWARENSIS" around the top and "1743" at the bottom. Inside the seal is a shield with the words "GRAMM", "METAPH", "RHETOR", "MATHEM", "ETHICA", and "PHYSICA" arranged around a central "SOL" and "MENTIS EST".

Exam #1

Chapters 1 and 2

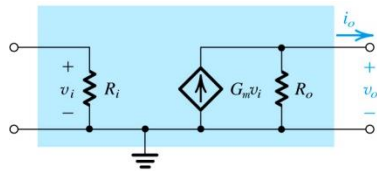
Solutions

I. Amplifier Types

In V Out I
Type Transconductance
Ideal Characteristics

$$R_i = \underline{\infty \Omega}$$

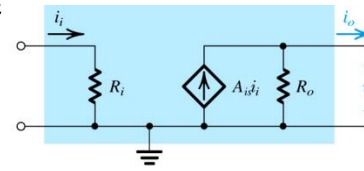
$$R_o = \underline{\infty \Omega}$$



In I Out I
Type Current
Ideal Characteristics

$$R_i = \underline{0 \Omega}$$

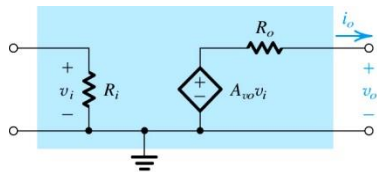
$$R_o = \underline{\infty \Omega}$$



In V Out V
Type Voltage
Ideal Characteristics

$$R_i = \underline{\infty \Omega}$$

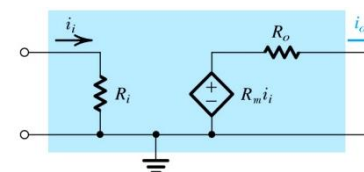
$$R_o = \underline{0 \Omega}$$



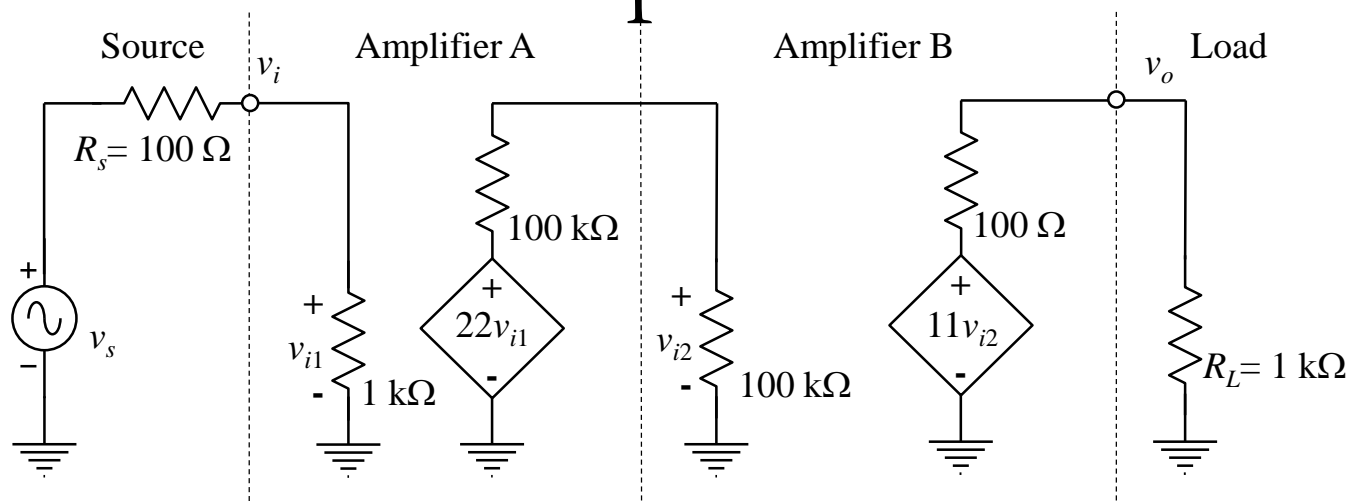
In I Out V
Type Transresistance
Ideal Characteristics

$$R_i = \underline{0 \Omega}$$

$$R_o = \underline{0 \Omega}$$



II. Amplifier Gain



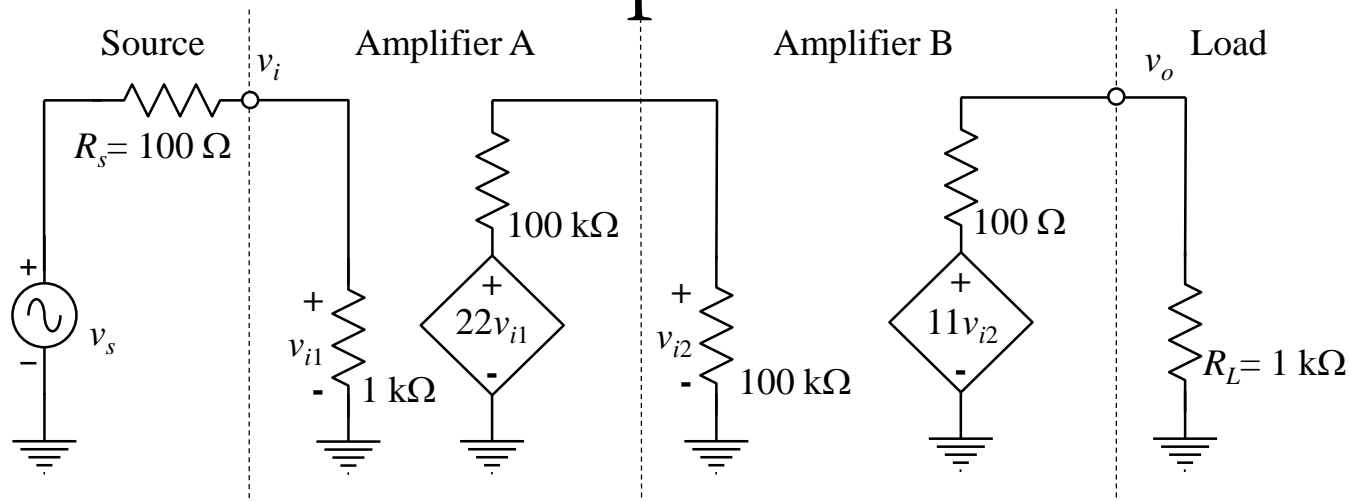
Find the cascaded amplifier voltage gain, A_v , as well as the overall circuit voltage gain both as V/V ratios and in dB. Show your work!

$$v_{inB} = v_i (22) \left(\frac{100\text{k}\Omega}{100\text{k}\Omega + 100\text{k}\Omega} \right) = 11v_i$$

$$v_o = 11v_{inB} \left(\frac{1\text{k}\Omega}{1\text{k}\Omega + 0.1\text{k}\Omega} \right) = 10v_{inB} = 10(11v_i) = 110v_i$$

$$\Rightarrow A_v \equiv \frac{v_o}{v_i} = 110 \text{ V/V} = 40.83 \text{ dB}$$

II. Amplifier Gain



Find the cascaded amplifier voltage gain, A_v , as well as the overall circuit voltage gain both as V/V ratios and in dB. Show your work!

$$\Rightarrow G_v \equiv \frac{v_o}{v_s} = A_v \frac{1 \text{ k}\Omega}{1.1 \text{ k}\Omega} = 110 \left(\frac{1}{1.1} \right) = 100 \text{ V/V} = 40.0 \text{ dB}$$



III. Definitions (10 points)

Answers:

- | | | |
|----------------------|--------------------------|----------------------------|
| A. Bipolar | F. Frequency Spectrum | K. Thevenin |
| B. Decade | G. Fundamental Frequency | L. Transducer |
| C. Decibel | H. Linearity | M. Transfer Characteristic |
| D. Discretization | I. Norton | N. Transfer Function |
| E. Fourier Transform | J. Octave | O. Unilateral |

J Change in frequency by a factor of 2; i.e. a doubling or halving of the frequency.

C Log based ratio or measurement of gain

E Mathematical tool for converting between time domain and frequency domain.



III. Definitions (10 points)

Answers:

- | | | |
|----------------------|--------------------------|----------------------------|
| A. Bipolar | F. Frequency Spectrum | K. Thevenin |
| B. Decade | G. Fundamental Frequency | L. Transducer |
| C. Decibel | H. Linearity | M. Transfer Characteristic |
| D. Discretization | I. Norton | N. Transfer Function |
| E. Fourier Transform | J. Octave | O. Unilateral |

L Device that converts real world, or physical, signals into electrical signals.

F The frequency components that make a signal.

O Signal flow is unidirectional, from input to output.

B Change in frequency by a factor of 10; i.e. an order of magnitude increase or decrease in frequency.



III. Definitions (10 points)

Answers:

- | | | |
|----------------------|--------------------------|----------------------------|
| A. Bipolar | F. Frequency Spectrum | K. Thevenin |
| B. Decade | G. Fundamental Frequency | L. Transducer |
| C. Decibel | H. Linearity | M. Transfer Characteristic |
| D. Discretization | I. Norton | N. Transfer Function |
| E. Fourier Transform | J. Octave | O. Unilateral |

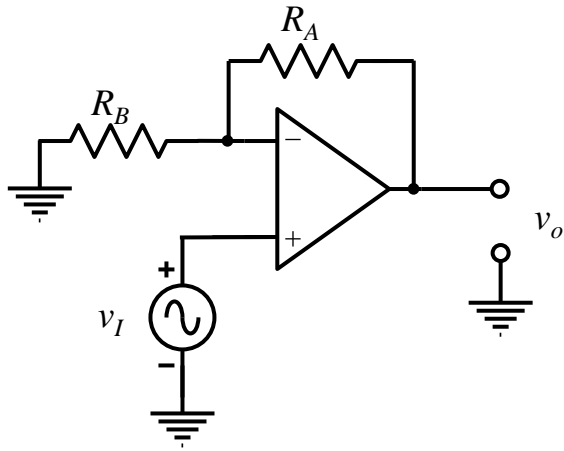
H Measurement of how close the output signal is to a scaled version of the input.

M The output voltage as a function of input voltage.

N Relation between the input and output of a linear time-invariant system with respect to frequency



IV. Solve for the closed loop gain



$$v_{Id} = \frac{v_O}{A} \approx 0$$

$$i_{R_B} = \frac{v_I}{R_B}$$

$$v_O = v_I + i_{R_B} R_A = v_I + \frac{v_I}{R_B} R_A = v_I \left(1 + \frac{R_A}{R_B} \right)$$

$$A_v \equiv \frac{v_O}{v_I} = 1 + \frac{R_A}{R_B}$$

Alternate derivation – voltage divider

$$v_- = v_O \left(\frac{R_B}{R_B + R_A} \right) = v_I \Rightarrow A_v \equiv \frac{v_O}{v_I} = \left(\frac{R_B + R_A}{R_B} \right) = 1 + \frac{R_A}{R_B}$$

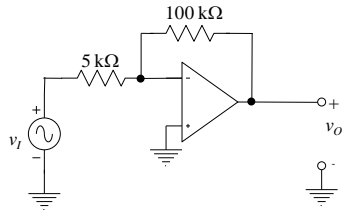


V. Ideal Op Amp

1. input impedance infinite Ω
2. output impedance zero Ω
3. common-mode gain zero V/V
4. common-mode rejection infinite V/V or dB
5. open-loop gain, A infinite V/V
6. bandwidth infinite Hz

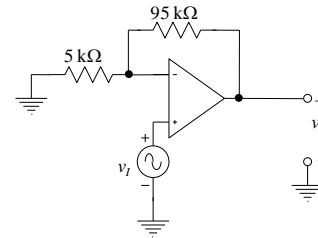


VI. Calculate the Voltage Gain



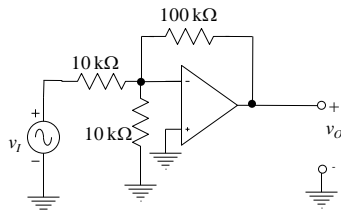
$$-100\text{k}/5\text{k} = -20$$

$$A_v = \underline{-20} \text{ V/V } \underline{26.0} \text{ dB}$$



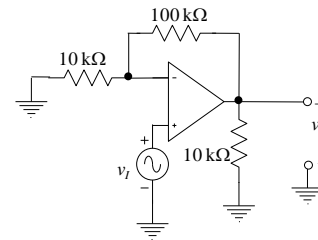
$$1 + 95\text{k}/5\text{k} = 20$$

$$A_v = \underline{20} \text{ V/V } \underline{26.0} \text{ dB}$$



$$-100\text{k}/10\text{k} = -10$$

$$A_v = \underline{-10} \text{ V/V } \underline{20} \text{ dB}$$

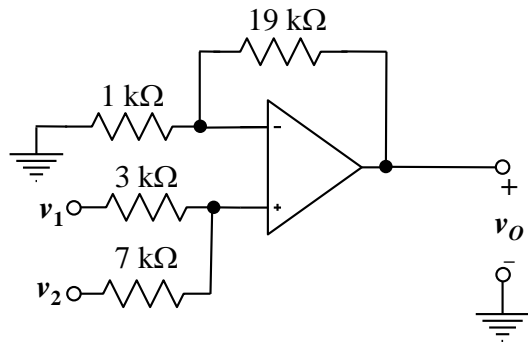


$$= 1 + 100\text{k}/10\text{k} = 11$$

$$A_v = \underline{11} \text{ V/V } \underline{20.83} \text{ dB}$$



VII. Superposition principle



Use the superposition principle to find the output voltage as a function of the two input voltages of the circuit shown.

Ground v_1 first

$$v_o = v_2 \left(\frac{3\text{k}\Omega}{3\text{k}\Omega + 7\text{k}\Omega} \right) \left(1 + \frac{19\text{k}\Omega}{1\text{k}\Omega} \right) = v_2 \left(\frac{3}{10} \right) (20) = 6v_2$$

Then ground v_2

$$v_o = v_1 \left(\frac{7\text{k}\Omega}{7\text{k}\Omega + 3\text{k}\Omega} \right) \left(1 + \frac{19\text{k}\Omega}{1\text{k}\Omega} \right) = v_1 \left(\frac{7}{10} \right) (20) = 14v_1$$

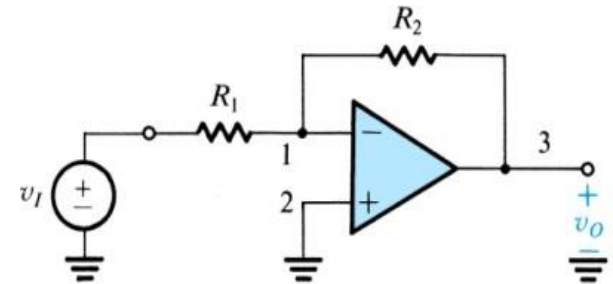
Then add the two outputs

$$v_o = 14v_1 + 6v_2$$

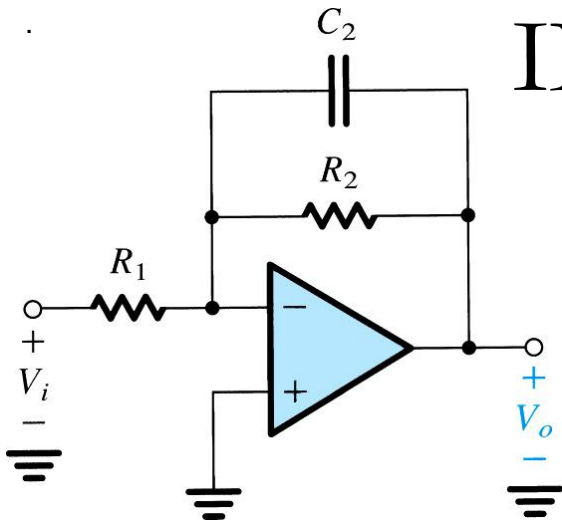
VIII. Inverting Amplifier Solutions

You are provided with an ideal op amp, one 10-k Ω , and two 40-k Ω resistors. *Using all three resistors* with series and parallel resistor combinations there are 8 different inverting-amplifier circuit topologies possible. Fill in the table below for all 8 configurations.

Config	R_1	R_2	v_o/v_i	R_{in}
1	10k Ω	40k Ω +40k Ω	-8 V/V	10 k Ω
2	10k Ω	40k Ω 40k Ω	-2 V/V	10 k Ω
3	40k Ω	10k Ω +40k Ω	-1.25 V/V	40 k Ω
4	40k Ω	10k Ω 40k Ω	-0.2 V/V	40 k Ω
5	40k Ω +40k Ω	10k Ω	-0.125 V/V	80 k Ω
6	40k Ω 40k Ω	10k Ω	-0.5 V/V	20 k Ω
7	10k Ω +40k Ω	40k Ω	-0.8 V/V	50 k Ω
8	10k Ω 40k Ω	40k Ω	-5 V/V	8 k Ω



Assuming that you want the magnitude of the gain to be more than 4x, which is the best configuration and why?



IX. Miller Integrator

For the Miller Integrator with feedback resistor circuit shown, answer the following questions:

Don't forget proper units.

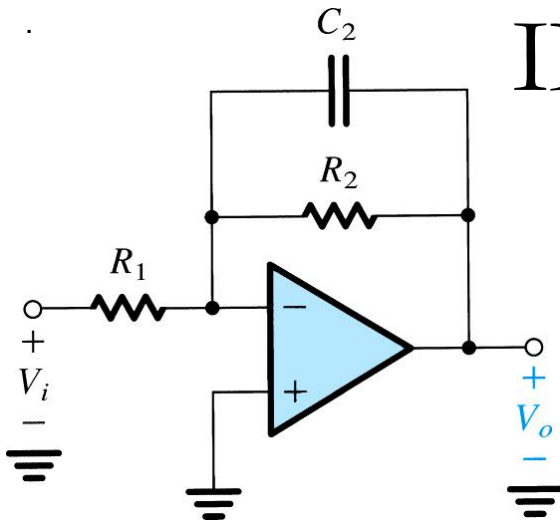
Derive an expression for the low pass transfer function $V_o(s)/V_i(s)$ in the form

$$T(j\omega) = \frac{K}{1 + j(\omega/\omega_0)}$$

$$Z_1 = R_1, Z_2 = R_2 \parallel (1/sC_2) = \frac{R_2}{1 + sC_2R_2}$$

$$\frac{V_o(s)}{V_i(s)} = -\frac{Z_2}{Z_1} = \frac{-R_2/R_1}{1 + sC_2R_2}$$

$$K = -\frac{R_2}{R_1} \quad \omega_0 = \frac{1}{C_2R_2}$$



IX. Miller Integrator

For the Miller Integrator with feedback resistor circuit shown, answer the following questions:

Don't forget proper units.

$$\frac{V_o(s)}{V_i(s)} = -\frac{Z_2}{Z_1} = \frac{-R_2/R_1}{1 + sC_2R_2}$$

Design the circuit to obtain a dc gain of 40 dB, a 3-dB frequency of 15.915 kHz, and an input resistance of 1 kΩ.

$$R_1 = 1\text{k}\Omega$$

$$K = -\frac{R_2}{R_1} = 40\text{dB} = 100\text{V/V} \Rightarrow R_2 = 100\text{k}\Omega$$

$$\omega_0 = \frac{1}{C_2R_2} = 2\pi f_0 = 2\pi \times 15.915\text{kHz} \Rightarrow C_2 = 100.0\text{pF}$$

X. Difference Amplifier Circuit

For a difference amplifier as shown the differential and common mode gains are given by the following:

$$A_d \equiv \frac{v_o}{v_{id}} = \frac{R_2}{R_1} \text{ with the condition that } \frac{R_2}{R_1} = \frac{R_4}{R_3}$$

$$A_{cm} \equiv \frac{v_o}{v_{icm}} = \frac{R_4}{R_4 + R_3} \left(1 - \frac{R_2}{R_1} \frac{R_3}{R_4} \right)$$

Analyze the difference amplifier shown to the right for the case $R_1 = R_3 = 4.7 \text{ k}\Omega$, and $R_2 = R_4 = 470 \text{ k}\Omega$.

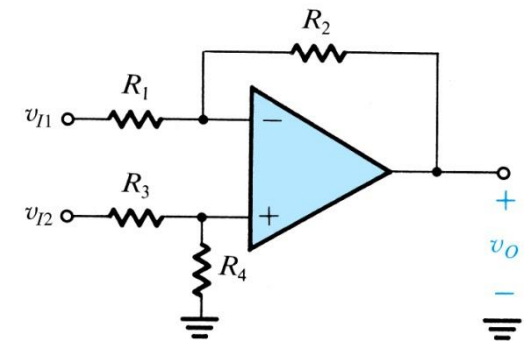
What is the differential input resistance R_{id} ? Find the common-mode gain, A_{cm} , the differential mode gain, A_d , and calculate the CMRR in dB. Don't forget proper units.

$$R_{id} = 4.7\text{k}\Omega + 4.7\text{k}\Omega = 9.4\text{k}\Omega$$

$$A_d = 470\text{k}\Omega / 4.7\text{k}\Omega = 100\text{V/V}$$

$$A_{cm} = 0\text{V/V}$$

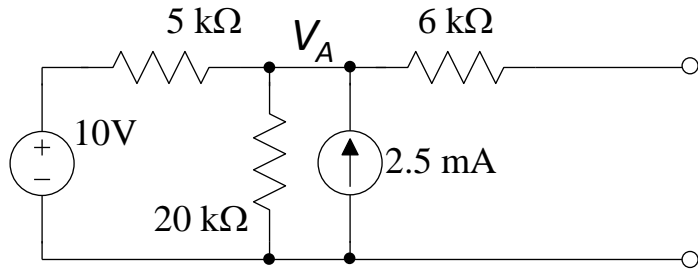
$$\text{CMRR} = \infty\text{V/V}$$



$$\text{CMRR} = 20 \log \left(\frac{|A_d|}{|A_{cm}|} \right)$$



E.C. Thevenin and Norton Equivalent Circuits – Nodal Solution



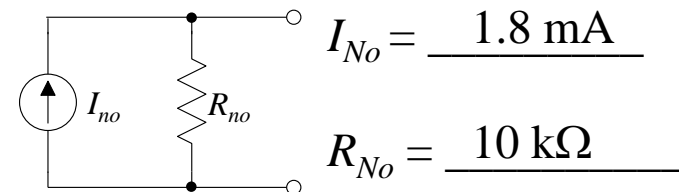
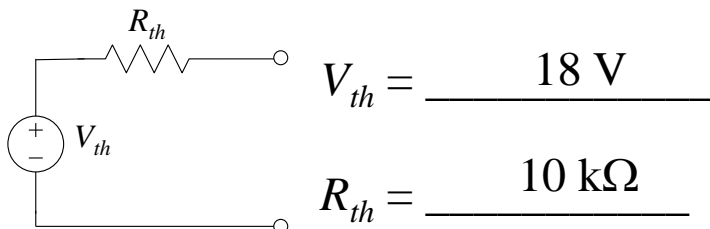
$$\frac{V_A - 10V}{5k\Omega} + \frac{V_A}{20k\Omega} - 2.5mA = 0$$

$$\frac{V_A}{5k\Omega} + \frac{V_A}{20k\Omega} - \frac{10V}{5k\Omega} - 2.5mA = 0$$

$$V_A \left(\frac{1}{5k\Omega} + \frac{1}{20k\Omega} \right) = V_A \left(\frac{5}{20k\Omega} \right) = 2mA + 2.5mA = 4.5mA$$

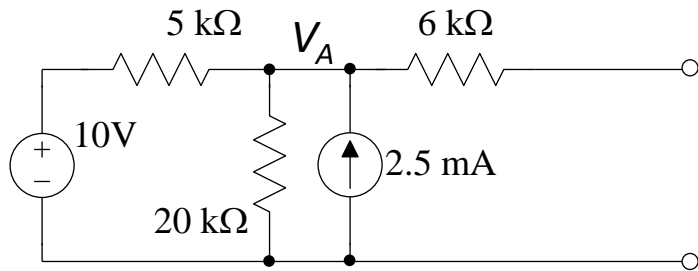
$$V_A = V_{th} = (4k\Omega \times 4.5mA) = 18V$$

$$I_{No} = \frac{V_{th}}{R_{th}} = \frac{18V}{10k\Omega} = 1.8mA$$





E.C. Thevenin and Norton Equivalent Circuits-Superposition Solution



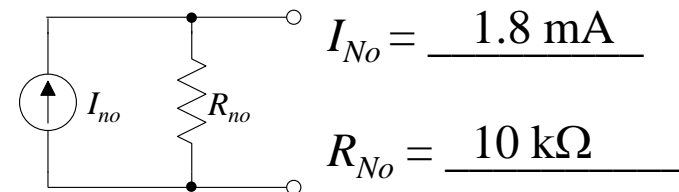
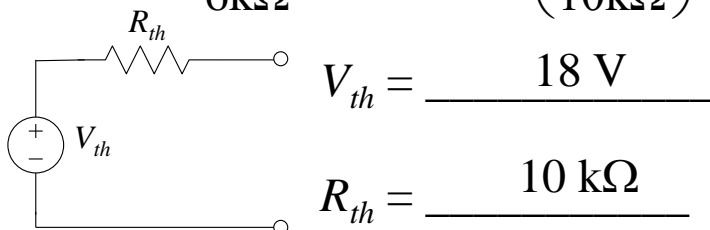
$$10V \left(\frac{20k\Omega}{20k\Omega + 5k\Omega} \right) = 8V$$

$$2.5mA (5k\Omega \parallel 10k\Omega) = 2.5mA (4k\Omega) = 10V$$

$$V_{th} = 10V + 8V = 18V$$

$$I_{No} = \frac{10V \left(\frac{20k\Omega \parallel 6k\Omega}{(20k\Omega \parallel 6k\Omega) + 5k\Omega} \right)}{6k\Omega} + 2.5mA \left(\frac{20k\Omega \parallel 5k\Omega}{(20k\Omega \parallel 5k\Omega) + 6k\Omega} \right)$$

$$= \frac{10V(0.48)}{6k\Omega} + 2.5mA \left(\frac{4k\Omega}{10k\Omega} \right) = 0.8mA + 1.0mA = 1.8mA$$





Exam #1 Results

Tests 92
Average 87.9 %
High 104% (2)
Low 46.5%

