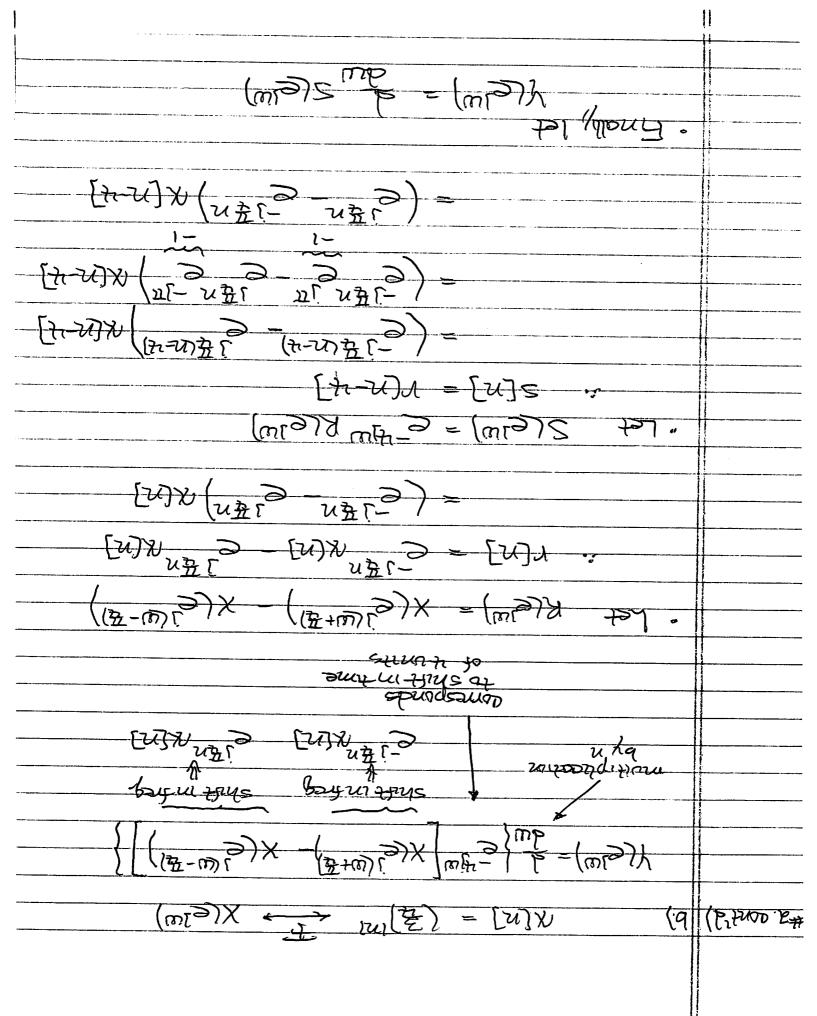
|     | SOLUTIONS TO EXAM #3 (5/14/19)   |
|-----|--|
| 本1. | a) y[n] + \( \frac{1}{2} \left[ \frac{1}{2} \right[ \frac{1}{2} \right] = 5 \kin] - \( \frac{1}{2} \kin \right[ \frac{1}{2} \right] - \( \frac{1}{2} \kin \right[ \frac{1}{2} \kin \right] - \( \frac{1}{2} \kin \rin \right] - \( \frac{1}{2} \kin \right] - \( \frac{1}{2} \kin \r |
|     | = 5χ(e <sub>1</sub> ω) - ξ e <sub>-1</sub> ω χ(e <sub>1</sub> ω) = 5χ(e <sub>1</sub> ω) - ξ e <sub>-1</sub> ω χ(e <sub>1</sub> ω)  |
|     | 1(6/m) [1+ 1 = 1m = = 3/m] = X(6/m) [5- 2 = 3/m]   |
|     | H(e/w) = Y(e/w) 1+ = = = = = = = = = = = = = = = = = =   |
|     | b) h[n] = 7-1 {H(e)w}  |
|     | $\frac{1+56.10}{1+56.10} = \frac{1+56.10}{2-26.20}$  |
|     | (1+ \frac{1}{4}e^{3w})(1-\frac{3}{3}e^{-3w})   |
|     | - A B<br>1+音e3w 1-音e-3w  |
|     | Let $v = e^{-1w}$ ,  H( $e^{1w}$ ) - A B $1 + \frac{1}{3}v + \frac{1}{3}v$   |
|     | A=H(e <sup>1w</sup> )(1+3v) = 5-75 U = 1-3v  = 5+7  = 1  |
|     | B=H(e)(1-35) = 5- 55   |
|     | = 5- \frac{5}{3} - \frac{5}{3} - \frac{1}{3} |

| *1 b. cont'2) | # H(e <sup>1w</sup> ) = 4 1<br>1+1=1w + 1-1=1w   |
|---------------|--|
|               | ₩ <b>∓</b> -′  |
|               | $h[n] = 4(-\frac{1}{2})^n u[n] + (\frac{1}{3})^n u[n]$   |
| #2.           | denning sum  |
|               | We will use proporties here:   |
|               | Let $y(n) = (\frac{1}{a})^n u(n) \Rightarrow y(e^{\frac{1}{a}u}) = \frac{1}{1-\frac{1}{a}e^{\frac{1}{a}u}}$  |
|               | Then, let $r[n] = (\frac{1}{2})^2 y(n-2)$  |
|               | in phase shift in frequency (Liw) = (4) e gw Y(Liw)  |
|               | Finally, $\chi(n) = e^{\int \frac{\pi}{4}n} r(n)$ phase shaft in time results  |
|               | shift in frequency  = X(elu) = R(ei(u-Ti))   |
|               | = (山) = ja(w-程) Y(ej(w-程))   |
|               | = L e = J = J = J = J = J = J = J = J = J =  |
|               | $= \frac{j}{4} = \frac{3}{1 - 1} = \frac{1}{3} = \frac{3}{1} $ |
|               | Tace   |
|               |  |



| tab contal                              | ~ y[n]= jns[n]  |
|---|---|
|   | = jn(e <sup>1#n</sup> e <sup>1#n</sup> ) x(n-4)   |
|   | aj sin #n   |
|   | $y[n] = -an(sin \frac{\pi}{4}n) \left(\frac{3}{4}\right)^{n-4}$   |
|   | 7-3   |
|   | c) w x(e)w) = \$\alpha(n)e^{-1wn}   |
|   | $N=-\infty$   |
|   | $\frac{1}{n} \times (e^{j0}) = \underbrace{\frac{1}{n}}_{n=-\infty} \times (n) e^{-jwn} = \underbrace{\frac{1}{n}}_{iv=0} \times (n)$   |
|   | <u> </u>  |
|   | $(ii)  N(n) = L \left( \frac{1}{2} \left( \frac{1}{2} \left( \frac{1}{2} \right) \right) \frac{1}{2} \frac{1}{$ |
|   | $\frac{(ii)}{X(n)} = \frac{1}{2\pi} \left\{ X(e^{(iv)}) e^{(iv)} dv \right\}$   |
|   | * ( X(e)w) e yw dw = 2 tt x[n]   n=4  |
|   |   |
|   | = 211(i)<br>= 211   |
|   |   |
| #3.                                     | a) Nyquist note = 2 Um, where Um is the highest frequency in the signal   |
|   | highest trequency in the signal   |
|   | Wm= a rad/sec   |
|   | 5. Nyquist rate = alum = 4 mad/sec  |
|   |   |
|   | b.) Sample at twice the Nyquest rate > W== 8 rad/sec<br>Spectrum repeats at the sample rate   |
|   | - yes on repeats at the somme rate.   |
|   |   |
|   | -10 -8 -4 -4 -3 0 2 4 6 8 20 W  |
| • | -10 -8 -6 -4 -2 0 2 4 6 8 10 W  |
| 11                                      |   |

•

| ·  |  |
|--|--|
| *3. cont'd)  | a) Sample at not the Nyquest vale > W= a rad/sec             |
|  | Spectrum repeats at the sample rate ->                       |
|  | repeats of speatrum will overlap                             |
|  |  |
|  |  |
|  | -4 -3 6 A 4  |
|  | 11   |
|  |  |
|  | Cannot recover original                                      |
|  | 2500xxx  |
|  |  |
| #4;  | a) 115 = 55+16 = Y(5)  |
|  | (a) $H(5) = \frac{55+16}{5^{2}+65+8} = \frac{1}{2}(5)$       |
|  | Y(s)(53+65+8) = X(s)(55+16)                                  |
|  | 1(3)(3+63+8)   |
|  | 52 Y(5) + 65 Y(5) + 8 Y(5) = 55 X(5) + 16 X(5)               |
|  | W X-1  |
|  |  |
|  | 3 4 1 + 6 gally + 8 M2) = 2 gally + 18 MM                    |
|  | de de  |
|  |  |
|  | b) H(5) = 55+16<br>(5+4)(5+2)                                |
|  |  |
|  | poles: H(s) -> 00 5=-2, 5=-4                                 |
|  | $\frac{1}{2}ens: H(s) \rightarrow 0$ $S = -16/5, S = \infty$ |
|  | Imfol x pole   |
|  | ० ५००  |
|  |  |
| To the state of th | -5 A -3 -2 -1 1 2 3 Retsh                                    |
|  |  |
|  |  |
|  |  |
| •  |  |

|             | w.03(15  |
|-------------|--|
| 4.b. conta) | c) /   -   |
|             |  |
|             |  |
|             | -5 X-4 -3 X-2 -1   |
|             |  |
|             |  |
| 1062        | of leftmost ) napt of naphtmost pole                         |
| 200         | of leftmost pole  Refs1<-4  Refs2>-2                         |
| 1           | signal RS signal   |
|             |  |
|             | acousal and stable   |
|             | between the poles  |
|             | -44Re4534-2  |
|             | 25 signa   |
|             |  |
|             | di hiti= 2-1/H(s)} ROC: Refs/7-2                             |
|             | causal   |
|             | $H(s) = \frac{5s+16}{5^{3}+65+8} = \frac{5s+16}{(5+4)(5+3)}$ |
|             |  |
|             | = A + B<br>5+4 5+2   |
|             | 377 312  |
|             | A= H(5)(5+4) = 55+16 =-4=2                                   |
|             |  |
|             | R=H(5/5+3) = 55+16 = 6=3                                     |
|             | 13=-2 5+4 3=-a   |
|             | 7 2  |
|             | H(=) = 3+4 = , Re(=) >-3                                     |
|             | -,,  |
|             | ht= a = 4 vt+ 3 = 2 vt                                       |
|             |  |

| #5.  | a) NH= et d [= 24 [= 24 ] * d2 [= et (+)]   |
|--|---|
| A children of the children of  | y2(t)   |
| A de la companya de l | 7,(t) (X3(t))   |
|  | $X(s) = X_{1}(s)X_{3}(s)$   |
| ar manager   | $X_{1}(s) = Z_{1}(s-1)$ $Y_{2}(s) = \frac{1}{5+1}$ Refs \( (-1)   |
|  | $Y_1(3) = -\frac{1}{5+a}$ , Refs \( \( -a \) \( X_2(3) = \( 5^2 \) \( Y_3(3) = \( 5^2 \) \( |
|  | $= \frac{5^{2}}{8^{2}}, Re^{3} < -1$ $X_{1}(5) = \frac{-5 - 1}{5 - 1 + 2} = \frac{-(5 - 1)}{5 + 1}$ $Re^{3} < -1 (5hifted)$   |
|  | Re[5] 4-1 (5hifted)   |
|  | " X(5) = X1(5) X2(5) = (1-5)52, Refs <-1  |
|  | b) There are three poles: -1, 1+j, 1-j  4) Causal? Yes, this system as he causal. If  the ROC is to the right of the rightmost pole, i.e., Rels! > 1, the system is causal.  4) Stable? Yes, this system can be stable.  If the ROC contains the yw-axis  (i.e., -1 < Rels! <1), the system is stable.  (w) Both causal and stable? No. For a system to be causal and stable, all the poles must be  in the LHP.  |

| 500m2)     | $R(s) = \frac{2s+3}{5(5+5)}$                       |
|------------|--|
|            | 5(5+5)   |
|            |  |
|            | White as to ot                                     |
|            | Use Inital Value Theorem                           |
|            | $h(0^+) = \lim_{s \to \infty} SX(s)$               |
|            | = 1m = 25+3  |
|            | 5-70 \$(5+5)                                       |
|            | - lim 25+3 - 2                                     |
|            | 570 575  |
|            | w htt) as t-> 0                                    |
|            | Use Final Value Theorem                            |
|            |  |
|            | 11m htt)= lim 5 x(5)                               |
|            | = 11m × 25+3                                       |
|            | 5-70 \$ (5+5)                                      |
|            | = lim 25+3 = 3                                     |
|            | 570 5+5 5  |
| 3/20 22    | 1 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1           |
| 2 tra 1 #1 |  |
|            | ₩Z   |
|            | 1+(5)= 1, Refs/>1 => not-stable, 1200 does         |
|            | 3-1 not contain ju-oxis                            |
|            | So, we must move the pole to the LITP              |
|            | So, we must more the poleto the LHP using feedback |
|            |  |
|            | X(t) + D > h(t) 1 (t)                              |
|            |  |
|            | I A K  |
|            |  |
|            |  |
|            |  |

| #1 (cont')   | From the feedback structure,  |
|--|---|
| 210000   | Y(s) = H(s) (X(s) - AY(s))  |
|  | Y(5)(1+AH(5)) = H(5)X(5)  |
|  | : 11 (s) - H(s)   |
|  | 1 + AH(3)   |
|  | <u> </u>  |
|  | 1 + A/(5-1)   |
|  |   |
|  | 5+(A-1)   |
|  |   |
|  | To make this system stable, the pole must be moved to the left half plane   |
|  | be moved to the left half plane   |
|  |   |
|  | A-1 > 0   |
|  | 2°. A>1   |
| Extra # 2  | When an impulse is input to a second-order system, based on the value of the damping ratio, three reactions are possible. As described in class, the three possible responses are called underdamped, critically damped and overdamped. In an underdamped system, because the damping ratio is low, the response rises and oscillates around the steady state. The amplitude of the oscillation decreases over time to zero. In a critically damped system, the damping ratio is just right and the response reaches the steady state as fast as possible without oscillating. In an overdamped system, because the damping ratio is high, it takes a longer time for the impulse response to achieve the final steady state. |
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| The second secon |   |
| *  |   |
|  |   |