PEKING UNIVERSITY

Advanced Fluid Mechanics Homework 5

College of Engineering 2001111690 袁磊祺

January 20, 2021

1

$$\frac{u}{U} = 1 - \exp\left(-\frac{v_0 y}{\nu}\right) \tag{1.1}$$

边界层位移厚度

$$\delta^* = \int_0^\infty \frac{U - u}{U} \, \mathrm{d}y = \int_0^\infty \exp\left(-\frac{v_0 y}{\nu}\right) \, \mathrm{d}y = \frac{\nu}{v_0}.$$
 (1.2)

粘性系数

$$\mu = \nu \rho, \tag{1.3}$$

表面摩擦力

$$\tau_0 = \mu \frac{\mathrm{d}u}{\mathrm{d}y}\Big|_{y=0} = \rho U v_0. \tag{1.4}$$

2

先统一一下符号标记

$$x = z, (2.1)$$

$$\sigma = r, (2.2)$$

$$v = u_{\theta}. \tag{2.3}$$

由 Vortical Flows 中的 (6.1.8b), 对于无粘情况,

$$\frac{\mathrm{D}}{\mathrm{D}t} \left(\frac{\omega_{\theta}}{r} \right) = \frac{1}{r^4} \frac{\partial C^2}{\partial z} = \frac{2C}{r^4} \frac{\partial C}{\partial z},\tag{2.4}$$

其中

$$C = vr. (2.5)$$

又根据 (6.1.4a)

$$\omega_r = -\frac{1}{r} \frac{\partial C}{\partial z},\tag{2.6}$$

$$\frac{\mathrm{D}}{\mathrm{D}t} \left(\frac{\omega_{\theta}}{r} \right) = -\frac{2v\omega_{r}}{r^{2}}.$$
(2.7)

3

在轴对称假设下, 流体的动能为

$$T = \pi \rho \int_{-\infty}^{+\infty} \int_{0}^{+\infty} \left(\psi \omega_{\theta} + V_{\theta}^{2} r \right) dr dz.$$
 (3.1)

对于 Hill 球涡,

$$V_{\theta} = 0, \tag{3.2}$$

$$\omega_{\theta}(r,z) = \begin{cases} -\frac{15}{2} \frac{U}{a^2} r, & R = \sqrt{r^2 + z^2} < a, \\ 0, & R = \sqrt{r^2 + z^2} > a, \end{cases}$$
(3.3)

$$\psi(r,z) = \begin{cases} -\frac{3}{4}Ur^2\left(1 - \frac{R^2}{a^2}\right) - \frac{3}{4}Ur^2\left(1 - \frac{R^2}{a^2}\right) - \frac{1}{2}Ur^2, & R = \sqrt{r^2 + z^2} < a, \\ \frac{1}{2}Ur^2\left(1 - \frac{a^3}{R^3}\right) - \frac{3}{4}Ur^2\left(1 - \frac{R^2}{a^2}\right) - \frac{1}{2}Ur^2, & R = \sqrt{r^2 + z^2} > a. \end{cases}$$
(3.4)

积分可得

$$T = \pi \rho \int_{-a}^{a} \int_{0}^{+\sqrt{a^{2}-z^{2}}} (\psi \omega_{\theta}) dr dz = \frac{10}{7} \pi \rho U^{2} a^{3}.$$
 (3.5)

4

在极坐标下, 方程

$$\nabla^2 \psi = c \psi \tag{4.1}$$

写为

$$\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial\psi}{\partial r}\right) + \frac{1}{r^2}\frac{\partial^2\psi}{\partial\theta^2} = c\psi. \tag{4.2}$$

把式子

$$\psi^{(i)} = cJ_1(kr)\sin\theta\tag{4.3}$$

代入式 (4.2), 并假设 c < 0, $\sin \theta \neq 0$, x = kr 可得

$$x^{2}J_{1}'' + xJ_{1}' - \left(\frac{c}{k^{2}}x^{2} + 1\right)J_{1} = 0.$$
(4.4)

当 $k = \sqrt{-c}$ 时, 式 (4.3) 正好是 m = 1 的贝塞尔方程的解.

在极坐标下, 流函数和速度的关系为

$$v_{\theta}^{(i)} = -\frac{\partial \psi^{(i)}}{\partial r} = -ckJ_1'(kr)\sin\theta, \quad v_r^{(i)} = \frac{1}{r}\frac{\partial \psi^{(i)}}{\partial \theta} = \frac{c}{r}J_1(kr)\cos\theta. \tag{4.5}$$

 $v_r = 0$ 时

$$J_1(kr_0) = 0. (4.6)$$

假设 kr_0 是 J_1 的第一个零点, 则

$$v_{\theta}^{(i)} = -ckJ_1'(kr_0)\sin\theta. \tag{4.7}$$

均匀来流的流函数

$$\psi^{(o)} = U_{\infty} \left(1 - \frac{a^2}{r^2} \right) r \sin \theta, \quad a = r_0.$$
 (4.8)

速度

$$v_{\theta}^{(o)} = -\frac{\partial \psi^{(o)}}{\partial r} = -U_{\infty} \left(1 + \frac{a^2}{r^2} \right) \sin \theta, \quad v_r^{(o)} = \frac{1}{r} \frac{\partial \psi^{(o)}}{\partial \theta} = U_{\infty} \left(1 - \frac{a^2}{r^2} \right) \cos \theta. \quad (4.9)$$

匹配

$$v_{\theta}^{(o)}(r=a) = v_{\theta}^{(i)}(r=a)$$
 (4.10)

得

$$U_{\infty} = ckJ_1'(kr_0)/2. \tag{4.11}$$

得内外流函数

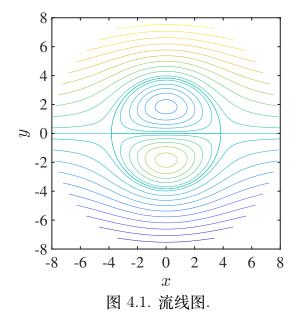
$$\psi = \begin{cases} cJ_1(kr)\sin\theta, & r < a, \\ \frac{1}{2}ckJ_1'(kr_0)\left(1 - \frac{a^2}{r^2}\right)r\sin\theta, & r > a. \end{cases}$$
(4.12)

其中 $k = \sqrt{-c}$, $a = r_0$.

假设 c = -1, 对于一阶贝塞尔函数, $r_0 = 3.8317$, 去流函数等值面, 可得流线图, 如图 4.1 所示.

5

如图 5.1 所示, 从右上角顺时针绕一圈, 箭头先从东北方向向北旋转, 然后返回为东北方向, 然后再重复一遍, 所以该奇点的指标为 0.



0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05

图 5.1. 流场矢量图.

6

由于 $\left(\frac{\partial^2 w}{\partial z^2}\right)_0 = -\left[\frac{1}{h_1}\left(\frac{\partial^2 u}{\partial x \partial z}\right) + \frac{1}{h_2}\left(\frac{\partial^2 v}{\partial y \partial z}\right)\right]_0$, 判定流动分离的条件是: 在分离线上

$$\begin{cases}
\left(\frac{\partial u}{\partial z}\right)_0 = 0, \\
\left(\frac{\partial^2 u}{\partial x \partial z}\right)_0 < 0, \\
\left(\frac{\partial^2 w}{\partial z^2}\right)_0 > 0 \quad \overrightarrow{\text{EX}} \left(\frac{1}{h_1} \frac{\partial^2 u}{\partial x \partial z} + \frac{1}{h_2} \frac{\partial^2 v}{\partial y \partial z}\right)_0 < 0.
\end{cases}$$
(6.1)

对应于书上的

$$\tau_{x,x} > 0,$$

$$\tau_y = 0, \quad \tau_{y,x} = 0,$$
(6.2)

$$\tau_{\mathbf{v}} = 0, \quad \tau_{\mathbf{v},x} = 0, \tag{6.3}$$

$$\tau_{y,y} < 0, \tag{6.4}$$

$$\tau_{y,y} < 0, \tag{6.4}$$

$$\nabla_{\pi} \cdot \boldsymbol{\tau} = \tau_{x,x} + \tau_{y,y} < 0. \tag{6.5}$$

注意两书的 x, y 标号是反的.

我从图书馆借了书,书内容太多,之前的部分我就不抄了.

7

根据三角翼的升力公式

$$L \approx \rho U \int_{W} y \omega_x \, \mathrm{d}S,\tag{7.1}$$

由于三角翼会卷起一个很强的涡, 并且是延着 x 方向, 即 ω_x 很大, 所以升力也很大.

如图 7.1 所示, 发动机的转子布满一圈三角形的叶片, 图示是正视图, 转动方向如 图中箭头所示.

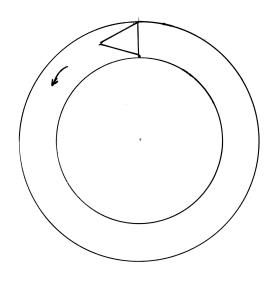


图 7.1. 发动机转子示意图.