

# 计算流体力学上机作业 3

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写程序计算 2D Euler 方程组的双马赫反射问题或前台阶问题（见讲义【CFDLect06-com03\_cn.pdf】的第 106-108 页）。数值格式：“Roe 或 HLLC 或 HLL 解法器或 KFVS” + “线性重构” + “显示的 Runge-Kutta 时间离散”。

计算动图可点击 <https://www.bilibili.com/video/BV1cp4y1t7Bc> 查看。

代码可点击 <https://github.com/circlelq/Computational-Fluid-Dynamics/tree/main/code2> 查看。

## 问题描述

前台阶问题

几何形状和结果 (密度等值线) 见示意图图 1.1.

初始时刻, 区域内充满均匀流  $(\rho, u, v, p) = (1.4, 3, 0, 1)$ . 输出时间  $t = 4$ . 上下边界为反射边界; 左边界为入流边界 (即左边界处流动为初始均匀流); 右边界为出流。

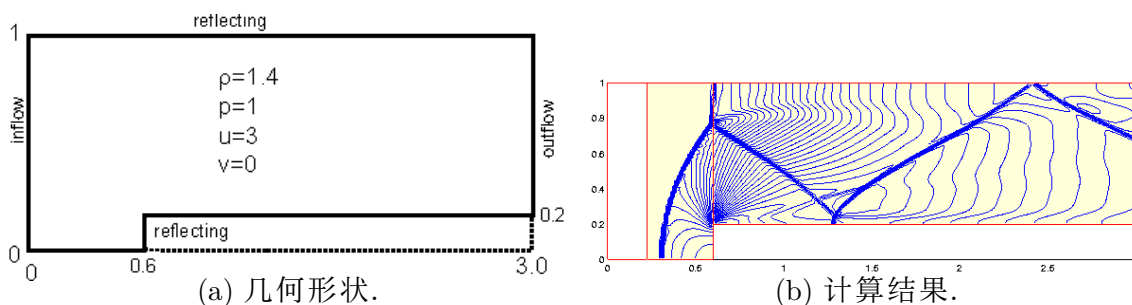


图 1.1. 几何形状和计算结果.

## 控制方程

### 二维无黏流动 Euler 方程组

采用理想气体模型. 不考虑体力、外部热源和流体源 (汇), 二维 Euler 方程组:

$$\mathbf{u}_t + \mathbf{f}_x + \mathbf{g}_y = \mathbf{0}, \quad (2.1)$$

其中

$$\mathbf{u} = \begin{pmatrix} \rho \\ \rho u \\ \rho v \\ E \end{pmatrix}, \quad \mathbf{f} = \begin{pmatrix} \rho u \\ \rho u^2 + p \\ \rho uv \\ (E + p)u \end{pmatrix}, \quad \mathbf{g} = \begin{pmatrix} \rho v \\ \rho uv \\ \rho v^2 + p \\ (E + p)v \end{pmatrix}. \quad (2.2)$$

其中  $\rho$  为流体密度,  $p$  为压力,  $u, v$  为  $x$  和  $y$  方向上速度分量,  $E$  为单位体积流体总能. 理想气体状态方程:

$$p = (\gamma - 1)\rho e = (\gamma - 1) \left[ E - \frac{1}{2}\rho(u^2 + v^2) \right]. \quad (2.3)$$

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$$H = (E + p)/\rho = \frac{\gamma p}{\rho(\gamma - 1)} + \frac{1}{2}(u^2 + v^2), \quad (2.4)$$

声速

$$a = \sqrt{\gamma p / \rho} = \sqrt{(\gamma - 1) \left[ H - \frac{1}{2}(u^2 + v^2) \right]}. \quad (2.5)$$

### 非线性 Jacobian 系数矩阵、特征值和特征矢量矩阵

把二维 Euler 方程组式 (2.1) 写成非守恒型形式:[张德良, 2010, P289]

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{A} \frac{\partial \mathbf{u}}{\partial x} + \mathbf{B} \frac{\partial \mathbf{u}}{\partial y} = \mathbf{0} \quad (2.6)$$

其中  $\mathbf{A}, \mathbf{B}$  为非守恒型方程组的非线性 Jacobian 系数矩阵, 由于流通量矢量  $\mathbf{f}, \mathbf{g}$  是流动量矢量  $\mathbf{u}$  的一次齐次函数, 则有:

$$\mathbf{A} \frac{\partial \mathbf{u}}{\partial x} = \frac{\partial \mathbf{f}}{\partial x}, \quad \mathbf{B} \frac{\partial \mathbf{u}}{\partial y} = \frac{\partial \mathbf{g}}{\partial y}. \quad (2.7)$$

(1) 非线性 Jacobian 系数矩阵

$$\mathbf{A}(\mathbf{u}) = \begin{pmatrix} 0 & 1 & 0 & 0 \\ \frac{\gamma-3}{2}u^2 + \frac{\gamma-1}{2}v^2 & (3-\gamma)u & (1-\gamma)v & \gamma-1 \\ -uv & v & u & 0 \\ u \left[ \frac{\gamma-2}{2}(u^2+v^2) - \frac{a^2}{\gamma-1} \right] & \frac{3-2\gamma}{2}u^2 + \frac{1}{2}v^2 + \frac{a^2}{\gamma-1} & (1-\gamma)uv & \gamma u \end{pmatrix} \quad (2.8)$$

$$\mathbf{B}(\mathbf{u}) = \begin{pmatrix} 0 & 0 & 1 & 0 \\ -uv & v & u & 0 \\ \frac{\gamma-1}{2}u^2 + \frac{\gamma-3}{2}v^2 & (1-\gamma)u & (3-\gamma)v & \gamma-1 \\ v \left[ \frac{\gamma-2}{2}(u^2+v^2) - \frac{a^2}{\gamma-1} \right] & (1-\gamma)uv & \frac{1}{2}u^2 + \frac{3-2\gamma}{2}v^2 + \frac{a^2}{\gamma-1} & \gamma v \end{pmatrix} \quad (2.9)$$

(2) 系数矩阵  $\mathbf{A}$ ,  $\mathbf{B}$  的特征值矩阵

$$\mathbf{\Lambda}_x = \mathbf{R}^{-1}\mathbf{A}\mathbf{L}^{-1} = \begin{pmatrix} \lambda_1 & 0 & 0 & 0 \\ 0 & \lambda_2 & 0 & 0 \\ 0 & 0 & \lambda_3 & 0 \\ 0 & 0 & 0 & \lambda_4 \end{pmatrix} = \begin{pmatrix} u & 0 & 0 & 0 \\ 0 & u & 0 & 0 \\ 0 & 0 & u-a & 0 \\ 0 & 0 & 0 & u+a \end{pmatrix} \quad (2.10)$$

$$\mathbf{\Lambda}_y = \mathbf{R}^{-1}\mathbf{B}\mathbf{L}^{-1} = \begin{pmatrix} \mu_1 & 0 & 0 & 0 \\ 0 & \mu_2 & 0 & 0 \\ 0 & 0 & \mu_3 & 0 \\ 0 & 0 & 0 & \mu_4 \end{pmatrix} = \begin{pmatrix} v & 0 & 0 & 0 \\ 0 & v & 0 & 0 \\ 0 & 0 & v-a & 0 \\ 0 & 0 & 0 & v+a \end{pmatrix} \quad (2.11)$$

(3) 系数矩阵  $\mathbf{A}$ ,  $\mathbf{B}$  的右特征矢量矩阵

由右特征矢量矩阵  $\mathbf{A}\mathbf{R}_x = \lambda\mathbf{R}_x$ ,  $\mathbf{B}\mathbf{R}_y = \mu\mathbf{R}_y$  得到它们的右特征矢量矩阵:

$$\mathbf{R}_x = \begin{pmatrix} 1 & 0 & 1 & 1 \\ u & 0 & u-a & u+a \\ 0 & 1 & v & v \\ \frac{1}{2}(u^2-v^2) & v & h-au & h+au \end{pmatrix} \quad (2.12)$$

$$\mathbf{R}_y = \begin{pmatrix} 0 & 1 & 1 & 1 \\ 1 & 0 & u & u \\ 0 & v & v-a & v+a \\ u & \frac{1}{2}(v^2-u^2) & h-av & h+av \end{pmatrix} \quad (2.13)$$

(4) 系数矩阵  $\mathbf{A}$ ,  $\mathbf{B}$  的左特征矢量矩阵

由左特征矢量公式  $\mathbf{L}_x \mathbf{A} = \lambda \mathbf{L}_x$ ,  $\mathbf{L}_y \mathbf{B} = \mu \mathbf{L}_y$ , 可得到左特

$$\mathbf{L}_x = \begin{pmatrix} 1 - \frac{\gamma-1}{2a^2} (u^2 + v^2) & \frac{\gamma-1}{a^2} u & \frac{\gamma-1}{a^2} v & \frac{\gamma-1}{a^2} \\ -\frac{\gamma-1}{2a^2} v (u^2 + v^2) & \frac{\gamma-1}{a^2} uv & 1 + \frac{\gamma-1}{a^2} v^2 & -\frac{\gamma-1}{a^2} v \\ \frac{\gamma-1}{4a^2} (u^2 + v^2) + \frac{u}{2a} & -\frac{\gamma-1}{2a^2} u - \frac{1}{2a} & -\frac{\gamma-1}{2a^2} v & \frac{\gamma-1}{2a^2} \\ \frac{\gamma-1}{4a^2} (u^2 + v^2) - \frac{u}{2a} & -\frac{\gamma-1}{2a^2} u + \frac{1}{2a} & -\frac{\gamma-1}{2a^2} v & \frac{\gamma-1}{2a^2} \end{pmatrix} \quad (2.14)$$

$$\mathbf{L}_y = \begin{pmatrix} -\frac{\gamma-1}{2a^2} u (u^2 + v^2) & 1 + \frac{\gamma-1}{a^2} u^2 & \frac{\gamma-1}{a^2} uv & -\frac{\gamma-1}{a^2} u \\ 1 - \frac{\gamma-1}{2a^2} (u^2 + v^2) & \frac{\gamma-1}{a^2} u & \frac{\gamma-1}{a^2} v & -\frac{\gamma-1}{a^2} \\ \frac{\gamma-1}{4a^2} (u^2 + v^2) + \frac{1}{2a} v & -\frac{\gamma-1}{2a^2} u & -\frac{\gamma-1}{2a^2} - \frac{1}{2a} & \frac{\gamma-1}{2a^2} \\ \frac{\gamma-1}{4a^2} (u^2 + v^2) - \frac{1}{2a} v & -\frac{\gamma-1}{2a^2} u & -\frac{\gamma-1}{2a^2} v + \frac{1}{2a} & \frac{\gamma-1}{2a^2} \end{pmatrix} \quad (2.15)$$

$b_1 = b_2 \frac{(u^2 + v^2)}{2}$ ,  $b_2 = \frac{\gamma-1}{a^2}$ , 则式可写成:

$$\mathbf{L}_x = \begin{pmatrix} 1 - b_1 & b_2 u & b_2 v & -b_2 \\ -b_1 v & b_2 uv & 1 + b_2 v^2 & -b_2 v \\ \frac{1}{2} (b_1 + \frac{u}{a}) & -\frac{1}{2} (b_2 u + \frac{1}{a}) & -\frac{1}{2} b_2 v & \frac{1}{2} b_2 \\ \frac{1}{2} (b_1 - \frac{u}{a}) & -\frac{1}{2} (b_2 u - \frac{1}{a}) & -\frac{1}{2} b_2 v & \frac{1}{2} b_2 \end{pmatrix}, \quad (2.16)$$

$$\mathbf{L}_y = \begin{pmatrix} -b_1 u & 1 + b_2 u^2 & b_2 uv & -b_2 u \\ 1 - b_1 & b_2 u & b_2 v & -b_2 \\ \frac{1}{2} (b_1 + \frac{v}{a}) & -\frac{1}{2} b_2 u & -\frac{1}{2} (b_2 v + \frac{1}{a}) & \frac{1}{2} b_2 \\ \frac{1}{2} (b_1 - \frac{v}{a}) & -\frac{1}{2} b_2 u & -\frac{1}{2} (b_2 v - \frac{1}{a}) & \frac{1}{2} b_2 \end{pmatrix}. \quad (2.17)$$

## Roe 算法

对于理性气体, 通过如下方法构造  $\hat{\mathbf{A}}$ :

$$\begin{cases} \bar{\rho} = \frac{\sqrt{\rho_r} \rho_\ell + \sqrt{\rho_\ell} \rho_r}{\sqrt{\rho_\ell} + \sqrt{\rho_r}} = \sqrt{\rho_\ell \rho_r} = \left[ \frac{1}{2} (\sqrt{\rho_r} + \sqrt{\rho_\ell}) \right]^2, \\ \bar{u} = \frac{\sqrt{\rho_\ell} u_\ell + \sqrt{\rho_r} u_r}{\sqrt{\rho_\ell} + \sqrt{\rho_r}}, \\ \bar{v} = \frac{\sqrt{\rho_\ell} v_\ell + \sqrt{\rho_r} v_r}{\sqrt{\rho_\ell} + \sqrt{\rho_r}}, \\ \bar{H} = \frac{\sqrt{\rho_\ell} H_\ell + \sqrt{\rho_r} H_r}{\sqrt{\rho_\ell} + \sqrt{\rho_r}}. \end{cases} \quad (3.1)$$

$$\hat{\mathbf{A}} = \mathbf{A}(\bar{\mathbf{u}}). \quad (3.2)$$

$$\hat{\mathbf{f}}(\mathbf{u}_j, \mathbf{u}_{j+1}) = \frac{\mathbf{f}(\mathbf{u}_j) + \mathbf{f}(\mathbf{u}_{j+1})}{2} - \frac{1}{2} \left| \hat{\mathbf{A}}_{j+1/2} \right| (\mathbf{u}_{j+1} - \mathbf{u}_j). \quad (3.3)$$

$$\hat{\mathbf{g}}(\mathbf{u}_j, \mathbf{u}_{j+1}) = \frac{\mathbf{g}(\mathbf{u}_j) + \mathbf{g}(\mathbf{u}_{j+1})}{2} - \frac{1}{2} \left| \hat{\mathbf{B}}_{j+1/2} \right| (\mathbf{u}_{j+1} - \mathbf{u}_j). \quad (3.4)$$

其中  $|\hat{\mathbf{A}}|$  定义为:  $|\hat{\mathbf{A}}| = \mathbf{R}|\hat{\mathbf{\Lambda}}|\mathbf{R}^{-1}$ ,  $|\hat{\mathbf{\Lambda}}| = \text{diag} \left\{ |\hat{\lambda}_1|, \dots, |\hat{\lambda}_m| \right\}$ , 可以得到半离散格式 [张德良, 2010, P294]

$$\frac{d}{dt} \mathbf{u}_{i,j} + \frac{1}{h} \left( \hat{\mathbf{f}}_{i+\frac{1}{2},j} - \hat{\mathbf{f}}_{i-\frac{1}{2},j} \right) + \frac{1}{h} \left( \hat{\mathbf{g}}_{i,j+\frac{1}{2}} - \hat{\mathbf{g}}_{i,j-\frac{1}{2}} \right) = 0. \quad (3.5)$$

然后再用三阶 TVD 性质的 RK 时间差分格式

$$\begin{aligned} u^{(1)} &= u^n + \Delta t L(u^n), \\ u^{(2)} &= \frac{3}{4}u^n + \frac{1}{4}u^{(1)} + \frac{1}{4}\Delta t L(u^{(1)}), \\ u^{n+1} &= \frac{1}{3}u^n + \frac{2}{3}u^{(2)} + \frac{2}{3}\Delta t L(u^{(2)}). \end{aligned} \quad (3.6)$$

其中  $L$  是空间离散算符.

## 边界条件

上下边界为反射边界; 左边界为入流边界 (即左边界处流动为初始均匀流); 右边界为出流. 对于刚性壁面, 满足华裔反射边界条件: 即在隔壁面法向方向上各物理量取一阶导数为 0, 这可以在壁面法向方向上采用镜面反射原则取值. 由此克制, 在水平壁面上  $v_w = 0$ , 竖直壁面上  $u_w = 0$ . 在各壁面切向方向上直接取流场中相邻点物理量的值. [张德良, 2010, P339]

## 参考文献

张德良. 计算流体力学教程. 高等教育出版社, 2010. 2, 5