

# 湍流 3

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代码等作业内容可在 <https://github.com/circlelq/Turbulence> 查看.

## 1

对于归一化的一维光滑平稳高斯过程  $X(t)$ , 即满足  $\langle X \rangle = 0$ ,  $\langle X^2 \rangle = 1$ , 记  $\dot{X} = \frac{dX}{dt}$ , 证明如下两个条件平均关系:  $\langle \ddot{X} | X = x \rangle = -\langle \dot{X}^2 \rangle x$ ;  $\langle \dot{X}^2 | X = x \rangle = \langle \dot{X}^2 \rangle$ . 提示: 应该首先说明或者证明  $\dot{X}(t)$  和  $\ddot{X}(t)$  也是高斯过程.

根据 [2, P45] 可得正态随机过程的导数也符合正态率, 并且  $X(t), \dot{X}(t)$  是独立的, 所以

$$\langle \dot{X}^2 | X = x \rangle = \langle \dot{X}^2 \rangle. \quad (1.1)$$

写出  $X_1(-\tau), X_2(0), X_3(\tau)$  三个随机变量的概率函数有

$$f(X_1, -\tau; X_2, 0; X_3, \tau) = \frac{(2\pi)^{-\frac{3}{2}}}{\sigma^3 \sqrt{D}} \exp \left[ -\frac{1}{2D\sigma^2} \sum_{i,k} D_{ik} x_i x_k \right] \quad (1.2)$$

其中  $D$  是矩阵

$$R_{ik} = \begin{pmatrix} 1 & R(\tau) & R(2\tau) \\ R(\tau) & 1 & R(\tau) \\ R(2\tau) & R(\tau) & 1 \end{pmatrix} \quad (1.3)$$

矩阵的行列式,  $D_{ik}$  是元素  $R_{ik}$  的余子式. 在假设  $R'(0) = 0$  的情况下, 根据

$$f''(t) = \lim_{\tau \rightarrow 0} \frac{f(t+\tau) - 2f(t) + f(t-\tau)}{\tau^2} \quad (1.4)$$

可计算得

$$\begin{aligned}
\langle \ddot{X} \mid X = x \rangle &= \lim_{\tau \rightarrow 0} \left\langle \frac{X_1(t + \tau) - 2X_2(t) + X_3(t - \tau)}{\tau^2} \right\rangle \\
&= \lim_{\tau \rightarrow 0} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{X_1(t + \tau) - 2X_2(t) + X_3(t - \tau)}{\tau^2} f(X_1, -\tau; X_2, 0; X_3, \tau) dX_1 dX_3 \\
&= -\langle \dot{X}^2 \rangle x
\end{aligned} \tag{1.5}$$

□

## 2

对于不可压均匀各向同性湍流, 试给出两空间点的涡量速度关联张量的最简表达式.

解:

定义二元涡量速度关联函数

$$R(\mathbf{r}, \mathbf{a}, \mathbf{b}) \equiv \langle \omega_a u'_b \rangle = R_{ij} a_i b_j. \tag{2.1}$$

由各向同性可得

$$R_{ij}(\mathbf{r}) = A_1(r^2) r_i r_j + B_1(r^2) \delta_{ij} \tag{2.2}$$

$$R_{11} = \langle \omega_1 u'_1 \rangle \equiv \langle \omega u \rangle f(r) = A_1 r^2 + B_1 \tag{2.3}$$

$$R_{22} = \langle \omega_2 u'_2 \rangle \equiv \langle \omega u \rangle g(r) = B_1 \tag{2.4}$$

其中  $\langle \omega u \rangle = \frac{1}{3} \langle \boldsymbol{\omega} \cdot \mathbf{u} \rangle$ . 由于速度有无散条件

$$\nabla \cdot \mathbf{u} = 0, \tag{2.5}$$

所以有

$$\frac{\partial R_{ij}}{\partial r_j} = 0, \tag{2.6}$$

得

$$R_{ij} = \langle \omega u \rangle \left[ -\frac{1}{2r} \frac{\partial f}{\partial r} r_i r_j + \left( f + \frac{r}{2} \frac{\partial f}{\partial r} \right) \delta_{ij} \right]. \tag{2.7}$$

其中  $f$  是关于  $r$  的函数.

对于不可压均匀各向同性湍流, 根据不可压条件 (连续性方程) 和湍流统计量与构型 (configuration) 的方向无关的特点, 通过标架旋转证明一点的速度梯度满足统计关系:

$$\left\langle \left( \frac{\partial u_1}{\partial x_2} \right)^2 \right\rangle = 2 \left\langle \left( \frac{\partial u_1}{\partial x_1} \right)^2 \right\rangle. \quad (3.1)$$

提示: 可参阅 G.I. Taylor 在 1935 年发表的关于均匀向同性湍流的有关论文.

为了书写方便, 记

$$u = u_1, v = u_2, w = u_3, x = x_1, y = x_2, z = x_3. \quad (3.2)$$

由不可压有

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \quad (3.3)$$

即

$$\frac{\partial u}{\partial x} = -\frac{\partial v}{\partial y} - \frac{\partial w}{\partial z}, \quad (3.4)$$

两边平方得

$$\begin{aligned} \left( \frac{\partial u}{\partial x} \right)^2 &= \left( \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right)^2 \\ &= \left( \frac{\partial v}{\partial y} \right)^2 + \left( \frac{\partial w}{\partial z} \right)^2 + 2 \frac{\partial v}{\partial y} \frac{\partial w}{\partial z}. \end{aligned} \quad (3.5)$$

取系综平均可得

$$\left\langle \left( \frac{\partial u}{\partial x} \right)^2 \right\rangle = \left\langle \left( \frac{\partial v}{\partial y} \right)^2 \right\rangle + \left\langle \left( \frac{\partial w}{\partial z} \right)^2 \right\rangle + \left\langle 2 \frac{\partial v}{\partial y} \frac{\partial w}{\partial z} \right\rangle \quad (3.6)$$

由各向同性湍流可得 [1]

$$\left\langle \left( \frac{\partial u}{\partial x} \right)^2 \right\rangle = \left\langle \left( \frac{\partial v}{\partial y} \right)^2 \right\rangle = \left\langle \left( \frac{\partial w}{\partial z} \right)^2 \right\rangle \quad (3.7)$$

所以式 (3.6) 化为

$$\left\langle \left( \frac{\partial u}{\partial x} \right)^2 \right\rangle = -2 \left\langle \frac{\partial v}{\partial y} \frac{\partial w}{\partial z} \right\rangle \quad (3.8)$$

对坐标进行  $45^\circ$  可得

$$\begin{cases} \sqrt{2}x' &= x + y \\ \sqrt{2}y' &= -x + y \\ z' &= z \end{cases} \quad (3.9)$$

$$\begin{cases} \sqrt{2}u' &= u + v \\ \sqrt{2}v' &= -u + v \\ v' &= v \end{cases} \quad (3.10)$$

Hence

$$\begin{cases} \frac{\partial u}{\partial x} &= \frac{1}{2} \left( \frac{\partial u'}{\partial x'} - \frac{\partial v'}{\partial x'} - \frac{\partial u'}{\partial y'} + \frac{\partial v'}{\partial y'} \right) \\ \frac{\partial v}{\partial x} &= \frac{1}{2} \left( \frac{\partial u'}{\partial x'} + \frac{\partial v'}{\partial x'} - \frac{\partial u'}{\partial y'} - \frac{\partial v'}{\partial y'} \right) \\ \frac{\partial w}{\partial x} &= \frac{1}{\sqrt{2}} \left( \frac{\partial w'}{\partial x'} - \frac{\partial w'}{\partial y'} \right) \end{cases} \quad (3.11)$$

$$\begin{cases} \frac{\partial u}{\partial y} &= \frac{1}{2} \left( \frac{\partial u'}{\partial x'} - \frac{\partial v'}{\partial x'} + \frac{\partial u'}{\partial y'} - \frac{\partial v'}{\partial y'} \right) \\ \frac{\partial v}{\partial y} &= \frac{1}{2} \left( \frac{\partial u'}{\partial x'} + \frac{\partial v'}{\partial x'} + \frac{\partial u'}{\partial y'} + \frac{\partial v'}{\partial y'} \right) \\ \frac{\partial w}{\partial y} &= \frac{1}{\sqrt{2}} \left( \frac{\partial w'}{\partial x'} + \frac{\partial w'}{\partial y'} \right) \end{cases} \quad (3.12)$$

$$\begin{cases} \frac{\partial u}{\partial z} &= \frac{1}{\sqrt{2}} \left( \frac{\partial u'}{\partial z'} - \frac{\partial v'}{\partial z'} \right) \\ \frac{\partial v}{\partial z} &= \frac{1}{\sqrt{2}} \left( \frac{\partial u'}{\partial z'} + \frac{\partial v'}{\partial z'} \right) \\ \frac{\partial w}{\partial z} &= \frac{\partial w'}{\partial z'} \end{cases} \quad (3.13)$$

表 3.1. 记号说明.

$\left(\frac{\partial u}{\partial x}\right)^2$	$\frac{\partial u}{\partial x} \frac{\partial u}{\partial y}$	$\left(\frac{\partial u}{\partial y}\right)^2$	$\frac{\partial u}{\partial y} \frac{\partial u}{\partial z}$	$\frac{\partial u}{\partial x} \frac{\partial v}{\partial x}$	$\frac{\partial u}{\partial x} \frac{\partial v}{\partial y}$	$\frac{\partial u}{\partial x} \frac{\partial v}{\partial z}$	$\frac{\partial u}{\partial y} \frac{\partial v}{\partial x}$	$\frac{\partial u}{\partial y} \frac{\partial v}{\partial z}$	$\frac{\partial u}{\partial z} \frac{\partial v}{\partial z}$
$a_1$	$a_2$	$a_3$	$a_4$	$a_5$	$a_6$	$a_7$	$a_8$	$a_9$	$a_{10}$

对式 (3.9) 求平方, 并利用各向同性可得以下等式

$$a_4 = a_7 = a_2 = a_5 = a_{10} = a_9 = 0. \quad (3.14)$$

$$a_1 = -2a_6, \quad (3.15)$$

$$a_1 - a_3 - a_6 - a_8 = 0, \quad (3.16)$$

$$a_1 - a_3 - a_6 - a_8 = 0, \quad (3.17)$$

$$a_1 + 2a_8 = 0, \quad (3.18)$$

$$a_1 = -2a_6 \quad (3.19)$$

$$a_1 = \frac{1}{2}a_3. \quad (3.20)$$

□

将不可压均匀各向同性湍流中两点纵向速度关联函数与一维能谱之间的傅立叶积分变换关系

$$\langle u^2 \rangle f(r) = \int_{-\infty}^{\infty} \phi_1(k) e^{ikr} dk \quad (4.1)$$

代入如下两点纵向速度关联函数与三维能谱之间的积分变换关系

$$E(k) = \frac{1}{\pi} \int_{-\infty}^{\infty} \langle u^2 \rangle f(r) (kr)^2 \left( \frac{\sin kr}{kr} - \cos kr \right) dr, \quad (4.2)$$

直接通过计算推出

$$E(k) = k^3 \frac{d}{dk} \left[ \frac{1}{k} \frac{d\phi_1(k)}{dk} \right]. \quad (4.3)$$

或者, 将

$$\langle u^2 \rangle f(r) = 2 \int_{-\infty}^{\infty} E(k) (kr)^{-2} \left( \frac{\sin kr}{kr} - \cos kr \right) dk \quad (4.4)$$

代入傅立叶逆变换关系

$$\phi_1(k) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \langle u^2 \rangle f(r) e^{-ikr} dr, \quad (4.5)$$

进行积分, 推出

$$\phi_1(k) = \frac{1}{2} \int_k^{\infty} \left( 1 - \frac{k^2}{\lambda^2} \right) \frac{E(\lambda)}{\lambda} d\lambda. \quad (4.6)$$

两个推导过程任选其一完成即可. 提示: 第一个推导利用  $\delta$  函数及其导数的性质; 第二个推导用到由如下积分关系

$$\frac{1}{2} \int_0^1 (1 - k^2) \cos kx dk = \frac{1}{x^2} \left( \frac{\sin x}{x} - \cos x \right) \quad (4.7)$$

带来的余弦变换.

将式 (4.4) 代入式 (4.5) 可得

$$\begin{aligned} \phi_1(k) &= \frac{1}{2\pi} \int_{-\infty}^{\infty} \langle u^2 \rangle f(r) e^{-ikr} dr \\ &= \frac{1}{2\pi} \int_{-\infty}^{\infty} 2 \int_{-\infty}^{\infty} E(\lambda) (\lambda r)^{-2} \left( \frac{\sin \lambda r}{\lambda r} - \cos \lambda r \right) d\lambda e^{-ikr} dr \\ &= \frac{1}{\pi} \int_{-\infty}^{\infty} E(\lambda) \lambda^{-2} \int_{-\infty}^{\infty} r^{-2} \left( \frac{\sin \lambda r}{\lambda r} - \cos \lambda r \right) e^{-ikr} dr d\lambda \\ &= \frac{1}{\pi} \int_{-\infty}^{\infty} E(\lambda) \lambda^{-2} \int_{-\infty}^{\infty} r^{-2} \left( \frac{\sin \lambda r}{\lambda r} - \cos \lambda r \right) \cos(kr) dr d\lambda \end{aligned} \quad (4.8)$$

其中

$$\begin{aligned}
 & 4\lambda \int_{-\infty}^{\infty} r^{-2} \left( \frac{\sin \lambda r}{\lambda r} - \cos \lambda r \right) \cos(kr) dr \\
 &= (\lambda - k)(\lambda + k) \text{Si}((\lambda + k)r) + (\lambda - k)(\lambda + k) \text{Si}((\lambda - k)r) \\
 &+ \frac{2k \sin(kr) \sin(\lambda r) + 2\lambda \cos(kr) \cos(\lambda r)}{r} - \frac{2 \cos(kr) \sin(\lambda r)}{r^2}
 \end{aligned} \tag{4.9}$$

其中

$$\text{Si}(x) = \int_0^x \frac{\sin(t)}{t} dt, \quad \text{Si}(+\infty) = \frac{\pi}{2}. \tag{4.10}$$

只有当  $(\lambda + k)$ ,  $(\lambda - k)$  同号时, 积分才不为 0. 又考虑到  $k > 0$ , 所以  $\lambda > k$ , 则

$$\phi_1(k) = \frac{1}{2} \int_k^{\infty} \left( 1 - \frac{k^2}{\lambda^2} \right) \frac{E(\lambda)}{\lambda} d\lambda. \tag{4.11}$$

□

## 5

用不同于教材中的方法证明教材 (2.3.42) 式:

$$\langle u^2 \rangle^{\frac{3}{2}} k(r) = 8\pi \int_0^{\infty} \frac{k^5 \Gamma(k)}{(kr)^4} (3 \sin kr - 3kr \cos kr - (kr)^2 \sin kr) dk. \tag{5.1}$$

教材并没有明说 (2.3.42) 是怎么得到的, 假设它是由 (2.3.41) 的反变换得到的, 那么下面给出另外一种证明方法. (2.3.41) 上面的一个式为:

$$\frac{1}{r^2} \frac{\partial}{\partial r} [r^3 K(r)] = 8\pi \int_0^{+\infty} k^6 \Gamma(k) \frac{\sin kr}{kr} dk. \tag{5.2}$$

把  $r^2$  乘过去再积分得

$$\begin{aligned}
 r^3 K(r) &= 8\pi \int_0^{+\infty} \int_0^r x^2 k^6 \Gamma(k) \frac{\sin kx}{kx} dx dk \\
 &= 8\pi \int_0^{+\infty} k^3 \Gamma(k) (\sin(kr) - kr \cos(kr)) dk
 \end{aligned} \tag{5.3}$$

带入

$$K(r) = \langle u^2 \rangle^{\frac{3}{2}} \frac{1}{r^4} \frac{\partial}{\partial r} (r^4 k) \tag{5.4}$$

得

$$\langle u^2 \rangle^{\frac{3}{2}} \frac{1}{r} \frac{\partial}{\partial r} (r^4 k) = 8\pi \int_0^{+\infty} k^3 \Gamma(k) (\sin(kr) - kr \cos(kr)) dk. \tag{5.5}$$

再次积分可得

$$\begin{aligned}
 \langle u^2 \rangle^{\frac{3}{2}} r^4 k &= 8\pi \int_0^{+\infty} \int_0^r x k^3 \Gamma(k) (\sin(kx) - kx \cos(kx)) dx dk \\
 &= 8\pi \int_0^{+\infty} k \Gamma(k) (3 \sin(kr) - 3kr \cos(kr) - k^2 r^2 \sin(kr)) dk.
 \end{aligned} \tag{5.6}$$

□

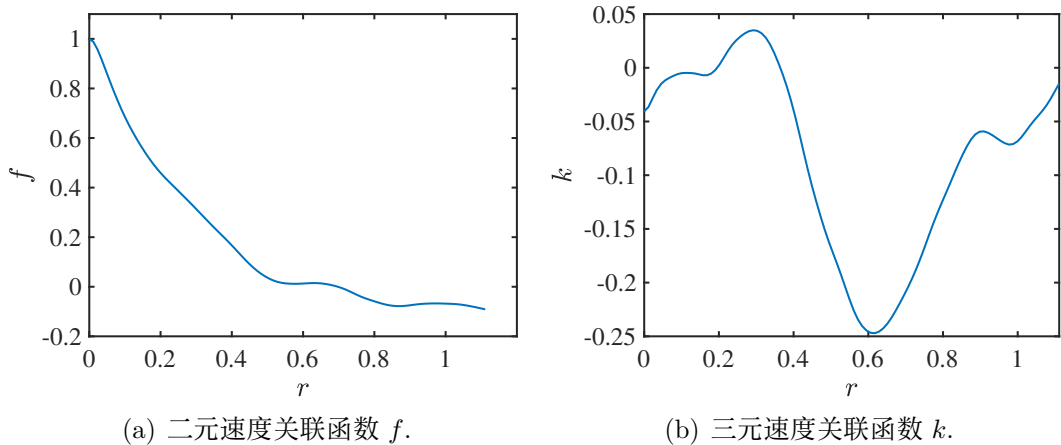


图 6.1. 近似均匀各向同性湍流中的关联函数.

## 6

自己从网上或者课题组内部获取实验测量或者直接数值模拟得到的湍流脉动速度信号的一段长时间的时间序列或者一定样本容量的空间序列. 完成下列两项任务:

1. 计算两点纵向的二阶和三阶速度关联系数  $f(r)$ ,  $k(r)$  并画出曲线 (可以用泰勒冻结假设);
2. 根据  $f(r)$  计算一维能谱  $\varphi_1(k)$  和三维能谱  $E(k)$  (在假设各向同性的情况下利用教材公式 (2.3.23)), 并画出曲线.

解:

这里选取的是杨延涛课题组的 RB 对流算例中的流场数据. 上板冷却, 下板加热,  $Ra = 1 \times 10^8$  中间区域近似为各向同性均匀湍流, 利用泰勒冻结假设, 对某一水平方向算相关函数取平均后可得图 1(a) 和 1(b). 三维能谱  $E(k)$  和  $f(r)$  的关系是

$$E(k) = \frac{1}{\pi} \int_0^{+\infty} \langle u^2 \rangle f(r) (kr)^2 \left( \frac{\sin kr}{kr} - \cos kr \right) dr. \quad (6.1)$$

一维能谱  $\varphi(k)$  和  $E(k)$  的关系是

$$\varphi_1(k_1) = \frac{1}{2} \int_{k_1}^{+\infty} \left( 1 - \frac{k_1^2}{k^2} \frac{E(k)}{k} \right) dk. \quad (6.2)$$

画图可得图 2(a) 和 2(b).

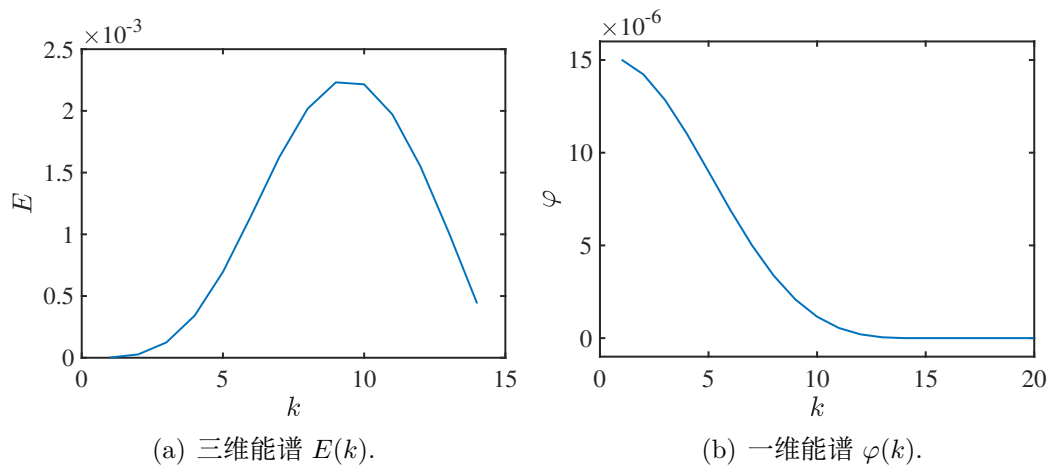


图 6.2. 能谱图.

## 参考文献

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