

# 1 The State Vector $\mathbf{Y}$

We define the complete state of the system as a single vector  $\mathbf{Y}$ :

$$\mathbf{Y} = [\mathbf{r}, \mathbf{v}, \mathbf{q}, \boldsymbol{\omega}, \mathbf{M}_{irr}]^T \quad (1)$$

Where:

- $\mathbf{r}$ : Position vector in the **ECI** frame ( $m$ ).
- $\mathbf{v}$ : Velocity vector in the **ECI** frame ( $m/s$ ).
- $\mathbf{q}$ : Attitude quaternion ( $\text{ECI} \rightarrow \text{Body}$ ), defined as  $[w, x, y, z]$ .
- $\boldsymbol{\omega}$ : Angular velocity vector in the **Body** frame ( $rad/s$ ).
- $\mathbf{M}_{irr}$ : Scalar irreversible magnetization for each hysteresis rod ( $A/m$ ).

# 2 The Differential Equation $\frac{d\mathbf{Y}}{dt}$

The system of first-order differential equations governing the state evolution is:

$$\frac{d\mathbf{Y}}{dt} = \begin{bmatrix} \dot{\mathbf{r}} \\ \dot{\mathbf{v}} \\ \dot{\mathbf{q}} \\ \dot{\boldsymbol{\omega}} \\ \dot{\mathbf{M}}_{irr} \end{bmatrix} = \begin{bmatrix} \mathbf{v} \\ \mathbf{g}_{total}(\mathbf{r}, t) \\ \frac{1}{2}\mathbf{q} \otimes [0, \omega_x, \omega_y, \omega_z]^T \\ \mathbf{I}^{-1}(\boldsymbol{\tau}_{total} - \boldsymbol{\omega} \times (\mathbf{I}\boldsymbol{\omega})) \\ \mathbf{f}_{hyst}(\mathbf{B}_{body}, \dot{\mathbf{B}}_{body}, \mathbf{M}_{irr}) \end{bmatrix} \quad (2)$$

## 2.1 Gravitational Acceleration

The acceleration  $\mathbf{g}_{total}$  is defined as the negative gradient of the geopotential  $V$ :

$$\mathbf{g}_{total} = -\nabla V(r, \theta, \lambda) \quad (3)$$

The potential  $V$  follows the EGM2008 model. `GeographicLib::GravityModel` returns the acceleration vector directly, which includes the central mass term and all spherical harmonic perturbations (zonal, tesseral, and sectoral).

## 2.2 Quaternion Normalization

To maintain the constraint  $\|\mathbf{q}\| = 1$ , the quaternion is explicitly normalized after **every successful integration step**:

$$\mathbf{q}_{next} = \frac{\mathbf{q} + \dot{\mathbf{q}}\Delta t}{\|\mathbf{q} + \dot{\mathbf{q}}\Delta t\|} \quad (4)$$

Frequent normalization prevents the accumulation of errors that could otherwise lead to unphysical rotations or "jumps" that destabilize adaptive-step solvers.

# 3 Simulation Workflow $f(t, \mathbf{Y})$

## 3.1 Time and Frame Setup

To synchronize with real-world observations (e.g., TLEs), we must account for the Earth's initial orientation:

### 1. Calculate Rotation Angle:

$\theta_{rot} = \theta_{GMST,0} + \omega_{\oplus} \cdot t$ , where  $\theta_{GMST,0}$  is the Greenwich Mean Sidereal Time at  $t = 0$ .

### 2. Rotation Matrix $\mathbf{R}_{ECIF}^{ECI}$ : Standard Z-axis rotation using $\theta_{rot}$ .

### 3. Position Conversion: $\mathbf{r}_{ECIF} = (\mathbf{R}_{ECIF}^{ECI})^T \mathbf{r}_{ECI}$ .

### 3.2 GeographicLib and Environmental Vectors

The `GravityModel` and `MagneticModel` return values in the Local Tangent Plane (ENU). These are rotated back to ECI for the ODE:

$$\mathbf{g}_{ECI} = \mathbf{R}_{ECEF}^{ECI} \cdot \mathbf{R}_{ENU}^{ECEF} \cdot \mathbf{g}_{ENU} \quad (5)$$

$$\mathbf{B}_{ECI} = \mathbf{R}_{ECEF}^{ECI} \cdot \mathbf{R}_{ENU}^{ECEF} \cdot \mathbf{B}_{ENU} \quad (6)$$

### 3.3 Magnetic Field Derivative

The material derivative captures field changes due to orbital motion:

$$\frac{D\mathbf{B}_{ECI}}{Dt} \approx \frac{\mathbf{B}_{ECI}(\mathbf{r} + \mathbf{v}\Delta t, t + \Delta t) - \mathbf{B}_{ECI}(\mathbf{r}, t)}{\Delta t} \quad (7)$$

In the Body frame, including the transport term (apparent change due to spacecraft rotation):

$$\frac{d\mathbf{B}_{body}}{dt} = \mathbf{R}_{ECI}^{Body}(\mathbf{q}) \frac{D\mathbf{B}_{ECI}}{Dt} - \boldsymbol{\omega} \times \mathbf{B}_{body} \quad (8)$$

### 3.4 Hysteresis Dynamics ( $\dot{\mathbf{M}}_{irr}$ )

For each rod  $i$ , we project the field  $H_i$  and its rate  $\dot{H}_i$  onto the rod's axis  $\mathbf{u}_i$ . The Jiles-Atherton evolution is:

$$\frac{dM_{irr,i}}{dt} = \dot{H}_i \cdot \frac{M_{an,i} - M_{irr,i}}{k \cdot \text{sign}(\dot{H}_i)} = \frac{M_{an,i} - M_{irr,i}}{k} |\dot{H}_i| \quad (9)$$

**Physicality and Stability Constraints:**

1. **Directional Constraint:** Magnetization must always move towards the anhysteretic curve. If  $(M_{an} - M_{irr})\dot{H}_i < 0$ , we set  $\dot{M}_{irr,i} = 0$  to prevent unphysical state excursions.
2. **Smoothing:** The  $\text{sign}(\dot{H}_i)$  function is approximated by  $\tanh(\beta\dot{H}_i)$  with  $\beta \approx 10^6$  to maintain continuity for the ODE solver.
3. **Singularity:** If  $|\dot{H}_i| < \epsilon$ , then  $\dot{M}_{irr,i} = 0$ .

### 3.5 Torque Dynamics

**Magnetic Torque:** Includes permanent magnets and the total rod magnetization (reversible + irreversible components):

$$\boldsymbol{\tau}_{mag} = \left( \mathbf{m}_{perm} + \sum [V_{rod,i}((1 - c)M_{irr,i} + cM_{an,i})\mathbf{u}_i] \right) \times \mathbf{B}_{body} \quad (10)$$

**Gravity Gradient Torque:**

$$\boldsymbol{\tau}_{grad} = \frac{3\mu}{\|\mathbf{r}_{ECI}\|^5} (\mathbf{r}_{body} \times (\mathbf{I} \cdot \mathbf{r}_{body})) \quad (11)$$