

## Advanced Computational Methods in Geotechnical Engineering

### Lecture

March 26, 2009

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✓ We need to know the excess porewater pressure at a desired time because we have to determine the vertical effective stress to calculate the consolidation settlement.

✓ Solution of the 1D consolidation equation can be found in two ways:

- Based on Fourier series expansion
- Based on Finite Difference Scheme.

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## 2. FD Solution of Terzaghi's Consolidation Equation

- The governing 1D Consolidation equation is:

$$\frac{\partial u}{\partial t} = C_v \frac{\partial^2 u}{\partial z^2}$$

Where,  $u$  is the excess pore water pressure,  $C_v$  is the coefficient of consolidation,  $z$  is the depth and  $t$  is time.

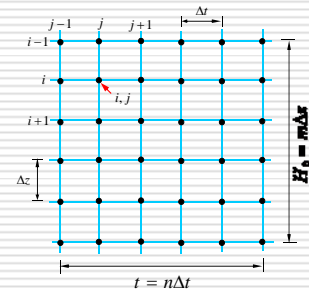
- The above equation allows us to predict the change in excess porewater pressure at various depths within the soil with time.

$$C_v = \frac{k}{m_v \gamma_w}$$

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- We will use Taylor's Expansion Theorem.

- First divide the domain into depth - time grid.



- **Columns:** time divisions & **Rows:** soil depth divisions.

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- Applying Taylor's series expansion to Terzaghi's eqn.

$$\frac{\partial u}{\partial t} = \frac{1}{\Delta t} (u_{i,j+1} - u_{i,j})$$

$$\frac{\partial^2 u}{\partial z^2} = \frac{1}{(\Delta z)^2} (u_{i+1,j} - 2u_{i,j} + u_{i-1,j})$$

$$\Rightarrow u_{i,j+1} = u_{i,j} + \frac{C_v \Delta t}{(\Delta z)^2} (u_{i+1,j} - 2u_{i,j} + u_{i-1,j}) \quad (2.1)$$

- Equation (1) is valid for non-boundary nodes.
- Special conditions apply to boundary nodes.

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- FDE at node 3:

$$\frac{du}{dx} = 1 \Rightarrow \frac{u_4 - u_2}{2\Delta x} = 1$$

- The FDE at an impermeable boundary is, thus:

$$\frac{\partial u}{\partial z} = 0 \Rightarrow \frac{u_{i+1,j} - u_{i-1,j}}{2\Delta z} = 0 \Rightarrow u_{i+1,j} = u_{i-1,j}$$

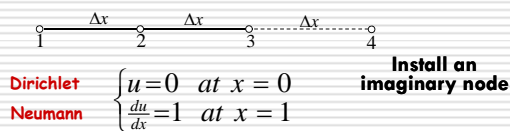
- And the governing consolidation equation becomes:

$$u_{i,j+1} = u_{i,j} + \frac{C_v \Delta t}{(\Delta z)^2} (2u_{i-1,j} - 2u_{i,j}) \quad (2.2)$$

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- For example, at an impermeable boundary, no flow across it can occur and, consequently:

$$\frac{\partial u}{\partial z} = 0 \Rightarrow \text{Neumann Boundary}$$



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- ※ Initial  $u$  distribution:- required to be determined first.

- For a layered soil with different  $k$  and  $C_v$ , Scott (1963) proposed the following FDE equation:

$$u_{i,j+1} = u_{i,j} + \frac{k_T + k_B}{k_B + k_T (C_v / C_{vs})} \frac{\Delta t}{(\Delta z)^2} \left( \frac{2k_T}{k_T + k_B} u_{i+1,j} - 2u_{i,j} + \frac{2k_B}{k_T + k_B} u_{i-1,j} \right)$$

where suffix  $T$  and  $B$  stand for top and bottom layers.

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### 2.1 Procedure to apply FDM to 1D consolidation problem

1. Divide the soil layer into a depth-time grid. Care must be taken in selecting  $\Delta t$  and  $\Delta z$ . For numerical convergence, researchers have proposed the following:

$$\alpha = \frac{C_v \Delta t}{(\Delta z)^2} < \frac{1}{2}$$

$\alpha = 0.25$  usually ensures convergence

2. Identify the boundary conditions. If the boundary is a drainage boundary,  $u$  is zero. If, however, the boundary is an impervious boundary, then no flow can occur across it and Eqn (2.2) has to be used.

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Table E2.1

Column	1	2	3	4	5	6
Depth	Time (yr)					
	0.00	0.1	0.2	0.3	0.4	0.5
0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.0	78.0	57.0	※			
2.0	72.0	※	※			
3.0	62.0	※	※			
4.0	48.0	※	※			
5.0	30.0	39.0	※			

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3. Estimate the distribution of initial  $u$ .

4. Calculate  $u$  at interior nodes using eqn. (2.1) and at impermeable boundary nodes using eqn. (2.2). If the boundary is permeable, then  $u$  is zero.

### EXAMPLE 2.1

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Table E2.1

Column	1	2	3	4	5	6
Depth	Time (yr)					
	0.00	0.1	0.2	0.3	0.4	0.5
0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.0	78.0	57.0	46.3	39.4	34.5	30.7
2.0	72.0	71.0	65.0	59.1	54.0	49.7
3.0	62.0	61.0	60.0	58.4	56.5	54.5
4.0	48.0	47.0	48.5	50.0	51.0	51.6
5.0	30.0	39.0	43.0	45.8	47.9	49.5

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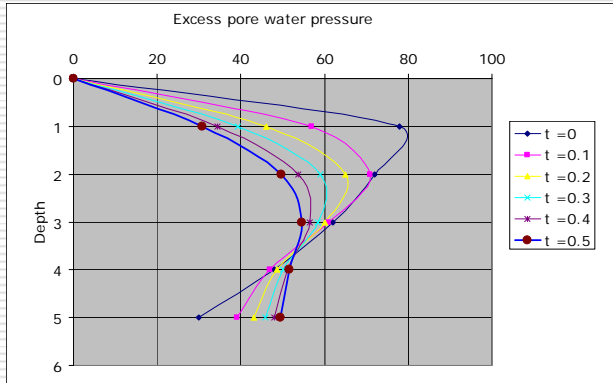


Figure E2.1

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### Assignment #2:

1. Redo example 2.1, assuming that the initial excess pore water pressure is distributed according to:

$$\Delta u_0 = \frac{180}{\sqrt{z}}$$

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