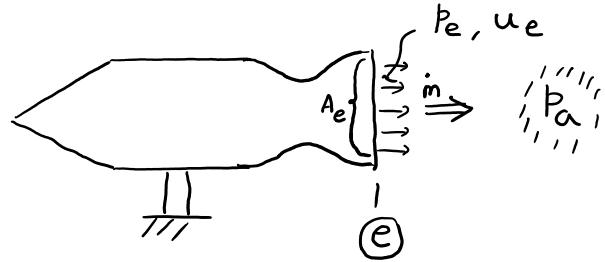


## Rockets



$$\tau = \dot{m}u_e + (p_e - p_a)A_e \quad (10\text{-}4)$$

$u_{eq}$  - equivalent exhaust velocity  
(aka) effective exhaust velocity

$$u_{eq} = \frac{\tau}{\dot{m}} = u_e + \frac{(p_e - p_a)A_e}{\dot{m}} \quad (10\text{-}5) \text{ & } (10\text{-}6)$$

since  $\dot{m} = \rho_e u_e A_e$ ,

$$u_{eq} = u_e + \frac{(p_e - p_a)A_e}{\rho_e u_e A_e} = u_e + \frac{(p_e - p_a)}{\rho_e u_e}$$

Using the ideal gas equation  $p = \rho R T$ ,

$$u_{eq} = u_e + \frac{RT_e}{u_e} \left( 1 - \frac{p_e}{p_a} \right) \quad [\text{verify}]$$

The specific impulse ( $I_{sp}$ ) of a rocket is

$$I_{sp} \stackrel{\text{def}}{=} \frac{\tau}{\dot{m}g_e} \quad \begin{matrix} [\text{thrust per unit weight}] \\ [\text{flow rate of propellant}] \end{matrix}$$

↗  
sea-level, earth ( $9.81 \text{ m/s}^2$ )

$$I_{sp} = \frac{u_{eq}}{g_e} \quad (10\text{-}7) \quad [\text{units of seconds}]$$

specific impulse of chemical rockets varies from 200 s to 450 s.

" " " nuclear " is around 900 s

" " " electrostatic thrusters is greater than 2000 s.

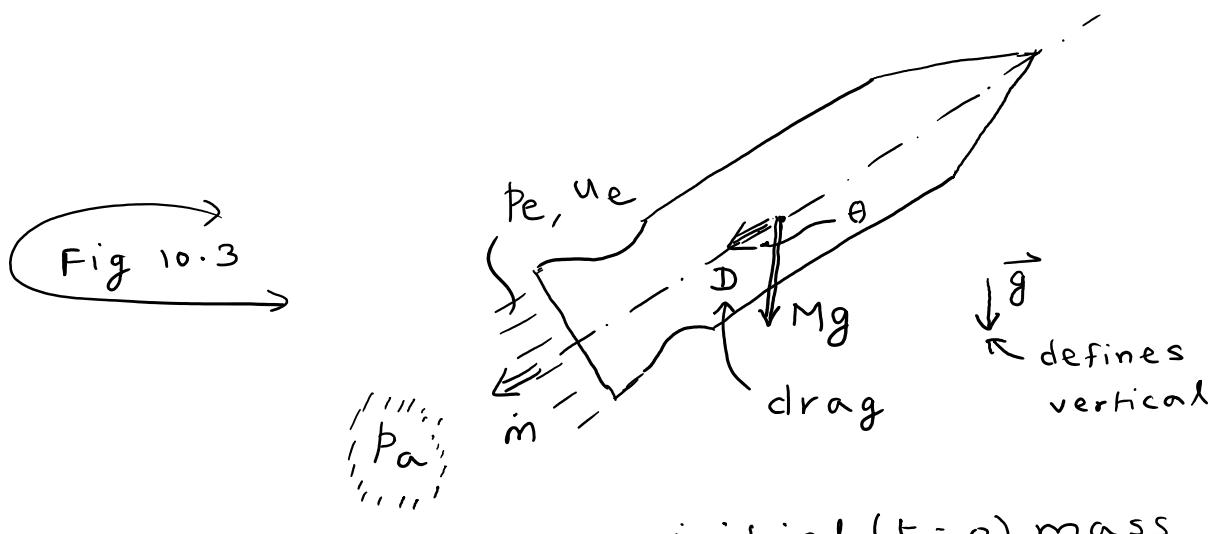
Example I<sub>sp</sub> values:

RD-170 (Atlas) : 309 s @ SL

RS-25 (SSME) : 453 s in vac.

R SRM : 267 s @ SL  
 solid motor  
 rocket  
 reusable

Vehicle acceleration, (sec 10.3)



$$\text{Mass : } \frac{dM}{dt} = -\dot{m} \Rightarrow M = M_0 - \dot{m}t$$

initial ( $t=0$ ) mass  
 mass of rocket at time  $t$

Burnout mass is  $M_b$

$$M_b = M_0 - \dot{m}t_b$$

burn time

Also, observe  $M_p = \dot{m}t_b$

$$M_b = M_0 - M_p$$

$$\text{Mass ratio } R \stackrel{\text{def}}{=} \frac{M_0}{M_b}$$

Momentum Equation :

$$M \frac{du}{dt} = \dot{m} u_{eq} - Mg \cos \theta - D$$

↑ accn. due to gravity  
↑ inclination of flight direction to vertical

Acceleration ( $a$ ) :

$$a = \frac{du}{dt} = \frac{\dot{m} u_{eq}}{M} - g \cos \theta - \frac{D}{M}$$

Launch accln ( $a_0$ ) :

$$(M = M_0) \quad a_0 = \frac{\dot{m} u_{eq}}{M_0} - g_e \cos \theta \quad \begin{matrix} \theta = 0 \text{ [typical]} \\ \text{vertical launch} \end{matrix}$$

$\uparrow \omega_{SL, \text{earth}}$

$$\Rightarrow a_0 = \frac{\dot{m} u_{eq}}{M_0} - g_e$$

Burnout accln ( $a_b$ ) :

( $M = M_b$ )

$$a_b^- = \frac{\dot{m} u_{eq}}{M_b} - g \cos \theta_b - \frac{D_b}{M_b}$$

$\uparrow$   
just before burnout

$$a_b^+ = -g \cos \theta_b - \frac{D_b}{M_b}$$

$\uparrow$   
just after burnout

$a_b$  cannot be found without knowledge of burnout altitude ( $g$  depends on altitude),

inclination angle at burnout ( $\theta_b$ ) and the drag ( $D_b$ ) then. The magnitude of  $a_{b^-}$  however, will be significantly larger than that of  $a_0$  since the propellant mass is a large fraction of the rocket initial mass (91% for the lunar rocket, 86% for the space shuttle, for example).

- \* Short burn time results in high  $\dot{m} \Rightarrow$  large  $a_{b^-}$ . Thus  $t_b$  should not be too small.
- \* Long burn time may result in insufficient  $a_0$ , and high gravity and drag losses (discussed later).
- \* Typical burn times for launch vehicles are on the order of several minutes {RSRM 2 min, SSME 8 min, lunar rocket 1.5 min (stage 1), 6 min (stage 2), 8 min (stage 3), Falcon 9 2.6 min (stage 1), 7 min (stage 2)}.

## Velocity Rise

The function of a rocket is to provide velocity rise to the payload. To find it, integrate the acceleration equation.

$$\frac{du}{dt} = \frac{\dot{m}}{M} u_{eq} - g \cos \theta - \frac{D}{M}$$

$$\text{since } \dot{m} = -\frac{dM}{dt},$$

$$\frac{du}{dt} = -\frac{u_{eq}}{M} \frac{dM}{dt} - g \cos \theta - \frac{D}{M}$$

$$\Rightarrow du = -u_{eq} \frac{dM}{M} dt - g \cos \theta dt - \frac{D}{M} dt \quad (10.9)$$

$$\begin{aligned} u &= u_b & M_b & \quad t = t_b & \quad t = t_b \\ \int du &= - \int_{u_0}^{u_b} u_{eq} \frac{dM}{M} dt & - \int_{t=0}^{t_b} g \cos \theta dt - \int_{t=0}^{t_b} \frac{D}{M} dt \end{aligned}$$

$$\Rightarrow (u_b - u_0) \equiv \Delta u_b = u_{eq} \ln \frac{M_0}{M_b} - \overline{g \cos \theta} t_b - \overline{\left(\frac{D}{M}\right)} t_b,$$

$$\text{where } \overline{g \cos \theta} = \frac{\int_0^{t_b} g \cos \theta dt}{t_b}, \text{ and } \overline{\left(\frac{D}{M}\right)} = \frac{\int_0^{t_b} \left(\frac{D}{M}\right) dt}{t_b}$$

are just concise representations of the gravity and drag integrals, respectively.

### Impulsive velocity rise ( $\Delta u_{b,imp}$ )

Impulsive velocity rise is defined to be the velocity rise attained with zero burn time ( $t_b = 0$ ).

$$\Delta u_{b,imp} = u_{eq} \ln \frac{M_0}{M_b}$$

$$\Delta u_b = \Delta u_{b,imp} - \frac{g \cos \theta}{\left(\frac{D}{M}\right)} t_b - \left(\frac{D}{M}\right) t_b^2$$

It is clear that finite burn times decrease the attainable velocity rise. Longer the burn, greater are the gravity and drag losses (mentioned earlier).

### Gravity

$$\frac{g}{g_e} = \left( \frac{R_e}{R_e + h} \right)^2 \quad (10.12)$$

$g$  - accn. due to gravity at altitude  $h$

$g_e$  - " " " " at earth's surface

$R_e$  - radius of the earth ( $R_e = 6378 \text{ km}$ )

### Drag

$$D = C_D \frac{1}{2} \rho u^2 A_f \quad (10.14)$$

D - drag

$$\rho - \text{density} \left\{ \begin{array}{l} \rho = a \exp(-bh^{1.15}), a = 1.2, \\ b = 2.9(10^{-5}), h \text{ in m}, \rho \text{ in } \frac{\text{kg}}{\text{m}^3} \end{array} \right\}$$

u - velocity

$A_f$  - frontal area

$C_D$  - drag coefficient {see Fig 10-4}

### Example

Consider a rocket

$$\dot{m} = 8740 \text{ kg/s}, u_e = 2600 \text{ m/s}, p_e = 71 \text{ kPa},$$

$$A_e = 11.35 \text{ m}^2, M_0 = 1,720,000 \text{ kg}, M_b = 680,000 \text{ kg}$$

vertical ascent ( $\theta = 0$ ),  $g = g_e$ . Neglect drag.

Find  $\tau_{SL}$ ,  $u_{eq,SL}$ ,  $I_{sp,SL}$ ,  $u_{eq,vac}$ ,  $I_{sp,vac}$ ,

$$a_0, a_{b^-}, a_{b^+}, \Delta u$$

$$\tau = \dot{m} u_e + (p_e - p_a) A_e$$

$$p_a = 101 \text{ kPa} \text{ at } SL.$$

$$\tau_{SL} = \dot{m} u_e + (p_e - p_{a,SL}) A_e$$

$$= (8740)(2600) + (71 - 101)(1000)(11.35)$$

$$= 2.24 \times 10^7 \text{ N}$$

$$u_{eq,SL} = \frac{\tau_{SL}}{\dot{m}} = \frac{2.24 \times 10^7}{8740} = 2563 \text{ m/s}$$

$$I_{sp,SL} = \frac{u_{eq,SL}}{g_e} = \frac{2563}{9.81} = 261 \text{ s}$$

$p_a = 0$  at vacuum

$$\begin{aligned} T_{vac} &= \dot{m} u_e + (p_e - p_{a,vac}) A_e \\ &= (8740)(2600) + (71 - 0)(1000)(11.35) \\ &= 2.35 \times 10^7 \text{ N} \end{aligned}$$

{  $p_e, u_e, m$  fixed for a rocket - important observation }

$$u_{eq,vac} = \frac{T_{vac}}{\dot{m}} = \frac{2.35 \times 10^7}{8740} = 2689 \text{ m/s}$$

$$I_{sp, vac} = \frac{u_{eq,vac}}{g_e} = \frac{2689}{9.81} = 274 \text{ s}$$

$$\begin{aligned} a_0 &= \frac{\dot{m} u_{eq,sl}}{M_0} - g_e = \frac{(8740)(2563)}{1,720,000} - 9.81 \\ &= 3.21 \text{ m/s}^2 = 0.33 g_e \end{aligned}$$

$$a_b^- = \frac{\dot{m} u_{eq,sl}}{M_b} - g_b \underbrace{\cos \theta_b^0}_{\substack{\uparrow \\ (\text{vertical ascent})}} - \frac{g_b}{M_b} \theta_b^0 \quad (\text{neglect drag})$$

$g_e$  (constant gravity)

$$= \frac{(8740)(2563)}{680,000} - 9.81 = 23.1 \frac{\text{m}}{\text{s}^2} = 2.36 g_e$$

$$\begin{aligned} \text{Burn Time } t_b &= \frac{M_p}{\dot{m}} = \frac{(M_0 - M_p)}{\dot{m}} \\ &= \frac{(1,720,000 - 680,000)}{8740} = 119 \text{ s} \end{aligned}$$

$$\Delta u_b = u_{eq} \ln \frac{M_0}{M_b} - \int_0^{t_b} g \cos \theta \, dt - \int_0^{t_b} \left( \frac{D}{M} \right) dt$$

$\int_0^{t_b} g \cos \theta \, dt = \int_0^{t_b} g_e \cos(\theta) \, dt = g_e \int_0^{t_b} dt = g_e t_b$   
 $\frac{g \cos \theta}{\cancel{g \cos \theta}} = \frac{\int_0^{t_b} g \cos \theta \, dt}{t_b} = \frac{g_e t_b}{t_b} = g_e$

$$\begin{aligned}
 \Delta u_b &= u_{eq} \ln \frac{M_0}{M_b} - \overline{g \cos \theta} t_b \\
 &= 2563 \ln \frac{1,720,000}{680,000} - (9.81)(119) \\
 &= 2378 - 1167 = 1211 \text{ m/s} = 1.21 \text{ km/s}
 \end{aligned}$$

Observe the significant magnitude of the gravity loss. In a LEO launch, the gravity and drag losses can amount to 20% of the  $\Delta u_b$  the rocket is designed to provide.