

In a chemical rocket, the propellant also serves as the energy source. Thus, these vehicles are energy-limited.

In a nuclear rocket, nuclear power is used to energize the propellant. The attendant temperature change is limited by material considerations, and these devices are also energy-limited.

Electrical rockets impart kinetic energy to the propellant without necessarily increasing its temperature, and thus enables attainment of high propellant energy levels and associated  $I_{sp}$ . The mass of the power plant, however, increases with the power generated, and, therefore, the performance of these devices is also limited.

$$\text{Thrust efficiency, } \eta \stackrel{\text{def}}{=} \frac{\frac{\dot{m} u_e^2}{2}}{P} \quad (10.40)$$

$$\text{Thrust specific mass, } \alpha \stackrel{\text{def}}{=} \frac{M_P + M_S}{P} \quad (10.39)$$

$\dot{m}$  - propellant mass flow rate

$u_e$  - propellant exhaust velocity

$M_P$  - mass of power plant

$M_S$  - mass of the structure

$$M_0 = M_L + (M_P + M_S) + M_P$$

$$M_b = M_L + (M_P + M_S)$$

$$I_{sp} = \frac{u_e}{g_e}$$

$$\Delta u_b = u_e \ln \frac{M_0}{M_b}$$

$$\frac{M_b}{M_0} = e^{-\frac{\Delta u_b}{u_e}} \quad (10.41)$$

Relating  $\frac{M_L}{M_0}$  to  $u_e$  (or  $I_{sp}$ )

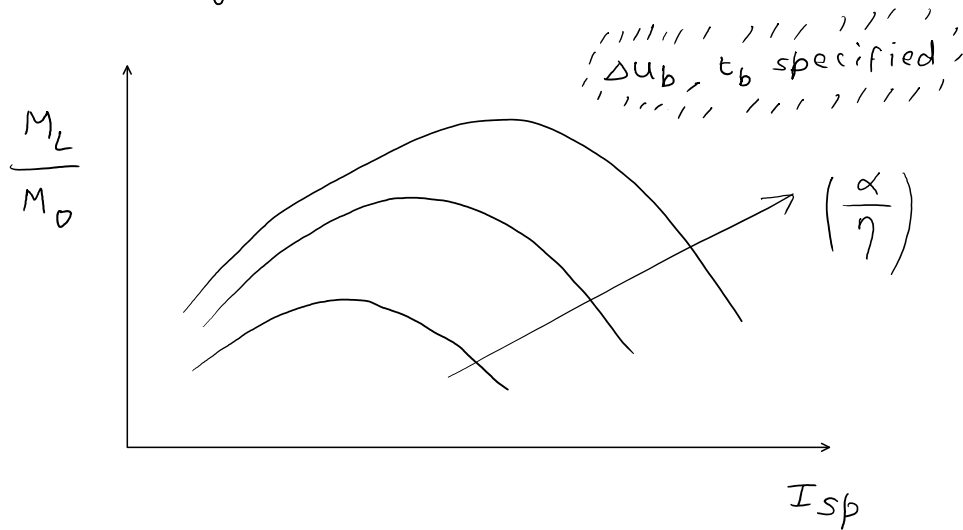
$$\frac{M_b}{M_0} = \frac{M_L}{M_0} + \frac{(M_P + M_S)}{M_0} \stackrel{(Eq 10.39)}{=} \frac{M_L}{M_0} + \frac{\alpha \dot{P}}{M_0} \stackrel{Eq (10.40)}{=} \frac{M_L}{M_0} + \frac{\alpha}{2\eta} \frac{\dot{m} u_e^2}{M_0}$$

$$\begin{aligned} (or) \quad \frac{M_b}{M_0} &= \frac{M_L}{M_0} + \frac{\alpha}{2\eta} \left( \frac{M_P}{t_b} \right) \frac{u_e^2}{M_0} = \frac{M_L}{M_0} + \frac{\alpha u_e^2}{2\eta t_b} \frac{M_P}{M_0} \\ &= \frac{M_L}{M_0} + \frac{\alpha u_e^2}{2\eta t_b} \left( 1 - \frac{M_b}{M_0} \right) \left[ M_P = (M_0 - M_b) \right] \end{aligned}$$

$$\Rightarrow \left( \frac{M_b}{M_0} \right) \left( 1 + \frac{\alpha u_e^2}{2\eta t_b} \right) = \frac{M_L}{M_0} + \frac{\alpha u_e^2}{2\eta t_b}$$

$$\begin{aligned} &\stackrel{Eq (10.41)}{\downarrow} e^{-\frac{\Delta u_b}{u_e}} \left( 1 + \frac{\alpha u_e^2}{2\eta t_b} \right) = \frac{M_L}{M_0} + \frac{\alpha u_e^2}{2\eta t_b} \\ (or) \quad &e^{-\frac{\Delta u_b}{u_e}} \left( 1 + \frac{\alpha u_e^2}{2\eta t_b} \right) = \frac{M_L}{M_0} + \frac{\alpha u_e^2}{2\eta t_b} \end{aligned}$$

$$\Rightarrow \frac{M_L}{M_0} = e^{-\frac{\Delta u_b}{u_e}} \left( 1 + \frac{\alpha u_e^2}{2\eta t_b} \right) - \frac{\alpha u_e^2}{2\eta t_b} \quad (10-43)$$



- \* For a given mission; that is given  $\Delta u_b$  and  $t_b$ , there exists an optimum  $I_{sp}$  that maximizes the  $\left(\frac{M_L}{M_0}\right)$  ratio. Unlike a chemical rocket, the optimum is not the highest  $I_{sp}$ .
- \* Due to long burns, the  $\Delta u_b$  that an electrical rocket vehicle has to generate for a mission will be much greater than the corresponding  $\Delta u_{b,imp}$  (see Fig 10.22). The vehicle can be advantageously employed, despite this penalty, due to its low propellant consumption (low  $\frac{M_P}{M_0}$ ).

Ex An electric thruster is used to raise a satellite orbit:

$$I_{sp} = 2000 \text{ s}, \quad T = 0.20 \text{ N}, \quad t_b = 4 \text{ weeks},$$

$$M_L = 100 \text{ kg}, \quad \eta = 0.5, \quad \alpha = 10 \frac{\text{kg}}{\text{kW}}. \quad \text{Find}$$

the mass of propellant required, the power required, the mass of power plant and structure, and the initial mass, the burnout mass and the  $\left(\frac{M_L}{M_0}\right)$  of the vehicle.  
Can the vehicle raise the payload from LEO to GEO?

$$u_e = I_{sp} g_e = (2000)(9.81) = 19620 \text{ m/s}$$

$$\dot{m} = \frac{T}{u_e} = \frac{0.20}{19620} = 1.02 (10^{-5}) \text{ kg/s}$$

$$t_b = 4 \text{ weeks} = (4)(7)(24)(3600) = 2.4192 (10^6) \text{ s}$$

$$M_p = \dot{m} t_b = (1.02)(10^{-5})(2.4192)(10^6) = 24.68 \text{ kg}$$

$$P = \frac{\frac{1}{2} \dot{m} u_e^2}{\eta} = \frac{\frac{1}{2} (1.02)(10^{-5})(19620)^2}{0.5} = 3926 \text{ W}$$

$$(\text{or}) P = 3.93 \text{ kW}$$

$$\alpha = \frac{M_p + M_s}{P} = 10 \frac{\text{kg}}{\text{kW}} \Rightarrow (M_p + M_s) = \alpha P = (10)(3.93) = 39.3 \text{ kg}$$

$$M_0 = M_L + (M_p + M_s) + M_p = (100 + 39.3 + 24.68) = 164 \text{ kg}$$

$$M_b = M_L + (M_P + M_S) = 139.3 \text{ kg}$$

$$\frac{M_L}{M_0} = 0.61$$

$$\Delta u_b = u_e \ln \frac{M_0}{M_b} = 19620 \ln \frac{164}{139.3} = 3203 \frac{\text{m}}{\text{s}} = 3.2 \frac{\text{km}}{\text{s}}$$

$$\text{Table 10.8} \Rightarrow (\Delta u_b)_{\text{req}} = 4.2 \text{ km/s}$$

No, the vehicle cannot raise the payload from LEO to GEO.