# THE QUADRATURE (90°) HYBRID

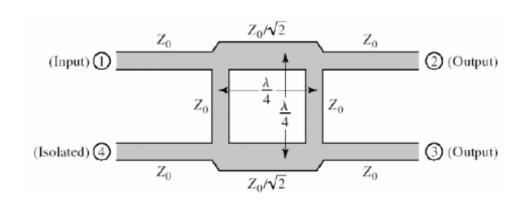
SINGLE-BOX BRANCHLINE COUPLER

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## Four Port Network: Quadrature (90°) Hybrid

#### Quadrature (90 degree) Hybrid:

- Directional Coupler
- Symmetric Coupler
- $\triangleright$  Coupling Factor = 3 dB



#### **Directional Coupler:**

- Lossless
- reciprocal
- matched-four port network

#### Symmetric Coupler:

- 90 degree phase shift

## Scattering Parameters Matrix

Coupling Factor:

$$-20 \log_{10} \beta = 3 dB$$

$$\beta = \alpha = \frac{1}{\sqrt{2}}$$

$$[S] = \begin{bmatrix} 0 & \alpha & j\beta & 0 \\ \alpha & 0 & 0 & j\beta \\ j\beta & 0 & 0 & \alpha \\ 0 & j\beta & \alpha & 0 \end{bmatrix} \longrightarrow [S] = \frac{1}{\sqrt{2}} \begin{bmatrix} 0 & 1 & j & 0 \\ 1 & 0 & 0 & j \\ j & 0 & 0 & 1 \\ 0 & j & 1 & 0 \end{bmatrix}$$

## Normalized Circuit

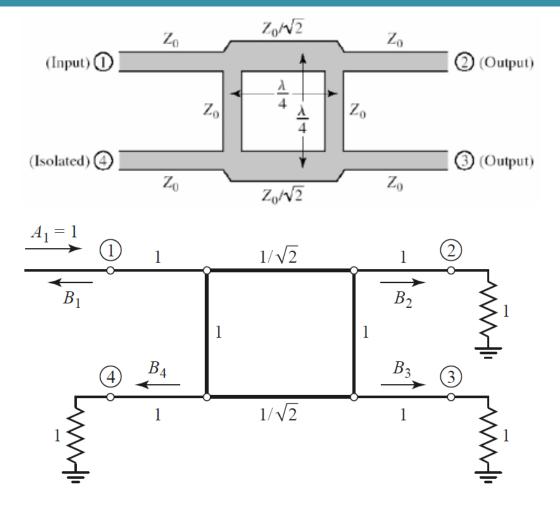
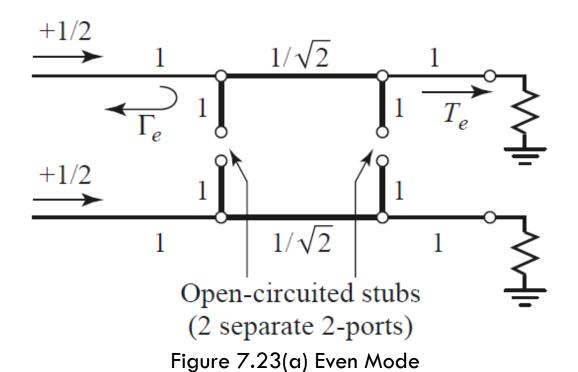


Figure 7.22 Normalized Form

## Even Mode Analysis



 $\begin{bmatrix} A & B \\ C & D \end{bmatrix}_{e} = \underbrace{\begin{bmatrix} 1 & 0 \\ j & 1 \end{bmatrix}}_{\text{Shunt}} \underbrace{\begin{bmatrix} 0 & j/\sqrt{2} \\ j\sqrt{2} & 0 \end{bmatrix}}_{\text{Transmission}} \underbrace{\begin{bmatrix} 1 & 0 \\ j & 1 \end{bmatrix}}_{\text{Shunt}} = \frac{1}{\sqrt{2}} \begin{bmatrix} -1 & j \\ j & -1 \end{bmatrix}$ 

$$\Gamma_e = \frac{A+B-C-D}{A+B+C+D} = 0,$$

$$T_e = \frac{2}{A+B+C+D} = \frac{-1}{\sqrt{2}}(1+j).$$

## Odd Mode Analysis

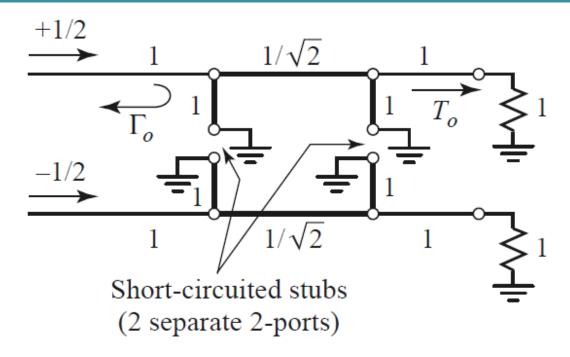


Figure 7.23(b) Odd Mode

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix}_o = \underbrace{\begin{bmatrix} 1 & 0 \\ -j & 1 \end{bmatrix}}_{\text{Shunt}} \underbrace{\begin{bmatrix} 0 & j/\sqrt{2} \\ j\sqrt{2} & 0 \end{bmatrix}}_{\text{Transmission}} \underbrace{\begin{bmatrix} 1 & 0 \\ -j & 1 \end{bmatrix}}_{\text{Shunt}} = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 & j \\ j & 1 \end{bmatrix}$$

$$T_o = 0,$$

$$T_o = \frac{1}{\sqrt{2}} (1 - j).$$

### Normalized Circuit

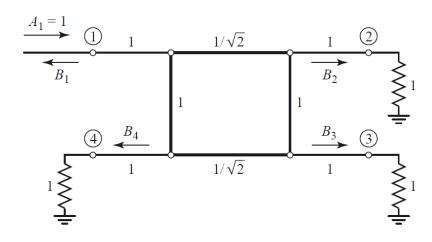


Figure 7.22 Normalized Form

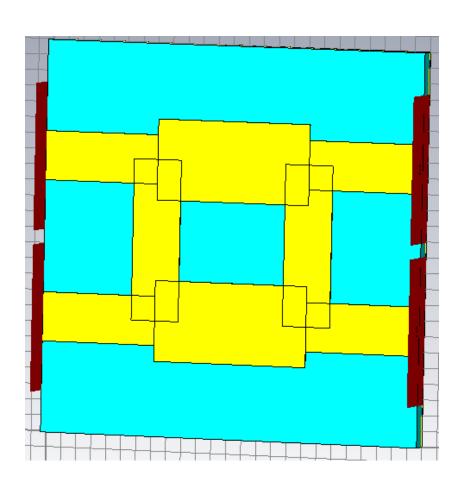
$$B_{1} = \frac{1}{2}\Gamma_{e} + \frac{1}{2}\Gamma_{o} = 0$$
 (port 1 is matched), (7.67a)  

$$B_{2} = \frac{1}{2}T_{e} + \frac{1}{2}T_{o} = -\frac{j}{\sqrt{2}}$$
 (half-power, -90° phase shift from port 1 to 2), (7.67b)  

$$B_{3} = \frac{1}{2}T_{e} - \frac{1}{2}T_{o} = -\frac{1}{\sqrt{2}}$$
 (half-power, -180° phase shift from port 1 to 3), (7.67c)  

$$B_{4} = \frac{1}{2}\Gamma_{e} - \frac{1}{2}\Gamma_{o} = 0$$
 (no power to port 4). (7.67d)

# Design Modeling

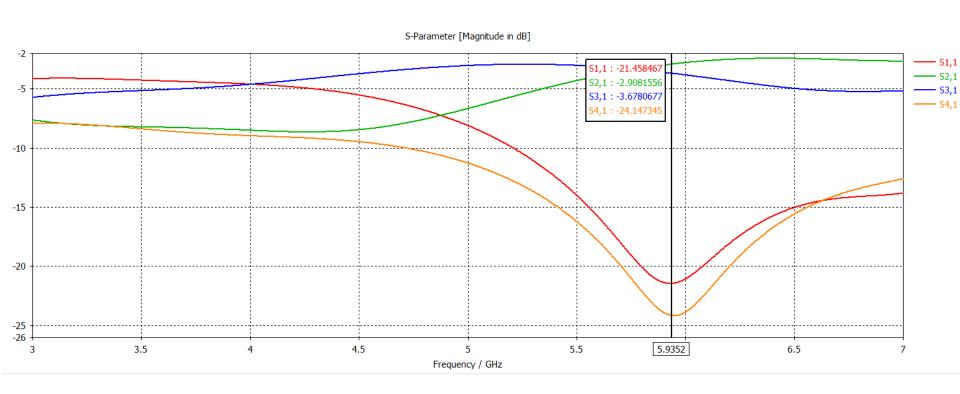


| Lines              | Width<br>(mm) | Length<br>(mm) |
|--------------------|---------------|----------------|
| 50Ω Line           | 5.15          | 10.059         |
| $35.36\Omega$ Line | 3.13          | 10.266         |

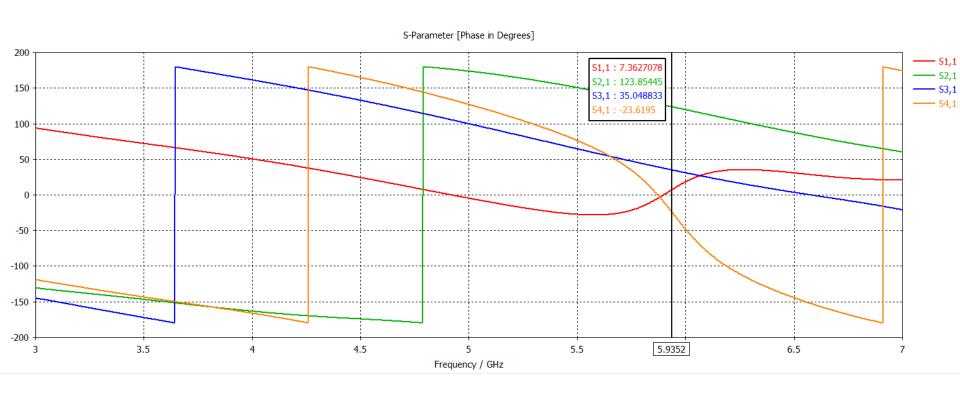
$$d = 1.160mm$$

$$\epsilon_r = 2.55$$

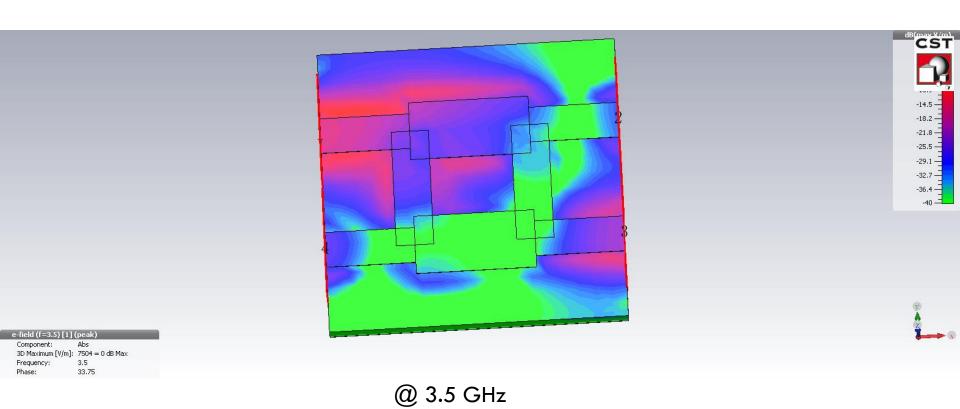
## **CST Simulation**



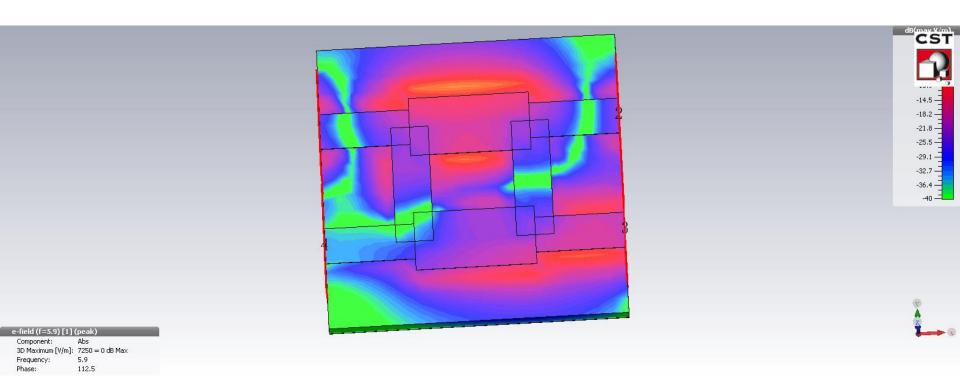
## **CST Simulation**



## **Surface Current Animation**



## **Surface Current Animation**



@ 5.9 GHz

#### Citations

- [1] David M. Pozar, Microwave Engineering. Hoboken: John Wiley & Sons, Inc, 2011.
- [2] Stuart M. Wentworth, Applied Electromagnetics: Early Transmission Lines Approach. Hoboken: John Wiley & Sons, Inc, 2006.
- [3] "Microstrip Line Calculator." InfoSphere. [Online]. Available: http://www1.sphere.ne.jp/i-lab/ilab/tool/ms\_line\_e.htm