# Chapter 12: Lead and Lag Compensators

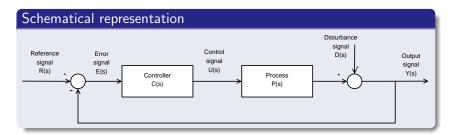
August 3, 2015

## Outline

Definition of compensators

2 Lead compensators

# Lead Compensator vs Lag Compensator



#### Transfer functions

Lead compensator :  $C(s) = K.\frac{s+\frac{1}{\tau}}{s+\frac{1}{\alpha\tau}}$  with  $0<\alpha<1$  Lag compensator :  $C(s) = K.\frac{s+\frac{1}{\tau}}{s+\frac{1}{\beta\tau}}$  with  $\beta>1$ 

# Lead Compensator vs Lag Compensator: zeros and poles

#### Transfer functions

Lead compensator :  $C(s) = K.\frac{s+\frac{1}{\tau}}{s+\frac{1}{\alpha\tau}}$  with  $0<\alpha<1$  Lag compensator :  $C(s) = K.\frac{s+\frac{1}{\tau}}{s+\frac{1}{\beta\tau}}$  with  $\beta>1$ 

#### Zeros and poles

Zeros:  $s = -\frac{1}{\tau}$ Poles:  $s = -\frac{1}{\alpha\tau}$  or  $s = -\frac{1}{\beta\tau}$ 

For lead compensators the pole lies more to the left in the complex plane than the zero and vice versa for lag compensators.

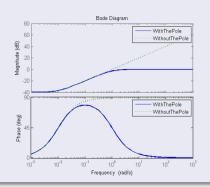
## Outline

Definition of compensators

2 Lead compensators

#### **Impact**

$$C(s) = K.\frac{s + \frac{1}{\tau}}{s + \frac{1}{\alpha \tau}}$$
 with  $0 < \alpha < 1$ 



#### **Impact**

- They push the pole of the closed loop system to the left.
  - Stabilisation of the system (see root locus)
  - Increase response speed (lead compensator will stimulate some larger frequencies)
- Increase of the phase margin: the phase of the lead compensator is positive for every frequency, and will hence only increase the phase.
- Thanks to the presence of a pole, the high frequencies (where most of the unwanted noise is located) are less amplified.

#### Design with Bode plots

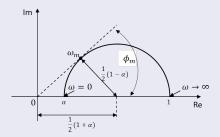
- Design process: tuning of the phase margin, with as a surplus (because we will have one extra degree of freedom) the tuning of the steady state error.
- Compensate for the excessive phase lag that is a result of the components of P(s).
- Increase in phase at gain crossover frequency (GCF) if GCF is around pole and zero of the lead compensator.
- Gain is impacted by the lead compensator: the GCF of P(s).C(s) is not equal to the GCF of P(s).

#### Design

- Required increase in phase gain:  $\phi$
- To compensate for increase GCF due to  $C(s) \Rightarrow \phi_m = \phi + 5^{\circ}$ . This will be needed to determinate  $\alpha$  and  $\tau$
- K will be used to tune the steady state error.

#### Determination of $\alpha$

Use polar plot of  $\frac{\alpha \cdot (j\omega\tau+1)}{i\omega\alpha\tau+1}$ 



$$\sin \phi_m = \frac{\frac{1}{2} \cdot (1 - \alpha)}{\frac{1}{2} \cdot (1 + \alpha)} = \frac{1 - \alpha}{1 + \alpha} \Rightarrow \alpha = \frac{1 - \sin \phi_m}{1 + \sin \phi_m}$$

 $\sin\phi_m = \frac{\frac{1}{2}.(1-\alpha)}{\frac{1}{2}.(1+\alpha)} = \frac{1-\alpha}{1+\alpha} \Rightarrow \alpha = \frac{1-\sin\phi_m}{1+\sin\phi_m}$  This relation relates the maximum phase-lead angle and the value of  $\alpha$ .

#### Determination of au

Tekening bodeplot zoals boek p 622. The tangent point  $\omega_m$  is the geometric mean of the two corner frequencies, so

$$\log \omega_m = \frac{1}{2} (\log \frac{1}{\tau} + \log \frac{1}{\alpha \tau})$$
 with  $\tau = \frac{1}{\omega}$   $\Rightarrow \omega_m = \frac{1}{\sqrt{\alpha \tau}}$ .

The lead compensator is a high pass filter.

#### Determination of the tangent point

Use the gain crossover frequency of P(s)C(s) as  $\omega_m$ :

$$|P(j\omega_{m})C(j\omega_{m})| = 1$$

$$|P(j\omega_{m})| K \frac{\sqrt{\frac{1}{\alpha\tau^{2}} + \frac{1}{\tau^{2}}}}{\sqrt{\frac{1}{\alpha\tau^{2}} + \frac{1}{\alpha^{2}\tau^{2}}}} = |P(j\omega_{m})| K\sqrt{\alpha} = 1$$

 $20 \log |P(j\omega_m)| = -20 \log(K\sqrt{\alpha})$ 

The value of the tangent point  $\omega_m$  can be determined from P(s)'s Bode plot, if you know K (the last freedom).

#### Determination of K

- Remember the steady state error for references of the shape:  $\frac{At^n \epsilon(\tau)}{n!}$  with  $\epsilon(t)$  the step function.
- We found the error constants  $K_p$ ,  $K_v$  and  $K_a$  as measures for the steady state error for a proportional (n=0), linear (n=1) and accelerating (n=2) reference.
- So these error constants can be used to find proper values of K:  $\lim_{s\to 0} K \frac{s+\frac{1}{\tau}}{s+\frac{1}{\tau}} s^n P(s) = K\alpha \lim_{s\to 0} s^n P(s)$

# Lead Compensation Techniques Based on the Frequency-Response Approach

#### Step 1

Find  $K\alpha$  from your steady-state requirement.

#### Step 2

Determine  $\phi$ , the amount with which you want to increase the PM; if the PM is OK, you dont need a lead compensator; a proportional controller with gain  $K\alpha$  suffices.

#### Step 3

Add 5°, to get  $\phi_m=\phi+5^\circ$  (if  $\phi_m>5^\circ$ , you will need more than one lead compensator). The addition of the lead compensator shifts the gain crossover frequency to the right and decreases the phase margin.

# Lead Compensation Techniques Based on the Frequency-Response Approach

#### Step 4

Youll find  $\alpha$  from this  $\phi_m$ :  $\alpha = \frac{1-\sin\phi_m}{1+\sin\phi_m}$  and hence also K (see step 1).

## Step 5

Find the desired  $\omega_m$  by looking at the Bode plot of P(s) and finding the frequency at which the gain equals  $-20 \log(K\sqrt{\alpha})$  dB.

#### Step 6

Find  $\tau$  as  $\frac{1}{\sqrt{\alpha}\omega_m}$ .

# Lead Compensation Techniques Based on the Frequency-Response Approach

#### Step 7

Verify if the system works as asked. Check the gain margin to be sure it is satisfactory. If not, repeat the design process by modifying the pole-zero location of the compensator until a satisfactory result is obtained.

#### Example

Given the system  $P(s) = \frac{4}{s(s+2)}$ . We want a phase margin of at least 50° and a steady state error for slope reference of maximal  $\frac{A}{20}$ .

## Example: Bode plot and phase diagram

Maken in MATLAB.

# Example

### Step 1

Steady-state requirement:  $K_v = \frac{20}{s}$ So,  $\lim_{s\to 0} sP(s)C(s) = \lim_{s\to 0} s\frac{s}{s(s+2)}K\alpha = 2K\alpha = 20$ .  $\Rightarrow K\alpha = 10$ 

#### Step 2

Phase margin of  $K(s)=18\,^\circ$  (see phase diagram)  $\Rightarrow \phi=32\,^\circ$ 

### Step 3

$$\phi_m = \phi + 5^{\circ} = 37^{\circ}$$

# Example

## Step 4

$$\alpha = \frac{1-\sin\phi_m}{1+\sin\phi_m} = 0.24$$

From step 1, we know that  $K = \frac{\alpha}{10} = 42$ 

### Step 5

Find  $\omega_m$ , the frequency at which the gain is  $-20 \log(K\sqrt{\alpha})$  dB.  $GCF(P(s)K\sqrt{\alpha}) = GCF(P(s)C(s)) \Rightarrow \omega_m = 9 \frac{rad}{s}$  (see Bode diagram next slide)

### Step 6

$$\tau = \frac{1}{\omega_m \sqrt{\alpha}} = 0.23$$

# Example

Step 7

Verify! MATLAB!!!!

# Summary lead compensators

### Evaluation of impact

- Pushing the poles to the left: this is not directly visible here, but is linked to the increased band width.
- The increase in bandwidth (this is linked to the response speed) and the increase in the phase margin were apparent in the Bode plot of P(s)C(s).
- A (small) decrease in the steady-state error occurs, since we designed it as such.
  - Why small? The steady-state error decreases when the DC gain gets larger, but a lead compensators impact on the gain is not really built to increase the DC gain, the shape of a lag compensator is much more fit for this.

## Summary lead compensators

#### Design with root locus

Design lead compensators with root locus for time-domain quantities - use dominant pole locations to fulfill overshoot, rise time, settling time, damping ratio, requirements.

## Outline

Definition of compensators

2 Lead compensators

Impact of lag compensators: Bode diagram

**MATLAB** 

#### Transfer function

$$C(s) = K \cdot \frac{s + \frac{1}{\tau}}{s + \frac{1}{\beta \tau}}$$
 with  $\beta > 1$ 

#### Impact of lag compensators: Bode diagram

- Lead compensators: increase the stability and tune the steady-state error by increasing the phase at the crossover frequency.
- Impact lag compensator = lead compensator, but different approach! By decreasing the gain, the gain crossover frequency comes down to a frequency at which the corresponding phase is higher.