### Outline

- 1 Linear differential equations
- 2 Laplace transform
- 3 Solving LDEs with the Laplace transform
- Properties of state-space representation
- Transfer functions
  - Impulse response and time constant
  - Relationship between state space and transfer functions
- Transient response analysis of first order and second order systems
  - First order systems
  - Second order systems

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#### The time response of a control system can be written as:

$$y(t) = y_{tr}(t) + y_{ss}(t)$$

where  $y_{tr}(t)$  is the transient response and  $y_{ss}(t)$  is the steady state response.

#### Definition

The transient response of a system is the time-difference between the change of the inputs and the change of the outputs: when the input of a system changes, the output does not change immediately but takes time to go to steady state.

# First order systems: stability

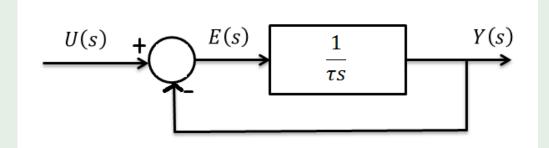
The most important characteristic of a dynamic system is absolute stability.

- A system is stable when it returns to equilibrium, if subject to initial condition
- A system is critically stable when oscillations of the output continue forever
- A system is unstable when the output diverges without bound from equilibrium, if subject to initial condition

# First order systems

#### Example

Unit step response of RC circuit, thermal system, ...



The transfer function is given by:  $\frac{Y(s)}{U(s)} = \frac{1}{\tau s + 1}$ 

- Laplace of unit-step is  $\frac{1}{s} \to \text{substituting } U(s) = \frac{1}{s}$ :  $Y(s) = \frac{1}{s} \cdot \frac{1}{\tau s + 1}$ ;
- Expanding into partial fractions gives

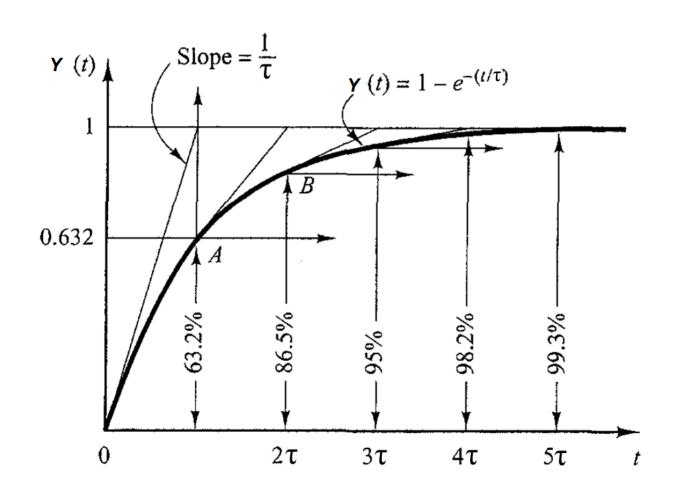
$$Y(s) = \frac{1}{s} - \frac{\tau}{\tau s + 1} = \frac{1}{s} - \frac{1}{s + \frac{1}{\tau}}.$$

# Unit step transient response

**1** 
$$Y(s) = \frac{1}{s} - \frac{\tau}{\tau s + 1} = \frac{1}{s} - \frac{1}{s + \frac{1}{\tau}};$$

- 2 Taking the inverse Laplace transform  $y(t) = 1 e^{-\frac{t}{\tau}}$ , for  $t \ge 0$ ;
- 3 At t = 0, the output y(t) = 0;
- At  $t = \tau$ , the output y(t) = 0.632, or y(t) has reached 63.2% of its total change  $y(\tau) = 1 e^{-1} = 0.632$ ;
- Slope at time t=0 is  $\frac{1}{\tau}$   $\frac{dy}{dt}|_{t=0}=\frac{1}{\tau}e^{-\frac{t}{\tau}}|_{t=0}=\frac{1}{\tau},$  where  $\tau$  is called the system time constant.

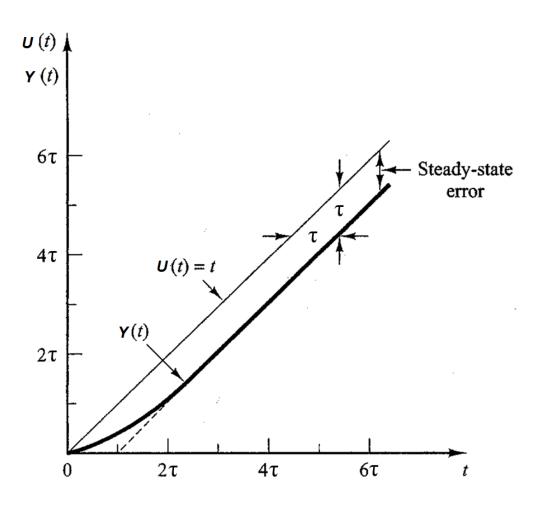
# Unit step transient response



# Unit ramp transient response

- ① Laplace transform of unit ramp is  $\frac{1}{s^2}$   $Y(s) = \frac{1}{\tau s + 1} \frac{1}{s^2}$ ;
- 2 Expanding into partial fractions gives  $Y(s) = \frac{1}{s^2} \frac{\tau}{s} + \frac{\tau^2}{\tau s + 1}$ ;
- Taking the inverse Laplace transform  $y(t) = t \tau + \tau e^{-\frac{t}{\tau}}$ , for  $t \ge 0$ ;
- The error signal e(t) is then  $e(t) = u(t) y(t) = \tau(1 e^{-\frac{t}{\tau}});$
- **5** For t approaching infinity, e(t) approaches  $\tau$   $e(\infty) = \tau$ .

# Unit ramp transient response



# Unit-Impulse Response

For a unit-impulse input, U(s) = 1 and the output is:

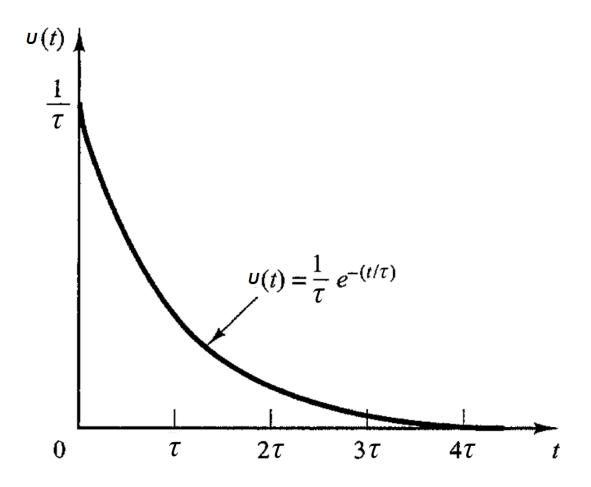
$$Y(s) = \frac{1}{\tau s + 1}.$$

The inverse Laplace transform gives:

$$y(t)=rac{1}{ au}e^{-rac{t}{ au}}, ext{ for } t\geq 0.$$

For 
$$t \to +\infty$$
,  $y(t) \to 0$ .

# Unit-Impulse Response



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# Second order systems

A second order system can generally be written as:

$$\frac{Y(s)}{U(s)} = H(s) = \frac{as^2 + bs + c}{ds^2 + es + f}$$

A system where the closed-loop transfer function possesses two poles is called a second-order system.

If the transfer function has two real poles, the frequency response can be found by combining the effects of both poles

# Second order systems

Sometimes the transfer function has two complex conjugate poles. In that case we have to find a different solution for finding the frequency response.

In order to study the transient behaviour, let us first consider the following simplified example of a second order system:

$$H(s) = \frac{c}{ds^2 + es + c}.$$

# Step response second order system

2 The transfer function can be rewritten as:

$$H(s) = \frac{\frac{c}{d}}{s^2 + \frac{e}{d}s + \frac{c}{d}}$$

$$= \frac{\frac{c}{d}}{\left[s + \frac{e}{2d} + \sqrt{\left(\frac{e}{2d}\right)^2 - \frac{c}{d}}\right] \left[s + \frac{e}{2d} - \sqrt{\left(\frac{e}{2d}\right)^2 - \frac{c}{d}}\right]};$$

- **3** The poles are complex conjugates if  $e^2 4dc < 0$ ;
- 4 The poles are real if  $e^2 4dc \ge 0$ .

To simplify the transient analysis, it is convenient to write:

• 
$$\frac{f}{d} = \omega_n^2$$
,

• 
$$\frac{e}{d} = 2\zeta\omega_n = 2\sigma$$

where  $\sigma$  is the attenuation,  $\omega_n$  is the natural frequency and  $\zeta$  is the damping ratio.

The transfer function can now be rewritten as

$$H(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega s + \omega_n^2}$$
 (= standard form).

The dynamic behavior of the second-order system can then be described in terms of only two parameters  $\zeta$  and  $\omega_n$ .

# Step response second order system

If  $0 < \zeta < 1$ , the poles are complex conjugates and lie in the left-half s-plane

- The system is then called underdamped
- The transient response is oscillatory

If  $\zeta=0$ , the **transient response doesn't die out**. If  $\zeta=1$ , the system is called **critically damped**. If  $\zeta>1$ , the system is called **overdamped**. We will now look at the unit step response for each of these cases.

# For the underdamped case $(0 < \zeta < 1)$ , the transfer function can be written as:

$$H(s) = \frac{\omega_n^2}{(s + \zeta \omega_n + j\omega_d)(s + \zeta \omega_n - j\omega_d)}$$

Where  $\omega_d$  is called the damped natural frequency  $\omega_d = \omega_n \sqrt{1 - \zeta^2}$ .

For a unit-step input we can write

$$Y(s) = \frac{\omega_n^2}{(s^2 + 2\zeta\omega_n s + \omega_n^2)s}.$$

# Underdamped system

Which can be rewritten as partial fractions

$$Y(s) = \frac{1}{s} - \frac{s + 2\zeta\omega_n}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$
$$= \frac{1}{s} - \frac{s + \zeta\omega_n}{s^2 + 2\zeta\omega_n s + \omega_n^2} - \frac{\zeta\omega_n}{s^2 + 2\zeta\omega_n s + \omega_n^2}.$$

It can be shown that

$$\mathcal{L}^{-1} \left[ \frac{s + \zeta \omega_n}{(s + \zeta \omega_n)^2 + \omega_d^2} \right] = e^{-\zeta \omega_n t} \cos(\omega_d t)$$

$$\mathcal{L}^{-1} \left[ \frac{\omega_d}{(s + \zeta \omega_n)^2 + \omega_d^2} \right] = e^{-\zeta \omega_n t} \sin(\omega_d t).$$

# Underdamped system

Therefore:

$$\begin{split} \mathcal{L}^{-1}\{Y(s)\} &= y(t) \\ &= 1 - e^{-\zeta\omega_n t} (\cos(\omega_d t) + \frac{\zeta}{\sqrt{1 - \zeta^2}} \sin(\omega_d t)) \\ &= 1 - \frac{e^{-\zeta\omega_n t}}{\sqrt{1 - \zeta^2}} \sin(\omega_d t + \tan^{-1}(\frac{\sqrt{1 - \zeta^2}}{\zeta})). \end{split}$$

It can be seen that the frequency of the transient oscillation is the damped natural frequency  $\omega_d$  and thus varies with the damping ratio  $\zeta$ .

# Underdamped system

The error signal is the difference between input and output

$$e(t) = y(t) - u(t)$$

$$= e^{-\zeta \omega_n t} (\cos(\omega_d t) + \frac{\zeta}{\sqrt{1 - \zeta^2}} \sin(\omega_d t))$$

The error signal exhibits a damped sinusoidal oscillation. At steady state, or at  $t = \infty$ , the error goes to zero.

# Underdamped system

If damping  $\zeta = 0$ , the response becomes **undamped** 

- Oscillations continue indefinitely;
- Filling in  $\zeta = 0$  into the equation for y(t) gives us:  $y(t) = 1 \cos(\omega_n t)$ , for  $t \ge 0$ ;
- We see that the system now oscillates at the natural frequency  $\omega_n$ ;
- If a linear system has any amount of damping, the undamped natural frequency cannot be observed experimentally, only  $\omega_d$  can be observed;
- $\omega_d$  is always lower than  $\omega_n$ .