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Surface Biology and Geology (SBG)



Level-4 Evapotranspiration L4 (JET) Algorithm Theoretical Basis Document

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List of Acronyms

ALEXI	Atmosphere–Land Exchange Inverse
ATBD	Algorithm Theoretical Basis Document
Cal/Val	Calibration and Validation
CONUS	Contiguous United States
ECOSTRESS	ECOsysteM Spaceborne Thermal Radiometer Experiment on Space Station
ET	Evapotranspiration
ESI	Evaporative Stress Index
EVI-2	Earth Ventures Instruments, Second call
FLIES	Forest Light Environmental Simulator
GEO	Group on Earth Observations
GEWEX	Global Energy and Water Cycle Exchanges Project
GLEAM	Global Land-surface Evaporation: the Amsterdam Methodology
GMAO	Global Modeling and Assimilation Office
HyspIRI	Hyperspectral Infrared Imager
IGBP	International Geosphere-Biosphere Program
iLEAPs	International Land Ecosystem-Atmospheric Processes Study
ISS	International Space Station
JET	Jet Propulsion Laboratory Evapotranspiration
L-2	Level 2
L-4	Level 4
LE	Latent heat flux
LST	Land Surface Temperature
MERRA	Modern Era Retrospective-Analysis for Research and Applications
METRIC	Mapping EvapoTranspiration at high-Resolution with Internalized Calibration
MODIS	MODerate-resolution Imaging Spectroradiometer
MPI-BGC	Max Planck Institute for Biogeochemistry
NSE	Nash-Sutcliffe Efficiency
PhyTIR	Prototype HyspIRI Thermal Infrared Radiometer
PM-MOD16	Penman-Monteith MOD16
PMBL	Penman-Monteith-Bouchet-Lhomme
PT-JPL	Priestley-Taylor Jet Propulsion Laboratory
RMSD	Root Mean Squared Difference
SBG	Surface Biology and Geology
SDS	Science Data System
SEBS	Surface Energy Balance System
STIC	Surface Temperature Initiated Closure
TIR	Thermal Infrared
VIC	Variable Infiltration Capacity
VIIRS	Visible Infrared Imaging Radiometer Suite
WUE	Water Use Efficiency

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1 Introduction

1.1 Purpose

Evapotranspiration (ET) is one of the main science outputs from the Surface Biology and Geology (SBG). ET is a Level-4 (L-4) product constructed from a combination of the SBG Level-2 (L-2) Land Surface Temperature (LST) product and auxiliary data sources. The rate of ET is controlled by many environmental and biological controls including: incoming radiation, the atmospheric water vapor deficit, soil water availability, and vegetation physiology and phenology (Brutsaert, 1982; Monteith, 1965; Penman, 1948). Therefore, to accurately model ET, it remains important to consider these variables. Scientists have been able to form models that ingest satellite observations that capture environmental and biological controls on ET across the globe. Because LST holds the unique ability to capture when and where plants experience stress, as observed by elevated temperatures, LST can inform which areas have a reduced capacity to evaporate or transpire water to the atmosphere (Allen et al., 2007). In this Algorithm Theoretical Basis Document (ATBD), we describe the Jet Propulsion Laboratory ET (JET) approach taken to resolve ET globally is the heritage from the ECOSTRESS mission that we consider as a set of candidate algorithms for SBG.

1.2 Scope and Objectives

In this ATBD, we provide:

1. Description of the ET parameter characteristics and requirements;
2. Description of the general form of the ET algorithms in the JET product workflow;
3. Required algorithm-specific adaptations specific to the SBG mission;
4. Required Auxiliary data products with potential sources and back-up sources;
5. Plan for the calibration and validation (Cal/Val) of the ET retrieval.

2 Parameter Description and Requirements

Attributes of the ET data produced by the SBG mission include:

- Spatial resolution of 60 m x 60 m;
- Diurnally varying temporal resolution to match the overpass characteristics of the International Space Station (ISS);
- Latency as required by the SBG Science Data System (SDS) processing system;

- Auxiliary Variables

Auxiliary variable	Equation	Source
Near-surface air temperature (T_a)	L4G MET	GEOS-5 FP tavg1_2d_slv_Nx product
Near surface dew point temperature (T_d)	Net radiation	GEOS-5 FP tavg1_2d_slv_Nx product
Relative humidity (RH)	L4G MET	GEOS-5 FP tavg1_2d_slv_Nx product
Soil moisture (SM)	L4G SM product	GEOS-5 FP tavg1_2d_Ind_Nx product

Table 1. Showing auxiliary variables and their respective equations, and data sources.

3.1 STARS NDVI and Albedo

For information on the STARS

3.2 Downscaled Meteorology and Soil Moisture

Near-surface air temperature (T_a) and relative humidity (RH) are sourced from the GEOS-5 FP tavg1_2d_slv_Nx product. Soil moisture (SM) is sourced from the GEOS-5 FP tavg1_2d_Ind_Nx product.

The T_a , RH, and SM inputs of the ET models are retrieved at low latency from the GEOS-5 FP dataset at coarse resolution, approximately a third of a degree. To improve the spatial fidelity of evapotranspiration processing, these coarse meteorological estimates are spatially downscaled to the fine spatial structure of the SBG surface temperature and STARS albedo. Future versions of this product will include a more robust method.

The ST, NDVI, and albedo are spatially aggregated to the GEOS-5 FP spatial resolution. A linear regression is calculated from these three variables as independent variables to the GEOS-5 FP variable as the dependent variable for each of the GEOS-5 FP variables. The coefficients from this regression are applied to the fine resolution SBG surface temperature and STARS albedo to produce a fine resolution estimate of air temperature, humidity, or soil moisture. This fine scale estimate is bias corrected by spatially aggregating to the GEOS-5 FP scale, measuring the bias against the GEOS-5 FP estimate, and spatially interpolating this coarse scale bias to the 60 m SBG grid, and subtracting this interpolated bias. Cloud-obstructed areas of are filled in with bi-cubically resampled GEOS-5 FP. The meteorology variables T_a and RH are recorded in the L4T MET and mosaicked into the L4G MET. The SM data is recorded in the L4T SM product and mosaicked into the L4G SM product.

3.3 Net Radiation

The generation of net radiation (R_n) involves the integrated retrieval of individual radiation balance components: downwelling shortwave radiation (R_{SD}), upwelling shortwave radiation (R_{SU}), downwelling longwave radiation (R_{LD}), and upwelling longwave radiation (R_{LU}) [Verma *et al.*, 2016]:

$$R_N = (R_{SD} - R_{SU}) + (R_{LD} - R_{LU}) \quad (7)$$

where α is the surface albedo.

NETRAD	Equations	Data Variable & Sources
R_{SD}	FLiES	Cloud Optical Thickness and Aerosol Optical Thickness (GEOS-5 FP)
R_{SU}	$R_{SU} = \alpha R_{SD}$	Land Surface Albedo (STARS)
R_{LD}	$R_{LD} = \sigma \varepsilon_A T_a^4$	Near Surface Air Temperature and Vapor Pressure (GEOS-5 FP)
R_{LU}	$R_{LU} = \sigma \varepsilon_S T_S^4$	Land Surface Temperature and Emissivity (ECO2LSTE)

Table 2. Showing radiation balance components and their respective equations, variables, and data sources

R_{SD} is calculated from an atmospheric radiative transfer model, the Forest Light Environmental Simulator (FLiES) [Iwabuchi, 2006; Kobayashi and Iwabuchi, 2008; Ryu *et al.*, 2011; Ryu *et al.*, 2012]. To speed processing, a neural network machine learning algorithm was trained on to generate R_{SD} from solar zenith angle, aerosol optical thickness, cloud optical thickness, land surface albedo, atmospheric profile height, aerosol type, and cloud height. R_{SU} is calculated from R_{SD} and land surface albedo as:

$$R_{SU} = \alpha R_{SD} \quad (8)$$

R_{LD} is calculated from Stefan-Boltzmann's Law:

$$R_{LD} = \sigma \varepsilon_A T_a^4 \quad (9)$$

$$\varepsilon_A = 1 - \left(1 + .467 \frac{E_a}{T_a}\right) \exp\left(-\sqrt{1.2 + 3 \frac{4.65 \cdot E_a}{T_a}}\right) \quad (10)$$

$$E_a = 2.171 * 10^{\left(10 * e^{-\frac{4157}{T_d} - 33.91}\right)} \quad (11)$$

where σ is the Stefan-Boltzmann constant ($5.67 \times 10^{-8} \text{ W m}^{-2} \text{ K}^{-4}$), ϵ_A is the atmospheric emissivity calculated from total atmospheric precipitable water (ζ) [Prata, 1996], T_a is near surface air temperature, Ea is the vapor pressure, and T_d is the near surface dew point temperature. T_a and T_d ($^{\circ}\text{C}$) are available from GEOS-5 [Verma et. al, 2016]:

R_{LU} is calculated from Stefan-Boltzmann's Law [Verma et. al, 2016]:

$$R_{LU} = \sigma \epsilon_S T_S^4 \quad (12)$$

where ϵ_S is the broadband surface emissivity and T_S is surface temperature available from the SGB LST_LSTE product.

We emphasize these data products provide data at unprecedented scales. Therefore, we solicit feedback on the quality and utility of these variables in their ability to advance science and scientific applications. A preliminary evaluation of the auxiliary data accuracy is presented in Section 5.

4 Evapotranspiration Retrieval: Jet Propulsion Laboratory EvapoTranspiration (JET)

The JPL EvapoTranspiration (JET) data provides a robust estimation of ET from multiple ET models. The JET product workflow incorporates ET data from four algorithms: Priestley Taylor-Jet Propulsion Laboratory model with soil moisture (PT-JPL_{SM}), the Penman Monteith MODIS Global Evapotranspiration Model (MOD16), Soil Temperature Initiated Closure (STIC) model, and the Breathing Earth System Simulator (BESS) model. We present descriptions of these models here, inherited from the ECOSTRESS mission, as candidates for SGB L4 evapotranspiration processing.

4.1 PT-JPL_{SM}: General Form

The PT-JPL_{SM} model relies on the Priestley-Taylor [1972] equation to resolve potential ET (PET). This formulation is removed from the need to parameterize stomatal and aerodynamic resistances and instead multiples the α coefficient (1.26) to the rate of equilibrium ET:

$$PT = \alpha \frac{\Delta}{\Delta + \gamma} R_N - G \quad (13)$$

where Δ is the slope of the saturation-to-vapor pressure curve (dependent on near surface air temperature, T_a , and atmospheric vapor pressure, e_a), γ is the psychrometric constant, and R_N is net radiation (W m^{-2}) and G is the ground heat flux (W m^{-2}). PET is given in units of R_N , or W m^{-2} , and is therefore considered as an energy variable, i.e., LE. To convert LE to ET, one can divide LE by the latent heat of vaporization (MJ kg^{-1}).

To reduce PET to actual ET (AET), *Fisher et al.* [2008] applied ecophysiological constraint functions (f -functions, unitless multipliers, 0-1) based on atmospheric moisture (vapor pressure deficit, VPD; and, RH) and vegetation indices (normalized difference and soil adjusted vegetation indices, NDVI and SAVI, respectively). While this model has been demonstrated to perform well at large scales in space and time, certain model assumptions of land-atmosphere equilibrium fall apart at finer spatial and temporal frequencies. As a result, the PT-JPL formulation from *Fisher et al.* [2008] has been shown to overestimate ET in arid regions. To overcome these limitations *Purdy et al.* [2018] modified the algorithm to incorporate explicit constraint from soil water availability. The driving equations in the PT-JPL_{SM} algorithm are:

$$AET = ET_s + ET_c + ET_i \quad (14)$$

$$ET_s = (f_{wet} + f_{rew}(1 - f_{wet}))\alpha \frac{\Delta}{\Delta + \gamma} (R_{ns} - G) \quad (15)$$

$$ET_c = (1 - f_{wet})f_{trm}f_gf_t\alpha \frac{\Delta}{\Delta + \gamma} R_{nc} \quad (16)$$

$$ET_i = f_{wet}\alpha \frac{\Delta}{\Delta + \gamma} R_{nc} \quad (17)$$

where ET_s , ET_c , and ET_i are evaporation from the soil, canopy and intercepted water, respectively, each calculated explicitly and summing to total AET. f_{wet} is relative surface wetness (RH^4) [Stone et al., 1977] representing the fraction of soil and canopy that delivers water to the atmosphere potential rate. f_{rew} is the relative extractable water defined as the difference between observed soil moisture (θ_{obs}) and soil moisture at the plant wilting point (θ_{wp}) divided by the difference of soil moisture at field capacity (θ_{fc}) and soil moisture at the plant wilting point ($\frac{\theta_{obs}-\theta_{wp}}{\theta_{fc}-\theta_{wp}}$). Canopy constraints include the fraction of green canopy ($f_g = f_{APAR}/f_{IPAR}$) [Zhang et al., 2005], plant temperature constraints ($f_t = \exp(-((T_{max}-T_{opt})/T_{opt})^2)$) [Potter et al., 1993; June et al., 2004], and plant and soil moisture controls (f_{trm}) [Purdy et al., 2018]. f_{APAR} is absorbed photosynthetically active radiation (PAR), f_{IPAR} is intercepted PAR, T_{max} is maximum air temperature, T_{opt} is T_{max} at $\max(R_n T_{max} \frac{SAVI}{VPD})$, G is the soil heat flux, and R_{nc} , R_{ns} are the net radiation ('c' for canopy and 's' for soil). f_{trm} combines both f_m the plant moisture control and soil moisture control on transpiration (f_{trew}) by weighting each constraint by the relative humidity as:

$$f_{trm} = (RH^{4(1-VWC)(1-RH)})f_m + (1 - RH^{4(1-VWC)(1-RH)})f_{trew} \quad (18)$$

During periods of high humidity, plant moisture is a stronger control than soil water control. During periods of low humidity, soil water control is greater (Figure 1).

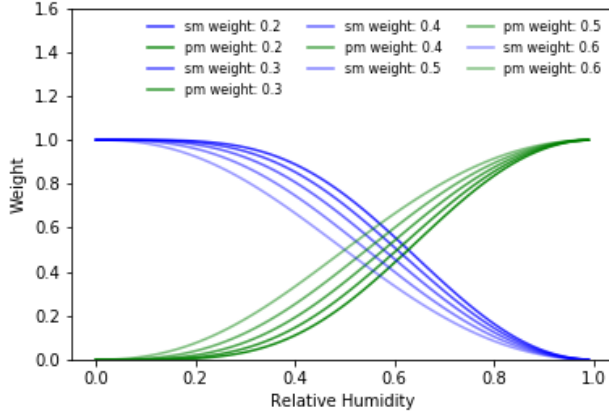


Figure 1. Plant moisture (green) and soil water control (blue) weight by relative humidity (x-axis) and VWC (legend values: 0.2-0.6). During periods of high relative humidity periods higher weights on plant moisture indicate more control from this scalar. During low humidity more weight is placed on soil water control.

The individual plant moisture and soil water constraints on transpiration are derived as:

(19)

$$f_m = \frac{f_{APAR}}{f_{APARmax}}$$

(20)

$$f_{trew} = 1 - \left(\frac{\theta_{cr} - \theta_{obs}}{\theta_{cr} - \theta_{wpch}} \right)^{CH_{scalar}}$$

where CH_{scalar} is a canopy height scalar that impacts the sensitivity of vegetation to soil water availability equal to \sqrt{CH} and capped between 1 and 5, θ_{cr} is the critical soil moisture at which soil water availability begins to constrain ET and computed as:

$$\theta_{cr} = \left(1 - \left(\frac{1}{1 + PET} - 0.1 \frac{1}{1 + CH} \right) \right) \left(\theta_{fc} - \frac{\theta_{WP}}{CH_{scalar}} \right) + \frac{\theta_{WP}}{CH_{scalar}} \quad (21)$$

The adjustment of θ_{fc} to θ_{cr} is removed from the dependence on land classification datasets and facilitates continuously mapping when soil water availability begins to limit transpiration within f_{trew} (Figure 2).

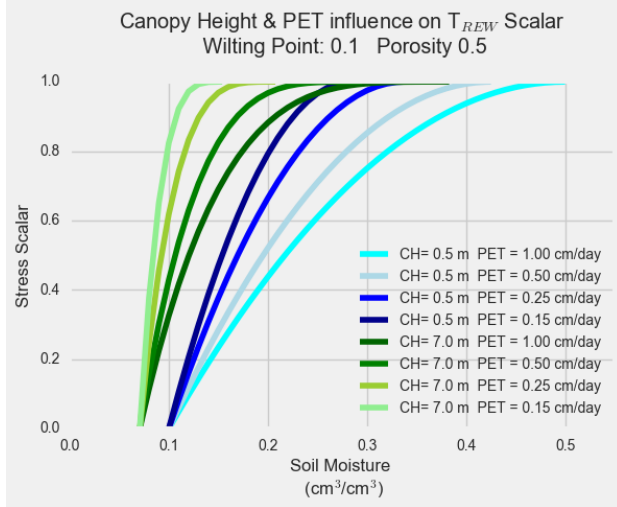


Figure 2. Supplemental figure from Purdy et al., 2018. f_{trew} on canopy height and PET (see legend). During high PET conditions soil water control begins sooner than during low PET conditions. Canopy height impacts when soil water control begins with taller canopies (greens) being less sensitive to surface soil water control than shorter canopies (blues).

4.1.1. Spatial Resolution Improvements

To maintain continuity with other SBG data products, ET from PT-JPL_{SM} is produced at 60 m. This required generating auxiliary variables such as NDVI, albedo (α), air temperature (T_a), relative humidity (RH), soil moisture (SM), canopy height, and soil properties at the same spatial resolution. Section 3 details how NDVI, albedo, air temperature, relative humidity, soil moisture, and net radiation were resampled or downscaled to fill this need. Soil properties and canopy height data were sourced from X and Y. We advise caution to users interested in highly heterogeneous land surfaces and meteorological conditions at length scales less than 1 km.

4.2 STIC: General Form

The Surface Temperature Initiated Closure (STIC) (latest version 1.3) is a one-dimensional SEB model treating soil-vegetation as a single unit [Mallick et al., 2015; 2018; 2022]. STIC directly integrates LST into the Penman-Monteith Shuttleworth-Wallace system of ET equations [Penman, 1965; Shuttleworth and Wallace, 1985] to solve the aerodynamic temperature, which is the most critical temperature for ET modeling. STIC assumes a first-order dependence of aerodynamic conductance (g_a) and canopy conductance (g_{cs}) on LST (through soil moisture availability and aerodynamic temperature (T_0)). Surface moisture availability (also called surface wetness) is first estimated as a function of LST, and then constrains g_a and g_{cs} conductances through the surface wetness in an analytical framework. In addition to LST, the inputs to STIC1.3 include radiation (net radiation), emissivity, albedo, fractional vegetation cover (FVC) (derived from NDVI), and meteorological inputs (air temperature, relative humidity, and incoming solar radiation).

The general approach to STIC is (and see flow diagram in Figure 1):

- (1) STIC solves the state equations to find analytical solution of T_0 , and the conductances (g_a and g_{cs}).
- (2) There are more unknowns in the state equations (e.g., aerodynamic vapor pressure components), these unknowns are initialized as a function of LST.
- (3) The additional unknowns are estimated iteratively by combining Penman-Monteith and Shuttleworth-Wallace equations

The state equations solved in Step 1 are as follows:

$$F_E = \frac{2\alpha s}{2s + 2\gamma + \gamma(1 + I_{SM}) \frac{g_a}{g_{cs}}} \quad (22)$$

$$T_0 = T_a + \frac{(e_0 - e_a)}{\gamma} \frac{(1 - F_E)}{F_E} \quad (23)$$

$$g_a = \frac{R_N - G}{\rho c_p [(T_0 - T_a) + \frac{(e_0 - e_a)}{\gamma}]} \quad (24)$$

$$g_{cs} = g_a \frac{(e_0 - e_a)}{(e_0^* - e_0)} \quad (25)$$

Where F_E is the evaporative fraction (defined as the fractional contribution of ET from total available energy), α is the Priestley-Taylor coefficient [*Priestley & Taylor, 1972*], s is the slope of the saturation vapor pressure at air temperature (T_a) (hPa/°C), γ is the psychrometric constant (hPa/°C), e_0^* and e_0 are the saturation vapor pressure and ambient vapor pressure at the canopy-air stream, also called source-sink height (hPa), R_N and G are net radiation and ground heat flux (W/m²), e_a is the atmospheric vapor pressure (hPa) at the level of T_a measurement, ρ is the air density (kg/m³), and c_p is the specific heat of air at constant pressure (J/kg/K).

I_{SM} describes the relative wetness or the intensity of water stress on a surface. This variable controls the transition from potential to actual evaporation, with I_{SM} tending to 1 on a unstressed wet surface, and 0 on a stressed dry surface. Since LST is extremely sensitive to surface water stress variations, it is used directly to estimate I_{SM} . For further details, refer to Mallick et al. [2018, 2022].

In Step 1, initial estimates of an initial estimate of e_0^* , e_0 , I_{SM} , and surface dew point temperature (T_{sd}), are obtained. The initial I_{SM} and R_N are used for an initial estimate of G . In

Step 2, initial estimates of the conductances, T_0 , F_E and sensible heat (H) and latent heat flux (LE) are obtained. In Step 3, the process is iterated by updating e_0^* , e_0 , I_{SM} , and α , and used to recalculate G, g_a , g_{cs} , T_0 , F_E , H, and LE until convergence of LE is obtained (10 – 15 iterations).

The major differences of version 1.3 [Mallick et al., 2022] from the previous version concern the calculation of G, which is calculated according to Santanello and Friedl [2003] with the following function:

$$\frac{G}{R_N} = c_g \left[\frac{2\pi(t_{g0} + 10800)}{t_g} \right] \quad (26)$$

Where c_g is the maximum proportion of G/R_N ; t_{g0} is time in seconds relative to solar noon, t_g is the factor that minimizes the deviation between G/R_N and governs the phase difference between G and R_N . c_g and t_g are linked to surface wetness I_{SM} with:

$$c_g = (1 - I_{SM})c_{gmax} + I_{SM}c_{gmin} \quad (27)$$

$$t_g = (1 - I_{SM})t_{gmax} + I_{SM}t_{gmin} \quad (28)$$

Using the values of c_{gmax} (0.35), c_{gmin} (0.05), t_{gmax} (100000 s), and t_{gmin} (74000 s). With the initial estimate of I_{SM} , initial G is estimated, and then updated in the iterative process. Further details are available in the supporting information of [Mallick et al. 2022].

For its implementation in SBG, we modified the STIC version 1.3 equation in the following ways:

- We use a different method to calculate dew point temperature (T_d) with relative humidity (RH) and air temperature (T_a):

$$T_d = T_a - ((100 - RH * 100) / 5)$$

- The inputs R_N , albedo, emissivity, NDVI, relative humidity, air temperature and incoming solar radiation are the same as used for other models in the JET product workflow. This is done in order to have more consistency in the input data.

4.3 MOD16: General Form

The MOD16 algorithm is rooted in the Penman Monteith equation with environmental constraints from vegetation cover, temperature, and atmospheric moisture deficits (Mu et al., 2011). Similar to the PT-JPLSM model, the MOD16 algorithm resolves evaporative fluxes from the soil, canopy, and intercepted water separately.

$$AET = ET_s + ET_c + ET_i \quad (29)$$

$$ET_s = \left(f_{wet} + (1 - f_{wet}) RH^{\frac{e_{sat} - e}{\beta}} \right) \frac{sA_c + \frac{\rho Cp(e_{sat} - e)}{r_{a_s}}}{\Delta + \gamma \left(1 + \frac{r_{s_s}}{r_{a_s}} \right)} \quad (30)$$

$$ET_s = (1 - f_{wet}) f_c \frac{sA_c + \frac{\rho Cp(e_{sat} - e)}{r_{a_s}}}{\Delta + \gamma \left(1 + \frac{r_{s_s}}{r_{a_s}} \right)} \quad (31)$$

$$ET_s = f_{wet} f_c \frac{sA_c + \frac{\rho Cp(e_{sat} - e)}{r_{a_s}}}{\Delta + \gamma \left(1 + \frac{r_{s_s}}{r_{a_s}} \right)} \quad (32)$$

Where f_{wet} is fraction of wet surface, RH is the relative humidity, s is the slope of saturated water vapor pressure to temperature ($d(e_{sat})/dT$); A is the available energy with subscripts to distinguish differences between the soil and canopy; ρ is the air density; Cp is the specific heat capacity of air; γ is the psychrometric constant; e is the actual water vapor pressure; r_a is the aerodynamic resistance; and r_s is the surface resistance. Vegetation-dependent environmental constraints on stomatal conductance are incorporated through the surface resistance in the formulation above.

4.4 BESS: General Form

BESS is a coupled biophysical modeling system that couples atmospheric and canopy radiative transfer processes with photosynthesis, stomatal conductance, and transpiration using (Ryu et al., 2011). BESS applies an equilibrium evaporation representation to resolve soil evaporation and solves a quadratic representation of the Penman Monteith model to estimate transpiration [Jiang et. al, 2016]:

$$AET = ET_s + ET_c \quad (33)$$

$$ET_s = \frac{s}{(s + \gamma)} (R_{ns} - G) RH^{VPD} \quad (34)$$

$$aET_c^2 + bET_c + c = 0 \quad (35)$$

$$a = \frac{r_a^2}{2[\rho_a C_p \gamma (r_a + r_c)]} \frac{d^2 e_{sat}(T_a)}{dT_a^2} \quad (36)$$

$$b = -1 - r_a \frac{de_{sat}(T_a)}{dT_a} \frac{1}{\gamma(r_a + r_c)} - \frac{R_{nj} r_a^2}{\rho_a C_p \gamma (r_a + r_c)} \frac{d^2 e_{sat}(T_a)}{dT_a^2} \quad (37)$$

$$c = \frac{\rho_a C_p D}{\gamma(r_a + r_c)} + \frac{r_a R_{nj}}{\gamma(r_a + r_c)} \frac{de_{sat}(T_a)}{dT_a} + \frac{1}{2} \frac{(r_a R_{nj})^2}{\rho_a C_p \gamma (r_a + r_c)} \frac{d^2 e_{sat}(T_a)}{dT_a^2} \quad (38)$$

where r_a is the aerodynamic; r_c is the canopy resistance; R_{nj} is the net radiation; ρ_a is the air density; γ is the psychrometric constant; $e_{sat}(T_a)$ is the saturated water vapor pressure at temperature T_a .

4.5 Daily Evapotranspiration Value

Differences in model structure provide a range in ET estimates to consider for each 70m pixel. Previous studies have shown the combination of an ensemble of modeled values provides improved or equal accuracy to any one given model [Kirtman et al., 2014]. Due to the limited number of models used within the ET algorithm, we adopt a simplified approach by taking the median value of the instantaneous JET products (PT-JPL_{SM}, MOD16, STIC, TSEB, & BESS). The evapotranspiration median value is used to provide a daily estimate of ET for each 60 m pixel. Additionally, the uncertainty is estimated as the standard deviation of the evapotranspiration for each pixel.

5 Calibration/Validation

5.1 ET evaluation

To evaluate remote sensing ET datasets requires ground observations at similar length scales and temporal frequencies. Eddy covariance (EC) towers provide year-round observations at frequencies (~30 minutes) and spatial scales (10's-100's m) that capture exchanges of water vapor from the land surface to the atmosphere necessary to evaluate the JET product workflow. Here, we employ EC observations from the Ameriflux network due to their data collection standards, availability, and distribution across various land uses in North and South America. We only include EC towers in our analysis that are within SBG observations (<58°N & > 58°S), have data during SBG mission (2018-Present), and have a long-term closure ration of greater than 0.70. This filtering resulted in 74 towers across 11 land uses for the JET product comparison (Figure 3).

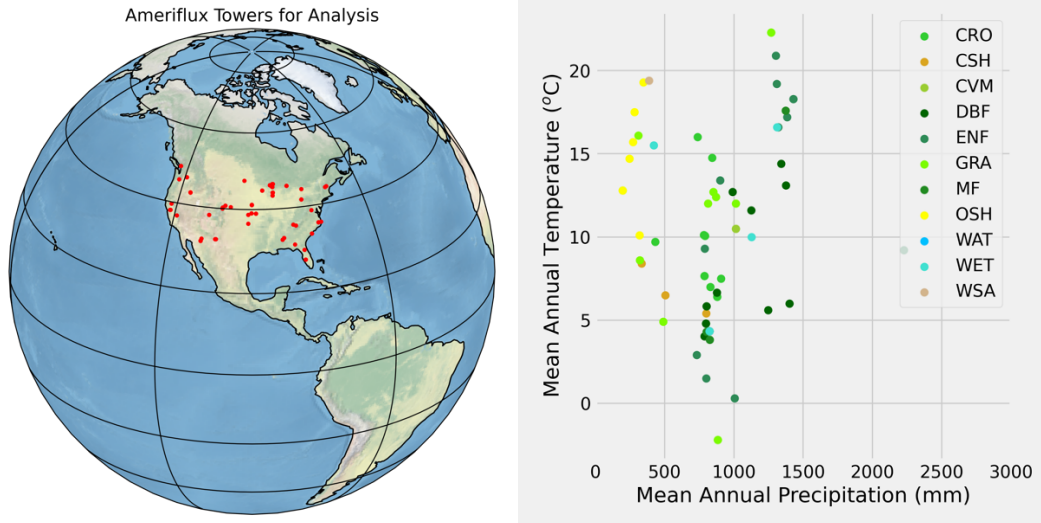


Figure 3. Left: Distribution of filtered Ameriflux towers across North America within SBG view. Right: Range in EC towers' mean annual precipitation (x-axis), temperature (y-axis) by vegetation class (color).

EC data from Ameriflux are post-processed for quality and to ensure surface energy budget closure. Surface energy balance variables including sensible heat, latent heat, ground heat flux, and net radiation were filtered for outliers according to a median of absolute deviation about the median approach [Papale et al., 2006]. Next, the surface energy budget was closed while preserving the Bowen Ratio, the ratio of sensible heat to latent heat, following the EBC_CF Method 1 and EBC_CF Method 2 procedures of the OneFLUX processing [Pastorello et al., 2020]. This closure approach yields energy closures according to the 25th, 50th, and 75th percentiles for dates spanning plus or minus 15 and 5 days respectively. Only cloud-free SBG observations are utilized in this analysis. Due to uncertainties and on-going debate about the surface energy imbalances from EC observations, we compute the statistics computed based on the best comparison across the raw observation and the closed budget options. We compute statistics of unbiased root mean square error, mean absolute bias, and the correlation coefficient.

Error Budget

The SBG ET products will target an error value of 1 mm per day with an estimated 0.1 mm of this attributed to instrument error. This target is consistent with established literature and validation work on the related PT-JPL ET, DisALEXI-JPL ET, MOD16 and MYD16 ET products in recent years. Fisher et al. (2019) found that the RMSE of PT-JPL instantaneous ET was 6%, with $R^2 = 0.88$, (overall RMSE was 41.3 W/m² compared to a mean of 182.0 W/m² and a range of 713.8 W/m²). An examination of the error propagation of PT-JPL ET from Halverson et al. finds that ET products exhibited strong responses to changes in vegetation and temperature; consistent with previous findings on DisALEXI-JPL ET which established that LST error within 1K enables ET estimates to be accurate to within 1mm/day (Cawse-Nicholson et al., 2020). In 2021, Cawse-Nicholson et. al, evaluated DisALEXI-JPL daily ET and found an RMSE of 0.81 mm/day. Mu et al. found that MOD16 and MYD16 exhibited an RMSE of 0.84 mm/day.

5.2 WUE Evaluation

BESS uses a carbon-water-coupled model to separately evaluate C3 and C4 species provided by a global map [Still, 2013 10.1029/2001GB001807] for a given pixel, the sum of that relative proportion of C3 and C4 in that pixel determines the GPP [Jiang et al., 2016]. The GPP product in kilograms of carbon per square meter estimated by BESS is ingested operationally into the data production stream to estimate water use efficiency (WUE). Process-based approaches like BESS have an advantage to represent the interaction between the soil system, plants, and atmosphere as an organic integration rather than ingesting GPP semi-empirically [Jiang et al., 2016]. The carbon uptake is divided by the daily ET in kilograms per square meter to determine the ratio of grams of carbon fixed to kilograms of water lost in units of ET. This ratio describes the WUE, higher values indicate more plant productivity, lower values indicate less productive plants.

$$WUE = \frac{GPP}{ET} \quad (39)$$

5.3 ESI Evaluation

The Evaporative Stress Index (ESI) is used as a climate indicator of agricultural drought and plant stress by comparison of ET to PET to determine anomalous reduction in ET relative to potential ET. PET is already calculated internally in the PT-JPL algorithm and can be used directly to compute the ESI without auxiliary information.

$$ESI = \frac{ET}{PET} \quad (29)$$

5.4 Auxiliary variable evaluation

EC towers commonly measure Ta, RH, and SM in addition to capturing exchanges of radiative energy, carbon, and water from the Earth's surface and atmosphere. We utilize the same Ameriflux data source. Instead of screening for surface energy balance closure, we only consider the quality of each variable when considering data for use in this evaluation. For soil moisture, we only utilize EC towers data from the National Ecological Observation Network (NEON) due to the number of soil moisture observations. Recently, the NEON towers provided a great comparison to evaluate the utility of remotely sensed soil moisture in forested and non-forested regions [Ayres et al., 2022]. For each variable we compute statistics of unbiased root mean square error, mean absolute bias, and the correlation coefficient.

6 Mask/Flag Derivation

For T_s and e_s , the ECOSTRESS L2 flags are used to provide quality information for the L4 ET product.

7 Metadata

- unit of measurement: Watts per square meter (W m^{-2})
- range of measurement: 0 to 3000 W m^{-2}
- projection: SBG swath
- spatial resolution: 60 m x 60 m
- temporal resolution: dynamically varying with precessing ISS overpass; instantaneous throughout the day, local time
- spatial extent: all land globally, excluding poleward $\pm 60^\circ$
- start date time: near real-time
- end data time: near real-time
- number of bands: not applicable
- data type: float
- min value: 0
- max value: 3000
- no data value: 9999
- bad data values: 9999
- flags: quality level 1-4 (best to worst)

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