

# ABE 201

# Biological Thermodynamics 1

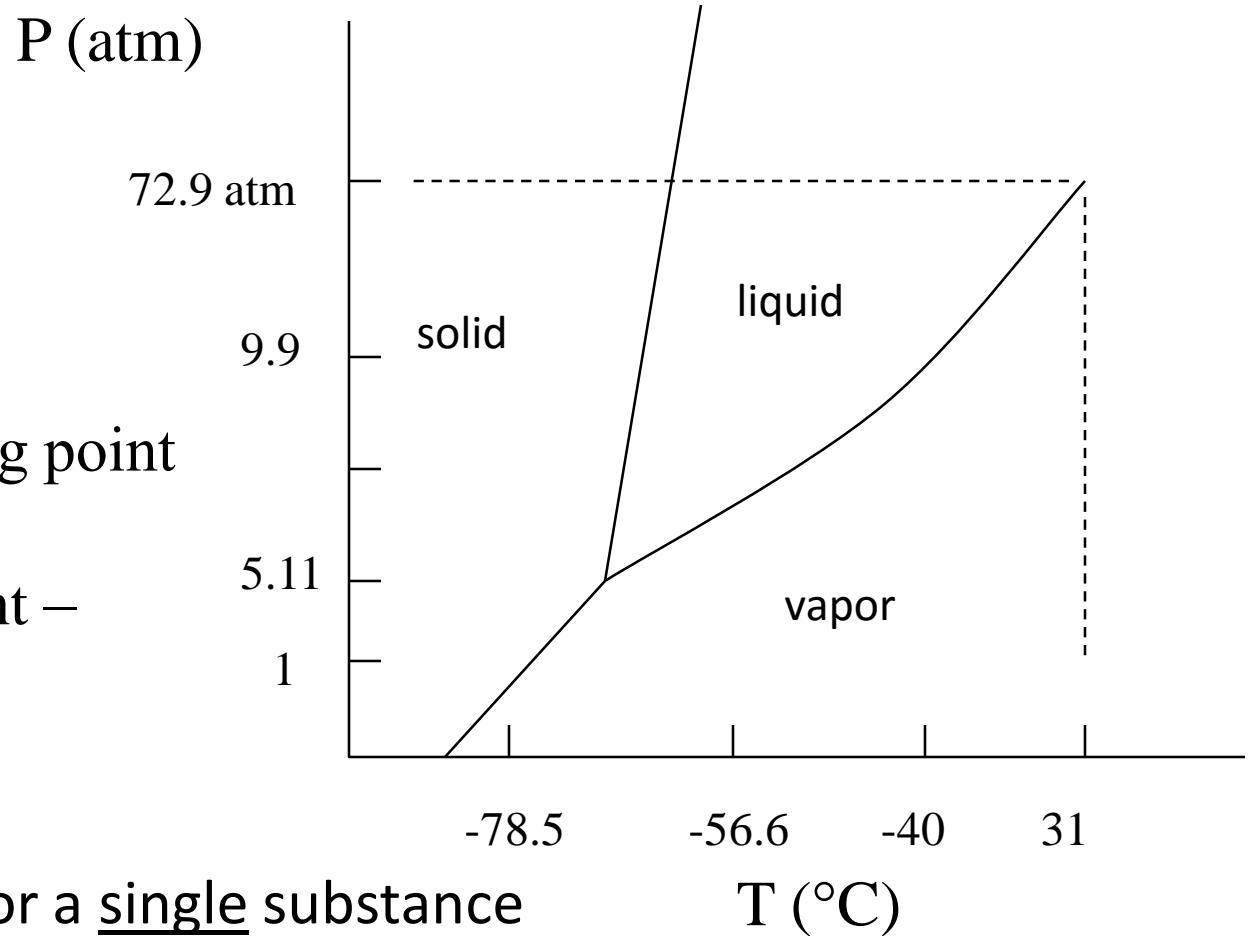
Module 7:  
Ideal and Non-Ideal Gas “Laws”

# Review

- Equations of state are mathematical expressions describing the relationship between state properties.
- Ideal gas law is simplest equation of state.
- Ideal gas law is a good approximation for dilute (low pressure) gases far from the critical point.
- Non-ideal gas equations use various approaches to account for deviation from ideality.

# Phases of Mater

1. Critical point –
2. Boiling point –  
“Normal” Boiling point
3. Melting point –
4. Sublimation point –
5. Triple point –



This is a diagram for a single substance  
at equilibrium.

# Ideal Gas Law

Given: A fire extinguisher holds 10.0 lb of CO<sub>2</sub> in a 20.0 ft<sup>3</sup> tank at 30.0°C. Using the ideal gas law holds, estimate the gauge pressure on the tank.

$$P V = n R T$$

$$10 \text{ lbm CO}_2 (1 \text{ lbmol} / 44.01 \text{ lb}) = 0.23 \text{ lbmol}$$

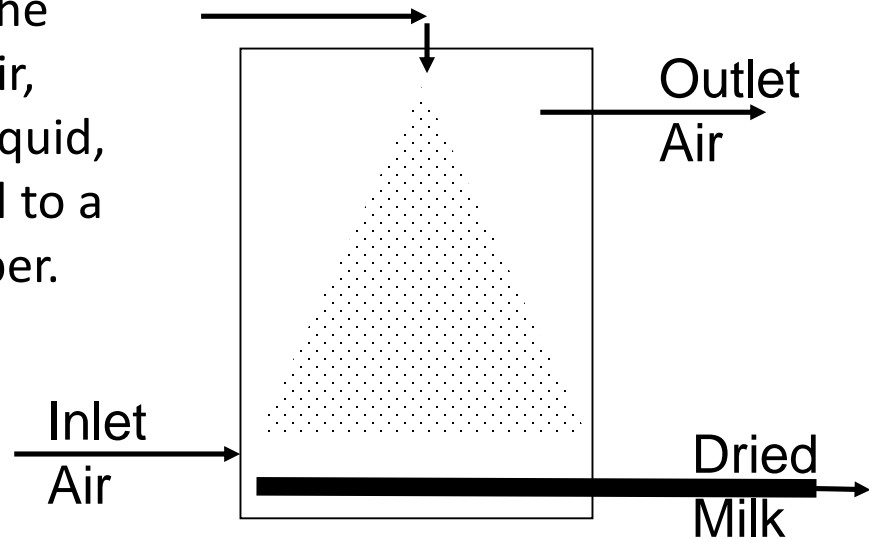
$$30\text{C} = 86\text{F} = (86 + 459.69) \text{ R} = 546 \text{ R}$$

$$P = (nRT)/V = (0.23 \text{ lbmol})(10.73 \text{ ft}^3\text{-psia}/(\text{lbmol R}))(546 \text{ R})/20\text{ft}^3$$

$$P = 67.4 \text{ psia} = (67.4 - 14.696)\text{psig} = 52.7 \text{ psig}$$

# Spray Dried Milk

Spray drying is a process in which a liquid containing suspended or dissolved solids is injected into a chamber through a spray nozzle or centrifugal disk atomizer. The resulting mist is contacted with hot air, which evaporates most or all of the liquid, leaving the dried solids powder to fall to a conveyor at the bottom of the chamber.



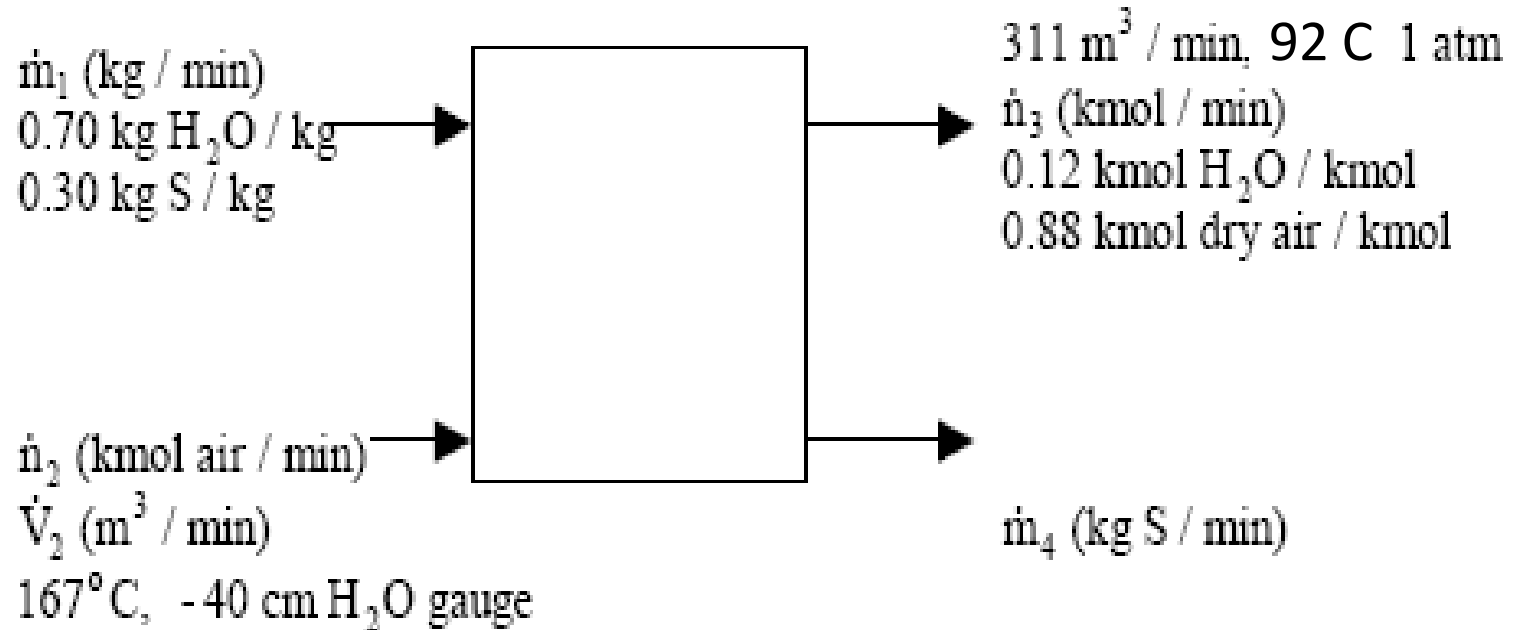
# Spray Dried Milk

Powdered milk is produced in a cylindrical spray dryer 6 m in diameter by 6 m high. Air enters at 167°C and -40 cm H<sub>2</sub>O (gauge). The milk feed contains 70% water by mass, all of which evaporates. The outlet air contains 12 mol% water and leaves the chamber at 92°C and 1 atm (absolute) at a rate of 311 m<sup>3</sup>/min.

- a) Calculate the production rate of dried milk and the volumetric flow rate of inlet air.
- b) Estimate the average upward velocity of the air (m/s) at the bottom of the dryer.
- c) What problem(s) would you predict if the velocity is too high?

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sis: Given flow rates of outlet gas. Assume ideal gas behavior



$$\text{a. } \dot{n}_3 = \frac{1 \text{ atm}}{365.2 \text{ K}} \left| \frac{311 \text{ m}^3}{\text{min}} \right| \frac{\text{kmol} \cdot \text{K}}{0.08206 \text{ m}^3 \cdot \text{atm}} = 10.38 \text{ kmol/min}$$

$$\text{H}_2\text{O balance: } 0.70 \dot{m}_1 = \frac{10.38 \text{ kmol}}{\text{min}} \left| \frac{0.12 \text{ kmol H}_2\text{O}}{\text{kmol}} \right| \frac{18.02 \text{ kg}}{\text{kmol}}$$

$$\Rightarrow \dot{m}_1 = 32.2 \text{ kg/min milk}$$

$$\text{S(olids) balance: } 0.30(32.2 \text{ kg/min}) = \dot{m}_4 \Rightarrow \underline{\underline{\dot{m}_4 = 9.6 \text{ kg S/min}}}$$

$$\text{Dry air balance: } \dot{n}_2 = 0.88(10.38 \text{ kmol/min}) \Rightarrow \dot{n}_2 = 9.13 \text{ kmol/min air}$$

$$\begin{aligned} \dot{V}_2 &= \frac{9.13 \text{ kmol}}{\text{min}} \left| \frac{0.08206 \text{ m}^3 \cdot \text{atm}}{\text{kmol} \cdot \text{K}} \right| \frac{440 \text{ K}}{(1033 - 40) \text{ cm H}_2\text{O}} \left| \frac{1033 \text{ cm H}_2\text{O}}{1 \text{ atm}} \right| \\ &= \underline{\underline{343 \text{ m}^3 \text{ air/min}}} \end{aligned}$$

$$\text{b. } u_{\text{air}} (\text{m/min}) = \frac{\dot{V}_{\text{air}} (\text{m}^3/\text{s})}{A (\text{m}^2)} = \frac{343 \text{ m}^3}{\text{min}} \left| \frac{1 \text{ min}}{60 \text{ s}} \right| \frac{1}{\frac{\pi}{4} \cdot (6 \text{ m})^2} = \underline{\underline{0.20 \text{ m/s}}}$$

- c. If the velocity of the air is too high, the powdered milk would be blown out of the reactor by the air instead of falling to the conveyor belt.



# Using Standard Volumes

- Oxygen flows into a reactor at 30 SCM per minute. Sensors at the inlet read 35°C and 1500 kPa(a). What is the actual volumetric flow rate?

$$PV=nRT$$

$$\begin{aligned}n &= PV/(RT) \\&= (1.013 \times 10^5 \text{ Pa})(30 \text{ m}^3)/(8.314 \text{ m}^3\text{-Pa}/(\text{mol-K}))(273 \text{ K}) \\&= 1340 \text{ mol O}_2/\text{min}\end{aligned}$$

$$V = nRT/P = (1340)(8.314)(35+273)/1500\text{e}3 = 2.3 \text{ m}^3/\text{min}$$

# Using the Virial Equation

Estimate the pressure in bars for carbon dioxide at 380 K and 0.311 L/mol using the virial equation. Compare this to the estimate from the ideal gas equation.

$$\frac{P\hat{V}}{RT} = 1 + \frac{B}{\hat{V}}$$

Needed Information:

$$B = \frac{RT_c}{P_c} (B_0 + \omega B_1)$$

$$T_c = 304.2 \text{ K}$$

$$B_0 = 0.083 - \frac{0.422}{T_r^{1.6}}$$

$$T_r = T/T_c$$

$$P_c = 72.9 \text{ atm}$$

$$P_r = P/P_c$$

$$\text{Accentric factor} = 0.225$$

$$B_1 = 0.139 - \frac{0.172}{T_r^{4.2}}$$

$$T_r > 0.686 + 0.439P_r$$

$$T_c = 304.2 \text{ K}, P_c = 72.9 \text{ atm}$$

$$T_r = 380/304.2 = 1.25, P_r = P/72.9$$

$$w = 0.225$$

$$PV/RT = 1 + B/V$$

$$B = RT_c(B_0 + wB_1)/P_c$$

$$B_0 = 0.083 - 0.422/T_r^{1.6} = 0.083 - 0.422/(1.25)^{1.6} = -0.212$$

$$B_1 = 0.139 - 0.172/T_r^{4.2} = 0.139 - 0.172/(1.25)^{4.2} = 0.072$$

$$B = 0.08206(304.2)(-0.212 + (0.225)*0.072)/(72.9) = -0.0670$$

$$P(0.311)/(0.08206)(380) = 1 - 0.0670/(0.311)$$

$$P = 78.7 \text{ atm}$$

$$PV^{\wedge} = RT$$

$$P = RT/V^{\wedge} = (0.08206)(380)/0.311 = 100 \text{ atm}$$

$$\text{Error} = (P_{\text{ideal}} - P) / P = (100 - 78.7) / 78.7 = 27\%$$

error

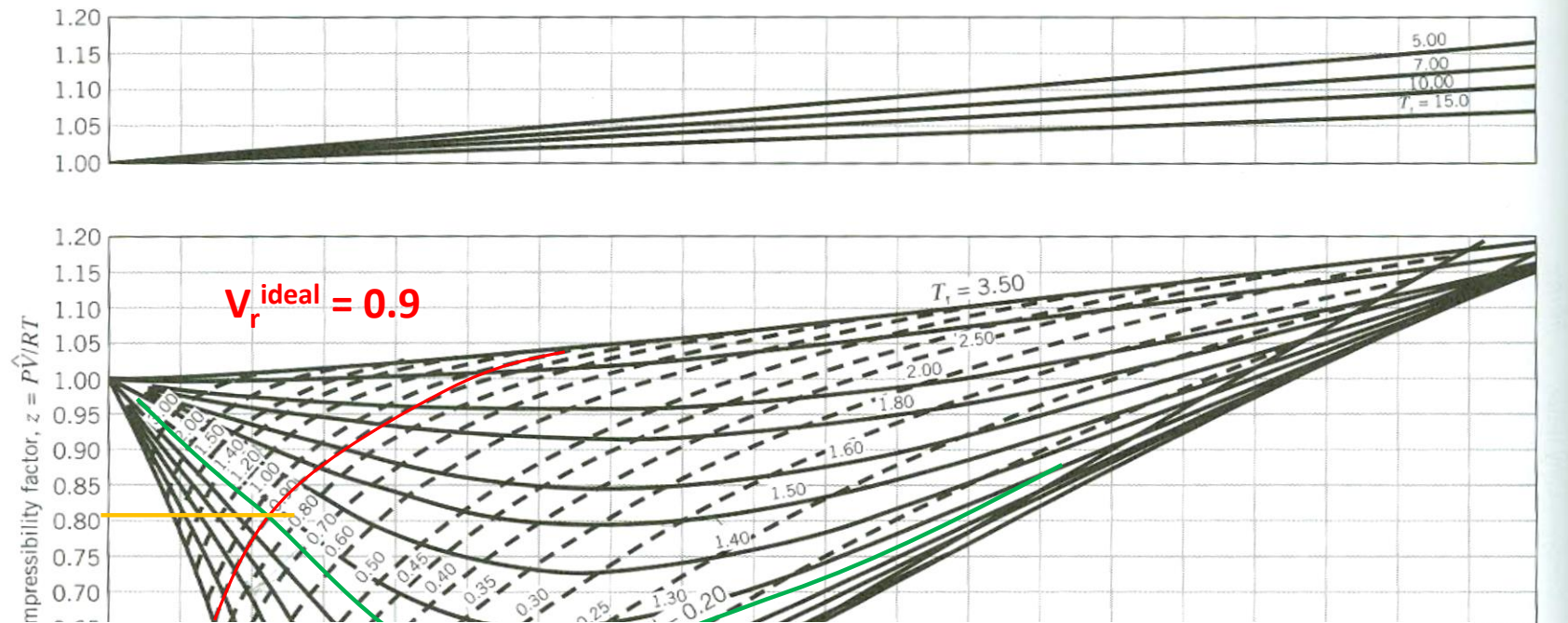
# Example:

- Estimate the pressure in atm for carbon dioxide at 380 K and 0.311 L/mol using the compressibility charts.

$$T_c = 304.2 \text{ K}, P_c = 72.9 \text{ atm}$$

$$T_r = 380\text{K}/304.2\text{K} = 1.25$$

$$\begin{aligned}\hat{V}_r^{\text{ideal}} &= \hat{V}P_c/RT_c \\ &= (0.311\text{L/mol})(72.9\text{atm})/(0.08206\text{atm}\cdot\text{L/mol}\cdot\text{K})(304.2\text{K}) \\ &= 0.908\end{aligned}$$



$$P\hat{V} / RT = z$$

$$P = zRT / \hat{V}$$

$$= 0.80(0.08206 \text{ atm} * L / \text{mol} * K)(380 K) / 0.311 L / \text{mol}$$

$$= 80.2 \text{ atm}$$