$$\frac{d}{d+}\left\{U+M\left(\frac{v^{2}}{2}+\psi\right)\right\} = \frac{k}{2}M_{n}\left(\hat{U}+\frac{v^{2}}{2}+\psi\right)_{k} + \hat{Q}$$

$$+ \frac{k}{2}M_{n}\left(\hat{P}\hat{U}\right)_{k}$$

$$= \frac{k}{2}M_{n}\left(\hat{P}\hat{U}\right)_{k}$$

$$= \frac{k}{2}M_{n}\left(\hat{P}\hat{U}\right)_{k}$$

$$\left[U+M\left(\frac{v^2}{z}+\Upsilon\right)\right]_{\frac{1}{2}}-\left[V+M\left(\frac{v^2}{z}+\Upsilon\right)\right]_{\frac{1}{2}}=$$

$$\sum_{k=1}^{K} \int_{+_{1}}^{+_{2}} \operatorname{Min} \left(\hat{H} + \frac{v^{2}}{2} + \gamma^{2} \right)_{N} dt + \frac{Q}{2} + \frac{W}{2}$$

$$Q = \int_{t_1}^{t_2} \dot{Q} dt \qquad W = W_s - \int_{V(t_i)}^{V(t_i)} \rho dV$$

$$W_{s} = \begin{cases} t_{z} \\ \dot{W}_{s} dt \end{cases}$$

$$\begin{cases} V(t_{z}) \\ \rho dV = \begin{cases} t_{z} \\ \rho \frac{dV}{dt} dt \end{cases}$$

$$V(t_{z}) \begin{cases} v(t_{z}) \\ v(t_{z}) \end{cases}$$

For BME'S — LVAD
For ABE'S — Compressor

$$M_1$$
 P_1
 P_2
 T_2
 W_S
 Q

Do open system analysis ->

- 1) Mass belong
- 2) Enrgy balance

to show that

$$Q + Ws = (\hat{H}_z - \hat{H}_i) \Delta M$$

where DM is flow in a smell time interval. + + +++++

Mass blow on compressor itself,

$$M(++\Delta+) = M(+) = \begin{cases} ++\Delta + \\ M_1 d + \\ M_2 d + = 0 \end{cases}$$
lets chooke by so $M_1 = constant$

$$M_2 = constant$$

$$M_2 = constant$$

$$M_1 = -\Delta M_2 = \Delta M_1 + \Delta M_2 = 0$$

$$\Delta M_1 = -\Delta M_2 = \Delta M_1$$

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$$= \Delta M_4 + \Delta M_4$$

$$= \Delta M_$$

$$\begin{cases}
M_{1} (\hat{H}_{1}) dt + \int_{1}^{t_{z}} M_{1}(\hat{H}_{2}) dt + Q + W_{s} \\
\hat{H}_{1} \text{ is not} & \hat{H}_{2} \text{ is not} \\
\text{changing in the changing in the changi$$