

Solution homework 6 - Fall 2017

Question 1

$$\text{mN} := 10^{-3} \cdot \text{N}$$

$$\theta := 2 \cdot \text{deg}$$

$$\theta = 0.035 \cdot \text{rad}$$

$$R_c := 30 \cdot \text{mm}$$

(a)

$$\Omega_c := \begin{pmatrix} 0.63 \\ 1.9 \\ 5.7 \\ 11 \\ 15 \\ 22 \\ 30 \end{pmatrix} \cdot \frac{\text{rad}}{\text{s}}$$

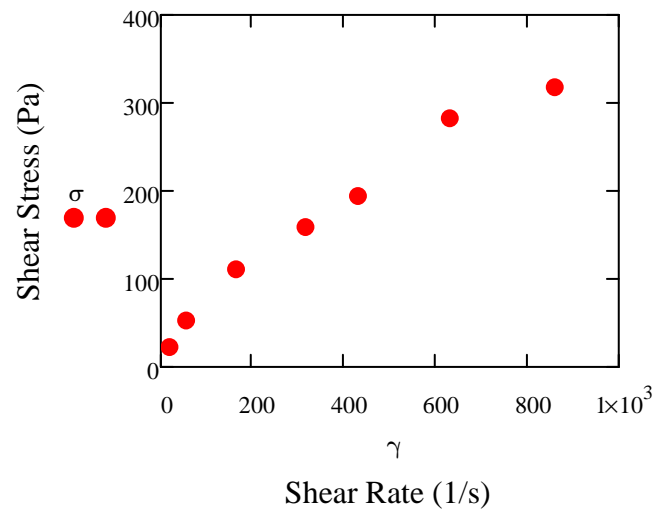
$$M := \begin{pmatrix} 1.3 \\ 3 \\ 6.3 \\ 9 \\ 11 \\ 16 \\ 18 \end{pmatrix} \cdot \text{mN} \cdot \text{m}$$

$$\gamma := \frac{\Omega_c}{\theta}$$

$$\gamma = \begin{pmatrix} 18 \\ 54.4 \\ 163.3 \\ 315.1 \\ 429.7 \\ 630.3 \\ 859.4 \end{pmatrix} \frac{1}{\text{s}}$$

$$\sigma := \frac{3 \cdot M}{2\pi \cdot R_c^3}$$

$$\sigma = \begin{pmatrix} 22.989 \\ 53.052 \\ 111.408 \\ 159.155 \\ 194.523 \\ 282.942 \\ 318.31 \end{pmatrix} \text{Pa}$$



(b) Determine the rheological parameters of the liquid

We can estimate a power regression to the shear stress versus shear rate data illustrated in the above plot. In MathCad that is done with the **genfit** function. Variables cannot contain units so below are defined shear rate and shear stress without units

$$\gamma_{\text{nu}} := \gamma \cdot s$$

$$\sigma_{\text{nu}} := \sigma \cdot \frac{1}{\text{Pa}}$$

$$f(x, k, n) := k \cdot x^n \quad \text{guess} := \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$\text{Fit} := \text{genfit}(\gamma_{\text{nu}}, \sigma_{\text{nu}}, \text{guess}, f)$$

Result of the Fit $\text{Fit} = \begin{pmatrix} 3.481 \\ 0.672 \end{pmatrix}$ $k_{\text{nu}} := \text{Fit}_0$ $n_{\text{nu}} := \text{Fit}_1$

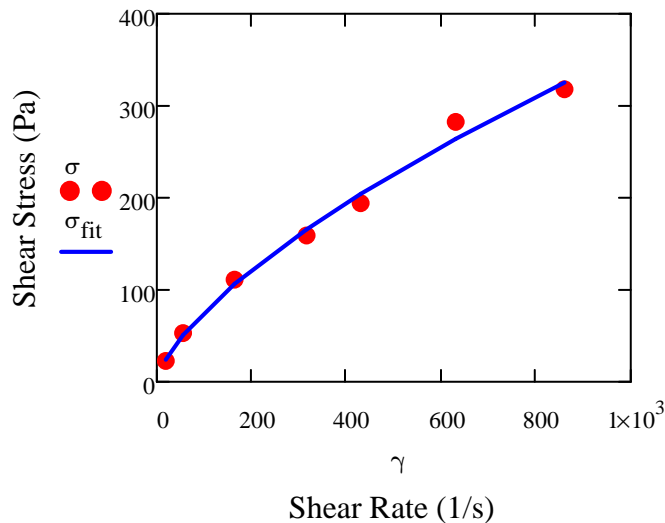
$$k = 3.481 \text{ Pa s}^{0.672}$$

$$n = 0.672$$

$$\sigma_{\text{fit}} := k_{\text{nu}} \cdot \gamma_{\text{nu}}^{n_{\text{nu}}} \cdot \text{Pa}$$

$$\sigma_{\text{fit}} = \begin{pmatrix} 24.303 \\ 51.013 \\ 106.699 \\ 165.937 \\ 204.37 \\ 264.327 \\ 325.55 \end{pmatrix} \text{ Pa}$$

Now the experimental data can be plotted with the fitted model



Question 2

This problem can be solved using excel and graphically, i.e. plot the data in excel and graphically solve the problem to estimate the shear stress at the wall and the shear rate. to avoid using plots instead this problem was using tools in MathCad that allow us directly interpolate the data used to construct the plot.

Let's first create two vectors, one is the pressure drop called Δp and the volumetric flowrate that we will call Q_v , in addition we are incorporating units to these variables

$$\Delta p := \begin{pmatrix} 18.9 \\ 24.3 \\ 29.6 \\ 42.8 \\ 56.1 \\ 70.8 \end{pmatrix} \cdot \text{kPa}$$

$$Q_v := \begin{pmatrix} 1.81 \cdot 10^{-7} \\ 5.89 \cdot 10^{-7} \\ 1.47 \cdot 10^{-6} \\ 8.34 \cdot 10^{-6} \\ 2.94 \cdot 10^{-5} \\ 8.83 \cdot 10^{-5} \end{pmatrix} \frac{\text{m}^3}{\text{s}}$$

$$D_{p_lab} := 0.01 \cdot \text{m} \quad L_{lab} := 1.5 \cdot \text{m}$$

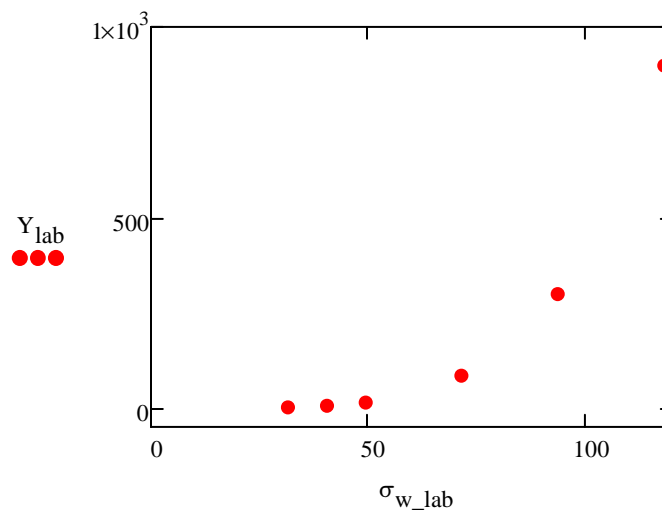
To perform the scale up procedure we have to plot $8u/D_p$ as a function of σ_w . For convenience we will call those parameters Y_{lab} and σ_{w_lab} , respectively. We need to calculate also the mean velocity that will be called u_{mean}

$$u_{mean} := \frac{Q_v}{\pi \cdot \left(\frac{D_{p_lab}}{2} \right)^2}$$

$$Y_{lab} := \frac{8 \cdot u_{mean}}{D_{p_lab}}$$

$$\sigma_{w_lab} := \frac{\Delta p \cdot \frac{D_{p_lab}}{2}}{2 \cdot L_{lab}}$$

Let's plot the data



As discussed once the plot is constructed we can get the information directly from the graph or by interpolation the data. Another option would be to fit the experimental data by an equation and get the parameters of the equation, A good fitting approach is the power-law model given by the equation $Y_{lab} = aX^b$ where X is

σ_{w_lab} . The following is taken from the help in MathCad Help to fit a power law equation to the data in the plot. See also Question 1:

$genfit(vx,vy,vg,F)$ return a vector containing the parameters that make the F of X. vx is the x-data and vy is the y-data, whereas vg is the vector with solutions. As in question 1 we need to get rid of the units

$$\Delta p_{no_units} := \frac{\Delta p}{Pa} \quad Q_{v_no_units} := \frac{Q_v}{\frac{m^3}{s}} \quad D_{p_lab_no_units} := \frac{D_{p_lab}}{cm}$$

$$L_{lab_no_units} := \frac{L_{lab}}{m} \quad u_{mean_no_units} := \frac{Q_{v_no_units}}{\pi \cdot \left(\frac{D_{p_lab_no_units}}{2} \right)^2}$$

$$Y_{lab_no_units} := \frac{Y_{lab}}{\frac{1}{s}} \quad \sigma_{w_no_units} := \frac{\sigma_{w_lab}}{Pa}$$

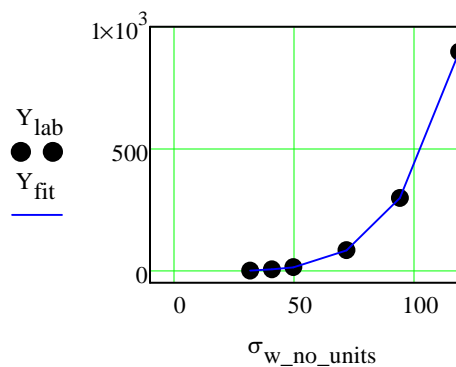
$$guess := \begin{pmatrix} 11 \\ 10 \end{pmatrix} \quad f_{question_2}(x,a,b) := a \cdot x^b$$

$$Y_{model_fit} := genfit(\sigma_{w_no_units}, Y_{lab_no_units}, guess, f_{question_2})$$

$$Y_{model_fit} = \begin{pmatrix} 1.536 \times 10^{-7} \\ 4.714 \end{pmatrix} \quad \begin{matrix} \text{--- a value} \\ \text{<--- b value} \end{matrix}$$

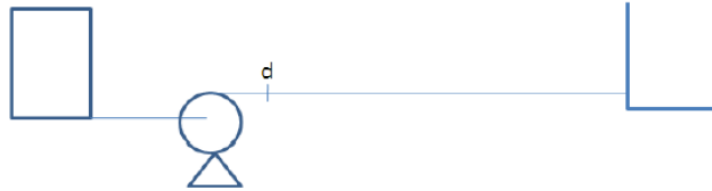
$$Y_{fit} := 1.536 \cdot 10^{-7} \cdot \sigma_{w_no_units}^{4.714}$$

Let's plot the experimental data and the model to check the model accuracy



The fit of the experimentl is very good as observed in the above graph

The factory situation is given in the figure below:



The static pressure drop, the kinetic pressure drop and the pressure drop in the pump, all can be considered to be 0. The pressure drop in the pump is zero because there is no pump between the pump discharge (d) and the exit. The balance of energy will be $p_d - p_o = \Delta p_f$ where p_o is the atmospheric pressure, therefore $p_{d_gauge} = \Delta p_f$ can be calculated from the factory situation where the dimensions of the factory piping system are known, and we can use the rheological model given by Y_{fit}

$$D_{factory} := 6 \cdot \text{cm}$$

$$L_{factory} := 65 \cdot \text{m}$$

$$Q_{factory} := 70 \cdot \frac{1}{\text{hr}}$$

$$Q_{fac_no_units} := \frac{Q_{factory}}{\frac{\text{m}^3}{\text{s}}} \quad u_{mean_fac} := \frac{Q_{factory}}{\pi \cdot \left(\frac{D_{factory}}{2} \right)^2} \quad Y_{factory} := \frac{8 \cdot u_{mean_fac}}{D_{factory}}$$

$$Y_{fac_no_units} := \frac{Y_{factory}}{\frac{1}{\text{s}}} \quad \sigma_{w_fac_no_units} := \left(\frac{Y_{fac_no_units}}{1.536 \cdot 10^{-7}} \right)^{\frac{1}{4.714}}$$

$$\sigma_{w_fac_no_units} = 27.4$$

$$\sigma_{w_fac} := \sigma_{w_fac_no_units} \cdot \text{Pa}$$

With that value we can calculate the pressure loss in the pipe

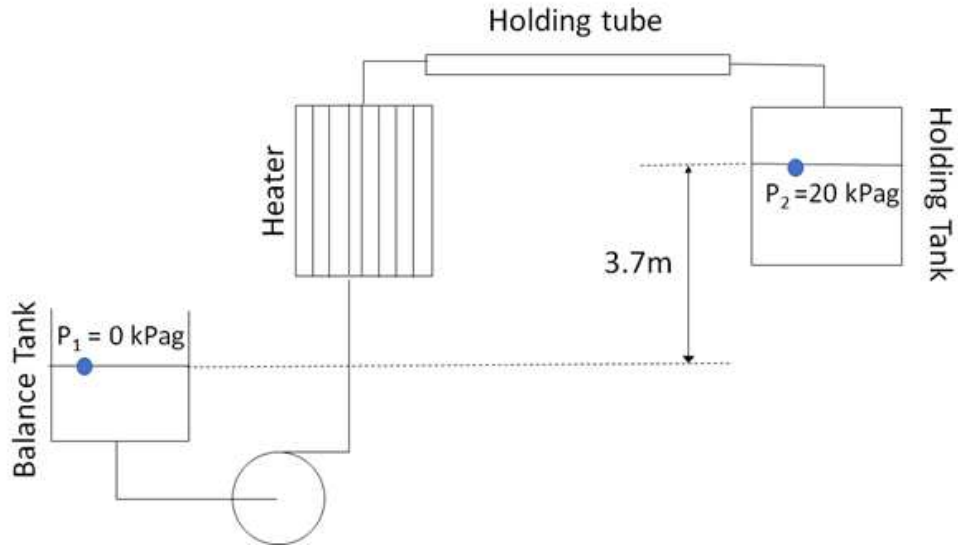
$$\Delta p_{f_factory} := \frac{\sigma_{w_fac} \cdot 2 \cdot L_{factory}}{D_{factory}^2} \quad \Delta p_{f_factory} = 118.64 \cdot \text{kPa}$$

$$p_d := \Delta p_{f_factory}$$

$$p_d = 118.64 \cdot \text{kPa}$$

Question 3

(a) Draw a diagram of the system



(b)

$$\Delta p_{\text{pump}} = (p_2 - p_1) + \Delta p_{k1-2} + \Delta p_{s1-2} + \Delta p_{f1-2}$$

Since 1 and 2 are over the surfaces, and they are not moving the fluid velocities at 1 and 2 are zero and $\Delta p_{k1-2} = 0$. If we consider the level zero at the level 1, then $h_1 = 0$ and $h_2 = 3.7\text{m}$

$$\rho_{\text{fluid}} := 995 \cdot \frac{\text{kg}}{\text{m}^3}$$

$$Q := 4000 \cdot \frac{\text{l}}{\text{hr}}$$

$$\eta_{\text{pump}} := 0.8$$

$$\eta_{\text{motor}} := 0.75$$

$$h_1 := 0 \cdot \text{m}$$

$$h_2 := 3.7 \cdot \text{m}$$

$$\Delta p_{s1-2} := \rho_{\text{fluid}} \cdot g \cdot (h_2 - h_1)$$

$$\Delta p_{s1-2} = 36.103 \cdot \text{kPa}$$

$$p_1 := 0 \cdot \text{kPa}$$

$$p_2 := 20 \cdot \text{kPa}$$

$$\Delta p_{f1-2} := 1250 \cdot \text{kPa}$$

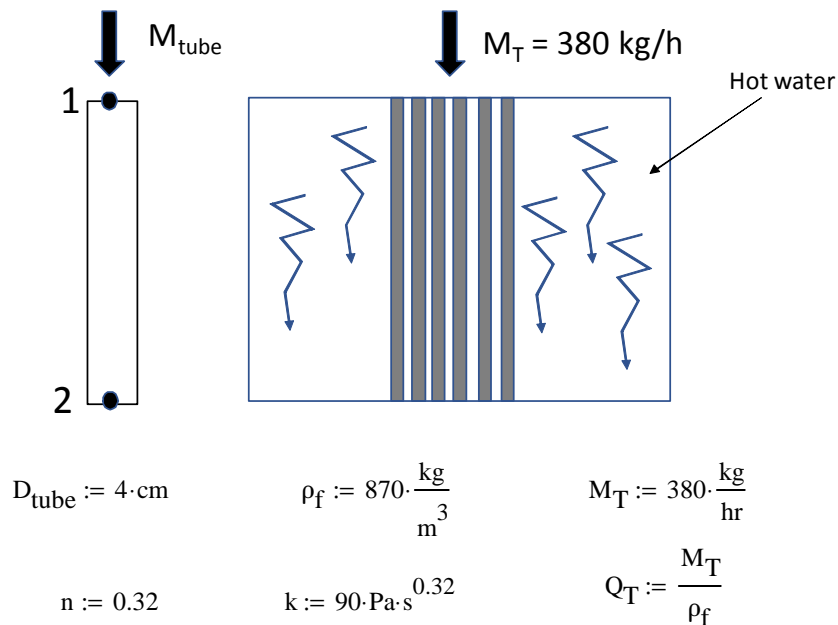
$$\Delta p_{\text{pump}} := (p_2 - p_1) + \Delta p_{s1-2} + \Delta p_{f1-2}$$

$$\Delta p_{\text{pump}} = 1306.1 \cdot \text{kPa}$$

$$\text{Power} := \frac{\Delta p_{\text{pump}} \cdot Q}{\eta_{\text{pump}} \cdot \eta_{\text{motor}}}$$

$$\text{Power} = 2.4 \cdot \text{kW}$$

Question 4



Let's consider a balance of mechanical energy between points 1 and 2 for a tube in the diagram shown above

$$\Delta p_{\text{pump}} = (p_2 - p_1) + \rho_f g (h_2 - h_1) + 1/2 \rho_f (u_2 - u_1)/\alpha +$$

Because the pipe is open to the atmosphere p_1 and p_2 are equals to the atmospheric pressure and $p_2 - p_1 = 0$. Also $h_2 - h_1 = -L$, where L is the length of the pipe. The diameters of the tube at 1 and 2 are equals there the kinetic change is zero, as well as Δp_{pump} because there is no pump between 1 and 2. Therefore if you use the mechanical balance between 1 and 2 we get

$$-\rho_f g L + \Delta p_{f1-2} = 0 \quad \rightarrow \quad \rho_f g L = 2Lk/R \cdot ((3n+1)/4n)^n \cdot ((4Q_{\text{tube}})/\pi R^3_{\text{tube}})^n$$

from the above equation we can calculate Q_{tube}

$$Q_{\text{tube}} := \left[\frac{\rho_f \cdot g \cdot \frac{D_{\text{tube}}}{2}}{2 \cdot k} \cdot \left(\frac{4 \cdot n}{3n + 1} \right)^n \right]^{\frac{1}{0.32}} \cdot \pi \cdot \frac{\left(\frac{D_{\text{tube}}}{2} \right)^3}{4}$$

$$Q_{\text{tube}} = 3.472 \times 10^{-6} \frac{\text{m}^3}{\text{s}}$$

$$N_{\text{tubes}} := \frac{Q_T}{Q_{\text{tube}}}$$

$$N_{\text{tubes}} = 35$$