ABE 307

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Friction Factors

Friction factor is a generalized variable that is useful for calculation of force exerted by fluid on the system for any kind of system. We will study the friction factor for two most common system encountered in engineering problems.

- a) Flow through channels/pipes such as pumping of fluids through pipes, extrusion, or blood flow through artery etc. The main goal in these cases is to get pressure drop with volumetric
- b) Flow around submerged objects such as fluid flow around heat exchanger tube, flow around particles in a mixing tank. The main goal in these cases is to find relationship between fluid velocity and drag exerted by the fluid on the submerged object.

Defining Friction Factor

torces exerted by the fluid on rugues.

Fluid > suyare FK + FS

F_K = Kinetic force. F_S = Static force.

We are interseted in kinetic forces.

A = characeteristic area

FK X AK

A = Characterisis

K = Kinetic energy per unit

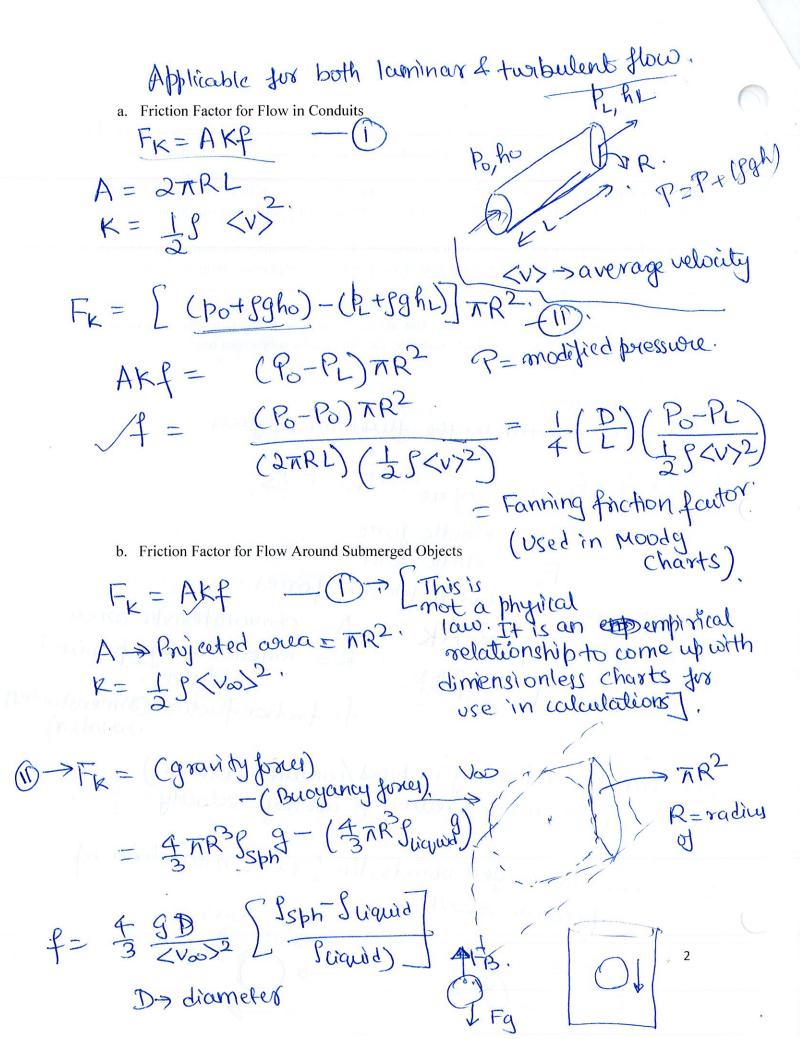
Volume.

F= fortion factor Carmensionless

variables). (polables)

- For fluid flowing in pipes/conduits (channel) Fix is in the direction of average velocity.
- For submerged objects, the force is in direction of approach velocity VO





Developing Friction Factor Charts for Calculations

Calculation of friction factor for all types of system will become time consuming, so we want an easier and quicker way to calculate these factors for a real system. Thus, we combine dimensional analysis with definition of friction factor to relate the friction factor to one of the dimensionless variables that defines the flow regime for a system.

a. Friction Factor Charts for Flow in Tubes

- Either laminar or Turbulent flow
- Steadily driven turbulent flow (ie turbulent flow with steady total throughput)

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Force in the z-direction on the inner wall of the tube

$$F_{R} = \int_{0}^{2\pi} \left| \frac{\partial x}{\partial x} \right|_{x=R} R d\theta dz - T$$

$$F_{IC} = \frac{1}{2} S \langle v_{z} \rangle^{2} (2\pi R L) f - T$$

Note: For Turbulent flow this force can be a function of time, due to fluctuations and the random

y profile. $f(t) = \int \int \int \frac{2\pi}{\sqrt{3}} R \cdot d\theta \cdot dz$ velocity profile.

1 9 < VZ>2 (2 TRL)

In turbulent flow, & dVZ will be a function of time.

To be able to use dimensionless numbers, we will change the friction factor in dimensionless form. Since, the empirical charts are developed

using model (or realed down versions of real 3 systems) we want these charts to be developed in mon-dimensionless form for results to

Define the following dimens	sionless quantities
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$$\sqrt{8} = x$$
, $V = \frac{V_z}{2}$; $\overline{t} = \frac{t}{D/\varpi cv_z}$

$$\overline{P} = \frac{P - P_o}{P < v_z > 2}$$
, $Re = \frac{P < v_z > D}{D}$, $\overline{Z} = \frac{Z}{D}$

Now, if you want to calculate then we can use the dimensionless form of Equation of motion to get v:2

Boundary conditions in Dimensionless Form

(1)
$$\sqrt{z} = R$$
, $\sqrt{z} = 0$, $\sqrt{z} = 1/2$, $\sqrt{z} = 0$.

 $\sqrt{z} = 8z$. \Rightarrow oniform velocity at in let

is integrated, it will only depend on Re, L/D and \bar{t} Finally, when the equation for P(Re, HD,t)

Next, when we time average the friction factor

Thus, measured friction factor only depends on Re and L/D. or Length to diameter ratio of the pipe.

After the fluid enters the pipe, till a certain length the velocity profile develops and after that the flow is fully developed and it will not depend on z. This entrance length is what is different in laminar and turbulent flow.

In case of Laminar flow, the entrance length is

In case of Turbulent flow, the entrance length is

Beyond the entrance length, the f is not dependent on L/D.

Readings: Please read Sections 6.1, 6.2, and 6.3

Examples from Book

Example 6.2.1: Calculation of Pressure Drop Required for a Given Flow Rate

What pressure gradient is required for fluid of density $\rho = 0.935$ gm/cc and viscosity $\mu = 1.95$ cp to flow in a horizontal, smooth, circular tube of inside diameter D = 3 cm at a mass flow rate of 1028 g/s.

$$f = \frac{102895}{Po-Pc} \frac{1}{1} \frac{D}{D} \times \frac{1}{12N^{2}}$$

$$Re = \frac{2\omega}{RRN}$$

$$Re = 2.29 \times 10^{4}$$

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$$Possesse gradient = \Delta P = Po-PL$$

$$L$$

$$Re = \frac{9 \times \sqrt{20}}{N}$$

$$W = \frac{9 \times \sqrt{20}}{N}$$

$$V_{2} = \frac{9}{N}$$

$$Re = \frac{9}{N}$$

$$Re = \frac{9}{N}$$

$$Re = \frac{9}{N}$$

$$Re = \frac{1}{N}$$

$$Re = \frac{1}{N}$$

Example 6.2.2: Calculation of flow rate for a given Pressure Drop

Determine the flow rate, in lbm/hr, of water at 68 deg F through a 1000-ft length of horizontal 8-in schedule 40 steel pipe (internal diameter 7.981in) under a pressure difference of 3.00 psi.

Assume
$$k/D = 2.3 \times 10^{-4}$$
 $\omega \rightarrow$
 $\uparrow = \Delta P \downarrow D$
 $\downarrow \downarrow \uparrow \checkmark \lor 2$

$$\Delta P = 3.00 ps$$

$$L = 1000 ft$$

$$Re = 9 < v_2 > D$$

$$M$$

$$D,$$

$$P, M$$

Re

Method A -> Recreating a new graph to use with the known parameters.

Develop New chast for Relif vs Re from our original

moody chart.

Re

$$f = \frac{(\text{ReJf})^2}{\text{Re}^2}$$

$$\log f = -2\log (\text{ReJf})$$

$$Re = \int (\text{NeJf})$$

$$\omega = \int (\text{NeJf})^2 d\theta$$

$$\omega = \int (\text{NeJf})^2 d\theta$$

$$\omega = \int (\text{NeJf})^2 d\theta$$

