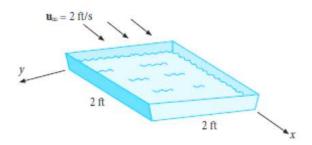
Homework 4 - Solutions ABE 30800 - Spring 2018

Question 1



There will be some heat transfer between the pan and the water, that energy is used to vaporize part of the water in the water pan. This problem is similar than the example problem given in class, but in this case we only need to estimate the heat transfer coefficient. As we know the coefficient is a function of the Reynolds number

Data

Temperatures are expressed in degree Farehnheit and transformed in degree Celsius. Absolute temperature in units of Kelvins (K)

$$\begin{split} T_{w1} &:= 95 & T_{surr1} &:= 80 & kJ &:= 1000 \cdot J \\ T_{w1C} &:= \frac{T_{w1} - 32}{1.8} & T_{surr1C} &:= \frac{T_{surr1} - 32}{1.8} \\ T_{w1C} &= 35 & T_{surr1C} &= 26.7 \\ T_{film1} &:= \frac{T_{w1C} + T_{surr1C}}{2} & T_{film1} &= 30.8 \\ T_{film1K} &:= \left(T_{film1} + 273\right) \cdot K & T_{film1K} &= 303.8 \cdot K \end{split}$$

Values of the air properties are taken at 300K (it will not change much respect to 303.8K)

$$\begin{split} \rho_1 &\coloneqq 1.17 \cdot \frac{kg}{m^3} & \mu_1 \coloneqq 1.85 \cdot 10^{-5} \cdot \frac{kg}{m \cdot s} & u_{inf1} \coloneqq 2 \cdot \frac{ft}{s} \\ k_1 &\coloneqq 0.026 \cdot \frac{W}{m \cdot K} & c_1 \coloneqq 1 \cdot \frac{kJ}{kg \cdot K} & Pr_1 \coloneqq 0.706 \\ L_1 &\coloneqq 2 \cdot ft & Re_{L1} \coloneqq \frac{L_1 \cdot \rho_1 \cdot u_{inf1}}{\mu_1} & Re_{L1} = 2.4 \times 10^4 & \text{Flow is laminar} \\ Nu_{L1} &\coloneqq 0.664 \cdot Re_{L1} \stackrel{\frac{1}{2}}{2} \cdot Pr_1 \stackrel{\frac{1}{3}}{3} & Nu_{L1} = 90.6 \\ h_{L1} &\coloneqq \frac{k_1 \cdot Nu_{L1}}{L_1} & h_{L1} = 3.9 \cdot \frac{W}{m^2 \cdot K} \end{split}$$

Question 2

The building is square with sides of 20m. Assume that the air surrounds the building so the heat transfer is through 4 sides. Let's calculate first the heat transfer coefficient h._{L2}

$$u_2 := 30 \frac{\text{km}}{\text{hr}}$$
 $L_2 := 20 \cdot \text{m}$ $T_{\text{air}2} := -10$ $T_{\text{w}2} := 10$ $T_{\text{film}2} := \frac{\left(T_{\text{air}2} + 273\right) + \left(T_{\text{w}2} + 273\right)}{2} \cdot \text{K}$ $T_{\text{film}2} = 273 \, \text{K}$

The properties of the air at 273k (let's use 270K) in the air table

$$\begin{split} \rho_2 &:= 1.30 \cdot \frac{kg}{3} & \mu_2 := 1.70 \cdot 10^{-5} \cdot \frac{kg}{m \cdot s} & k_2 := 0.0238 \frac{W}{m \cdot K} \\ c_2 &:= 1 \cdot \frac{kJ}{kg \cdot K} & \text{Pr}_2 := 0.716 \\ \\ \text{Re}_{L2} &:= \frac{u_2 \cdot \rho_2 \cdot L_2}{\mu_2} & \text{Re}_{L2} = 1.3 \times 10^7 & \text{Turbulent flow} \\ \\ \text{Nu}_{L2} &:= 0.036 \cdot \text{Re}_{L2}^{\frac{4}{5}} \cdot \text{Pr}_2^{\frac{1}{3}} & \text{Nu}_{L2} = 1.6 \times 10^4 \\ \\ \text{h}_{L2} &:= \frac{k_2 \cdot \text{Nu}_{L2}}{L_2} & \text{h}_{L2} = 18.5 \cdot \frac{W}{m^2 \cdot K} \\ \\ Q_{2_per_length} &:= h_{L2} \cdot \left(4 \cdot L_2 \right) \cdot \left(T_{w2} - T_{air2} \right) \cdot K \\ \\ \\ Q_{2_per_length} &= 3 \times 10^4 \cdot \frac{W}{m} \end{split}$$

Question 3

$$\begin{split} \text{m3_dot} &:= 200 \cdot \frac{\text{gm}}{\text{s}} & \text{D}_3 := 2 \cdot \text{cm} & \text{T}_{\text{w3}} := 80 & \text{T}_{\text{w3}K} := \left(\text{T}_{\text{w3}} + 273\right) \cdot \text{K} \\ & \text{T}_{\text{tw3}} := 200 & \text{T}_{\text{tw3}K} := \left(\text{T}_{\text{tw3}} + 273\right) \cdot \text{K} \\ & \text{T}_{\text{film3K}} := \frac{\text{T}_{\text{w3K}} + \text{T}_{\text{tw3K}}}{2} & \text{T}_{\text{film3K}} = 413 \, \text{K} \\ & \text{T}_{\text{film3}} := \frac{\text{T}_{\text{film3K}}}{1 \cdot \text{K}} - 273 & \text{T}_{\text{film3}} = 140 & \text{degree Celsius} \end{split}$$

Properties of Saturated liquid water at 140°C are:

$$\rho_{\text{W3}} := 921.7 \cdot \frac{\text{kg}}{\text{m}^3} \qquad \qquad c_3 := 4.38 \frac{\text{kJ}}{\text{kg} \cdot \text{K}} \qquad \qquad k_{\text{W3}} := 0.683 \cdot \frac{\text{W}}{\text{m} \cdot \text{K}} \qquad \qquad \text{Pr}_3 := 1.24$$

$$\begin{array}{lll} \mu_{3} \coloneqq 0.197 \cdot 10^{-3} \cdot \frac{kg}{m \cdot s} & u_{3} \coloneqq \frac{4 \cdot m3 _ dot}{\rho_{w3} \cdot \pi \cdot D_{3}^{-2}} & u_{3} = 0.7 \frac{m}{s} \\ \\ Re_{D3} \coloneqq \frac{u_{3} \cdot \rho_{w3} \cdot D_{3}}{\mu_{3}} & Re_{D3} = 6.5 \times 10^{4} & Turbulent Flow \\ \\ Nu_{D3} \coloneqq 0.023 \cdot Re_{D3}^{-\frac{4}{5}} \cdot Pr_{3}^{-0.4} & Nu_{D3} = 176.8 \\ \\ h_{D3} \coloneqq \frac{k_{w3} \cdot Nu_{D3}}{D_{3}} & h_{D3} = 6 \times 10^{3} \cdot \frac{W}{m^{2} \cdot K} \\ \\ Q_{3} \coloneqq h_{D3} \cdot \pi \cdot D_{3} \cdot \left(T_{tw3K} - T_{w3K}\right) & Q_{3} = 45.5 \cdot \frac{kW}{m} \\ \\ Q_{3} \coloneqq 1.9 \cdot cm & u_{new} \coloneqq \frac{4 \cdot m3 _ dot}{\rho_{w3} \cdot \pi \cdot D_{new}^{-2}} \\ \\ Re_{D_new} \coloneqq \frac{u_{new} \cdot \rho_{w3} \cdot D_{new}}{\mu_{3}} & Re_{D_new} = 6.8 \times 10^{4} & Turbulent Flow \\ \\ Nu_{D_new} \coloneqq \frac{u_{new} \cdot \rho_{w3} \cdot D_{new}}{\mu_{3}} & Re_{D_new} = 184.2 \\ \\ h_{D_new} \coloneqq \frac{k_{w3} \cdot Nu_{D_new}}{D_{new}} & h_{D_new} = 6.6 \times 10^{3} \cdot \frac{W}{m^{2} \cdot K} \\ \\ Q_{3_new} \coloneqq h_{D_new} \cdot \pi \cdot D_{new} \cdot \left(T_{tw3K} - T_{w3K}\right) & Q_{3_new} = 47.4 \cdot \frac{1}{m} \cdot kW \\ \end{array}$$

The heat gain is increased because the velocity of the fluid is increased when the diameter decreases. However, the result woud be different if the scale formed has a low thermal conductivity but no information is giving so we cannot evaluate this. The increase of roughness may promote turbulence and increase the heat transfer coefficient.

Question 4

(a)
$$D_{per} := 30 \cdot cm$$
 $L_{per} := 1.8 \cdot m$ $T_{body} := 37 \cdot K$ $u_{wind} := 5 \cdot \frac{m}{s}$ $T_{air4} := 35 \cdot K$
$$T_{film4} := \frac{\left(T_{body} + 273 \cdot K\right) + \left(T_{air4} + 273 \cdot K\right)}{2}$$
 $T_{film4} = 309 \, K$

Let's use the properties of air at 310K

$$\begin{split} \rho_4 &\coloneqq 1.138 \cdot \frac{kg}{m^3} \qquad c_4 \coloneqq 1.007 \cdot \frac{kJ}{kg \cdot K} \qquad \mu_4 \coloneqq 1.893 \cdot 10^{-5} \cdot \frac{kg}{m \cdot s} \\ k_4 &\coloneqq 0.027 \cdot \frac{W}{m \cdot K} \qquad \text{Pr}_4 \coloneqq 0.705 \\ \text{Re}_{D4} &\coloneqq \frac{u_{wind} \cdot \rho_4 \cdot D_{per}}{\mu_4} \qquad \text{Re}_{D4} = 9 \times 10^4 \\ \text{From Table} \qquad B &\coloneqq 0.027 \qquad n \coloneqq 0.805 \\ \text{Nu}_{D4} &\coloneqq B \cdot \text{Re}_{D4}^{\quad n} \cdot \text{Pr}_4^{\quad \frac{1}{3}} \qquad \boxed{\text{Nu}_{D4} = 234.2} \qquad h_4 \coloneqq \frac{k_4 \cdot \text{Nu}_{D4}}{D_{per}} \qquad h_4 = 21.1 \cdot \frac{W}{m^2 \cdot K} \\ q_4 &\coloneqq h_4 \cdot \pi \cdot D_{per} \cdot L_{per} \cdot \left(T_{body} - T_{air4}\right) \qquad \boxed{q_4 = 71.5W} \\ \text{for calm day} \qquad h_{calm} &\coloneqq 3.6 \cdot \frac{W}{m^2 \cdot K} \qquad q_{4calm} &\coloneqq h_{calm} \cdot \left[\pi \cdot D_{per} \cdot L_{per} \cdot \left(T_{body} - T_{air4}\right)\right] \\ \boxed{q_{4calm} = 12.2W} \qquad \text{much lower value of heat loss} \end{split}$$

If the velocity of the air increases to 10 m/s and the temperatures decreases to 10°C

$$\begin{aligned} \mathbf{u}_{\text{wind_new}} &\coloneqq 10 \cdot \frac{\mathbf{m}}{\mathbf{s}} & \mathbf{T}_{\text{air_new}} &\coloneqq 10 \cdot \mathbf{K} \\ \\ \mathbf{T}_{\text{film_new}} &\coloneqq \frac{\left(\mathbf{T}_{\text{air_new}} + 273 \cdot \mathbf{K}\right) + \left(\mathbf{T}_{\text{body}} + 273 \cdot \mathbf{K}\right)}{2} & \mathbf{T}_{\text{film_new}} &= 296.5 \, \mathbf{K} \end{aligned}$$

Let's use values of tables at 295K

$$\begin{split} \rho_{new} &\coloneqq 1.19 \cdot \frac{kg}{m^3} \quad \mu_{new} \coloneqq 1.82 \cdot 10^{-5} \cdot \frac{kg}{m \cdot s} \quad k_{new} \coloneqq 0.026 \cdot \frac{W}{m \cdot K} \quad Pr_{new} \coloneqq 0.706 \end{split}$$

$$Re_{new} &\coloneqq \frac{u_{wind_new} \cdot \rho_{new} \cdot D_{per}}{\mu_{new}} \quad Re_{new} = 2 \times 10^5 \end{split}$$

From the Table B = 0.027 and n = 0.805

$$Nu_{D_4new} := B \cdot Re_{new}^{n} \cdot Pr_{new}^{\frac{1}{3}}$$

$$Nu_{D_4new} = 438$$

$$h_{new} := \frac{k_{new} \cdot Nu_{D_4new}}{D_{per}}$$

$$h_{new} = 38 \cdot \frac{W}{m^2 \cdot K}$$

$$q_{new} \coloneqq h_{new} \cdot \pi \cdot D_{per} \cdot L_{per} \cdot \left(T_{body} - T_{air_new} \right) \qquad \qquad \boxed{q_{new} = 1.7 \cdot kW} \qquad \qquad \text{Significantly larger loss in a windy day}$$

Question 5

$$\begin{split} T_{air5} &:= 15 \cdot K & T_m &:= -0.5 \cdot K & k_{unf} &:= 0.55 \cdot \frac{W}{m \cdot K} \\ \rho_{unf} &:= 950 \cdot \frac{kg}{m^3} & \Delta H_f &:= 335 \cdot \frac{kJ}{kg} & h &:= 20 \cdot \frac{W}{m^2 \cdot K} \end{split}$$

Scenary 1 - there is convection from one side

$$\begin{split} & \underbrace{\textbf{y1}} \text{ - there is convection from one side} & x_{1_side} \coloneqq 2.5 \cdot \text{cm} \\ & t_{F1} \coloneqq \frac{\Delta H_f \cdot \rho_{unf}}{T_{air5} - T_m} \cdot \left(\frac{x_{1_side}}{2 \cdot k_{unf}} + \frac{x_{1_side}}{h} \right) & \underbrace{t_{F1} = 10.4 \cdot \text{hr}}_{} \end{split}$$

Scenary 2 - there is convection from one side

$$x_{2_side} := 1.25 \cdot cm$$

$$t_{F2} := \frac{\Delta H_{f} \cdot \rho_{unf}}{T_{air5} - T_{m}} \cdot \left(\frac{x_{2_side}^{2}}{2 \cdot k_{unf}} + \frac{x_{2_side}}{h} \right)$$

$$t_{F2} := \frac{\Delta H_{f} \cdot \rho_{unf}}{T_{air5} - T_{m}} \cdot \left(\frac{x_{2_side}^{2}}{2 \cdot k_{unf}} + \frac{x_{2_side}}{h} \right)$$