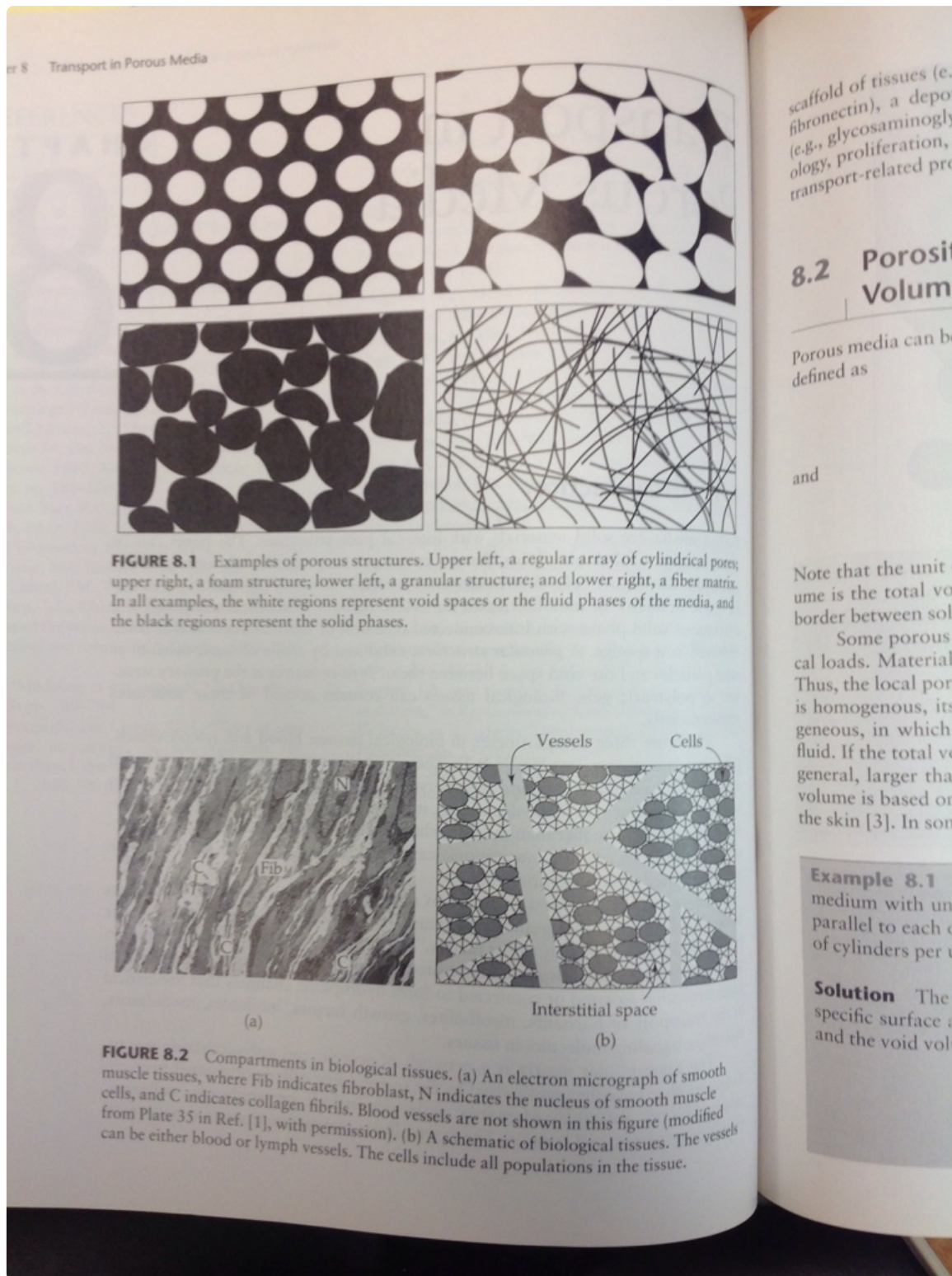


Porous media are solid materials with internal pore structures. Porous structures vary significantly among different media as shown below.

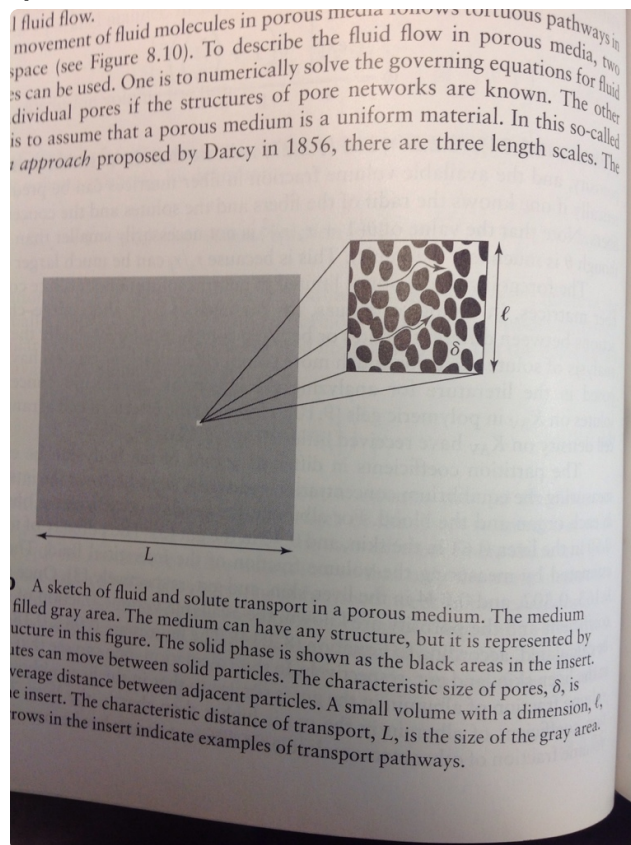


A regular array of cylindrical pores can be found in micro or nanofabricated materials. A foam structure is composed of a continuous solid phase with interconnected channels or isolated pores and is often observed as a sponge. A granular structure exhibited by a pile of sand, consists of solid particles and the void space between them. A fiber matrix is the primary structure in polymer gels. Biological tissues can contain several of these structures simultaneously.

Definitions:

specific surface  $s$  = Total interface area/total volume

porosity  $\epsilon$  = void volume/total volume



One can average all the properties over a length scale of  $l$  to obtain smooth volume averaged properties. Therefore, one can still consider the porous medium as a continuum over length scale  $l$ .

$\bar{v}$  = velocity of fluid volume averaged over  $\ell^3$ .

$\bar{v}_f$  = velocity of fluid volume averaged through pores.

$$\bar{v} = \epsilon \bar{v}_f$$

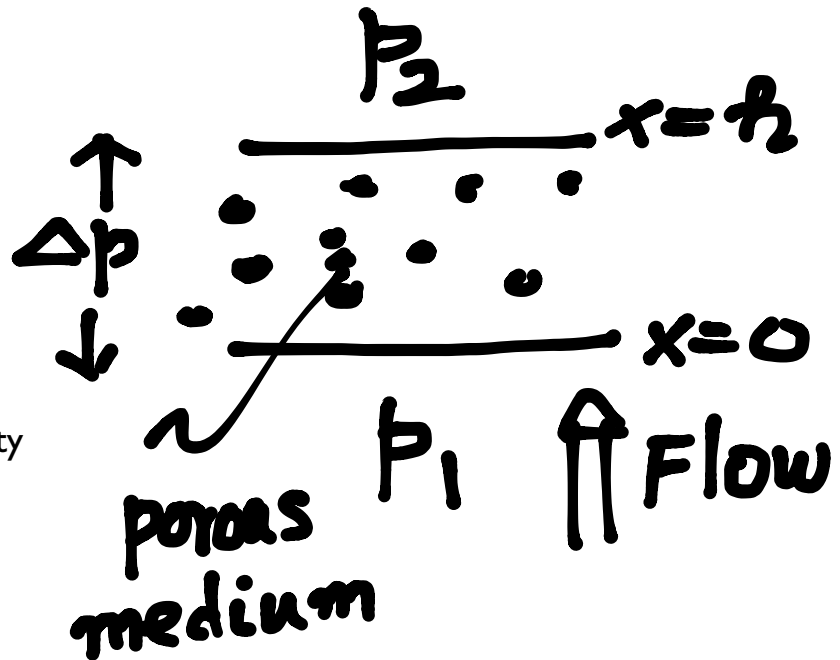
Continuity:

$$\nabla \cdot \bar{v} = 0$$

Darcy's law:

$$\bar{v} = -K \nabla p$$

$K$  = hydraulic conductivity



Substituting in equation of continuity, one obtains,

$$\nabla \cdot \{-K \nabla p\} = 0$$

For constant  $K$  (homogeneous medium), one obtains,

$$\nabla \cdot \nabla p = 0$$

$$\boxed{\nabla^2 p = 0} \quad \text{Laplace Equation}$$

One dimensional flow in rectangular coordinates:

$$\frac{d^2 p}{dx^2} = 0$$

$$\frac{dp}{dx} = C_1 \quad p = C_1 x + C_2$$

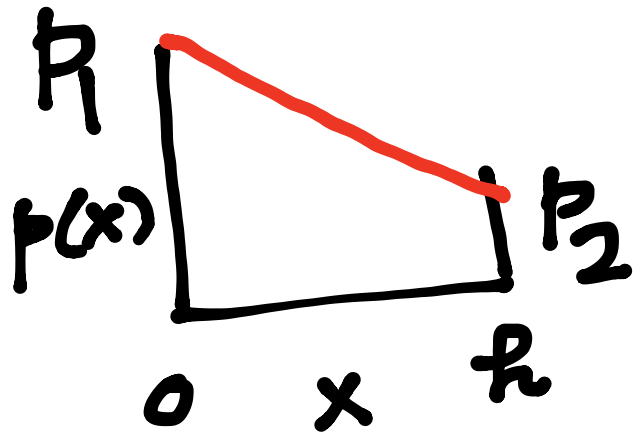
$$x=0 \quad p=p_1 \Rightarrow C_2 = p_1$$

$$x=h \quad p=p_2$$

$$\circ \circ \quad p_2 = C_1 h + p_1$$

$$C_1 = (p_2 - p_1)/h$$

$$\circ \circ \quad p = p_1 - (p_1 - p_2) \left( \frac{x}{h} \right)$$

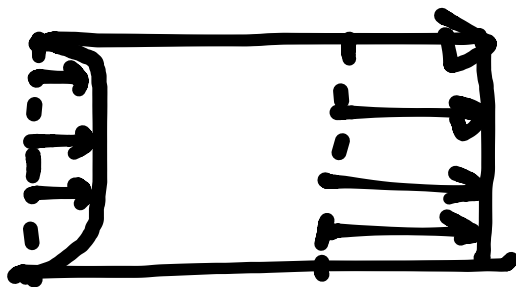


$$v_x = -K \frac{dp}{dx} = -K C_1$$

$$v_x = K \frac{(p_1 - p_2)}{h} \quad \text{Flux}$$

Note that  $v_x$  is constant. Therefore,  $\frac{v_x}{f_x} = \frac{v_x}{\epsilon}$  is also a constant. In other

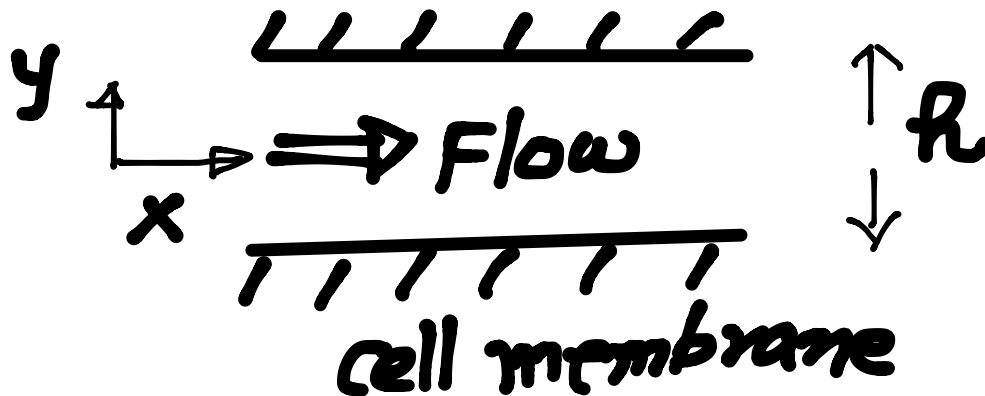
the resistance to flow near the wall is much greater than the viscous resistance. Therefore, if you plot the velocity profile within a pore, you will obtain a flat velocity profile with a steep gradient near the wall. Therefore, Darcy's law does NOT satisfy NO SLIP condition. Darcy's law is valid only for dense porous materials or for low values of hydraulic conductivity  $K$ .



Darcy's law is applicable only when the porous medium is dense, i.e. The permeability is low. When the resistance of fluid flow is not large, the approximation of no slip at the wall breaks down. Consequently, one cannot use Darcy's law. The equation of motion has to be modified as

$$\underbrace{\mu \nabla^2 \vec{v}}_{\text{Viscous resistance}} - \frac{1}{K} \vec{v} - \nabla p = 0$$

Let us examine interstitial flow through cells. The two cell membranes are separated by  $h$  (see schematic below).



$$\frac{\partial v_x}{\partial x} = 0 \quad (1)$$

$$\frac{\partial p}{\partial y} = 0 \quad (2)$$

Lubrication approximation

$$\mu \frac{\partial^2 v_x}{\partial y^2} - \frac{\mu}{R} v_x - \frac{\partial p}{\partial x} = 0$$

or,  $\underbrace{\mu \frac{\partial^2 v_x}{\partial y^2} - \frac{\mu}{R} v_x}_{\text{function of } y} = \frac{\partial p}{\partial x}$  (3)

(3a)

$\underbrace{\text{function of } x}_{\text{BRINKMAN EQN.}}$

$$\therefore \mu \frac{\partial^2 v_x}{\partial y^2} - \frac{\mu}{R} v_x$$

$$= \frac{\partial p}{\partial x} = B$$

*constant*

$$\therefore \frac{d^2 V_x}{dy^2} - \frac{1}{R} V_x = \frac{B}{\mu} \quad (4)$$

The solution to the above equation is

$$V_x = C_1 \sinh\left(\frac{y}{\sqrt{R}}\right) + C_2 \cosh\left(\frac{y}{\sqrt{R}}\right) - \frac{R}{\mu} B \quad (5)$$

$$\text{B.C.:-} \quad y=0 \quad \frac{dV_x}{dy} = 0 \quad (6)$$

$$y = h \quad v_x = 0 \quad (7)$$

$$v_x = -\frac{R}{\mu} B \left[ 1 - \frac{\cosh(y/\sqrt{R})}{\cosh(h/2\sqrt{R})} \right] \quad (8)$$

One can evaluate the volumetric flow rate per unit cross sectional area from

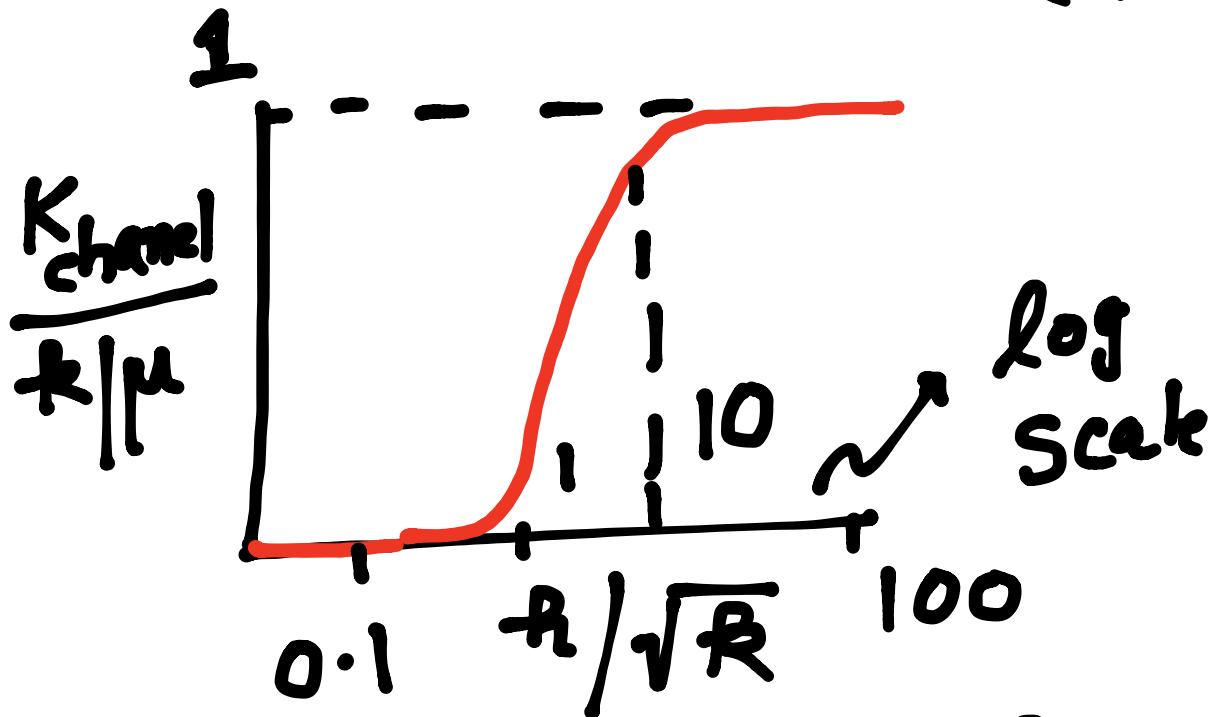
$$q = \frac{1}{h} \int_{-h/2}^{h/2} v_x dy$$

$$= -\frac{R}{\mu} B \left[ 1 - \frac{2\sqrt{R}}{h} \tanh\left(\frac{h}{2\sqrt{R}}\right) \right]$$

The effective hydraulic conductivity is defined as the ratio of fluid flux to pressure gradient and is given by



$$K_{\text{channel}} = \frac{k}{\mu} \left[ 1 - \frac{2\sqrt{k}}{h} \tanh\left(\frac{h}{2\sqrt{k}}\right) \right] \quad (9)$$



If  $\frac{h}{\sqrt{k}} > 10$ ,  $K_{\text{channel}} \approx \frac{k}{\mu}$

Darcy's Law  
Valid