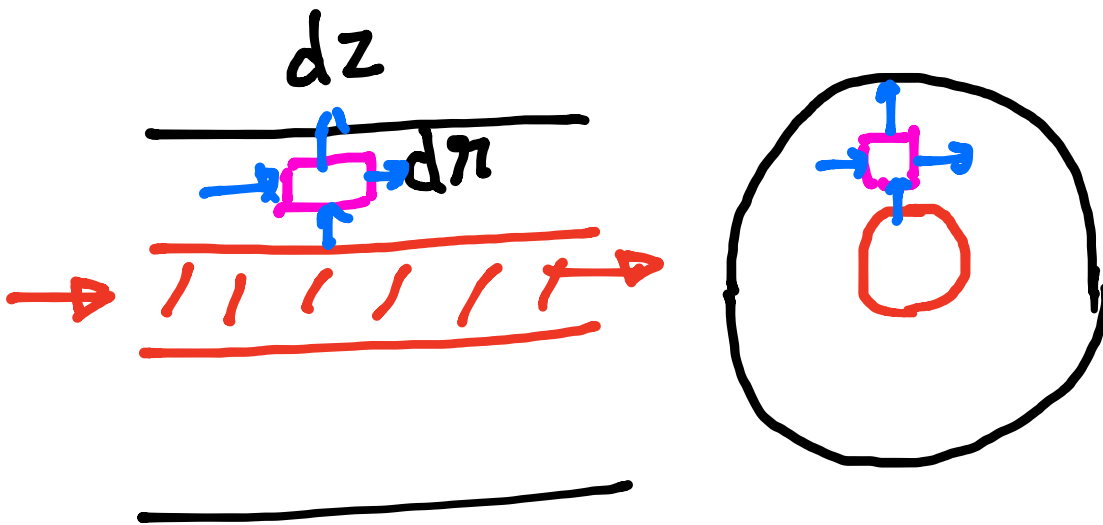


1. The schematic of capillary with surrounding tissue is shown below.



(a) A mass balance for the volume element gives,

$$\text{Rate in at } r = -D \frac{\partial C}{\partial r} \bigg|_r 2\pi r dz$$

$$\text{Rate out at } r+dr = -D \frac{\partial C}{\partial r} \bigg|_{r+dr} 2\pi (r+dr) dz$$

$$\text{Rate in at } z = -D \frac{\partial C}{\partial z} \bigg|_z 2\pi r dr$$

$$\text{Rate out at } z+dz = -D \frac{\partial C}{\partial z} \bigg|_{z+dz} 2\pi r dr$$

$$\text{Rate of consumption} = 2\pi r dr dz R_{O_2}$$

At steady state, rate in - rate out = rate of consumption. Dividing this equation by

$2\pi r dr dz$ and taking the limit as dr and dz tending to zero, one obtains,

$$\frac{D}{r} \frac{\partial}{\partial r} \left(r \frac{\partial C}{\partial r} \right) + D \frac{\partial^2 C}{\partial z^2} = R_{O_2} \quad (1)$$

(b) Boundary conditions,

$$r = R_c \quad C(R_c, z) = C_{\text{blood}}(z) \quad (2)$$

$$r = R_o, \quad -D \frac{\partial C}{\partial r} = 0 \quad \forall z \quad (3)$$

$$z = 0 \quad C(R_c, 0) = C_{\text{blood}, 0} \quad (4)$$

$$z = L \quad \left. \frac{\partial C}{\partial z} \right|_{R_c, L} = 0 \quad (5)$$

(c) Neglecting axial diffusion, eq. (1) becomes

$$\frac{D}{r} \frac{d}{dr} \left(r \frac{dc}{dr} \right) = R_{O_2} \quad (6)$$

case (i)

$$R_{O_2} = \frac{R_{\text{max}} C}{K_M + C}$$

$$K_M \ll C \Rightarrow R_{O_2} = R_{\text{max}}$$

For a fixed axial distance of L_1 , we get,

$$\frac{D}{r} \frac{d}{dr} \left(r \frac{dc}{dr} \right) = R_{\text{max}} \quad (7)$$

with the boundary conditions

$$r = R_c \quad C(R_c, L_1) = C_{\text{blood}}(L_1) \quad (8)$$

$$r = R_o \quad -D \frac{dC(L_1, r)}{dr} = 0 \quad (9)$$

Following the class notes, the solution is given by

$$c(r, L_1) = c_{\text{blood}}(L_1) + \frac{R_{\max} R_0^2}{2D} \left[\frac{1}{2} \left\{ \left(\frac{r}{R_0} \right)^2 - \left(\frac{R_c}{R_0} \right)^2 \right\} - \ln \left(\frac{r}{R_c} \right) \right] \quad (10)$$

case (ii) $K_M \gg C$

$$\therefore R_0 = \frac{R_{\max} C}{K_M}$$

For a fixed L_1 , we get,

$$\frac{D}{r} \frac{d}{dr} \left(r \frac{dc}{dr} \right) = \frac{R_{\max} C}{K_M} \quad (11)$$

with the same boundary conditions (8) and (9)

Defining $R^* = \frac{R_{\max}}{K_M D}$, the above equation can be written as

$$r^2 c'' + r c' + R^* r^2 c = 0 \quad (12)$$

Defining $y = R^{1/2} \frac{r}{R_0}$, the above equation can be recast as

$$y^2 \frac{d^2 c}{dy^2} + y \frac{dc}{dy} + y^2 c = 0 \quad (13)$$

The solution is given by

$$c(L_1, y) = J_0(y) \quad (14)$$

The boundary conditions are

$$y = R^{1/2} \frac{r}{R_0} \quad c(L_1, y) = c_{\text{blood}} \quad (15)$$

$$y = R^{1/2} \frac{r}{R_0} \quad \frac{dc}{dy}(L_1, y) = 0 \quad (16)$$

Since $J_0'(y) = J_1(y)$ from boundary condition (16), the solution can be written as,

$$y = \sum_{n=1}^{\infty} A_n J_0\left(\frac{\lambda_n}{R_c^{1/2}} y\right)$$

where λ_n are zeroes of $J_1(y)$ from boundary condition (16). From boundary condition (15), one obtains

$$C_{\text{blood}}(L_1) = \sum_{n=1}^{\infty} A_n J_0\left(\frac{\lambda_n}{R_c^{1/2}} y\right) \quad (17)$$

The coefficients A_n can be determined from orthogonality of Bessel function.

(d) The rate of consumption of oxygen at axial distance L_1 is given by

$$R(L_1) = \int_{R_c}^{R_0} 2\pi r R_{O_2} \{C(r, L_1)\} dr \quad (18)$$

one needs to substitute the solution of oxygen concentration $C(r, L_1)$ for the two cases in the above equation to determine the rate of oxygen consumption.

(e) A mass balance for oxygen in the capillary between z and $z+dz$ gives,

$$\text{Rate in at } z = \pi R_c^2 v C_{\text{blood}}(z)$$

$$\text{Rate out at } z+dz = \pi R_c^2 v C_{\text{blood}}(z+dz)$$

Rate of consumption = $2\pi R_c dz R(z)$, where $R(z)$ is given by eq. (18) evaluated at z (instead of L_1).

Dividing the mass balance equation by dz and simplifying, one obtains

$$v R_c \frac{dC_{\text{blood}}}{dz} = -2 R(z) \quad (19)$$

which can be solved to give the following

$$C_{\text{blood}}(z) = C_{\text{blood}}(0) - \frac{2}{v R_c} \int_0^z R(z') dz' \quad (20)$$

3. a. For steady state one dimensional transport gives



$$\frac{dN_{iz}}{dz} = 0, \quad i=1,2$$

$$\frac{dN_{Na^+}}{dz} = 0; \quad \frac{dN_{Cl^-}}{dz} = 0.$$

b. Since there is potential difference across the membrane, the expressions for flux for cation and anion are given by

$$N_+ = -D_+ \left[\frac{dc_+}{dz} + \frac{z_+ c_+ F}{RT} \frac{d\psi}{dz} \right]$$

$$N_- = -D_- \left[\frac{dc_-}{dz} + \frac{z_- c_- F}{RT} \frac{d\psi}{dz} \right]$$

c. Electrical neutrality implies

$$z_+ N_+ + z_- N_- = 0$$

$$\text{or, } z_+ N_+ = -z_- N_-$$

d. Applying electrical neutrality to the flux equation, one obtains

$$z_+ D_+ \left[\frac{dc_+}{dz} + \frac{z_+ c_+ F}{RT} \frac{d\psi}{dz} \right] = -z_- D_- \left[\frac{dc_-}{dz} + \frac{z_- c_- F}{RT} \frac{d\psi}{dz} \right]$$

simplifying the above equation, we get

$$\frac{d\psi}{dz} = - \left(\frac{D_+ - D_-}{z_+ D_+ - z_- D_-} \right) \frac{RT}{F} \frac{1}{c_+} \frac{dc_+}{dz}$$

For NaCl, $z_+ = 1$; $z_- = -1$

Integrating the above equation, one obtains

$$\psi(L) - \psi(0) = \left(\frac{D_+ - D_-}{D_+ + D_-} \right) \frac{RT}{F} \ln \left(\frac{c_0}{c_L} \right)$$

Substitute for D_+ , D_- , c_0 and c_L to calculate the potential difference