2.4 RLC Circuit Model



• Sum the voltage drops:

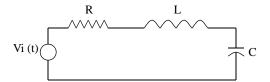
$$V_{in} - V_R - V_L - V_C = 0$$

• Use table for relationships:

$$V_{in} - Ri - Ldi/dt - 1/C \int i dt = 0$$

• Substitute:

i = dq/dt q: electric charge [coulomb]



$$L\frac{d^2q}{dt^2} + R\frac{dq}{dt} + \frac{1}{C}q = V_{in}$$

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2.4 RLC, Capacitor voltage as output



• Using table again:

$$V_c = 1/C \int i dt = q/C$$

• Final differential equation:

$$LC\frac{d^2V_C}{dt^2} + RC\frac{dV_C}{dt} + V_C = V_{in}$$

• Circuit and equation is easily verified in the lab. Remember the basic form.

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2.4 Important Modeling Point: Analogies



• Notice the RLC and MBK equations:

$$L\frac{d^2q}{dt^2} + R\frac{dq}{dt} + \frac{1}{C}q = V_{in} \qquad m\frac{d^2y}{dt^2} + b\frac{dy}{dt} + k \cdot y = F$$

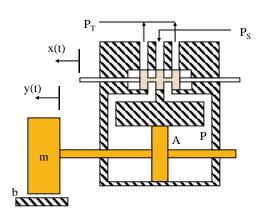
- Same analogies made in table of energy relationships (i.e. mass = inductor)
- Two energy storage devices, both 2nd order systems.
- It is important to feel comfortable with modeling different system types.

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2.4 Hydraulic Positioning Example



- Force Amplifier
 - > No feedback for the case shown here.
- Assume basic linear equations. Later sections derive them.
- Model includes several domains.



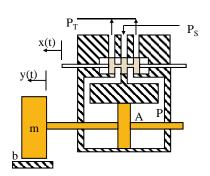
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2.4 Hydraulic Servo - Equations



- Valve flow: Q = (dQ/dx) x (dQ/dP)
- $P = K_x X K_p P$

- Piston flow: Q = A dy/dt
- Force balance: $\sum F = m y'' = P A b y'$
 - ➤ P = load pressure



Solve valve equation for P:

$$P = -Q/K_P + (K_x/K_P) x$$

Substitute into force balance:

$$\sum F = m y'' = (-Q/K_P + (K_x/K_P) x) A - b dy/dt$$

Eliminate Q with piston flow equation:

 $m y'' = (-A y'/K_p + (K_x/K_p) x) A - b y'$

Combine inputs and outputs:

$$m\frac{d^2y}{dt^2} + \left(\frac{A^2}{K_p} + b\right)\frac{dy}{dt} = \frac{AK_x}{K_p}x$$

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2.4 Hydraulic Servo - Summary



- Equation of motion:
- Type 1 system:
 - ➤ y is not present
 - > x must be integrated to get y
- Results in motion whenever $x \neq 0$
- Already has been linearized
 - ➤ About what point and how?
 - > We will soon see

$$m\frac{d^2y}{dt^2} + \left(\frac{A}{K_P} + b\right)\frac{dy}{dt} = \frac{AK_x}{K_P}x$$

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2.4 Hydraulic Servo - Assumptions



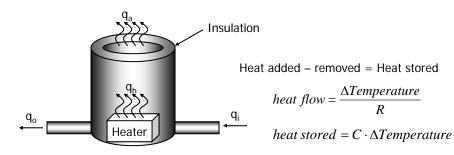
- Linearized about some point.
- Spool dynamics and mass ignored
 Would require additional force balance
- Mass-less fluid
- Incompressible fluid
- Without these assumptions, result would be a sixth order non-linear differential equation.

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2.4 Thermal System Example



- Common home water heater model
 - > Assume uniform water temperature inside the heater.
 - ➤ See textbook pg 55



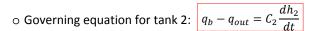
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2.4 Liquid Level System Example

- Common system in many industries
 - ➤ Simplified case of hydraulic systems
 - Flow in flow out = Rate of change in stored volume

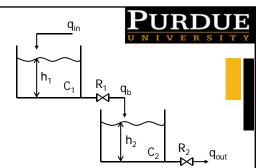
$$q_{in} - q_{out} = C \frac{dh}{dt}$$

O Governing equation for tank 1: $q_{in} - q_b = C_1 \frac{dh_1}{dt}$



$$q_b = \frac{h_1}{R_1} \qquad q_{out} = \frac{h_2}{R_2}$$

$$R_1 C_1 \frac{dh_1}{dt} + h_1 = R_1 q_i$$
 $R_2 C_2 \frac{dh_2}{dt} + h_2 = \frac{R_2}{R_1} h_1$

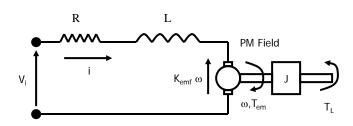


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2.4 DC Permanent Magnet Motor Model



- o R = armature resistance
- o L = armature inductance
- o K_{emf} = back emf constant
- o K_T = torque constant
- o V_i = applied voltage
- o i = armature current
- o T_{em} = electromagnetic torque
- \circ J = motor and load inertia
- \circ ω = rotor rotational velocity



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2.4 DC Permanent Magnet Motor Model



- ➤ Voltage Drops
 - Around loop = 0
- Newton' Law
 - o Summation of Torque

$$L\frac{di}{dt} = V_i - R \cdot i - K_{emf} \cdot \omega \qquad \qquad J\frac{d\omega}{dt} = T_{em} - T_L = K_T \cdot i - T_L$$

$$J\frac{d\omega}{dt} = T_{em} - T_L = K_T \cdot i - T_L$$

Variables are coupled via back emf, State Space is the easiest:

$$\begin{bmatrix} i \\ \dot{\omega} \end{bmatrix} = \begin{bmatrix} -\frac{R}{L} & -\frac{K_{emf}}{L} \\ +\frac{K_{T}}{J} & 0 \end{bmatrix} \begin{bmatrix} i \\ \omega \end{bmatrix} + \begin{bmatrix} +\frac{1}{L} & 0 \\ 0 & +\frac{1}{J} \end{bmatrix} \begin{bmatrix} V_{in} \\ T_{L} \end{bmatrix}$$

2.4 DC Motor Summary



- Same basics applied as before
- Two domains represented
 - > Electrical and Mechanical
 - \triangleright Both equations formed by Σ efforts = 0
- Larger systems can usually be broken down into the basic physical relationships illustrated in the table.

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