## Sterilization Homework

**ABE 557** 

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## Problem 5.2-3: Unsteady-State Heating of a Stirred Tank

A vessel is filled with 0.0283 m<sup>3</sup> of water initially at 288.8 K. The vessel, which is well stirred, is suddenly immersed in a steam bath held at 377.6 K. The overall heat transfer coefficient U between the steam and water is 1136 W/m<sup>2</sup>.K and the area is 0.372 m<sup>2</sup>. Neglecting the heat capacity of the walls and agitator, calculate the time in hours to heat the water to 338.7 K. [Hint: Since the water is well-stirred, its temperature is uniform. Show that Eq. 5.2-3 holds by starting with Eq. 5.2-1).]

```
volume = 0.0283; % units = m^3
To_water = 288.8; % units = K
T_steam = 377.6; % units = K
U = 1136; % units = W/m^2.K
area = 0.372; % units = m^2
Tf_water = 338.7; % units = K
```

### Equation 5.2-1

$$UA(T_{\infty} - T)dt = c_n \rho VdT$$

$$\frac{\mathrm{dt}}{c_n \rho V} = \frac{\mathrm{dT}}{\mathrm{UA}(T_{\infty} - T)}$$

$$\frac{t}{c_p \rho V} = -\frac{1}{\text{UA}} \ln \left( \frac{|T_{\infty} - T_f|}{|T_o - T_{\infty}|} \right)$$

$$t = -\frac{1}{\text{UA}} \ln \left( \frac{|T_{\infty} - T_f|}{|T_{\rho} - T_{\infty}|} \right) c_p \rho V$$

```
cp_water = 4.179; % units = J/g.K
rho_water = 997; % units = kg/m^3
rho_water = rho_water * 1000; % units = kg / m^3 * g / kg = g / m^3

t = (-1 / (U * area)) * cp_water * rho_water * volume * log(abs((T_steam - Tf_water)/(To_water t = t / 3600; % units = s * h / s = h
fprintf('The time required to heat the water from %.1f K to %.1f K is %.2f hours.',To_water,Tf_
```

The time required to heat the water from 288.8 K to 338.7 K is 0.06 hours.

# **Problem 5.4-5: Cooling Beef with Convective Resistance**

A large slab of beef is 45.7 mm thick and is at an initial uniform temperature of 37.78 degrees C. It is being chilled at the front surface in a chilled air blast at -1.11 degrees C with a convective heat-transfer coefficient of  $h = 38.0 \text{ W/m}^2\text{.K}$ . The rear face of the meat is insulated. The thermal conductivity of the beef is k = 0.498 W/m.K and alpha = 4.464e-4 m^2/h. Using a numerical method with five slices and M = 4.0, calculate the temperature profile after 0.27 h.

```
x = 45.7; % units = mm
x = x / 1000; % units = mm * m / mm = m
Ti_meat = 37.78 + 273.17; % units = K
T_air = -1.11+ 273.15; % units = K
h = 38.0; % W/m^2.K
k = 0.498; % W/m.K
alpha = 4.464e-4; % m^2/h
m = 4.0;
slices = 5;
del_x = x / slices; % units = m
t = 0.27; % units = h
```

## Equation 5.4-2: for n = 2, 3, 4

$$_{t+\Delta t}T_n = \frac{1}{M} \left( _t T_{n+1} + (M-2)_t T_n + _t T_{n-1} \right)$$

## Equation 5.4-3

$$M = \frac{\Delta x^2}{\alpha \Delta t}$$

$$\Delta t = \frac{M\alpha}{\Delta x^2}$$

## Equation 5.4-7: for n = 1

$$_{t+\Delta t}T_{1} = \frac{1}{M} \left( 2N_{t}T_{a} + \left( M - (2N+2)_{t}T_{1} + 2_{t}T_{2} \right) \right)$$

### Equation 5.4-8

$$N = \frac{h\Delta x}{k}$$

### Equation 5.4-10: for insulated face, n = 5

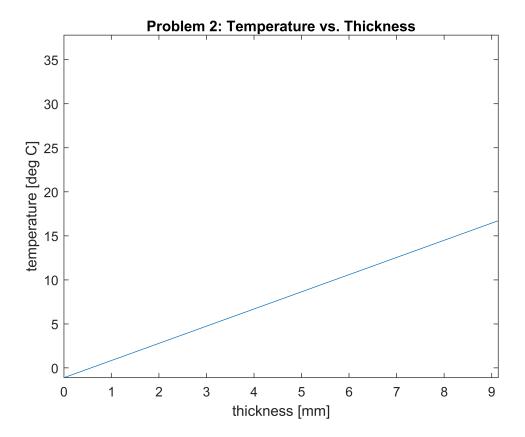
$$_{t+\Delta t}T_{f} = \frac{1}{M} \left( (M-2)_{t}T_{f} + 2_{t}T_{f-1} \right)$$

```
t_T1 = Ti_meat;
t_T2 = Ti_meat;
t_T3 = Ti_meat;
t_T4 = Ti_meat;
t_T5 = Ti_meat;
```

```
del_t = (del_x ^ 2) / (m * alpha); % units = h
N = h * del x / k;
while ti < t
             ti = ti + del t;
             tdelt_T1 = (1/m) * (2 * N * T_air + (m - (2 * N + 2)) * t_T1 + 2 * t_T2);
             tdelt T2 = (1/m) * (t T3 + (m - 2) * t T2 + t T1);
             tdelt_T3 = (1/m) * (t_T4 + (m - 2) * t_T3 + t_T2);
             tdelt_T4 = (1/m) * (t_T5 + (m - 2) * t_T4 + t_T3);
             tdelt_{T5} = (1/m) * ((m - 2) * t_{T5} + 2 * t_{T4});
             t T1 = tdelt T1;
             t_T2 = tdelt_T2;
             t_T3 = tdelt_T3;
             t T4 = tdelt T4;
             t_T5 = tdelt_T5;
end
x = [0, 1 * del_x * 1000, 2 * del_x * 1000, 3 * del_x * 1000, 4 * del_x * 1000, 5 
T = [T_air - 273.15, t_T1 - 273.15, t_T2 - 273.15, t_T3 - 273.15, t_T4 - 273.15, t_T5 - 273.15]
fprintf('The temperature at node 1 is %.2f, at node 2 is %.2f, at node 3 is %.2f, at node 4 is
 The temperature at node 1 is 16.72, at node 2 is 27.59, at node 3 is 34.02, at node 4 is 36.79, and at node 5 is
plot(x,T);
ylim([T_air - 273.15,Ti_meat - 273.15]);
```

xlim([0, del\_x \* 1000]);
xlabel('thickness [mm]')
ylabel('temperature [deg C]')

title('Problem 2: Temperature vs. Thickness')



# **Problem 9.12-5: Process Time and Numerical Integration**

The following time-temperature data were obtained for the heating, holding, and cooling of a canned food product in a retort, the temperature being measured in the center of the can. The F0 value used is 2.60 min and z is 10 deg C/18 deg F. Calculate the F0 value for this process and determine if the thermal processing is adequate. Use SI and English units.

```
t = [0, 20, 40, 60, 80, 90, 100]; % units = min
T_c = [43.3, 79.3, 96.1, 108.9, 111.1, 107.2, 71.1]; % units = deg C
T_f = [110, 165, 205, 228, 232, 225, 160]; % units = deg F
F0 = 2.60; % units = min
z_c = 10; % units = deg C
z_f = 18; % units = deg F
```

### **Equation 9.12-16**

$$F_0 = \int_{t=0}^{t=t} 10^{\frac{T-250}{z}} dt$$
 (English Units)

$$F_0 = \int_{t=0}^{t=t} 10^{\frac{T-121.1}{z}} dt$$
 (SI Units)

```
 F0_f = ((10^{(T_f(1) - 250)/z_f}) + 10^{(T_f(2) - 250)/z_f})/2) * (t(2)-t(1))) + ((10^{(T_f(2) - 50)/z_f})/2) * (t(2)-t(2))) + ((10^{(T_f(2) - 50)/z_f})/2) * (t(2)-t(2)) *
```

The F0 value in English units is 4.51 mins and in SI units is 4.52 mins.

```
if ((F0_f + F0_c)/2) >= F0
    fprintf('Therefore, the thermal process is adequate.')
else
    fprintf('Therefore the thermal process is inadequate.')
end
```

Therefore, the thermal process is adequate.

# **Problem 9.12-6: Sterility Level of Fermentation Medium**

The aqueous medium in a fermentor is being sterilized and the time-temperature data obtained are as follows. The reaction velocity constant k in min $^-1$  for \_\_\_ can be represented as (see below) where T = K. The contamination level N0 = 1e12 spores. Calculate the sterility level N at the end and V.

```
t = [0, 10, 20, 25, 30, 35]; % units = min
T_c = [100, 110, 120, 120, 110, 100]; % units = deg C
T_k = T_c + 273.15; % units = K
k = 7.94e38 * exp((-68.7e3) ./ (1.987 .* T_k)); % units = min^-1
N0 = 1e12; % units = spores
```

#### Equation 9.12-1

$$\frac{dN}{dt} = -kN$$

#### Equation 9.12-3

$$\ln \frac{N_0}{N} = kt$$

#### Equation 9.12-4

$$N = N_0 e^{-kt}$$

```
N_{final} = N0 * exp(-k(6) * t(6)); % units = spores
```

### **Equation 9.12-17**

$$\nabla = \ln \frac{N_0}{N}$$

```
V = log(N0/N_final);
fprintf("The final sterility level is %.2d and the V is %.2f.", N_final, V)
```

The final sterility level is 2.02e+11 and the V is 1.60.

### Problem 9.12-7: Time for Pasteurization of Milk

Calculate the time in min at 62.8 degrees C for pasteurization of milk. The F0 value to be used at 65.6 degrees C is 9.0 min. The z value is 5 degrees C.

```
T = 62.8; % units = deg C
F0 = 9.0; % units = minutes
T1 = 65.6; % units = deg C
z = 5; % units = deg C
```

### **Equation 9.12-19**

$$F_0 = t10^{\frac{T - T_1}{z}}$$

$$t = \frac{F_0}{10^{\frac{T-T_1}{z}}}$$

```
t = F0 / (10 ^ ((T-T1)/z)); % units = minutes
fprintf('The time to pasteurize is %.2f min.',t)
```

The time to pasteurize is 32.68 min.

# Rederive Equation 5.4-20 for a cylinder with convection not ignoring cp.

### **Equation 5.4-20**

$$_{t+\Delta t}T_{n}=\frac{1}{M}\left(\frac{2n+1}{2n}_{t}T_{n+1}+(M-2)_{t}T_{n}+\frac{2n-1}{2n}_{t}T_{n-1}\right)$$

## Equation 5.4-19

$$\frac{k\left[2\pi\left(n+\frac{1}{2}\right)\Delta x\right]}{\Delta x}\left({}_{t}T_{n+1}-{}_{t}T_{n}\right)-\frac{k\left[2\pi\left(n-\frac{1}{2}\right)\Delta x\right]}{\Delta x}\left({}_{t}T_{n}-{}_{t}T_{n-1}\right)=\frac{2\pi\Delta x^{2}\rho c_{p}}{\Delta t}\left({}_{t+\Delta t}T_{n}-{}_{t}T_{n}\right)$$

## Adding Convection assuming only radial motion

$$\frac{(k+h)\left[2\pi\left(n+\frac{1}{2}\right)\Delta x\right]}{\Delta x}\left({}_{t}T_{n+1}-{}_{t}T_{n}\right)-\frac{(k+h)\left[2\pi\left(n-\frac{1}{2}\right)\Delta x\right]}{\Delta x}\left({}_{t}T_{n}-{}_{t}T_{n-1}\right)=\frac{2\pi\Delta x^{2}\rho c_{p}}{\Delta t}\left({}_{t+\Delta t}T_{n}-{}_{t}T_{n}\right)$$

$$(k+h)\left[\left(n+\frac{1}{2}\right)\right]\left({}_{t}T_{n+1}-{}_{t}T_{n}\right)-(k+h)\left[\left(n-\frac{1}{2}\right)\right]\left({}_{t}T_{n}-{}_{t}T_{n-1}\right)=\frac{\Delta x^{2}\rho c_{p}}{\Delta t}\left({}_{t+\Delta t}T_{n}-{}_{t}T_{n}\right)$$

$$\frac{(k+h)\Delta t}{\Delta x^2\rho c_p}\left(\left[\left(n+\frac{1}{2}\right)\right]\left({}_{t}T_{n+1}-{}_{t}T_{n}\right)-\left[\left(n-\frac{1}{2}\right)\right]\left({}_{t}T_{n}-{}_{t}T_{n-1}\right)\right)=\left({}_{t+\Delta t}T_{n}-{}_{t}T_{n}\right)$$

$$\begin{split} &_{t+\Delta t}T_{n} = \frac{(k+h)\Delta t}{\Delta x^{2}\rho c_{p}} \left( \left( \frac{2n+1}{2n} \right)_{t}T_{n+1} - \left( \frac{4n^{2}-1}{4n^{2}} \right)_{t}T_{n} + \left( \frac{2n-1}{2n} \right)_{t}T_{n-1} \right) + {}_{t}T_{n} \\ &_{t+\Delta t}T_{n} = \frac{(k+h)\Delta t}{\Delta x^{2}\rho c_{p}} \left( \left( \frac{2n+1}{2n} \right)_{t}T_{n+1} + \left( \frac{\Delta x^{2}\rho c_{p}}{(k+h)\Delta t} - \frac{4n^{2}-1}{4n^{2}} \right)_{t}T_{n} + \left( \frac{2n-1}{2n} \right)_{t}T_{n-1} \right) \\ &_{t+\Delta t}T_{n} = \left( \frac{1}{M} + \frac{h\Delta t}{\Delta x^{2}\rho c_{p}} \right) \left( \left( \frac{2n+1}{2n} \right)_{t}T_{n+1} + \left( M + \frac{\Delta x^{2}\rho c_{p}}{h\Delta t} - \frac{4n^{2}-1}{4n^{2}} \right)_{t}T_{n} + \left( \frac{2n-1}{2n} \right)_{t}T_{n-1} \right) \\ &_{t+\Delta t}T_{n} = \left( \frac{1}{M} + \frac{h\Delta t}{\Delta x^{2}\rho c_{p}} \right) \left( \left( \frac{2n+1}{2n} \right)_{t}T_{n+1} + \left( M + \frac{\Delta x^{2}\rho c_{p}}{h\Delta t} - 2 \right)_{t}T_{n} + \left( \frac{2n-1}{2n} \right)_{t}T_{n-1} \right) \end{split}$$