
Fermentation Homework

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Problem 1

The air supply to a fermenter was turned off for a short period of time and then restarted. A value for C^* of 7.3 mg/l has been determined for the operating conditions. Use the tabular measurements of dissolved oxygen (DO) values to estimate the oxygen uptake rate and kLa of this system.

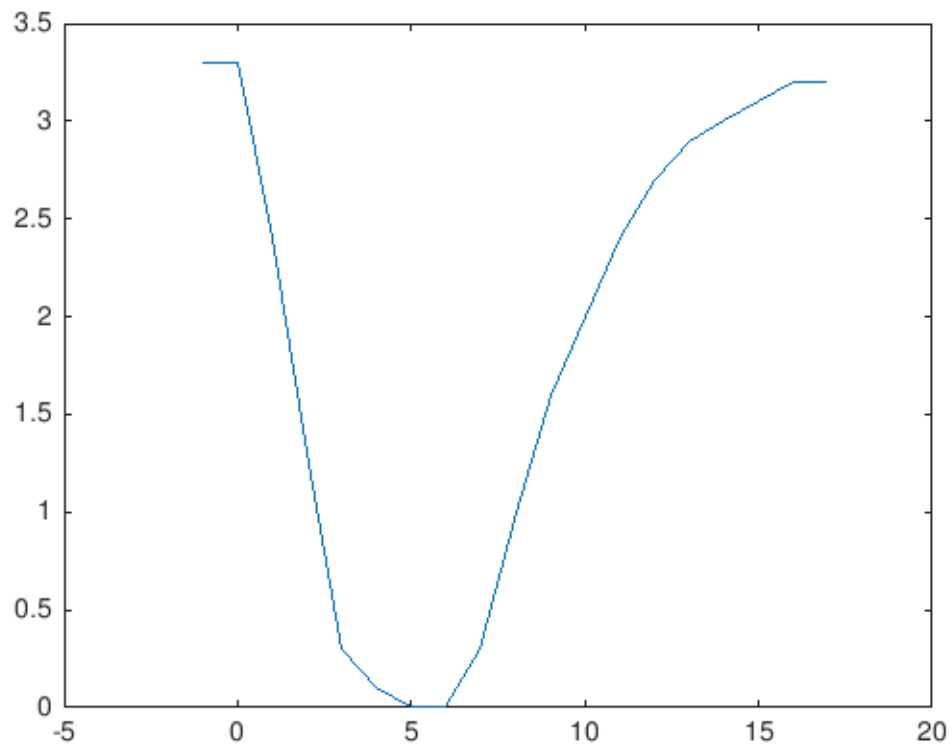
```
time = -1:1:17; % units = minutes
DO = [3.3, 3.3, 2.4, 1.3, 0.3, 0.1, 0.0, 0.0, 0.3, 1.0, 1.6, 2.0, 2.4,
      2.7, 2.9, 3.0, 3.1, 3.2, 3.2]; % units = mg/l
c_star = 7.3; % units = mg/l
```

Equations:

- $dcl/dt = OTR - OUR$
- $OTR = kLa * (c_star - cl)$
- $OUR = qo2 * X$

Plot DO vs. time

```
plot(time, DO)
```



The negative slope of the curve represents the OUR (oxygen uptake rate). Slope from $t = 0$ to $t = 3$ minutes used to calculate OUR.

```
OUR = (DO(5) - DO(2)) / (time(5) - time(2)) * -1; % units = mg/l-min
fprintf('The oxygen uptake rate is %.2f mg/l-min.\n',OUR);
```

The oxygen uptake rate is 1.00 mg/l-min.

The positive slope of the curve represents the OTR - OUR. Substituting the OTR equation into the dc_l/dt equation and solving for kla gives:

- $kla = (dc_l/dt + OUR) / (c_{star} - c_l)$

To solve for kla , I will assume a constant positive slope between the times $t = 10$ to $t = 12$ minutes and use the c_l from $t = 11$ minutes.

```
dcldt = (DO(14) - DO(12)) / (time(14) - time(12)); % units = mg/l-min
cl = DO(13); % units = mg/l
kla = (dcldt + OUR) / (c_star - cl); % units = min^-1
```

Converting the units of kla from min^{-1} to hour^{-1}

```
kla = kla * 60; % units = min^-1 * min/hour = hour^-1
fprintf('The kla is %.2f h^-1.\n',kla);
```

The kla is 16.53 h⁻¹.

Problem 2

A value of $kla = 30 \text{ h}^{-1}$ has been determined for a fermenter at its maximum practical agitator rotational speed and with air being sparged at $0.5 \text{ l gas/l reactor volume-min}$. *E. coli* with a qO_2 of $10 \text{ mmol O}_2/\text{g-dry wt-h}$ are to be cultured. The critical dissolved oxygen concentration is 0.2 mg/l . The solubility of oxygen from air in the fermentation broth is 7.3 mg/l at 30 deg C .

- Part a: What maximum concentration of *E. coli* can be sustained in this fermenter under aerobic conditions?
- Part b: What concentration could be maintained if pure oxygen was used to sparge the reactor?

```
kla = 30; % units = h^-1
air = 0.5; % units = l gas / l reactor volume-min
qo2 = 10; % units = mmol O2 / g-dry wt-h
crit = 0.2; % units = mg/l
o2sol = 7.3; % units = mg/l
t = 30; % units = deg C
```

Part a

Equations:

- $OUR = qo_2 * X = kla * (c_{star} - cl)$

Qo_2 and kla are given. C_{star} is the solubility of oxygen and the cl is the critical oxygen concentration. Rearranging to solve for X :

- $X = kla * (c_{star} - cl) / qo_2$

Substituting in given values:

- $X = kla * (o2sol - crit) / qo_2$

convert qo_2 to use mg oxygen instead of mmol oxygen

```
qo2 = qo2 * 15.999; % units = mg O2 / g-dry wt-h
X = kla * (o2sol - crit) / qo2; % units = mg oxygen * g-dry wt E. coli
    * h / h * mg oxygen * l = g-dry wt E. coli/l
fprintf('The maximum concentration of E. coli using air is %.2f g-dry
    wt E. coli / l.\n',X);
```

The maximum concentration of *E. coli* using air is $1.33 \text{ g-dry wt E. coli / l}$.

Part b

Equations:

Air is 21% oxygen, so using pure oxygen would increase the partial pressure of oxygen from $0.21 * \text{total pressure}$ to $1 * \text{total pressure}$. Assuming the pressure of the sparged gas is 1 atm , the new c_{star} is:

```
c_star = o2sol * 1 / 0.21; % units = mg/l * atm / atm = mg/l
X = kla * (c_star - crit) / qo2; % units = mg oxygen * g-dry wt E.
    coli * h / h * mg oxygen * l = g-dry wt E. coli/l
```

```
fprintf('The maximum concentration of E. coli using pure oxygen is
%.2f g-dry wt E. coli / l.\n',X);
```

The maximum concentration of E. coli using pure oxygen is 6.48 g-dry wt E. coli / l.

Problem 3

- Part a: Estimate the required cooling-water flow rate for a 100,000-l fermenter with an 80,000-l working volume when the rate of oxygen consumption is 100 mmol O₂/l-h. The desired operating temperature is 35 deg C. A cooling coil is to be used. The minimum allowable temperature differential between the cooling water and the broth is 5 deg C. Cooling water is available at 15 deg C. The heat capacities of the broth and the cooling water are roughly equal.
- Part b: Estimate the required length of the cooling coil if the coil has a 2.5-cm diameter and the overall heat transfer coefficient is 1420 J/s-m²-deg C.

```
vol = 100000; % units = l
work_vol = 80000; % units = l
qo2 = 100; % units = mmol O2/l-h.
t_desired = 35; % units = deg C
min_deltat = 5; % units = deg C
t_water = 15; % units = deg C
c_water = 1.0; % units = Kcal/kg-deg C
c_broth = c_water; % assumption from part a
d = 2.5; % units = cm
h = 1420; % units = J/s-m^2-deg C
```

Part a

Equations:

- $Q = 0.12 * qo2$ (Equation 6.29 from text)

```
Q = 0.12 * qo2; % units = Kcal/l-h
```

Multiply by working volume of the tank to get the heat produced by the entire tank, not just 1 L.

```
Q = Q * work_vol; % units = Kcal/h
```

- $Q = m * cp * \Delta T$

Rearranging to solve for mass flow rate:

- $m = Q / (cp * \Delta T)$

Find the delta T of the water:

- $\Delta T = t_{final} - t_{initial}$
- $t_{final} = t_{broth} - \min_{\Delta T}$

```
deltaT = (t_desired - min_deltat) - t_water; % units = deg C
```

Solve for mass flow rate:

```
m = Q / (c_water * deltaT); % units = Kcal * kg * deg C / h * Kcal *
deg C = kg water / h
fprintf('The required flow rate of cooling water is %.2f kg/h.\n',m);
```

The required flow rate of cooling water is 64000.00 kg/h.

Part b

Equations:

- $Q = U * A * \Delta T_{lm}$ (where ΔT_{lm} is the log mean difference of the temperature)
- $\Delta T_{lm} = (\Delta T_1 - \Delta T_2) / \log(\Delta T_1 / \Delta T_2)$
- ΔT_1 = desired fermenter temperature - initial water temperature
- ΔT_2 = desired fermenter temperature - final water temperature

Rearranging to solve for the surface area of the pipe:

- $A = Q / (U * \Delta T_{lm})$

Here U is the given h value.

```
deltat1 = t_desired - t_water; % units = deg C
deltat2 = min_deltat; % units = deg C
deltaTlm = (deltat1 - deltat2) / log(deltat1 / deltat2); % units = deg
C
```

Convert Q to units J/s to use the above equation

```
Q = Q / 3600; % units = Kcal/h * h / s = Kcal/s
Q = Q * 4184; % units = Kcal/h * J/Kcal = J/h
A = Q / (h * deltaTlm); % units = * s * m^2 * deg C / J * s * deg C =
m^2
```

- $A = \pi * d * l$

Rearranging the surface area equation for the length of the pipe:

- $l = A / (\pi * d)$

Convert d from cm to m

```
d = d / 100; % units = cm * m/cm
l = A / (pi * d); % units = m^2 / m = m
fprintf('The required pipe length to cool the fermentation broth is
%.2f m.\n',l);
```

The required pipe length to cool the fermentation broth is 924.58 m.

Problem 10

E. coli have a maximum respiration rate, q_{O_2max} , of about 240-mg O_2 /g-dry wt-h. It is desired to achieve a cell mass of 20 g dry wt/l. The k_{La} is 120 h^{-1} in a 1000-l reactor (800 l working volume). A gas stream enriched in oxygen is used (i.e., 80% O_2) which gives a value of $C^* = 28$ mg/l. If oxygen becomes limiting,

growth and respiration slow; for example, $q_{o2} = (q_{o2max} * c_l) / (0.2 \text{ mg/l} + c_l)$, where c_l is the dissolved oxygen concentration in the fermenter. What is c_l when the cell mass is at 20 g/l?

```
qo2max = 240; % units = mg O2/g-dry wt-h
cell_mass = 20; % units = g dry wt/l
kla = 120; % units = h^-1
vol = 1000; % units = l
working_vol = 800; % units = l
o2_gas = 0.8; % units = %
c_star = 28; % units = mg/l
```

Equations:

- $q_{o2} * X = kla * (c_{star} - c_l)$
- $q_{o2} = (q_{o2max} * c_l) / (0.2 + c_l)$

Substitute the second equation into the first.

- $(q_{o2max} * c_l * X) = kla * (c_{star} - c_l) * (0.2 + c_l)$

Use MATLAB solver to find the value of c_l

```
eqn = @(cl) ((qo2max * cl * cell_mass) - kla * (c_star - cl) * (0.2 +
    cl));
initial_guess = rand();
sol = fzero(eqn, initial_guess);
fprintf('The cl value is %.2f mg/l.\n', sol);
```

The c_l value is 0.44 mg/l.

Problem 14

A stirred-tank reactor is to be scaled down from 10 m³ to 0.1 m³. The dimensions of the large tank are $d_t = 2\text{m}$; $d_i = 0.5\text{m}$; $n = 100\text{ rpm}$.

- Part a: Determine the dimensions of the small tank (d_t , d_i , h) by using geometric similarity.
- Part b: What would be the required rotational speed of the impeller in the small tank if the following criteria were used?

```
# Constant tip speed
# Constant impeller Re number
```

```
vol_large = 10; % units = m^3
vol_small = 0.1; % units = m^3
dt_large = 2; % units = m
di_large = 0.5; % units = m
n_large = 100; % units = rpm
```

Part a

Equations:

- $V = \pi * (d_t/2)^2 * h$

Rearranging to solve for h:

- $V / (\pi * (dt/2)^2) = h$

h/dt must remain constant between the large and small reactors: $h_large / dt_large = h_small / dt_small = h_to_dt$
 dt/di must remain constant between the large and small reactors: $dt_large / di_large = dt_small / di_small = dt_to_di$

```
h_large = vol_large / (pi * (dt_large/2) ^ 2); % units = m^3 / m^2 = m
h_to_dt = h_large / dt_large;
dt_to_di = dt_large / di_large;
```

Substitute the ratio of height to diameter into the volume equation solved for small height and solve for the new diameter.

- $h_small = h_to_dt * dt_small$
- $vol_small = \pi * (dt_small/2)^2 * h_to_dt * dt_small$
- $vol_small = \pi * dt_small^3 * h_to_dt / 4$
- $dt_small = ((vol_small * 4) / (\pi * h_to_dt))^{(1/3)}$

```
dt_small = ((vol_small * 4) / (pi * h_to_dt)) ^ (1/3); % units =
m^3^1/3 = m
h_small = h_to_dt * dt_small; % units = m
di_small = dt_small / dt_to_di; % units = m
fprintf('The height of the small reactor is %.2f m, the tank diameter
of the small reactor is %.2f m, and the impeller diameter of the
small reactor is %.2f m.\n',h_small,dt_small,di_small);
```

The height of the small reactor is 0.69 m, the tank diameter of the small reactor is 0.43 m, and the impeller diameter of the small reactor is 0.11 m.

Part b

Part 1 Equations:

- $N * Di$ must stay constant
- $n_large * di_large = n_small * di_small$

Rearranging to solve for n_small:

- $n_small = n_large * di_large / di_small$

```
n_small = n_large * di_large / di_small; % units = rpm
fprintf('The new speed of the impellor is %.2f rpm.\n',n_small);
```

The new speed of the impellor is 464.16 rpm.

Part 2 Equations:

- $N * Di^2 * \rho / \mu$ must stay constant
- $n_large * di_large^2 * \rho / \mu = n_small * di_small^2 * \rho / \mu$

Cancelling rho and mu as they are constants and solving for n_small:

- $n_{\text{small}} = n_{\text{large}} * d_{\text{large}}^2 / d_{\text{small}}^2$

```
n_small = n_large * di_large^2 / (di_small^2); % units = rpm  
fprintf('The new speed of the impellor is %.2f rpm.\n',n_small);
```

The new speed of the impellor is 2154.43 rpm.

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