

## CODE

## COMMENTARY

Post-tensioned slab-column connections with  $f_{pe}$  in each direction not meeting the requirements of 8.6.2.1 can be designed as nonprestressed slab-column connections in accordance with 8.2.3.

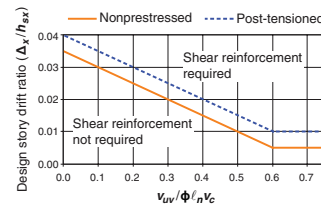


Fig. R18.14.5.1—Illustration of the criteria of 18.14.5.1.

**18.14.5.2** The shear reinforcement requirements of 18.14.5.1 need not be satisfied if (a) or (b) is met:

- (a)  $\Delta_x/h_{sx} \leq 0.005$  for nonprestressed slabs
- (b)  $\Delta_x/h_{sx} \leq 0.01$  for unbonded post-tensioned slabs with  $f_{pe}$  in each direction meeting the requirements of 8.6.2.1

**18.14.5.3** Required slab shear reinforcement shall provide  $v_s \geq 3.5\sqrt{f'_c}$  at the slab critical section and shall extend at least four times the slab thickness from the face of the support adjacent to the slab critical section.

**18.14.6** Wall piers

**18.14.6.1** Wall piers not designated as part of the seismic-force-resisting system shall satisfy the requirements of 18.10.8. Where the general building code includes provisions to account for overstrength of the seismic-force-resisting system, it shall be permitted to calculate the design shear force as  $\Omega_o$  times the shear induced under design displacements,  $\delta_o$ .

**R18.14.6** Wall piers

**R18.14.6.1** Section 18.10.8 requires that the design shear force be determined according to 18.7.6.1, which in some cases may result in unrealistically large forces. As an alternative, the design shear force can be determined as the product of an overstrength factor and the shear induced when the wall pier is displaced by  $\delta_o$ . The overstrength factor  $\Omega_o$  included in FEMA P749, ASCE/SEI 7, and the 2018 IBC can be used for this purpose.