

Underlying simplifications and assumptions of thermal comfort models as proxies of occupant comfort

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Abstract

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1. Introduction

As there are many different types of heating and cooling systems that are widely available, we want to investigate particularly the implications of radiant systems in contrast to all-air systems since the contrast would be larger. This is because the radiant systems do not need to explicitly condition the air temperature,

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which will result in smaller heating and cooling load since water and other working fluids are better heat carriers. In the meantime, radiant systems appear to have comparable if not better thermal comfort implications according to existing studies, hence forming good comparison to the prevailing air-based heating/cooling systems in the US.

Unlike air temperature, or the targeted fluid/surface temperature that are often used in the control of air or radiant systems, relative humidity (RH) is a much less commonly observed control variable. Relative-humidity-based control is currently used in more strictly-controlled environments such as piano rooms, archival storage rooms and specialized medical facilities. RH-based control is currently very expensive for residential or large commercial projects to consider. This is not only because the demand of RH-specific environments is less common, but also because the value of RH is codependent on the condition of the moist air condition, and cannot be easily controlled through a feedback control loop.

The moist air in a room is a mixture of both dry air and water vapor. Dry air has properties that are very close to ideal gas while the water vapor is ideal gas, we model their mixture using the ideal gas law and can estimate this mixture's remaining properties (pressure, humidity ratio and enthalpy) when a specific set of property (temperature and RH, in this example) is given. Graphically, this is also often explained by the psychrometric chart published by ASHRAE. However, the actual psychrometric processes that air conditioners undergoes is a myth to most users, since the feedback variable that most of their systems would allow them to control is only the air temperature. Although ASHRAE does recommend RH to be maintained between 30% to 60%, adding humidity to the air is still a secondary concern when people are purchasing and installing home air conditioning systems.

According to some latest research, the health implications of RH can be significant, although often in a delayed and indirect manner. Reports on RH below 20% could cause eye irritation and dryness/stuffiness complaints, and ultra-low RHs below that may even cause eye and air pathway and skin symptoms. RH below 10% could even desiccate the mucous membrane over time and lead to further agitation with both the eye and nasal cavity. Conversely, higher RH levels also have the potential to deteriorate building materials and grow mold that may lead to respiratory symptoms among building occupants. However, the RH that would allow rapid growth of bacteria and viruses are often found to be at least 75%, which is much higher than the mandate from ASHRAE or ISO 7730 (30% to 70%). There is, ultimately, very little regulation or guidelines regarding what the RH inside a room should be kept at, and anything above 30% and below 60% is acceptable. This is potentially also the reason why RH is much less controlled in conventional systems.

Existing literature have already established the link between energy savings and expanded set points of air. The verified energy potentials were demonstrated through air-based systems in simulated building cases through different climates. This included both the sensible and latent heat following the underlying hypothesis of the building case used and the occupancy density that was selected. Using radiant systems may prevent the excessive energy usage needed to remove the latent heat in the air in the summer. The relationship between the sensible and latent cooling load is less often studied but has seen some recent advances: new concepts

such as the enthalpy degree days and latent enthalpy days were proposed in contrast to the cooling degree day method used in estimating annual cooling loads.

In this study, we hope to take advantage of the existing literature to understand the benefit of further expanding the set point temperatures through the usage of radiant systems. This would include discussions on the energy savings from preventing the latent loads that would otherwise have occurred when using all-air systems, as well as the improvement of RH without additional humidifiers for the heating season. To better illustrate the energy saving potentials and the corresponding improvement in RH, we will run the analysis through hypothetical household located across the 48 continental states in the US to illustrate the energy and humidity potentials that can be found across different areas.

2. Methodology

2.1. Base Assumptions

Hoping to create a generic building energy footprint for comparison across the United States, we are assuming an average household with average square footage, household member counts, and energy consumption profiles that are made publicly available by the Department of Energy and US Census. For the purpose of this study, we consider only the residential conditioning systems. For this purpose, we assume the size of the household to be 2.52 occupants (cite US. Census.), which requires no more than 37.8 CFM of fresh air according to ASHRAE. In order to estimate the required fresh air rate, we assume the size of the house through the average size of buildings built (cite DOE?) as 2392 squared feet. As according to ASHRAE Standard 62, the newly-built buildings are instructed to achieve an infiltration rate of 2 CFM per every 100 squared feet, this allows us to estimate the ventilation rate of the hypothetical average house to have 47.84 CFM through infiltration. This is above the required fresh air amount for 2.52 hypothetical occupants in the average household in the United States. Assuming the height of the houses to be 9 feet, we obtained a fresh air percentage of 18 per cent, which allowed us to estimate the condition of the mixed air with a targeted indoor air condition and outdoor air condition. The set points and the psychrometric processes we are assuming are introduced separated in the subsequent sections.

2.2. Cooling, Heating and Enthalpy Degree Days

Degree Day (DD) is a method that ASHRAE currently still recommend using when measuring how outdoor air temperature variation may impact the energy use. It compares the outdoor temperature to a defined base temperature, which is naturally a temperature-based method used to explain building energy consumption. As we are attempting to illustrate the differences between the radiant and air-based differences, DD is an apparent choice that circumvents the selection of more explicit building systems. In degree-day theory, the base temperature separates times where buildings need conditioning from times it does not. This applies to both the heating and the cooling case, or otherwise known as cooling degree day (CDD) and heating degree day (HDD) methods. (Use equations for both here). The base case can often be considered the equivalent of set-point temperature, and is recommended to be set at 18.3 C(65 F) by ASHRAE.

However, as both the CDD and HDD method are based solely on the outdoor dry-bulb temperature, the latent loads are apparently overlooked. This is particularly true for the cooling scenario. Researchers have proposed alternative such as the enthalpy degree days (EDD), where the enthalpy of the air of the day can be compared to the base case enthalpy. Huang et al. first suggested the possibility of estimating the latent loads through a concept known as latent enthalpy degree day, while Krese et al. further perfected it by suggesting the EDD approach in 2012 through 2013. This is further assessed in a more recent research by Jimeno and Schulters where they proposed a Degree of Enthalpy Gradient, or DEG. It is a new advancement in the direction of assessing the latent load in buildings by combining the heating and the cooling demands and creates extra difficulty in analyzing the cooling and heating cases independently for us.

The heating and cooling season is done with the building systems.

2.2.1. Cooling Processes

For the cooling scenario, conventional air handling units uses evaporative cooling to cool the outdoor air down to set point per the design of the cooling system. This process can be simplified on the psychrometric chart as the air temperature from the outdoor condition being cooled down to the set point at the desired indoor condition. Previous study has demonstrated the clear energy benefit of expanding the set points, yet had yet to unravel the latent energy benefit caused by the changes in set point temperature.

We want to compare the impacts of having different set points specifically focusing on the differences in latent loads, which we are showing in the psychrometric process in the figure above. While maintaining the same level of desired RH, the changes in the energy demand is not fully reflected by the changes in dry bulb air temperature. We can explicitly compare the overall (latent and sensible) and sensible load by comparing the cooling degree days and the enthalpy degree days of identified set points for the cooling season and the outdoor temperature.

Psychrometrically speaking, this process is shown in Figure 1, when air is cooled from the outdoor condition with high dry-bulb temperature and relative humidity, eventually reaching the four different set points at the same desired level of RH: 50%. The differences between the end-state enthalpy can be easily characterized by Δh for the different set points and the outdoor temperature. We will compare this with the resulting hourly cooling degree days of each specific weather file. Following the definition of CDD by ASHRAE, we calculate the cooling degree days with Equation 1. Here, the cooling degree days for a defined reference temperature is $CDD_{t_{bal}}$ for a specific defined reference temperature t_{bal} . The rest of the parameters here are n as the number of days over the desired period, and $\bar{t}_{o,i}$ as the daily average outdoor temperature ($^{\circ}C$). For our purpose of the analysis, to analyze the different set points of the indoor air condition, we will use four different t_{bal} values. The ASHRAE recommended set point range is $74^{\circ}F$ to $80^{\circ}F$ in the summer, while a typical radiant cooled space will use $75^{\circ}F$ ($24^{\circ}C$) air temperature with no greater than 50% RH, which is the equivalent of a lower dew point temperature (approx. $12.2^{\circ}C$) to avoid condensation. The lowest will therefore be $18.3^{\circ}C$ as suggested by ASHRAE for CDD calculation, with two extra data points as suggested by ASHRAE to be $23.3^{\circ}C$ ($74^{\circ}F$) as well as $26.67^{\circ}C$ (or $80^{\circ}F$, as recommended set point by ASHRAE) and up to $28^{\circ}C$ (Sui

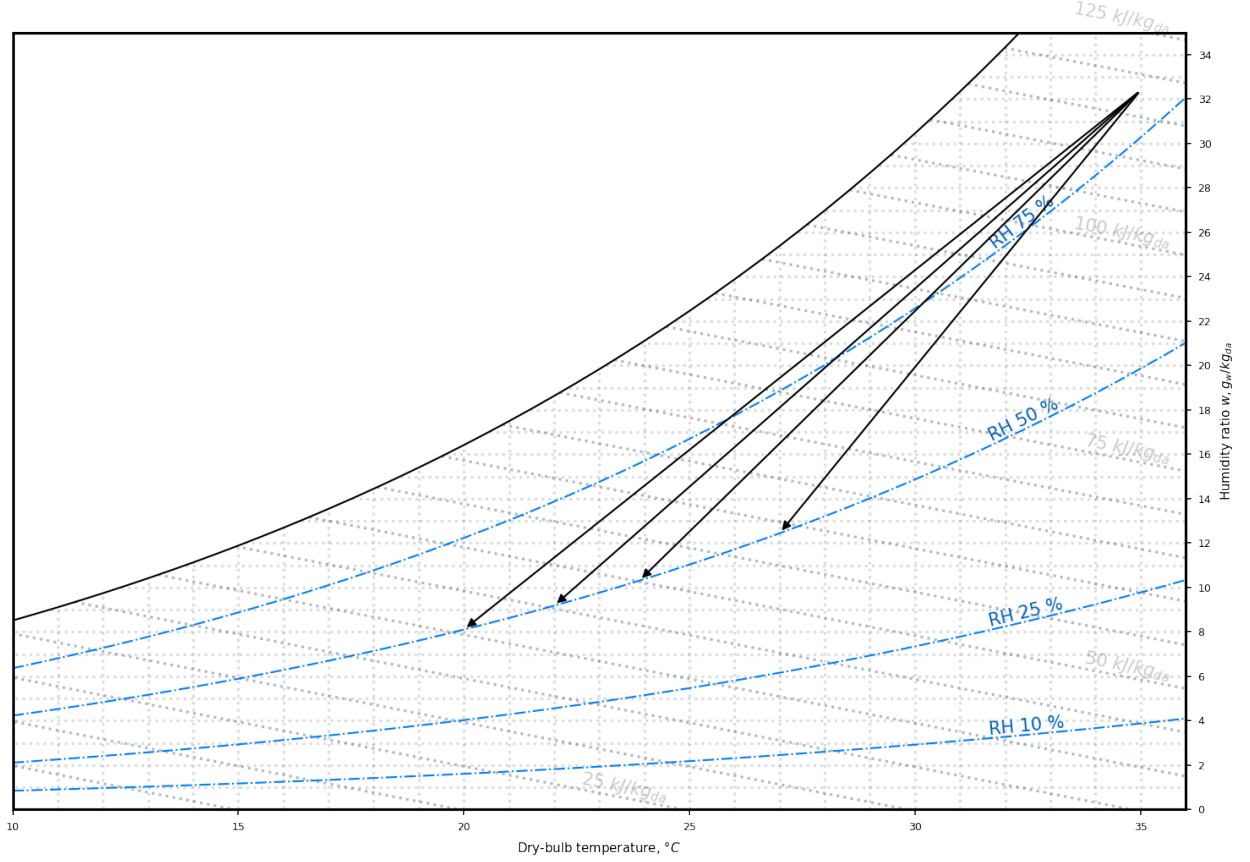


Figure 1: Example psychrometric processes under different set points for the cooling scenario.

& Zhang, 2015) for the indoor air temperature in radiantly cooled environment.

$$CDD_{t_{bat}} = \sum_{i=1}^n (\bar{t}_{o,i} - t_{bat})^+ \quad (1)$$

To characterize the variations of the latent loads relating to only the enthalpy differences, the same set of dry bulb temperatures are used, while the enthalpy degree days are calculated similarly using Equation 2. Here, we characterize the total enthalpy differences between the state of the outdoor air ($\bar{h}_{o,i}$) that needs to be conditioned to a specific set point with enthalpy (h_{bat}).

$$EDD = \sum_{i=1}^n (\bar{h}_{o,i} - h_{bat}) \quad (2)$$

To compare the sensible with the latent demand, the output from Equation 1 (in Kelvin) needs to be compared with the output from Equation 2 (kJ/kg of dry air). To achieve the same resulting unit, we will be multiplying the CDD values with the equation to calculate c_p with Equation 3, where the specific heat (kJ/kg · K) can be calculated with a given humidity ratio w . Multiplying CDD obtained through Equation 1 with corresponding c_p , we may therefore obtain a specific enthalpy of dry air that is comparable to specific

enthalpy of moist air obtained via Equation 2/

$$c_p = 1.005 + 1.884w \quad (3)$$

This calculation is aimed at emphasizing the amount of additional cooling needed when the feedback control variable is only dry bulb air temperature instead of both air and relative humidity. As is highlighted with green in the graph we generated, assuming the same amount of cooling capability but targeting only the dry bulb temperature instead of air mixture at different set points, the sizing

2.2.2. Heating Processes

For the heating scenario, we will be operating under two stages of hypothesis. The first hypothesis we want to examine is there being no extra humidifier for the winter condition (i.e. no blue arrows in Figure 2). The relative humidity would obviously be much higher when the set point is lower for radiant systems, and vice versa for the air-based system. Assuming a constant-humidity ratio heating process, we may therefore estimate the resulting RH for an average state during the heating season.

With respect to the set points, we will be assuming sensible heating only, where the outdoor air is heated up with the same humidity ratio. Following the indoor air temperature guideline recommended by ASHRAE, which is $68^{\circ}F$ to $74^{\circ}F$ (20 to $23^{\circ}C$) for winter, we will be using these temperatures as the base condition to be compared with. For the radiant scenario, since the radiant surfaces are often kept at a higher temperature, we will be setting the indoor air temperature slightly higher than that of the dew point temperature of assumed indoor air condition – which we assume to have a RH at 50%. This is equivalent of dew point temperatures at TD1 and TD2 $^{\circ}C$.

Similar to the psychrometric process in the cooling case, we are expressing the heating of air in the psychrometric chart underneath. Since the majority of the heating is accomplished through furnaces and air conditioners, the outdoor air is assumed to go through a constant-humidity-ratio process as it is heated sensibly. Without additional humidifiers, the resulting RH could reach beneath 30% (as indicated in the figure), and potentially lead risks of the occupants' wellbeing. Even when considering additional humidifiers, the energy that needs to be added to the air can also be characterized as additional energy demands (as marked by the red arrows in illustration we created).

It is, therefore, crucial to provide an estimation of the overall energy demand necessary to deliver air that is warm enough for all-air systems or radiant system, and additionally air that is moist enough to avoid strain on the respiratory system of the occupants. We believe it is crucial to highlight the energy savings in both the cooling and the heating condition when considering expanded set points. Using the psychrometric-driven approach, we are hoping to conduct both spatial and statistical analysis on the resulting RH and energy demand across continental US with the NOAA data we collected.

Beyond the first hypothesis, we would also like to assume an alternative scenario where humidifiers are used to ensure a satisfying humidity condition. This is expressed with the blue arrows in Figure 2. With the

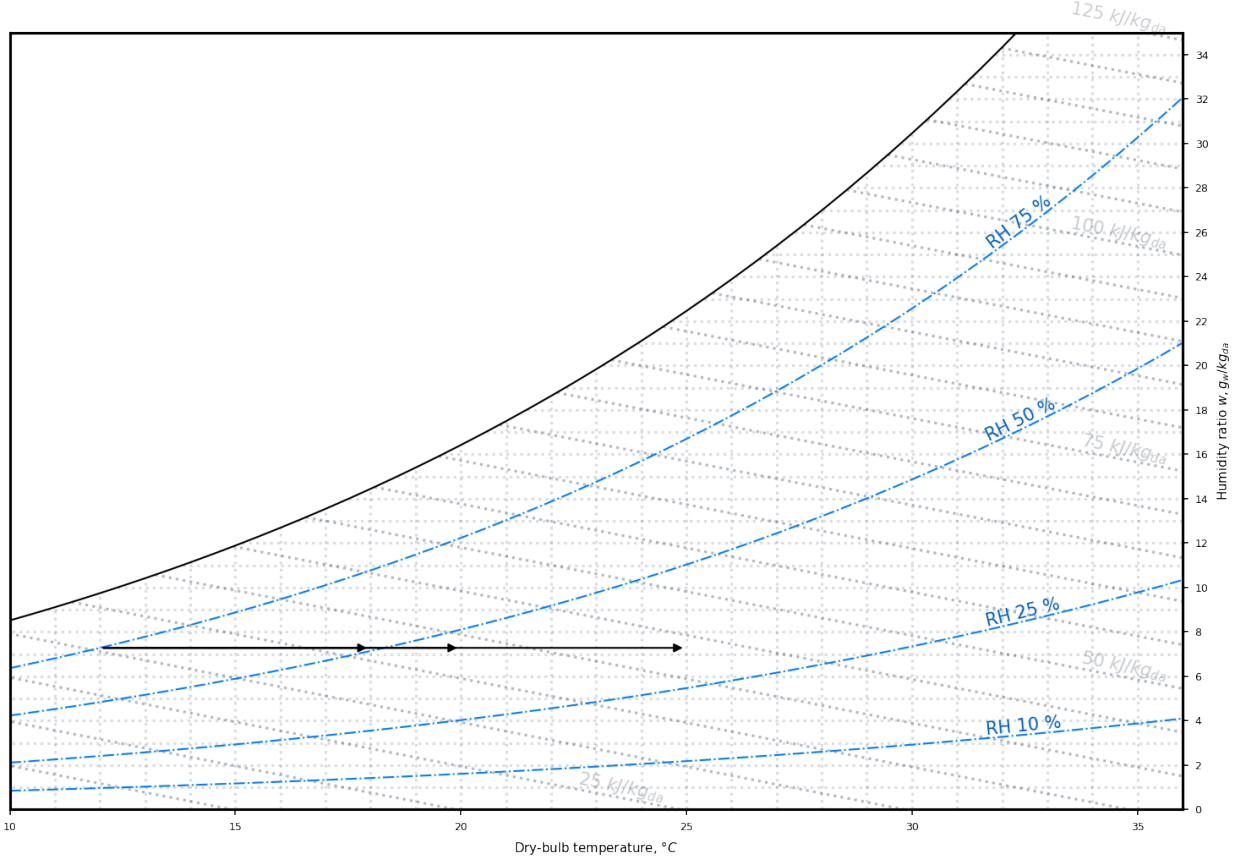


Figure 2: Example psychrometric processes under different set points for the heating scenario.

added humidity into the air, the added latent load for all-air systems can be considered as the load that is not often characterized in the existing literature. Without specifying the systems that are used in this process and their respective efficiencies, analyzing only the required latent load that needs to be added to the moist air through humidifier can help us understand the extra energy that is necessary when attempting to achieve desirable RH condition for the indoor environment across different set points.

The RH difference will be compared with the mean value. The energy saving percentage will be compared with daily average? monthly average? heating season?

2.3. Data Collection and Processing

As we are interested in understanding the potential energy savings and RH improvement across continental US, we need the weather data collected from major cities across the continent with resolution smaller than every hour. The ISD-lite dataset made available by NOAA (National Oceanographic Association of America) provides air temperature, relative humidity and geographic location at weather stations across major city centers and airports across continental US. This data is publicly available on NOAA's ftp server. We downloaded a total of 13,800 files for the monitored weather in 2018 for the purpose of this analysis. Since the climate

zones, as we are plotting in Figure 3.

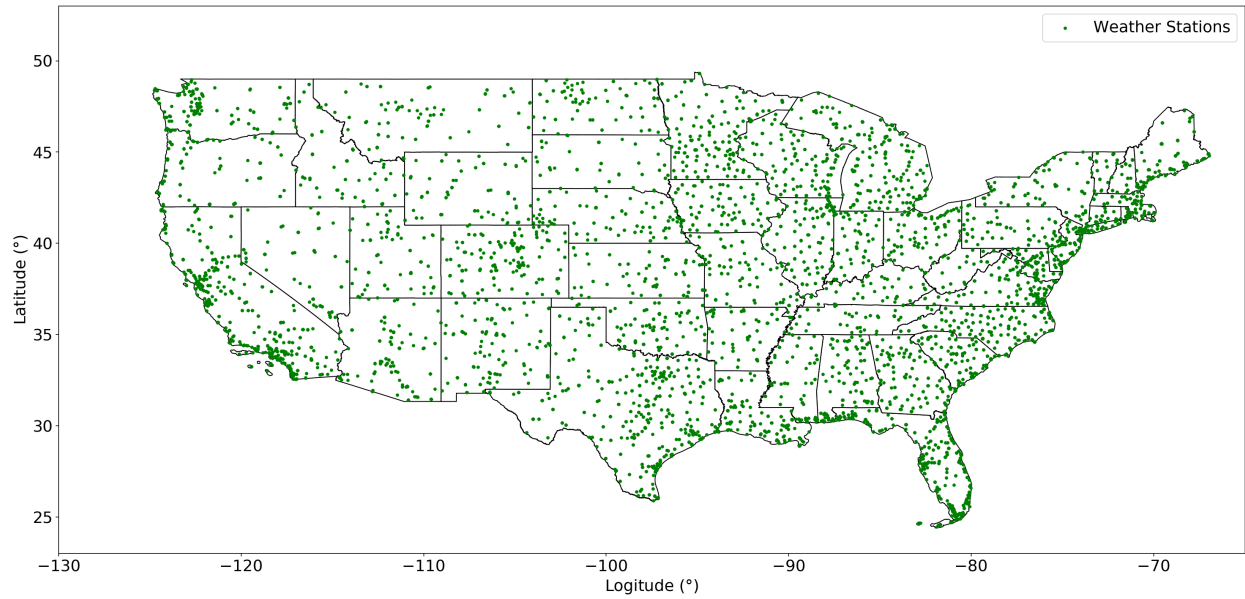


Figure 3: Locations of climate station files clipped to the USGS geometry in NOAA ISD-lite, 2017.

Upon scraping the NOAA ftp server for the 2018 weather files, we used the pandas data frame library in Python to clean up and regroup the files into time-stamped weather data, and re-sampled on an hourly rate. We also used the CoolProps library to calculate the enthalpy of moist air at different states, and appended the resulting hourly enthalpy states. The resulting weather files will therefore have the air temperature, relative humidity, specific enthalpy for 8760 hours in 2018 across all the stations. We are plotting an example of the data collected in one of the weather stations in Figure 4.

We will primarily divide our analysis into two parts. The first part focuses on the energy savings of the cooling scenario and the RH improvements for the average heating/cooling condition for the weather stations.

The second part will examine the entire time series of weather data across different climate zones.

3. Results

3.1.

3.2. *Environmental Parameters Simplifications*

4. Latest Efforts in addressing the absence of occupant in OCC

4.1. *Subjective feedback*

4.2. *Objective measurement*

5. Conclusion

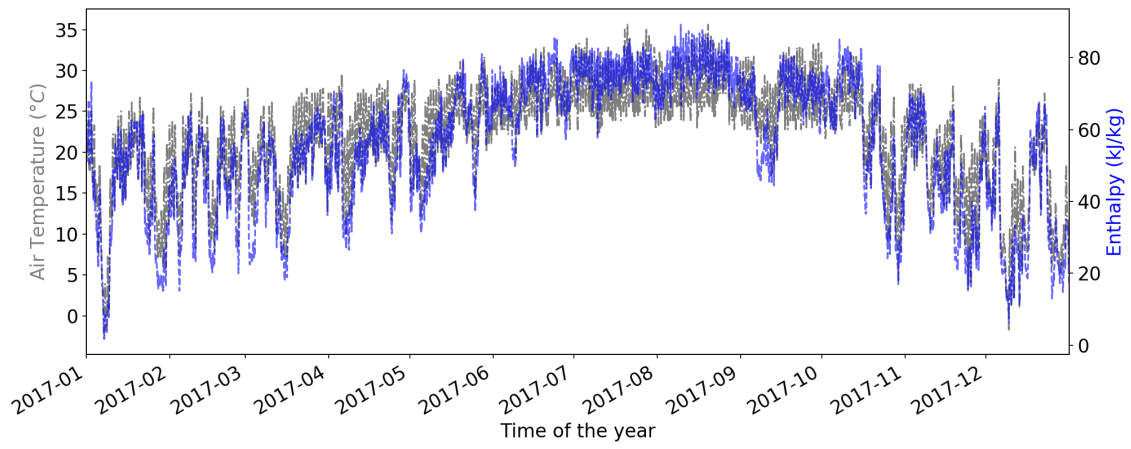


Figure 4: Processed Outdoor Dry-bulb temperature against outdoor specific enthalpy for the weather station in Station ID.