## Gas Temperature from Heat Flux and Thermocouple Data

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#### Introduction

The gas temperature can change quickly in a reacting gas flow or in the gas flow produced from the rapid reaction of energetic materials. The use of thermocouples to measure that gas temperature can be inaccurate as that gas temperature changes rapidly. Use of heat flux gauges and/ or different sized thermocouples can be used with a energy balance model to regress or calculate the gas temperature.

Below is one way of doing so where the following steps are followed:

- First estimate the gas temperature from the heat flux data based on the following equation:  $HF = \epsilon \cdot \sigma \cdot (T_{gas}^4 T_{gauge}^4) + h \cdot (T_{gas} T_{gauge}^4)$ , where HF is the measured heat flux. This equation is simply the heat flux due to convection and radiation to the heat flux gauge. Make an estimate of the heat transfer coefficient, h, as a function of time based on the expected gas velocity. Also make an estimate of the radiation term  $\epsilon$ .
- Then complete an energy balance for the thermocouple bead scenario based on the heat equation as there could be heat lost down the arms of the
  thermocouple wire connected to the bead: ρcp∂T∂t=∂∂r(k∂T∂r)+ Q with ρ as density, cp as heat capacity, T as the temperature, k as the thermal
  conductivity, and .Q as the heat input rate. The heat equation is discretized in space to give a set of Ordinary Differential Equations (ODEs) in time.
- Using the above energy balance and the above estimated gas temperature, the thermocouple temperature can be found. That calculated thermocouple temperature can then be compared to the actual thermocouple temperature.

I realize that instead of the above steps, the measured heat flux and the temperature can be used to solve for the heat transfer coefficients and thus the gas temperature. I wanted to do that too but I ran out of time. The answers found would be similar.

#### Solver details

The above equations were solved using the Gekko solver: see <a href="https://gekko.readthedocs.io/en/latest/">https://gekko.readthedocs.io/en/latest/</a> (Beal, L.D.R., Hill, D., Martin, R.A., and Hedengren, J. D., GEKKO Optimization Suite, Processes, Volume 6, Number 8, 2018, doi: 10.3390/pr6080106) with the Python code adapted from APMonitor (see <a href="https://apmonitor.com/do/index.php/Main/PartialDifferentialEquations">https://apmonitor.com/do/index.php/Main/PartialDifferentialEquations</a>). This sheet is recommended to run in a GekkoEnv (Gekko Environment in Anaconda). In other words, you'll need to install Gekko to run this sheet. See the links for installation instructions.)

```
In [1]: | The parabolic PDE equation describes the evolution of temperature

2  # for the interior region of the rod. This model is modified to make

3  # one end of the rod fixed and the other temperature at the end of the

4  # rod calculated.

5  import numpy as np

6  import pandas as pd

7  from gekko import GEKKO

8  import matplotlib.pyplot as plt
```

#### Import temperature data

Temperature probe at Station I is next to the wall and Station J is at the center of the tunnel. All thermocouples are 36 gauge with a metal cup surrounding each one. The heat flux gauge is also at Station J.

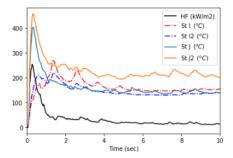
```
In [2]: N
                1 data = pd.read_csv('../../JupFiles/files/36gaugetempsm.csv', header=0)
                    data = data.set index('Time')
                 3 data = data.dropna()
In [3]: H 1 data.describe()
    Out[3]:
                         HF kWm2
                                           St I2
                                                        St J2
                count 1001.000000 1001.000000 1001.000000 1001.000000 1001.000000
                mean 14.787461 143.570613 201.452277 153.519139 147.774337
                std 28.118533 17.246051 43.512356 20.720468 30.788072
                       -1.375612 7.945966 7.972047 7.709273 7.963827
                 25% 0.907196 136.655590 172.036760 147.091720 137.624950
                        9.965841 140.951920 207.524200 152.564410 142.523990
                 75% 15.497542 147.113490 223.091600 154.016620 147.263730
                 max 254.048542 218.704830 456.649170 267.624570 402.126560
In [4]: № 1 #data.plot() #data from testing on March 24, 2021
                    plt.figure()
                    plt.plot(data.index,data['HF klwm2'],'k-',label='HF (kW/m2)')
                plt.plot(data.index,data['St I'],'r-.',label='St I $\,(^oC$)')

plt.plot(data.index,data['St I'],'b-.',label='St I $\,(^oC$)')

plt.plot(data.index,data['St I'],'b-.',label='St I2 $\,(^oC$)')

plt.plot(data.index,data['St J'],label='St J $\,(^oC$)')

plt.plot(data.index,data['St J2'],label='St J2 $\,(^oC$)')
                 8 plt.xlabel('Time (sec)')
                 9 plt.xlim([0,10])
                10 #plt.vlim([0.1000])
                11 plt.legend(loc=1)
                12 plt.show()
```



Notice that the thermocouple gauges at the wall measured a temperature significantly less than those in the middle of the tunnel, except for a few times after the initial 1-second interval.

# Use the heat flux data to solve for the gas temperature assuming a emissivity and heat transfer coefficient

Note that the radiation term is an estimate only as the gas absorptivity and the emissivity of the gas together with the emissivity of the heat flux gauge is all in one term.

```
In [5]: N
               1 #parameters
                  4 hm = 800
                              #max heat transfer coefficient multiplier (heat transfer is a function of time as it depends on the reynold:
               5 hn = 50
                                 #min heat transfer coefficient
               6 sbz = 5.67e-8 #stefan bolzmann constant W/m2/K4
                7 c2k
                                                # Celcius to Kelvin
                            = 273.15
               8 Tgauge = 6 + c2k #temperature of the guage
               10 tarr = np.array(data.index)[1:] #time
               sigma = 15; mua = 0; mul = 0.49 #parameters for heat transfer coefficient

##c = mul*(hm-hn)/sigma/tarr*np.exp(-0.5*((np.log(tarr)-mua)/sigma)**2) + hn #convective heat transfer coefficient, W/m2,

hc = hm/(tarr+1.3)**1.8 + hn #this is estimated based on the expected flow rate of the gases passing the heat flux gauge
               14 | mheat = np.array(data['HF kWm2'])[1:]*1000 #units of W/m2
               16 mh = GEKKO(remote = False)
               18 mh.time = tarr
               19 | Tg = mh.Var(Tgauge) # initial gas temperature
               20 theat = mh.MV()
               21 theat.value = mheat
               22 htc = mh.MV()
               23 htc.value = hc
               #equation to solve for each time
## tequation(theat == em*vF*sbz*(Tg**4-Tgauge**4) + htc*(Tg-Tgauge))
               27 #mh.Obj(0.35-qrad/qtot)
               28 # simulation
               29 mh.options.IMODE = 4
               30 mh.solve()
                   4
```

#### Gas temperature estimate

```
In [6]: H
               1 plt.figure()
                   tm = mh.time
                   plt.plot(tm,Tg,'r-',label='Gas temperature')
               4 plt.ylabel('Gas temperature, K')
5 plt.xlabel('Time (sec)')
                   #plt.ylim([0,2000])
                   #plt.legend(loc=1)
                8
                   plt.show()
                 900
                 800
                 700
                 600
                 500
               Gas
                                      10
                                             15
```

#### Convective heat transfer coefficient estimate

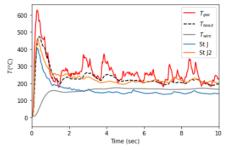
The heat transfer coefficient is highest when the gas velocity is highest. This estimate can be compared to a gas velocity calculation using the Nusselt number correlations that are functions of the Reynolds number. Modeling can be used to estimate the gas velocity in the tunnel or it can be measured experimentally.

## Compare the actual to the calculated thermocouple result

Now use the gas temperature found above to get the thermocouple temperature, then compare the results to the actual temperatures measured. This approach is similar to that reported by P. Wang et al. in "Influence of surrounding gas temperature on thermocouple measurement," Case Studies in Thermal Engineering 19 (2020) 100627.

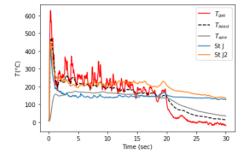
```
In [8]: 📕
                       1 # Thermocouple temperature profile
                                                                           # number of wire segments of the thermocouple (conduction of heat down the wire)
                                           = 50
                         2 seg
                                            = 3.14159
                         3 pi
                                                                              # pi
                        4 dia
                                             = 0.025/1000
                                                                             #thermocouple wire diameter (m)
                                                                      # wire length (m)
                                             = 0.05
                             L
                             L_seg
                                                                             # length of a segment (m)
                                                                               #thermocouple bead diameter (m)
                        7 bdia
                                            = 0.075/1000
                                            = 4/3*pi*(bdia/2)**3 #bead volume
                        8 bVol
                                             = 4*pi*(bdia/2)**2 - 0.5*pi*dia**2 #bead surface area (with area subtracted for wires)
                        9 bAr
                      10 Ar
                                             = 2 * 0.25 * pi * dia**2  # wire (2) cross-sectional area (m)
                      11 As
                                            = pi * dia * L_seg * 2 # surface (2) heat transfer area (m^2)
                                                                           # thermal conductivity in Nickel-Cr (W/m-K)
# density of Nickel-Cr (kg/m^3)
                      12 keff
                                            = 30
                                            = 8600
                      13 rho
                                                                              # heat capacity of Nickel-Cr (J/kg-K)
                      14 ср
                                             = 500
                      15
                                                                            #view factor of the thermocouple gauge (its in a cylindrical cup open at the top) #estimate of the emissivity radiation factors #surrounding item temperatures
                      16 vFt
                                            = 0.1
                      17 emh
                                            = em
                                           = Tgauge
                      18 Tsurr
                      19
                      20 m = GEKKO(remote=False) # create GEKKO model
                      21
                      22 m.time = mh.time
                      23 hconv = m.MV()
                      24 hconv.value = hc
                      25 Ts = m.MV()
                      Ts.value = Tg.value #the gas temperature is the surroundings temperature from the previous solution #^{27} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #^{18} #
                      28 #bfrac.value = mul*0.99/sigma/tarr*np.exp(-0.5*((np.log(tarr)-mua)/sigma)**2)
                      30 T = [m.Var(Tsurr) for i in range(seg)] # initial temperature of the segments (°C)
                      31 flag = [m.Param(1) if i<int(2) else m.Param(0) for i in range(seg)] # flag showing wheather or not the segment is expose
                      33
                     47 # first segment
                     48 m.Equation(rho*bVol*cp*T[0].dt() == \
                                                      keff*Ar*(T[0]-T[1])/((L_seg+bdia)/2) \
                    50
                                                  + (hconv*(Ts-T[0]) + em*vFt*sbz*(Ts**4-T[0]**4) + emh*(1-vFt)*sbz*(Tsurr**4-T[0]**4))*bAr*flag[0])
                    51 #second seament
                    52 m.Equation(rho*Ar*L_seg*cp*T[1].dt() == \
keff*Ar*(T[0]-T[1])/((L_seg+bdia)/2) \
                     54
                                                   keff*Ar*(T[1]-T[2])/L_seg
                    55
                                                   + (hconv*(Ts-T[1]) + em*vFt*sbz*(Ts**4-T[1]**4) + emh*(1-vFt)*sbz*(Tsurr**4-T[1]**4))*As*flag[1])
                     56 # middle segments
                     57 m.Equations([rho*Ar*L seg*cp*T[i].dt() == \
                                                      keff*Ar*(T[i-1]-T[i])/L_seg \
keff*Ar*(T[i]-T[i+1])/L_seg \
                                                   + (hconv*(Ts-T[i]) + em*vFt*sbz*(Ts**4-T[i]**4) + emh*(1-vFt)*sbz*(Tsurr**4-T[i]**4))*As*flag[i] for i in r.
                    60
                    61 # last seament
                    62 m.Equation(rho*Ar*L_seg*cp*T[seg-1].dt() == \
63 keff*Ar*(T[seg-2]-T[seg-1])/L_seg \
- keff*Ar*(T[seg-1]-Tsurr)/L_seg )
                     66 # simulation
                     67 m.options.IMODE = 7
                     68 m.solve()
```

• •



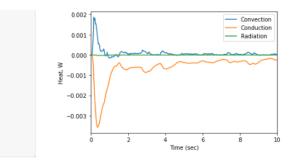
From the above plot, the calculated bead temperature (black dashed line) is similar to the station gauge temperatures indicating the estimated gas temperature and heat flux coefficients are close to the actual values. The gas temperature is sometimes 100 to 200 degrees above the thermocouple temperature and at other times equal to the thermocouple temperature.

Note also that the heat flux gauge is also much more responsive than the thermocouple gauge.



Note that at long times (>10 seconds), the calculated bead temperature does not agree with the measured temperature as the effect of the heated dust present near the thermocouple is not accounted for in the model. However, the gas temperature (predicted from the heat flux measured) does show a decay.

#### Conduction, Convection, and Radiation Amounts



From the above plot, it appears that radiation is not a large factor but the conduction down the length of the thermocouple wire should be included.

#### Benefits of 30 gauge thermocouple in addition to 36 gauge

If a 30 gauge thermocouple is also at the same location as the 36 gauge thermocouple, the different sizes can be used to also benchmark the gas temperature estimate in a similar way as was done with the heat flux gauge. Plotted below are a 36 gauge and 30 gauge thermocouple profiles given the above results.

## Gas Temperature from Thermocouple Temperature

Although not done here, a model could be written to calculate the gas temperature from the thermocouple data. Having data for both 36 and 30 gauge thermocouples at the same position would be helpful in doing so.