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# ORIFICE FLOW

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**Keywords** Spiritual Safety, Process Safety, Chemical Engineering, Risk Assessment

## Learning Outcomes

- Estimate flow through an orifice for incompressible liquids, compressible gases (choked and unchoked flow), and two-phase flow for flashing fluids.
- Perform preliminary sizing of a relief valve for liquid, gas, and two-phase flow scenarios.
- Understand the application of the mechanical energy balance to calculate fluid velocity and pressure drops.
- Identify appropriate discharge coefficients for different fluid types to account for frictional losses

## Reading

- Foundations of Spiritual and Physical Safety: with Chemical Processes; Chapter VI.3.2 (Orifice Flow) through Sec. VI.4.

## 1 Mechanical Energy Balance

### Note

Constant Density, Frictionless, Constant Temperature Flow

$$\frac{\Delta P}{\rho g} + \frac{\Delta u^2}{2g} + \Delta z + \frac{F}{g} = \frac{-W_s}{\dot{m}g} \quad (1)$$

where  $\Delta P$  is the change in pressure,  $\Delta u$  is the change in velocity,  $\Delta z$  is the change in elevation,  $\rho$  is density,  $F$  is the frictional losses, and  $W_s$  is the shaft work with respect to two points in the system.

If there is no friction and constant density and no shaft work and no change in elevation, the mechanical energy balance simplifies to:

**Note**

$$\frac{\Delta P}{\rho g} + \frac{\Delta u^2}{2g} = 0 \quad (2)$$

or assuming that the flow points are inside a tank where  $P = P_o$  and  $u = 0$  and outside the tank where  $P = P_{atm}$  and  $u = u$ , then

$$\frac{P_o}{\rho} - \frac{P_{atm}}{\rho} = \frac{u^2}{2} \quad (3)$$

or

$$u = \sqrt{2 \left( \frac{P_o - P_{atm}}{\rho} \right)} \quad (4)$$

## 2 Incompressible Flow through an Orifice

Thus for incompressible flow, the velocity of the fluid can be determined from the pressure drop across an orifice. Although the flow is usually not frictionless, the velocity can be estimated from the pressure drop and the density of the fluid according to:

$$\dot{m} = AC_d \sqrt{2\rho \Delta P} \quad (5)$$

or

$$\dot{n} = \frac{AC_d}{M_w} \sqrt{2\rho \Delta P} \quad (6)$$

where  $\dot{m}$  is the mass flow rate,  $\dot{n}$  is the molar flow rate,  $M_w$  is the molecular weight,  $A$  is the area of the orifice,  $\rho$  is the density of the fluid,  $C_d$  is the discharge coefficient, and  $\Delta P$  is the pressure drop across the orifice. For liquid flow, an estimate of the discharge coefficient is 0.65.

## 3 Gaseous flow through an Orifice: General Case

The flow of a gas through an orifice is also derived from an energy balance assuming adiabatic and frictionless flow. The flow is characterized by the pressure ratio,  $P_o/P_{atm}$  and associated Mach number,  $Ma$ .  $P_o$  is the absolute pressure of the volume. The Mach number can be found from:

$$Ma = \min \left( 1, \sqrt{ \frac{2}{\gamma - 1} \left( \left( \frac{P_o}{P_{atm}} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right) } \right) \quad (7)$$

where  $\gamma$  is the ratio of specific heats (1.4 for air). The flow is choked when  $Ma = 1$  and unchoked when  $Ma < 1$ .

The molar flow rate is given by:

$$\dot{n} = P_o A C_d \sqrt{\frac{\gamma}{RT M_w}} Ma \left[ 1 + \frac{(\gamma - 1)}{2} Ma^2 \right]^{\frac{\gamma+1}{2-2\gamma}} \quad (8)$$

where  $R$  is the gas constant and  $T$  is the temperature,  $P_o$  is the absolute pressure inside the vessel,  $C_d$  is the discharge coefficient (typically about 0.9). If you use all SI units (Pascal, meters, kilograms, mole: so pressure in pascal, area in meters, R in J/mol/K, and Mw in kg/mol), you'll get mole per second for  $\dot{n}$ . See Perry's Handbook for Chemical Engineers Equation 6-118 for more information.

## 4 Flashing Two Phase Flow Estimate

$$\dot{m} = f \frac{\Delta H_v A}{\nu_{fg}} \sqrt{\frac{1}{C_p T_s}} \quad (9)$$

where  $\dot{m}$  is the mass flow rate,  $f$  is a factor depending on the scenario (less than 1),  $\Delta H_v$  is the heat of vaporization,  $A$  is the area of the orifice,  $\nu$  is the specific volume change of the liquid as it flashes ( $\nu_g - \nu_l$ ),  $C_p$  is the heat capacity of the fluid, and  $T_s$  is the saturation temperature of the fluid at the set pressure. See Chapter 4 of Crowl and Louvar for more information.

## 5 Relief Valve Sizing

The above equations can be rearranged to solve for the area of the orifice,  $A$ , for a given flow rate and other conditions. Note that the discharge coefficient,  $C_d$ , is a function of the geometry of the orifice and the flow conditions. The discharge coefficient is typically determined experimentally with viscosity, downstream piping, backpressure, and other factors influencing the value. Estimates for some of those parameters can be found in Chapter 10 of Crowl and Louvar. For a preliminary estimate, a value of 0.65 is often used for liquid flow and 0.9 for gas flow.

Relief valve sizing in some instances does required verification with actual flow per the AMSE Boiler and Pressure Vessel Code.

### Note

See in-class examples

Download a pdf of the example using freeform here: <physical/supportfiles/GasFlowExample311.pdf>

### 5.1 In Class Example: Venting CO<sub>2</sub> from 2L Bottle

A two liter bottle is half filed with water. There is a relief valve on the top designed to relieve at 60 psig with a flow of 61 scfm. What is the flow rate of CO<sub>2</sub> through the relieve per the above equations?

```
import numpy as np

#first find the Mach number
gamma = 1.3 #specific heat capacity ratio for CO2, estimate
P1 = 60 + 12.5 #initial pressure, estimate, psia
Patm = 12.5 # atmospheric pressure, psia
Ma = min(1, np.sqrt(2/(gamma - 1)*((P1/Patm)**((gamma - 1)/gamma) - 1))) #Mach number

Ma

1

#now calculate the molar flow rate
R = 8.314 # gas constant, J/(mol*K)
Temp = 295 # temperature, K
Area = np.pi/4*(1/4*0.0254)**2 # area of the pipe, m^2
Cd = 0.9 # discharge coefficient
```

```
Mw = 0.04401 # molar mass of CO2, kg/mol
# molar flow rate, mol/s
ndot = P1*6894.76*Area*Cd*np.sqrt(gamma/(R*Temp*Mw))*Ma*(1+(gamma -1)/2*Ma**2)**((gamma+1)/(2 -2*gamma))
print(f'The molar flow rate is {ndot:0.2f} mol/s')
```

The molar flow rate is 0.92 mol/s

```
#now convert that molar flow rate into scfm, PV = nRT
Tstandard = 298.15 # standard temperature, K
Pstandard = 101325 # standard pressure, Pa
scmps = ndot*R*Tstandard/Pstandard #units of m^3/s
scfm = scmps*60*(3.281**3)
print(f'The flow rate in scfm is {scfm:0.1f}')
```

The flow rate in scfm is 47.4

Why is this number different than the reported flow rate of CO<sub>2</sub> through the relief valve? Could the diameter of the relief be slightly larger?

How would you get the generation rate of CO<sub>2</sub> from the sublimation of dry ice?

$$Q = hA(T_{water} - T_{ice})mdot = Q/\Delta H_{vap} \quad (10)$$

Does area ( $A$ ) change? How would you get the heat transfer coefficient ( $h$ )?

#### Action Items

1. Compare Eq. VI.27([Guymon, 2025](#)) to the mechanical energy balance equation in your fluid mechanics textbook. Explain how they agree or disagree including differences in perhaps the molar volume versus density and the molar flow rate and the mass flow rate. What assumptions are made in the derivation?
2. Derive the mechanical energy balance if we had two inlet fluid flows (instead of one as is typically used in the mechanical energy balance) into the control volume and one fluid flow out.

## References

C. Guymon. *Foundations of Spiritual and Physical Safety: with Chemical Processes*. 2025.