Engineering breakdown voltage in a pn-junction diode

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Abstract—**For this lab, the goal is to design a one-sided abrupt silicon pn-junction diode. This diode must have a breakdown voltage of at least 60V with a forward-bias current of 50mA when applying 0.625V. We know that the minority carrier lifetimes are $\tau_0 = 2 \times 10^{-7} s$. The parameters to engineer are doping density and cross-sectional area.**

INTRODUCTION

For this pn-junction experiment, the *PN Junction Lab* from nanoHUB.org was used [1].

PART I: ANALYTICAL DESIGN

Since we are using silicon, $\mu_n = 1350$ cm^2/Vs and $\mu_p = 480$ cm^2/Vs. And, I assume $T = 300$ K.

Using the Shockley diode equation, we can back-solve for the reverse saturation current I_s in our diode:

$$I_D = I_s(e^{V_D/V_{th}} - 1)$$
$$\implies I_s = I_D(e^{V_D/V_{th}} - 1)^{-1}$$
$$= (0.050)(e^{0.625/0.0259} - 1)^{-1}$$
$$= 1.655 \times 10^{-12} \text{ A}$$

We will use this quantity to match the reverse saturation current density J_s with doping densities and the device cross-sectional area.

A one-sided abrupt pn-junction will have either $N_d >> N_a$ or vice-versa, so choosing the former, a n^+p-junction will be made. This means the doping density in the low-doped region of the one-sided junction $N_B = N_a$. So, rearranging Equation (7.61) from the textbook:

$$N_a = \frac{\epsilon_s E_{crit}^2}{2qV_B}$$
$$= \frac{11.7(8.854 \times 10^{-14})(4 \times 10^5)^2}{2(1.6 \times 10^{-19})(60)}$$
$$\boxed{N_a = 8.633 \times 10^{15} \text{ cm}^{-3}}$$

Here, I assumed the critical electric field of silicon is 4×10^5V/cm.

Then, since this is a n^+p-junction, I will just choose N_d to be some value larger than N_a. I found graphically, when solving for the donor doping density using the equation for J_s, the function was asymptotic, so it is somewhat arbitrary when choosing the donor doping density. However, it would not make sense to make this value arbitrarily large, since larger and larger doping densities will not affect the device performance after enough doping. The donor doping density I chose was:

$$\boxed{N_d = 1 \times 10^{19} \text{ cm}^{-3}}$$

From here, we can calculate for the reverse saturation current density J_s using a form of Equation (8.27) from the textbook:

$$J_s = qn_i^2 \left(\frac{1}{N_a}\sqrt{\frac{D_n}{\tau_{n0}}} + \frac{1}{N_d}\sqrt{\frac{D_p}{\tau_{p0}}} \right)$$

Using the Einstein Relation, $D/\mu = kT/q$, the equation can be rearranged:

$$J_s = n_i^2 \sqrt{qkT} \left(\frac{1}{N_a}\sqrt{\frac{\mu_n}{\tau_0}} + \frac{1}{N_d}\sqrt{\frac{\mu_p}{\tau_0}} \right)$$
$$= (1.5 \times 10^{10})\sqrt{6.624 \times 10^{-40}} \left(\frac{1}{8.633 \times 10^{15}}\sqrt{\frac{1350}{2 \times 10^{-7}}} \right.$$
$$\left. + \frac{1}{1 \times 10^{19}}\sqrt{\frac{480}{2 \times 10^{-7}}} \right)$$
$$\boxed{J_s = 5.514 \times 10^{-11} \text{ A/cm}^2}$$

Now, we can find the cross-sectional area A, since $I_s = AJ_s$.

$$A = I_s/J_s$$
$$= (1.655 \times 10^{-12})/(5.514 \times 10^{-11})$$
$$\boxed{A = 0.03 \text{ cm}^2}$$

PART II: VERIFICATION USING NANOHUB SIMULATIONS

In the *PN Junction Lab* simulator, the input parameters are in Figure 1, and the doping profile derived in Part I is shown in Figure 2.

Once the simulator have solved for the diode device characteristics, we see that for $V_D = 0.625$ V that $J_D = 1.71751$ A/cm^2. If we use the cross-sectional area from Part I, $A = 0.03$ cm^2, then we get the forward-bias diode current to be:

$$I_D = AJ_D$$
$$= (0.03)(1.71751)$$
$$= 0.0515$$
$$\boxed{I_D = 51.5 \text{ mA}}$$
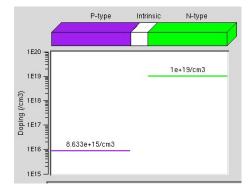
Fig. 1. Input Parameters in Simulator

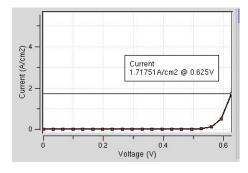Fig. 2. Doping Profile in Simulator

Fig. 3. IV-Characteristics in Simulator

ANSWERS TO QUESTIONS

What is the built-in potential in equilibrium, V_{bi}?

$$V_{bi} = V_t \ln\left(\frac{N_a N_d}{n_i^2}\right)$$

$$= (0.0259) \ln\left(\frac{(8.633 \times 10^{15})(1 \times 10^{19})}{(1.5 \times 10^{10})^2}\right)$$

$$= 0.870$$

$$\therefore \boxed{V_{bi} = 0.870 \text{ V}}$$

What is the maximum electric field, E_{max}?

For the doping concentration in Silicon, $E_{max} = 4 \times 10^5$ V/cm.

Is it possible to arbitrarily increase doping concentration?

It is not practical to do so. Like I mentioned in Part I, J_s approaches a finite value as $N_d \to \infty$. So, it is most efficient to choose the lowest possible doping density to achieve the current necessary, since it will be most cost-effective.

Do you obtain the same forward-bias current from these two calculations? Why or why not?

The currents are the same once I varied the p-type and n-type lengths in the simulator. In this case, the p-type region was $11\mu m$ and the n-type region was $7\mu m$. My guess is this changes the lengths over which the charge carriers diffuse in the diode, which is directly proportional to the current in the device.

What happens to the I-V curve if the temperature is increased to 500K? Why?

When re-simulating with $T = 500$K, the I-V curve drastically increases in value. The new forward-bias diode current density for the same forward-bias voltage is $J_D = 1176.59$ A/cm^2, which means the forward-bias diode current is $I_D = 35.3$ A.

This is because the diode current is proportional to the intrinsic carrier density squared, and the intrinsic carrier density is exponentially dependent on temperature.

$$I_D \propto n_i^2 \propto e^{-E_g/kT}$$

Using simulations, discuss what happens to the I-V curve if carrier lifetimes are increased by a factor of 100 (that is recombination is suppressed).

Re-simulating the device with $\tau_0 = 2 \times 10^{-5}$ s, and $T = 300$K, the forward-bias diode current density for the same forward-bias voltage is $J_D = 1.62108$ A/cm^2, which means the forward-bias diode current is $I_D = 48.6$ mA. Which is a slight decrease to our original current.

This is expected since the reverse saturation current is inversely dependent on the square roots of the minority carrier lifetimes.

REFERENCES

[1] e. a. Vasileska, Dragica, "Pn junction lab," https://nanohub.org/resources/pntoy, 2014.