

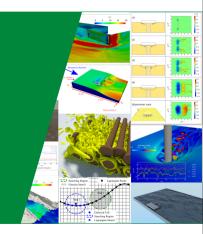
中国农业大学 流体机械与流体工程系

2024年春季《计算流体动力学编程实践》

2.3 有限体积法编程 一维稳态扩散问题

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- ▶ 有限体积法空间离散
- ▶ 一维稳态扩散方程离散的一般形式
- ▶ 案例分析
 - 案例1: 一维稳态无源热传导
 - 案例2: 一维稳态有源热传导
 - 案例3: 一维稳态有源热传导带通量边界
 - 案例4: 二维稳态有源热传导

离散 discretisation

- ▶ 通用输运方程很少存在解析解,这就是为什么需要数值分析方法
- ▶ 离散是指用一组线性表达来表示所求的微分方程
- ▶ 有很多中离散方法,包括:有限差分法(FDM, finite difference method)、有限单元法(FEM, finite element method)、有限体积法(FVM, finite volume method)
- ▶ 这门课我们主要介绍OpenFOAM所使用的FVM

- ▶ 将控制方程在控制体积上进行积分
- ▶ 假定适合的分布函数
- ▶ 将分布函数代入并完成积分,整理化简得离散化方程

扩散是高浓度向低浓度输移的过程

▶ 完整通用输运方程

$$\frac{\partial \phi}{\partial t} + \underbrace{\nabla \cdot (\phi \mathbf{u})}_{\text{convection term}} - \underbrace{\nabla \cdot (\gamma \nabla \phi)}_{\text{diffusion term}} = \underbrace{\mathbf{S}_{\phi}}_{\text{source term}}$$
temopral derivative 对流项 扩散项 is source term is source term is source.

▶ 简化的稳态扩散方程

$$\nabla \cdot (\gamma \nabla \phi) + \mathbf{S}_{\phi} = 0 \tag{2}$$
diffusion term source term



扩散是高浓度向低浓度输移的过程

▶ 完整通用输运方程:

$$\frac{\partial \phi}{\partial t} + \underbrace{\nabla \cdot (\phi \mathbf{u})}_{\text{convection term}} - \underbrace{\nabla \cdot (\gamma \nabla \phi)}_{\text{diffusion term}} = \underbrace{\mathbf{S}_{\phi}}_{\text{source term}}$$
时间偏导

▶ 简化的稳态扩散方程

$$\underbrace{\nabla \cdot (\gamma \nabla \phi)}_{\text{diffusion term}} + \underbrace{\mathbf{S}_{\phi}}_{\text{source term}} = 0$$
(2)

扩散是高浓度向低浓度输移的过程

▶ 完整通用输运方程:

$$\underbrace{\frac{\partial \phi}{\partial t}}_{\text{temopral derivative}} + \underbrace{\nabla \cdot (\phi \mathbf{u})}_{\text{convection term}} - \underbrace{\nabla \cdot (\gamma \nabla \phi)}_{\text{diffusion term}} = \underbrace{\mathbf{S}_{\phi}}_{\text{source term}} \tag{1}$$

▶ 简化的稳态扩散方程

有限体积法(FVM)离散

▶ 在控制体积上进行积分

$$\int_{CV} \nabla \cdot (\gamma \nabla \phi) dV + \int_{CV} S_{\phi} dV = \int_{A} \mathbf{n} \cdot (\gamma \nabla \phi) dA + \int_{CV} S_{\phi} dV = 0$$
 (3)

▶ 以简化后的—维方程为何

$$\frac{d}{dx}\left(\gamma\frac{d\phi}{dx}\right) + S = 0\tag{4}$$

有限体积法(FVM)离散

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▶ 以简化后的一维方程为例

$$\frac{d}{dx}\left(\gamma\frac{d\phi}{dx}\right) + S = 0\tag{4}$$

$$\frac{d^2\phi}{dx^2} + S = 0$$
 $\phi|_{x=0} = 1$, $\phi|_{x=L} = 0$ 一维稳态扩散稳态 (5)

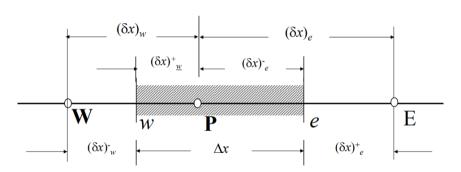


图: 一维问题空间区域的离散化

(5)

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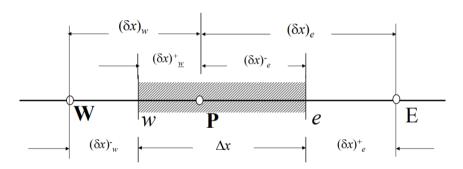
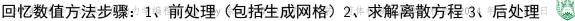
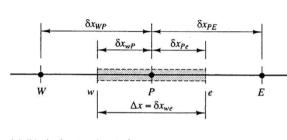


图: 一维问题空间区域的离散化



OpenFOAM® 中一维稳态扩散方程



扩散方程积分形式:

$$\int_{A} \mathbf{n} \cdot (\gamma \nabla \phi) dA + \int_{CV} S dV = 0$$

$$\frac{d}{dx}\left(\gamma \frac{d\phi}{dx}\right) + S = 0$$

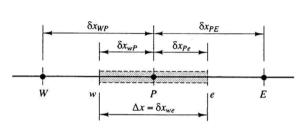
OpenFOAM®中使用3D网格处理1D、2D计算问题 使用FVM进行率数。

$$\int_{A} \mathbf{n} \cdot (\gamma \nabla \phi) dA + \int_{CV} S dV = 0$$

$$\left(\gamma A \frac{d\phi}{dx} \right)_{e} - \left(\gamma A \frac{d\phi}{dx} \right)_{w} + \overline{S} \Delta V = 0$$



OpenFOAM® 中一维稳态扩散方程



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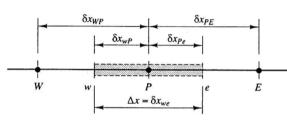
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扩散方程FVM离散形式:

$$\left(\gamma A \frac{d\phi}{dx}\right) - \left(\gamma A \frac{d\phi}{dx}\right) + \overline{S}\Delta V = 0$$

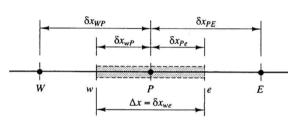
线性分布假设下w和e上的扩散系数:

$$\gamma_w = \frac{\gamma_W + \gamma_P}{2}, \ \gamma_e = \frac{\gamma_P + \gamma_E}{2}$$

利用中心差分计算导数 (梯度):

$$\left(\frac{d\phi}{dx}\right)_e = \frac{\phi_E - \phi_P}{\delta x_{PE}}, \quad \left(\frac{d\phi}{dx}\right)_w = \frac{\phi_P - \phi_W}{\delta x_{WP}}$$





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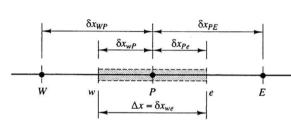
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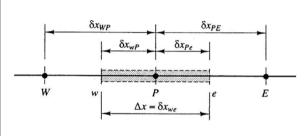
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OpenFOAM® 中一维稳态扩散方程



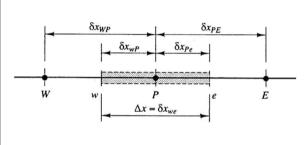
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交界面上的扩散通量 diffusive fluxes at interfaces

$$\left(\gamma A \frac{d\phi}{dx}\right)_e = \gamma_e A_e \frac{\phi_E - \phi_P}{\delta x_{PE}}$$
$$\left(\gamma A \frac{d\phi}{dx}\right)_w = \gamma_w A_w \frac{\phi_P - \phi_W}{\delta x_{WP}}$$





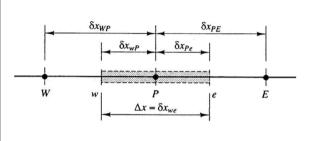
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$$\gamma_w = \frac{\gamma_W + \gamma_P}{2}, \ \gamma_e = \frac{\gamma_P + \gamma_E}{2}$$

gradient scheme (梯度格式)

$$\left(\frac{d\phi}{dx}\right)_e = \frac{\phi_E - \phi_P}{\delta x_{PE}}, \quad \left(\frac{d\phi}{dx}\right)_w = \frac{\phi_P - \phi_W}{\delta x_{WP}}$$





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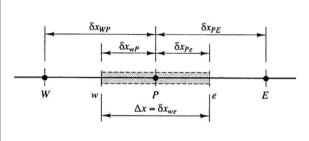
在算例目录中的system/fvScheme中存在

laplacian(nu,U) Gauss linear corrected;

Gauss <interpolationScheme> <snGradScheme> (其中sn=>surface normal)

laplacian(nu,U)数学表达:
$$\nabla \cdot (\nu \nabla U) \Rightarrow \frac{d}{dx} \left(\gamma \frac{d\phi}{dx} \right)$$





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源项S通常与变量 ϕ 相关,如果用线性方式表达:

$$\overline{S}\Delta V = S_u + S_n \phi_P$$

(6)

将所有离散项代入一维稳态扩散方程 $\frac{d}{dx}\left(\gamma\frac{d\phi}{dx}\right)+S=0$

$$\gamma_e A_e \frac{\phi_E - \phi_P}{\delta x_{PF}} - \gamma_w A_w \frac{\phi_P - \phi_W}{\delta x_{WP}} + (S_u + S_p \phi_P) = 0$$

整理后得到

$$\underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e + \frac{\gamma_w}{\delta x_{WP}} A_w - S_p\right)}_{a_B} \phi_P = \underbrace{\left(\frac{\gamma_w}{\delta x_{WP}} A_w\right)}_{a_W} \phi_W + \underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e\right)}_{a_E} \phi_E + S_u \quad (8)$$

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FVM 离散-源项 source term

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整理后得到

$$\underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e + \frac{\gamma_w}{\delta x_{WP}} A_w - S_p\right)}_{a_P} \phi_P = \underbrace{\left(\frac{\gamma_w}{\delta x_{WP}} A_w\right)}_{a_W} \phi_W + \underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e\right)}_{a_E} \phi_E + S_u \tag{8}$$

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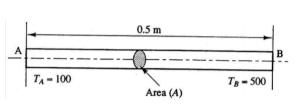
$$\underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e + \frac{\gamma_w}{\delta x_{WP}} A_w - S_p\right)}_{a_B} \phi_P = \underbrace{\left(\frac{\gamma_w}{\delta x_{WP}} A_w\right)}_{a_W} \phi_W + \underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e\right)}_{a_E} \phi_E + S_u \quad (8)$$

$$\underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e + \frac{\gamma_w}{\delta x_{WP}} A_w - S_p\right)}_{a_P} \phi_P = \underbrace{\left(\frac{\gamma_w}{\delta x_{WP}} A_w\right)}_{a_W} \phi_W + \underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e\right)}_{a_E} \phi_E + S_u$$

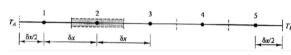
一般形式:

$$a_P \phi_P = a_W \phi_W + a_E \phi_E + S_u \tag{9}$$

对于靠近计算域边界的控制体积,需要根据特定的边界条件对该方程进行修改



铁棒总长0.5m,平均分成5份,每份长度 $\delta x=0.1m$

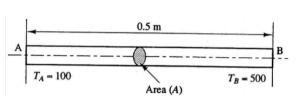


控制方程

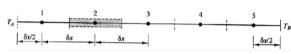
$$\frac{d}{dx}\left(k\frac{dT}{dx}\right) = 0\tag{10}$$

共有五个网格, 2、3、4是内部网格, 1和5是与边界相邻网格

边界条件: $T_A = 100, T_B = 500$ $k = 1000W/m/K和A = 10 \times 10^{-3}m^2$



铁棒总长0.5m, 平均分成5份, 每份长度 $\delta x = 0.1m$



控制方程

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内部网格离散

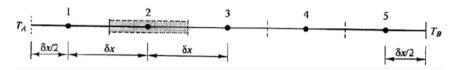
离散方程的一般形式:

$$\underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e + \frac{\gamma_w}{\delta x_{WP}} A_w - S_p\right)}_{a_P} \phi_P = \underbrace{\left(\frac{\gamma_w}{\delta x_{WP}} A_w\right)}_{a_W} \phi_W + \underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e\right)}_{a_E} \phi_E + S_u$$

对于内部网格2、3、4, 离散方程可写成:

$$a_P T_P = a_W T_W + a_E T_E + S_u \tag{11}$$

其中 $a_W = \frac{k}{\delta x}A$, $a_E = \frac{k}{\delta x}A$, $a_P = a_W + a_E = 2\frac{k}{\delta x}A$ 2024年春季《计算流体动力学编程实践》 by 徐云成 @ 中国农业大学 流体机械与流体工程系 2024 年 2 月 27 日

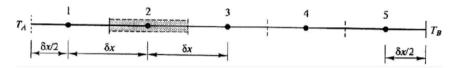


假设网格1中心与边界A之间温度呈线性分布. 边界网格1的离散方程:

$$kA\left(\frac{T_E - T_P}{\delta x}\right) - kA\left(\frac{T_P - T_A}{\delta x/2}\right) = 0$$
 (12)

整理后得到

$$\left(\frac{k}{\delta x}A + \frac{2k}{\delta x}A\right)T_P = 0 \cdot T_W + \left(\frac{k}{\delta x}A\right)T_E + \left(\frac{2k}{\delta x}A\right)T_A \tag{13}$$

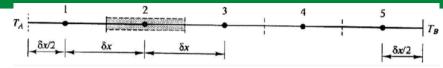


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边界网格离散:
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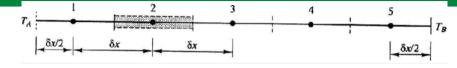
一般形式

$$\underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e + \frac{\gamma_w}{\delta x_{WP}} A_w - S_p\right)}_{a_P} \phi_P = \underbrace{\left(\frac{\gamma_w}{\delta x_{WP}} A_w\right)}_{a_W} \phi_W + \underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e\right)}_{a_E} \phi_E + S_u$$

观察 \Rightarrow 相当于源项 $(S_u + S_P T_P)$:

$$S_u = \frac{2kA}{\delta x}T_A$$
, $S_P = -\frac{2kA}{\delta x}$





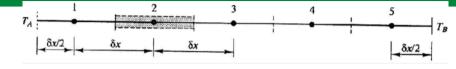
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一般形式:
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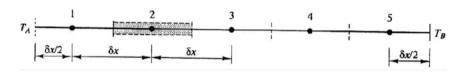
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$$S_u = \frac{2kA}{\delta x}T_A$$
, $S_P = -\frac{2kA}{\delta x}$



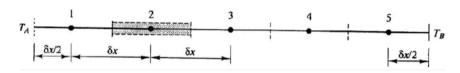


网格1:
$$\left(\frac{k}{\delta x}A + \frac{2k}{\delta x}A\right)T_P = 0 \cdot T_W + \left(\frac{k}{\delta x}A\right)T_E + \left(\frac{2k}{\delta x}A\right)T_A$$

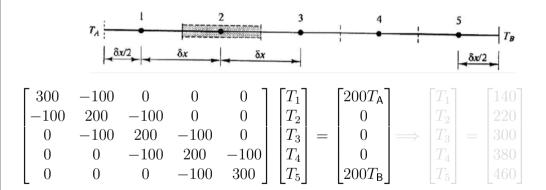
网格2、3、4: $\left(\frac{2k}{\delta x}A\right)T_P = \left(\frac{k}{\delta x}A\right)T_W + \left(\frac{k}{\delta x}A\right)T_E$

网格5: $\left(\frac{k}{\delta x}A + \frac{2k}{\delta x}A\right)T_P = \left(\frac{k}{\delta x}A\right)T_W + 0 \cdot T_E + \left(\frac{2k}{\delta x}A\right)T_B$

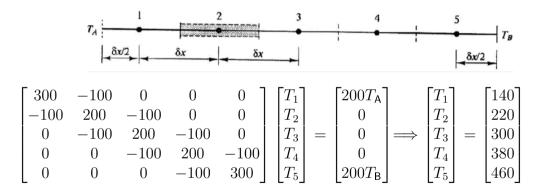
铁棍的横截面A可以消掉,整个计算与A无关



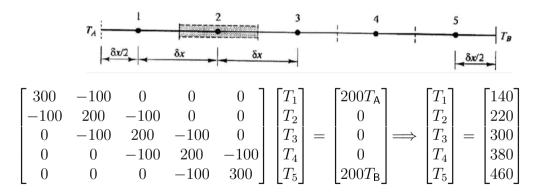
网格1:
$$\left(\frac{k}{\delta x}A + \frac{2k}{\delta x}A\right)T_P = 0 \cdot T_W + \left(\frac{k}{\delta x}A\right)T_E + \left(\frac{2k}{\delta x}A\right)T_A$$
 网格2、3、4: $\left(\frac{2k}{\delta x}A\right)T_P = \left(\frac{k}{\delta x}A\right)T_W + \left(\frac{k}{\delta x}A\right)T_E$ 网格5: $\left(\frac{k}{\delta x}A + \frac{2k}{\delta x}A\right)T_P = \left(\frac{k}{\delta x}A\right)T_W + 0 \cdot T_E + \left(\frac{2k}{\delta x}A\right)T_B$ 铁棍的横截面 A 可以消掉,整个计算与 A 无关



1000T'' = 0, T(x = 0) = 100, $T(x = 0.5) = 500 \implies T(x) = 800x + 100$



1000T'' = 0, T(x = 0) = 100, $T(x = 0.5) = 500 \implies T(x) = 800x + 100$



 $1000T'' = 0, T(x = 0) = 100, T(x = 0.5) = 500 \implies T(x) = 800x + 100$

代码解读

```
该案例已放至code_practice/diffusionEqs/
案例名字为1D_rod
求解器名字为steadyDiffusionFoam
关键代码
```

```
fvScalarMatrix TEqn
(
    fvm::laplacian(DT, T)
);

//save the matrix and source to a file
saveMatrix(TEqn);
```

TEqn.solve();

```
fvScalarMatrix TEqn
(
    fvm::laplacian(DT, T)
);

//save the matrix and source to a file
saveMatrix(TEqn);
```

TEqn.solve();

 控制方程离散后构成一个线性方程 组Ax = b, 储存在fvScalarMatrix。 这里fvScalarMatrix是一个重要的 类(class), 定义了一个对象(object): TEqn

fvm::laplacian(DT, T)表示用隐性 格式离散 $\nabla \cdot (D_T) \nabla T$, D_T 是扩散系 数。

fvScalarMatrix通常不会直接考虑 边界条件

· 边界条件是通过源项的方式 $(S_u + S_P T_P)$ 添加进系数矩阵,是在TRange galve() 中宗成

```
fvScalarMatrix TEqn
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    fvm::laplacian(DT, T)
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TEqn.solve();
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 控制方程离散后构成一个线性方程 组Ax = b, 储存在fvScalarMatrix。 这里fvScalarMatrix是一个重要的 类(class), 定义了一个对象(object): TEqn

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abla T$, D_T 是扩散系 数。

- fvScalarMatrix通常小会直接考虑 边界条件
- 边界条件是通过源项的方式 $(S_u + S_P T_P)$ 添加进系数矩阵,

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fvScalarMatrix TEqn
(
    fvm::laplacian(DT, T)
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 控制方程离散后构成一个线性方程 组Ax = b, 储存在fvScalarMatrix。 这里fvScalarMatrix是一个重要的 类(class), 定义了一个对象(object): TEqn

格式离散 $\nabla \cdot (D_T) \nabla T$, D_T 是扩散系数。 • fvScalarMatrix通常不会直接考虑

fvm::laplacian(DT, T)表示用隐性

- 边界条件
- 边界条件是通过源项的方式 $(S_n + S_p T_p)$ 添加进系数矩

```
fvScalarMatrix TEqn
(
    fvm::laplacian(DT, T)
);

//save the matrix and source to a file
saveMatrix(TEqn);
```

TEqn.solve();

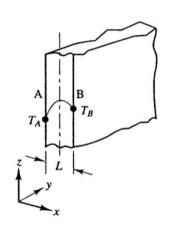
 控制方程离散后构成一个线性方程 组Ax = b, 储存在fvScalarMatrix。 这里fvScalarMatrix是一个重要的 类(class), 定义了一个对象(object): TEqn

· fvm::laplacian(DT, T)表示用隐性 格式离散▽·(D_T)▽T, D_T是扩散系 数。 · fvScalarMatrix通常不全直接考虑

- ► fvScalarMatrix通常不会直接考虑 边界条件
- ▶ 边界条件是通过源项的方 式 $(S_u + S_P T_P)$ 添加进系数矩阵,是 在TEan.solve()中完成

案例1: 代码使用说明

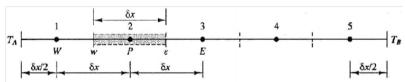
```
利用git工具下载代码
git clone https://gitee.com/cfdxu/cau of course.git
或者更新文件
cd cau of course
git fetch --all; git pull
进入储存代码的文件夹
cd code_practice/diffusionEqs/
解压缩文件包,内含有steadyDiffusion算例和求解器
tar xzf steadyDiffusionFoam.tgz
编译steadyDiffusionFoam求解器
cd steadyDiffusionFoam/steadyDiffusionFoam/
wmake
进入1D rod算例, 并运行算例
cd ../1D_rod/; ./Allrun
```



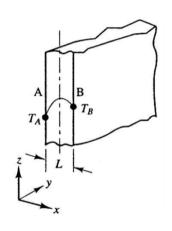
控制方程

$$\frac{d}{dx}\left(k\frac{dT}{dx}\right) + q = 0\tag{14}$$

有一块平板,厚度为L=2cm,热传导系数k=0.5W/m/K,平均分布的热源 $q=10^6W/m^3$,A、B两面的温度分别为 $100^{\circ}C$ 和 $500^{\circ}C$ 。该问题在一维上模拟时,仅考虑x方向。



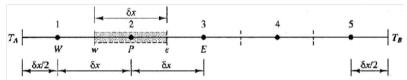
该平板平均分成5份,每份长度 $\delta x = 0.0.004m$



控制方程

$$\frac{d}{dx}\left(k\frac{dT}{dx}\right) + q = 0\tag{14}$$

有一块平板,厚度为L=2cm,热传导系数k=0.5W/m/K,平均分布的热源 $q=10^6W/m^3$,A、B两面的温度分别为 $100^{\circ}C$ 和 $500^{\circ}C$ 。该问题在一维上模拟时,仅考虑x方向。

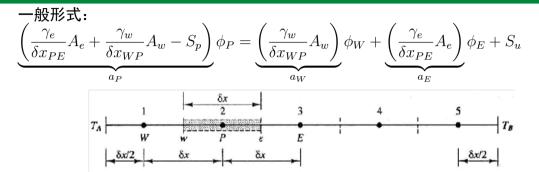


该平板平均分成5份,每份长度 $\delta x = 0.0.004m$

024年春季《计算流体动力学编程类选有五个网格,国名业3学4是内部网格。程1和5是边界网格

内部网格离散

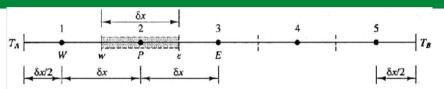
4/43



对于内部网格2、3、4, 离散方程可写成:

$$a_P T_P = a_W T_W + a_E T_E + S_u \tag{15}$$

其中 $a_W=rac{k}{\delta x}A$, $a_E=rac{k}{\delta x}A$, $a_P=a_W+a_E-S_P=2rac{k}{\delta x}A$, $S_u=qA\delta x$, $S_P=0$ 2024年春季《计算流体动力学编程实践》 by 徐云成 @ 中国农业大学 流体机械与流体工程系 2024 年 2 月 27 日

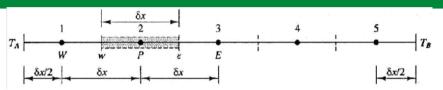


假设网格1中心与边界A之间温度呈线性分布,边界网格1的离散方程:

$$kA\left(\frac{T_E - T_P}{\delta x}\right) - kA\left(\frac{T_P - T_A}{\delta x/2}\right) + qA\delta x = 0$$
 (16)

整理后得到

$$\left(\frac{k}{\delta x}A + \frac{2k}{\delta x}A\right)T_P = 0 \cdot T_W + \left(\frac{k}{\delta x}A\right)T_E + qA\delta x + \left(\frac{2k}{\delta x}A\right)T_A \tag{17}$$

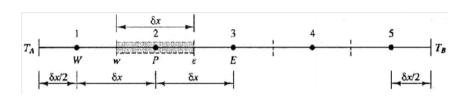


假设网格1中心与边界A之间温度呈线性分布,边界网格1的离散方程:

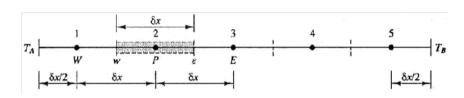
$$kA\left(\frac{T_E - T_P}{\delta x}\right) - kA\left(\frac{T_P - T_A}{\delta x/2}\right) + qA\delta x = 0$$
 (16)

整理后得到

$$\left(\frac{k}{\delta x}A + \frac{2k}{\delta x}A\right)T_P = 0 \cdot T_W + \left(\frac{k}{\delta x}A\right)T_E + qA\delta x + \left(\frac{2k}{\delta x}A\right)T_A \tag{17}$$

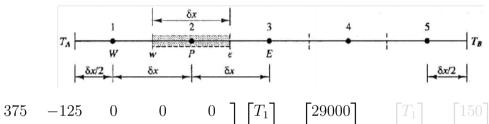


网格1:
$$\left(\frac{k}{\delta x}A + \frac{2k}{\delta x}A\right)T_P = 0 \cdot T_W + \left(\frac{k}{\delta x}A\right)T_E + \left(\frac{2k}{\delta x}A\right)T_A + qA\delta x$$
网格2、3、4: $\left(\frac{2k}{\delta x}A\right)T_P = \left(\frac{k}{\delta x}A\right)T_W + \left(\frac{k}{\delta x}A\right)T_E + qA\delta x$
网格5: $\left(\frac{k}{\delta x}A + \frac{2k}{\delta x}A\right)T_P = \left(\frac{k}{\delta x}A\right)T_W + 0 \cdot T_E + \left(\frac{2k}{\delta x}A\right)T_B + qA\delta x$
平板的面积 A可以消掉。整个计算与 A无关



网格1:
$$\left(\frac{k}{\delta x}A + \frac{2k}{\delta x}A\right)T_P = 0 \cdot T_W + \left(\frac{k}{\delta x}A\right)T_E + \left(\frac{2k}{\delta x}A\right)T_A + qA\delta x$$
网格2、3、4: $\left(\frac{2k}{\delta x}A\right)T_P = \left(\frac{k}{\delta x}A\right)T_W + \left(\frac{k}{\delta x}A\right)T_E + qA\delta x$
网格5: $\left(\frac{k}{\delta x}A + \frac{2k}{\delta x}A\right)T_P = \left(\frac{k}{\delta x}A\right)T_W + 0 \cdot T_E + \left(\frac{2k}{\delta x}A\right)T_B + qA\delta x$

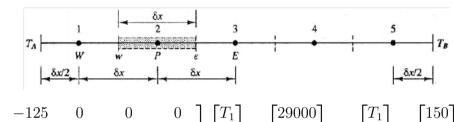
平板的面积A可以消掉,整个计算与A无关



$$\begin{bmatrix} -125 & 250 & -125 & 0 & 0 \\ 0 & -125 & 250 & -125 & 0 \\ 0 & 0 & -125 & 250 & -125 \\ 0 & 0 & 0 & -125 & 375 \end{bmatrix} \begin{bmatrix} T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 4000 \\ 4000 \\ 4000 \\ 29000 \end{bmatrix} \Longrightarrow \begin{bmatrix} T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 218 \\ 254 \\ 258 \\ 230 \end{bmatrix}$$

解析解:
$$T(x) = \left| \frac{T_B - T_A}{L} + \frac{q}{2k}(L - x) \right| x + T_A$$

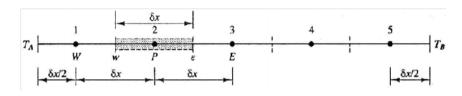




$$\begin{bmatrix} 375 & -125 & 0 & 0 & 0 \\ -125 & 250 & -125 & 0 & 0 \\ 0 & -125 & 250 & -125 & 0 \\ 0 & 0 & -125 & 250 & -125 \\ 0 & 0 & 0 & -125 & 375 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 29000 \\ 4000 \\ 4000 \\ 4000 \\ 29000 \end{bmatrix} \Longrightarrow \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 150 \\ 218 \\ 254 \\ 258 \\ 230 \end{bmatrix}$$

解析解:
$$T(x) = \left| \frac{T_B - T_A}{L} + \frac{q}{2k}(L - x) \right| x + T_A$$





$$\begin{bmatrix} 375 & -125 & 0 & 0 & 0 \\ -125 & 250 & -125 & 0 & 0 \\ 0 & -125 & 250 & -125 & 0 \\ 0 & 0 & -125 & 250 & -125 \\ 0 & 0 & 0 & -125 & 375 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 29000 \\ 4000 \\ 4000 \\ 4000 \\ 29000 \end{bmatrix} \Longrightarrow \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 150 \\ 218 \\ 254 \\ 258 \\ 230 \end{bmatrix}$$

解析解:
$$T(x) = \left[\frac{T_B - T_A}{L} + \frac{q}{2k}(L - x)\right]x + T_A$$

```
该案例已放至code_practice/diffusionEqs
案例名字为1D_plate_with_src
求解器名字为steadyDiffusionWithSourceFoam 关键代码
```

```
fvScalarMatrix TEqn
(
    fvm::laplacian(DT, T)
    +q
);
```

```
pr pr [ 0 2 -1 0 0 0 0 ] 0.5;
q q [ 0 0 -1 1 0 0 0 ] 1E6;
```



```
该案例已放至code_practice/diffusionEqs
案例名字为1D_plate_with_src
求解器名字为steadyDiffusionWithSourceFoam 关键代码
```

```
fvScalarMatrix TEqn
(
    fvm::laplacian(DT, T)
    +q
);
```

热传导系数 D_T 和热源q在constant/transportProperties中定义

```
DT DT [ 0 2 -1 0 0 0 0 ] 0.5;
q q [ 0 0 -1 1 0 0 0 ] 1E6;
```

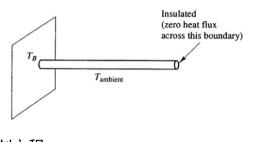
```
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案例名字为1D_plate_with_src
求解器名字为steadyDiffusionWithSourceFoam 关键代码
```

```
fvScalarMatrix TEqn
    fvm::laplacian(DT, T)
   +q
```

热传导系数 D_T 和热源q在constant/transportProperties中定义

```
DT
                DT [ 0 2 -1 0 0 0 0 ] 0.5;
                q [ 0 0 -1 1 0 0 0 ] 1E6;
q
```

质量(kg);长度(m);时间(s);温度(K);摩尔数(mol);电流(A);光强度(cd)



一根长L=1m棍子放置在温度恒定为 $T_{\infty}=20\circ C$ 的环境中, $n^2=25/m^2$ 。其中一端(A)绝热的(insulated),没有热通量,即 $\mathbf{n}_x\cdot(\nabla T)=0$ 另一端(B)保持恒温 $T_B=100\circ C$ 解析解是

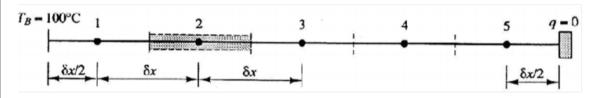
控制方程

$$\frac{d}{dx}\left(\frac{dT}{dx}\right) - n^2(T - T_{\infty}) = 0 \tag{18}$$

$$\frac{T(x) - T_{\infty}}{T_B - T_{\infty}} = \frac{\cosh[n(L - x)]}{\cosh(nL)} \tag{19}$$

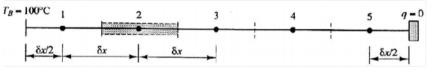
其中 $n^2=hp/(kA)$,h是对流热传导系数,p是圆周长, T_{∞} 是环境温度

网格离散化



该平板平均分成5份,每份长度 $\delta x=0.2m$ 共有五个网格,2、3、4是内部网格,1和5是边界网格 一般形式:

$$\underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e + \frac{\gamma_w}{\delta x_{WP}} A_w - S_p\right)}_{a_P} \phi_P = \underbrace{\left(\frac{\gamma_w}{\delta x_{WP}} A_w\right)}_{a_W} \phi_W + \underbrace{\left(\frac{\gamma_e}{\delta x_{PE}} A_e\right)}_{a_E} \phi_E + S_u$$

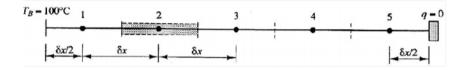


对于内部网格2、3、4, 离散方程可写成:

$$a_P T_P = a_W T_W + a_E T_E + S_u \tag{20}$$

其中 $a_W = \frac{1}{\delta x}$, $a_E = \frac{1}{\delta x}$, $a_P = a_W + a_E - S_P = \frac{2}{\delta x} + n^2 \delta x$,

$$S_u = n^2 \delta x T_\infty$$
 , $S_P = -n^2 \delta x$ 2024年春季《计算流体动力学编程实践》 by 徐云成 @ 中国农业大学 流体机械与流体工程系 2024年2月27日

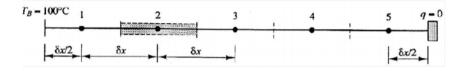


假设网格1中心与边界B之间温度呈线性分布,边界网格1的离散方程:

$$\left(\frac{T_E - T_P}{\delta x}\right) - \left(\frac{T_P - T_B}{\delta x/2}\right) - \left[n^2(T_P - T_\infty)\delta x\right] = 0$$
(21)

整理后得到

$$\left(\frac{1}{\delta x} + \frac{2}{\delta x} + n^2 \delta x\right) T_P = 0 \cdot T_W + \left(\frac{1}{\delta x}\right) T_E + n^2 \delta x T_\infty + \left(\frac{2}{\delta x}\right) T_B \tag{22}$$



假设网格1中心与边界B之间温度呈线性分布,边界网格1的离散方程:

$$\left(\frac{T_E - T_P}{\delta x}\right) - \left(\frac{T_P - T_B}{\delta x/2}\right) - \left[n^2 (T_P - T_\infty) \delta x\right] = 0$$
(21)

整理后得到

$$\left(\frac{1}{\delta x} + \frac{2}{\delta x} + n^2 \delta x\right) T_P = 0 \cdot T_W + \left(\frac{1}{\delta x}\right) T_E + n^2 \delta x T_\infty + \left(\frac{2}{\delta x}\right) T_B \tag{22}$$

$$T_B = 100^{\circ}\text{C}$$
 1 2 3 4 5 $q = 0$

观察:
$$\left(\frac{1}{\delta x} + \frac{2}{\delta x} + n^2 \delta x\right) T_P = 0 \cdot T_W + \left(\frac{1}{\delta x}\right) T_E + n^2 \delta x T_\infty + \left(\frac{2}{\delta x}\right) T_B \Rightarrow$$
相当

于源项 $(S_u + S_P T_P)$

$$S_u = \frac{2}{\delta x} T_{\mathsf{B}}, \quad S_P = -\frac{2}{\delta x}$$

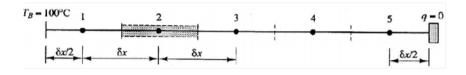


$$T_B = 100^{\circ}\text{C}$$
 1 2 3 4 5 $q = 0$ $\delta x/2$ δx δx

观察:
$$\left(\frac{1}{\delta x} + \frac{2}{\delta x} + n^2 \delta x\right) T_P = 0 \cdot T_W + \left(\frac{1}{\delta x}\right) T_E + n^2 \delta x T_\infty + \left(\frac{2}{\delta x}\right) T_B \Rightarrow$$
相当

于源项
$$(S_u + S_P T_P)$$
:

$$S_u = \frac{2}{\delta x} T_{\mathsf{B}}, \quad S_P = -\frac{2}{\delta x}$$



边界网格5与边界网格1的离散方式不同,边界网格5右侧的面的通量为零

$$\left[0 - \left(\frac{T_P - T_W}{\delta x}\right)\right] - \left[n^2 (T_P - T_\infty) \delta x\right] = 0 \tag{23}$$

整理后得到

$$\left(\frac{1}{\delta x} + n^2 \delta x\right) T_P = \frac{1}{\delta x} \cdot T_W + 0 \cdot T_E + n^2 \delta x T_\infty \tag{24}$$

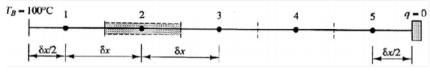
网格离散

$$T_B = 100^{\circ}\text{C}$$
 1 2 3 4 5 $q = 0$ $\delta x/2$ δx δx

网格1:
$$\left(\frac{1}{\delta x} + \frac{2}{\delta x} + n^2 \delta x\right) T_P = 0 \cdot T_W + \left(\frac{1}{\delta x}\right) T_E + n^2 \delta x T_\infty + \left(\frac{2}{\delta x}\right) T_B$$

网格2、3、4: $\left(\frac{2}{\delta x} + n^2 \delta x\right) T_P = \left(\frac{1}{\delta x}\right) T_W + \left(\frac{1}{\delta x}\right) T_E + n^2 \delta x T_\infty$

网格5: $\left(\frac{1}{\delta x} + n^2 \delta x\right) T_P = \frac{1}{\delta x} \cdot T_W + 0 \cdot T_E + n^2 \delta x T_\infty$

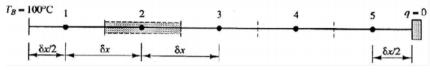


$$\begin{bmatrix} 20 & -5 & 0 & 0 & 0 \\ -5 & 15 & -5 & 0 & 0 \\ 0 & -5 & 15 & -5 & 0 \\ 0 & 0 & -5 & 15 & -5 \\ 0 & 0 & 0 & -5 & 10 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 1100 \\ 100 \\ 100 \\ 100 \\ 100 \end{bmatrix} \Longrightarrow \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 64.22 \\ 36.91 \\ 26.50 \\ 22.60 \\ 22.30 \end{bmatrix}$$

解析解是

$$\frac{T(x) - T_{\infty}}{T_B - T_{\infty}} = \frac{\cosh[n(L - x)]}{\cosh(nL)}$$





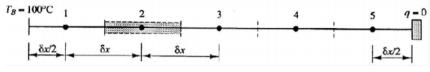
$$\begin{bmatrix} 20 & -5 & 0 & 0 & 0 \\ -5 & 15 & -5 & 0 & 0 \\ 0 & -5 & 15 & -5 & 0 \\ 0 & 0 & -5 & 15 & -5 \\ 0 & 0 & 0 & -5 & 10 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 1100 \\ 100 \\ 100 \\ 100 \end{bmatrix} \Longrightarrow \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 64.22 \\ 36.91 \\ 26.50 \\ 22.60 \\ 22.30 \end{bmatrix}$$

解析解是

$$\frac{T(x) - T_{\infty}}{T_B - T_{\infty}} = \frac{\cosh[n(L - x)]}{\cosh(nL)}$$



建立系数矩阵方程



$$\begin{bmatrix} 20 & -5 & 0 & 0 & 0 \\ -5 & 15 & -5 & 0 & 0 \\ 0 & -5 & 15 & -5 & 0 \\ 0 & 0 & -5 & 15 & -5 \\ 0 & 0 & 0 & -5 & 10 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 1100 \\ 100 \\ 100 \\ 100 \end{bmatrix} \Longrightarrow \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 64.22 \\ 36.91 \\ 26.50 \\ 22.60 \\ 22.30 \end{bmatrix}$$

解析解是

$$\frac{T(x) - T_{\infty}}{T_B - T_{\infty}} = \frac{\cosh[n(L - x)]}{\cosh(nL)}$$



```
该案例已放至code_practice/diffusionEqs
案例名字为1D_rod_convective_cooling
求解器名字为steadyDiffusionWithCoolingFoam
关键代码
```

```
fvScalarMatrix TEqn
(
    fvm::laplacian(T)
    ==
    fvm::Sp(alpha,T)
    - alpha*Tinf
);
```

```
其中\operatorname{alpha}: \alpha = n^2\operatorname{Tinf}: T_{\infty}\operatorname{ATEX}代码\operatorname{ST}_{-}\operatorname{infty}\operatorname{fvm}: \operatorname{Sp}(\operatorname{alpha}, \operatorname{T})
```

```
vw:: Sp(alpha,T)
\downarrow
原项(S_u + S_P T_P)
内部网格: S_P = -n^2 \delta x
B边界网格: S_P = -\frac{2}{\delta x}
```

lpha和环境温度Tinf在constant/transportProperties中定义 lpha alpha [0-20000]25;

);

```
该案例已放至code_practice/diffusionEqs
案例名字为1D_rod_convective_cooling
求解器名字为steadyDiffusionWithCoolingFoam
关键代码
fvScalarMatrix TEqn
```

```
ScalarMatrix TEqn fvm::Sp(alpha fvm::Sp(S_u + S_p T_p fvm::Sp(S_u + S_p T_p fvm::Sp(alpha, fvm::Sp(alpha) fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:fvm:f
```

其中

 $alpha: \alpha = n^2$

PTFX代码\$T_\infty\$

Tinf T_{∞}

lpha和环境温度Tinf在constant/transportProperties中定义 lpha alpha [0-20000]25;

```
该案例已放至code_practice/diffusionEqs
案例名字为1D_rod_convective_cooling
求解器名字为steadyDiffusionWithCoolingFoam
关键代码

fvScalarMatrix TEqn
(
fvm::laplacian(T)
```

fvm::Sp(alpha,T)

- alpha*Tinf

);

```
alpha: \alpha = n^2
 Tinf:T_{\infty}
 PTFX代码$T_\infty$
 fvm::Sp(alpha,T)
 源项(S_u + S_P T_P)
内部网格: S_P = -n^2 \delta x

B边界网格: S_P = -\frac{2}{\delta x}
```

其中

alpha和环境温度Tinf在constant/transportProperties中定义
alpha alpha [0 -2 0 0 0 0 0] 25;
T 2 2024年春季《计算流体动力学编程实践》 [by 徐 名成 @ 中国农业大学] 流华机械与流体工程系 2024年2月27日

关键代码

alpha

该案例已放至code_practice/diffusionEqs

求解器名字为steadyDiffusionWithCoolingFoam

案例名字为1D_rod_convective_cooling

```
fvScalarMatrix TEgn
                                                       fvm::Sp(alpha,T)
             fvm::laplacian(T)
                                                       源项(S_u + S_P T_P)
                                                      内部网格: S_P = -n^2 \delta x

B边界网格: S_P = -\frac{2}{\delta x}
             fvm::Sp(alpha,T)
           - alpha*Tinf
        );
alpha和环境温度Tinf在constant/transportProperties中定义
```

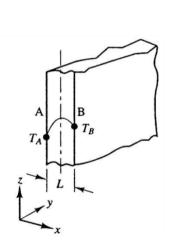
alpha [0 -2 0 0 0 0 0] 25; Tipf4年春季《计算流体动力学编刊中载》 [bv 0余 0成 0 1 国 0 0 大 0 1 流 2 0 6 械 与流体工程系 2024 年 2 月 27 日

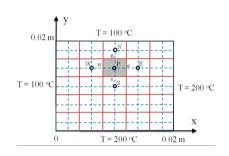
其中

Tinf: T_{∞}

 $alpha: \alpha = n^2$

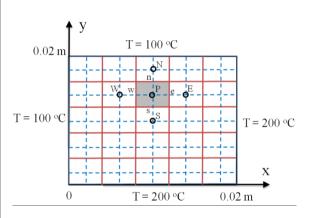
PTFX代码\$T_\infty\$





控制方程: $\frac{d}{dx}\left(k\frac{dT}{dx}\right) + \frac{d}{dy}\left(k\frac{dT}{dy}\right) + q = 0$

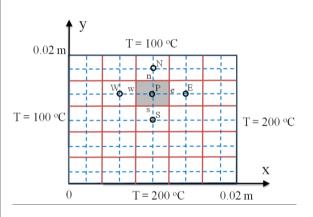
有一块二维平板, $2cm \times 2cm$,热传导系数k = 0.5W/m/K,平均分布的热源 $q = 10^6W/m^3$,上、左两面温度恒定为 $100^{\circ}C$,下、右两侧温度恒定为 $200^{\circ}C$ 。



x和y方向平均分成5份,总共25个控制体积/网格单元

- ▶ 对于指定阴影部分的内部网格P,存在四个边n, e, s, w, 分别对应四个相邻 网格N, E, S, W
- ▶ 对中心在P的控制体积,积 $分(\int_{CV})$ 应该发生在阴影部分
- ▶ 对于各边上的通量以及相关插值计算,处理方式与一维问题一样

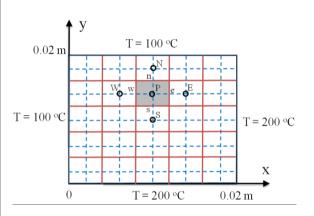
$$\int_{CV} \nabla \cdot (\gamma \nabla \phi) dV + \int_{CV} S_{\phi} dV = 0$$
$$\int_{A} \mathbf{n} \cdot (\gamma \nabla \phi) dA + \int_{CV} S_{\phi} dV = 0$$



x和y方向平均分成5份,总共25个控制体积/网格单元

- ▶ 对于指定阴影部分的内部网格P,存在四个边n, e, s, w,分别对应四个相邻网格N, E, S, W
- ▶ 对中心在P的控制体积,积分(\int_{CV})应该发生在阴影部分
- ► 对于各边上的通量以及相关插值计 算,处理方式与一维问题一样

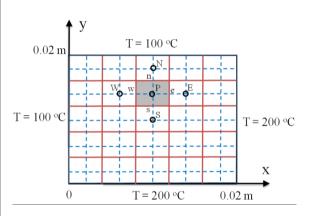
$$\int_{CV} \nabla \cdot (\gamma \nabla \phi) dV + \int_{CV} S_{\phi} dV = 0$$
$$\int_{A} \mathbf{n} \cdot (\gamma \nabla \phi) dA + \int_{CV} S_{\phi} dV = 0$$



x和y方向平均分成5份,总共25个控制体积/网格单元

- ▶ 对于指定阴影部分的内部网格P,存在四个边n, e, s, w, 分别对应四个相邻 网格N, E, S, W
- ▶ 对中心在P的控制体积,积 $f(\int_{CV})$ 应该发生在阴影部分
- 对于各边上的通量以及相关插值计算,处理方式与一维问题一样

$$\int_{CV} \nabla \cdot (\gamma \nabla \phi) dV + \int_{CV} S_{\phi} dV = 0$$
$$\int_{A} \mathbf{n} \cdot (\gamma \nabla \phi) dA + \int_{CV} S_{\phi} dV = 0$$



x和y方向平均分成5份,总共25个控制体积/网格单元

- ▶ 对于指定阴影部分的内部网格P,存在四个边n,e,s,w,分别对应四个相邻网格N,E,S,W
- ▶ 对中心在P的控制体积,积 $f(\int_{CV})$ 应该发生在阴影部分
- 对于各边上的通量以及相关插值计算,处理方式与一维问题一样

$$\int_{CV} \nabla \cdot (\gamma \nabla \phi) dV + \int_{CV} S_{\phi} dV = 0$$
$$\int_{A} \mathbf{n} \cdot (\gamma \nabla \phi) dA + \int_{CV} S_{\phi} dV = 0$$

该案例已放至code_practice/diffusionEqs 案例名字为2D_plate_with_src 求解器名字为steadyDiffusionWithSourceFoam 关键代码

```
fvScalarMatrix TEqn
(
    fvm::laplacian(DT, T)
    +q
):
```

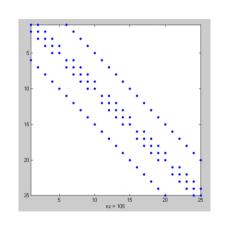
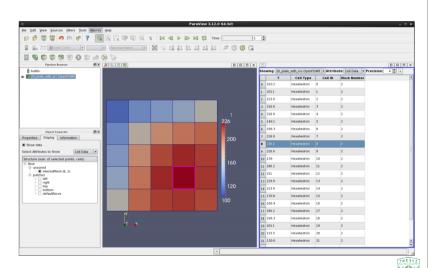


图: 系数矩阵A的对称结构



对于每一个控制体积 (网格单元),可以通 过ParaView检 查cellID和field value



总结

主要介绍了稳态热传导问题 $\nabla \cdot (\gamma \nabla \phi) + S_{\phi} = 0$

▶ 离散后方程的一般形式(\sum 是对所有相邻边界通量 ϕ_{nb} 求和)

$$a_P \phi_P = \sum a_{nb} \phi_{nb} + S_u$$

▶ 系数*a*_P满足以下关系

$$a_P = \sum a_{nb} - S_P$$

- ▶ 源项的一般形式 $S_{\phi}\Delta V = S_u + S_P \phi_P$
- ▶ 边界处理方式: 切断联系、引入边界通量

Thank you.

欢迎私下交流,请勿私自上传网络,谢谢!

