



# Signal Processing for GNSS Reflectometry

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CNES supervision: **Laurent Lestarquit**

A wide-angle photograph of a large, multi-arched stone bridge, likely the Pont Neuf in Toulouse, France. The bridge spans a dark, calm river or canal. Its reflection is perfectly mirrored in the water below, creating a symmetrical scene. The bridge is made of light-colored stone and features several large, rounded arches. In the background, a city skyline with various buildings and a prominent dome is visible under a clear blue sky.

# Introduction

# I The example of sea height

How to estimate water level?

# I

# The example of sea height

## In situ approaches

- Local measurements:
  - flood level markers,
  - GPS buoys.
- Need of a lot of data points to get a global coverage...



[parc-cotentin-bessin.fr](http://parc-cotentin-bessin.fr)



[ndbc.noaa.gov](http://ndbc.noaa.gov)

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## Remote sensing approaches

- Remote measurements:
  - radar flood gauge,
  - satellites.
- Local to global coverage.



[water.weather.gov](http://water.weather.gov)



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## In situ approaches

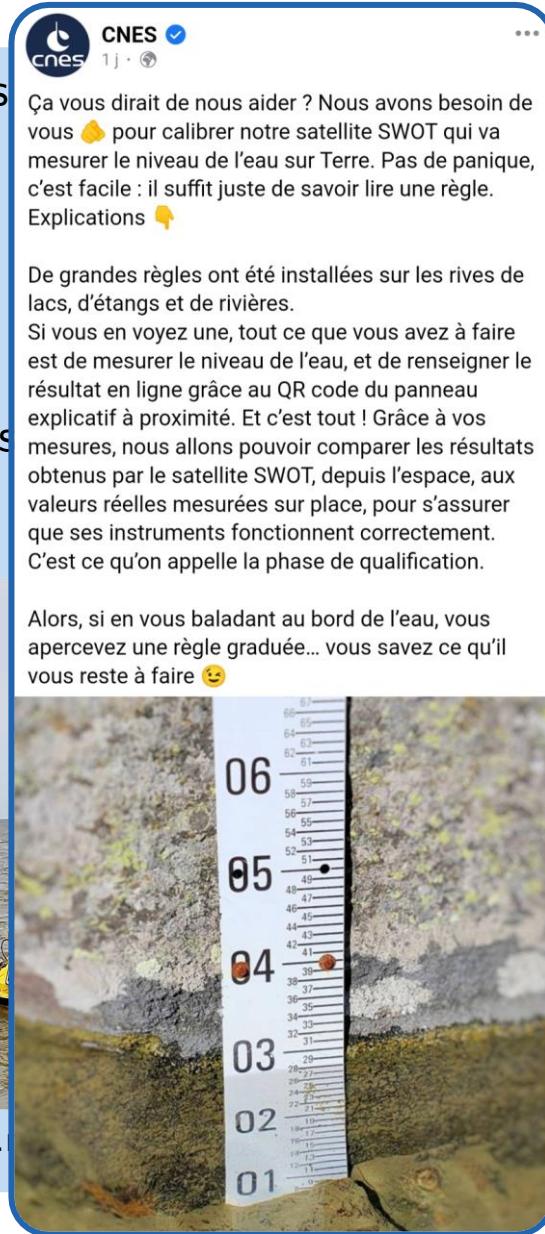
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Ça vous dirait de nous aider ? Nous avons besoin de vous 🙏 pour calibrer notre satellite SWOT qui va mesurer le niveau de l'eau sur Terre. Pas de panique, c'est facile : il suffit juste de savoir lire une règle. Explications 🙏

De grandes règles ont été installées sur les rives de lacs, d'étangs et de rivières. Si vous en voyez une, tout ce que vous avez à faire est de mesurer le niveau de l'eau, et de renseigner le résultat en ligne grâce au QR code du panneau explicatif à proximité. Et c'est tout ! Grâce à vos mesures, nous allons pouvoir comparer les résultats obtenus par le satellite SWOT, depuis l'espace, aux valeurs réelles mesurées sur place, pour s'assurer que ses instruments fonctionnent correctement. C'est ce qu'on appelle la phase de qualification.

Alors, si en vous baladant au bord de l'eau, vous apercevez une règle graduée... vous savez ce qu'il vous reste à faire 😊

## Remote sensing approaches

### Measurements:

- flood gauge,

buoies.

global coverage.



[her.gov](http://her.gov)



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# Global Navigation Satellite System (GNSS)



Positioning system.



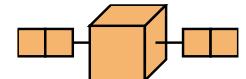
# GNSS principle



Positioning system.

# I GNSS principle

Satellite A

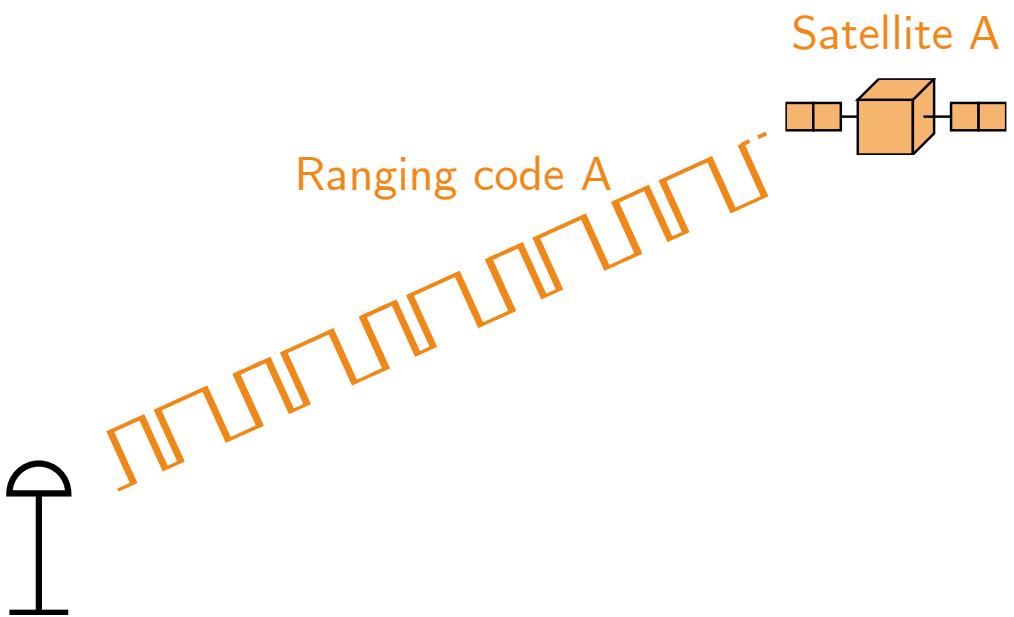


Positioning system.

Satellite constellations: GPS, GALILEO, BeiDou, GLONASS and others.

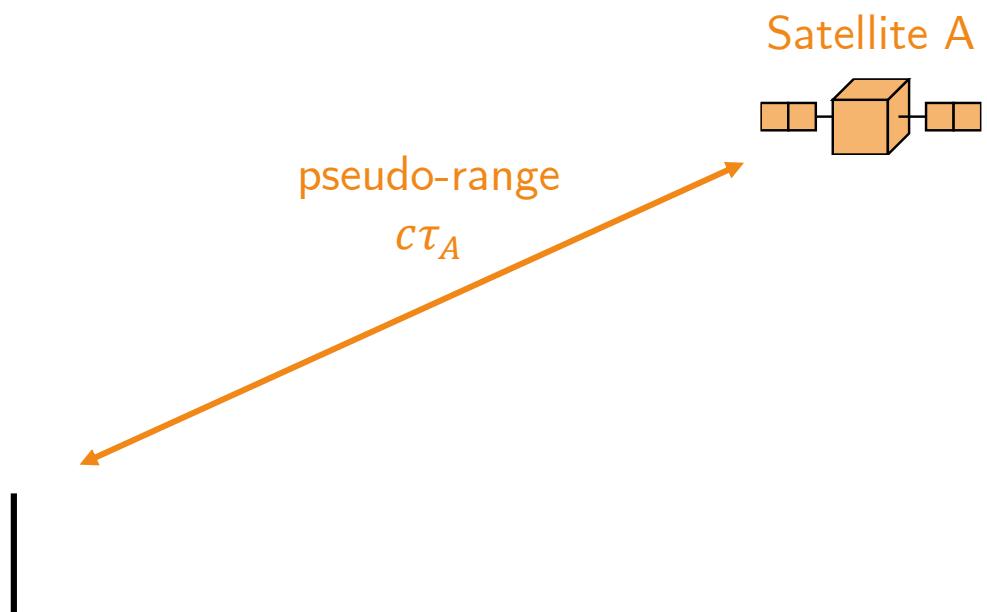


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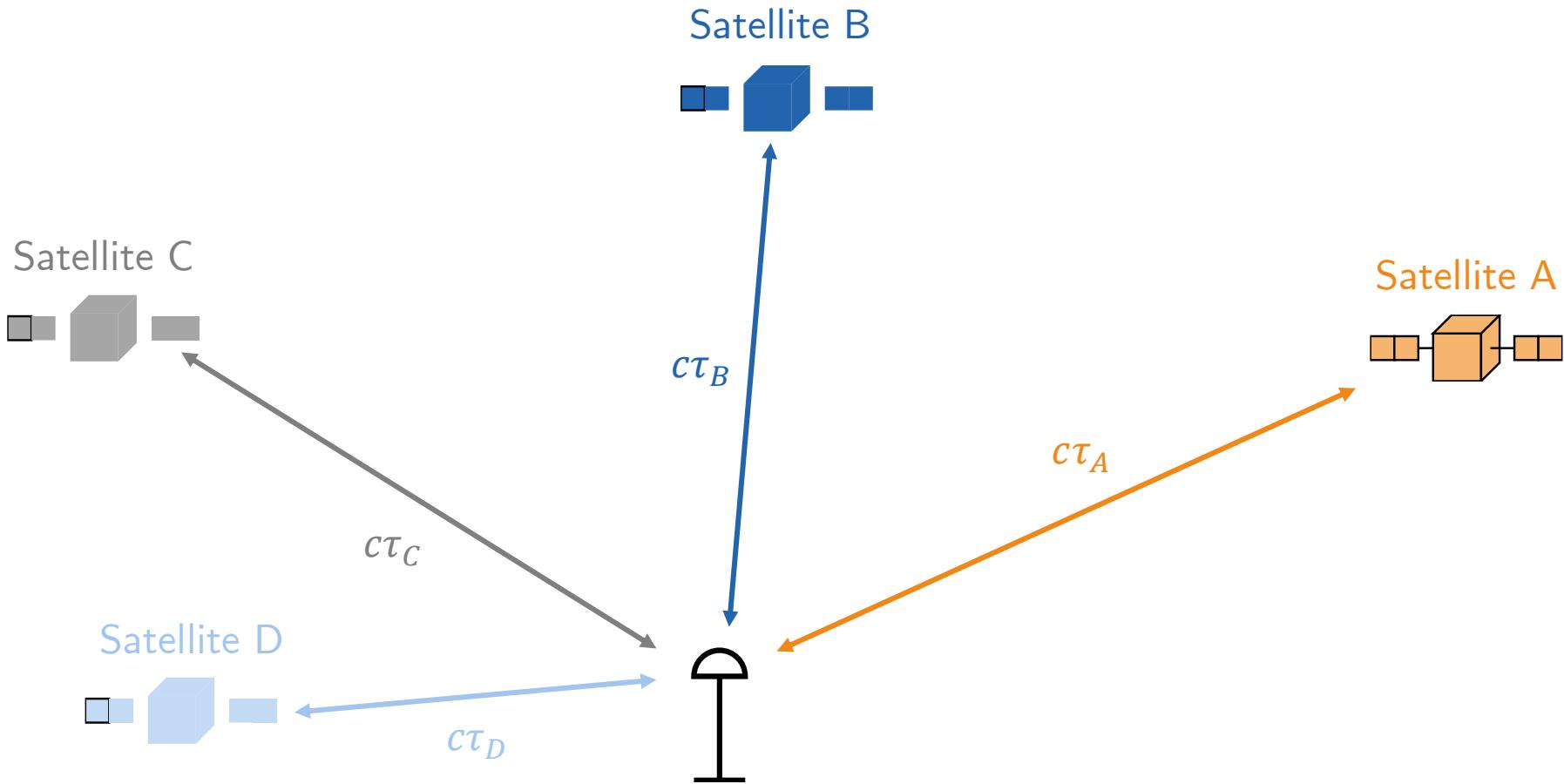
# GNSS principle



Pseudo-range  $\neq$  geometric distance:  
tropospheric delay, ionospheric delay, clock biases and others to be compensated.

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# GNSS principle



Position Velocity Timing (PVT) solution:  
trilateration using three satellites + 1 satellite to estimate the receiver clock bias.



# GNSS signal processing

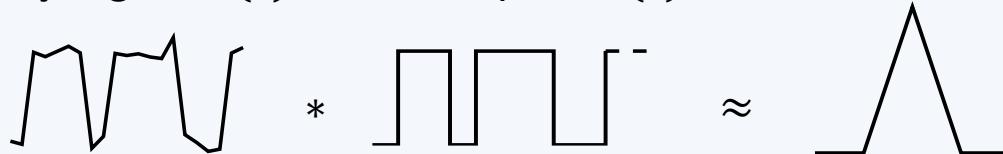
Satellite B



Standard GNSS signal processing:

- range estimation: time-delay estimation,
- cross-correlation.

noisy signal  $x(t)$     clean replica  $s(t)$





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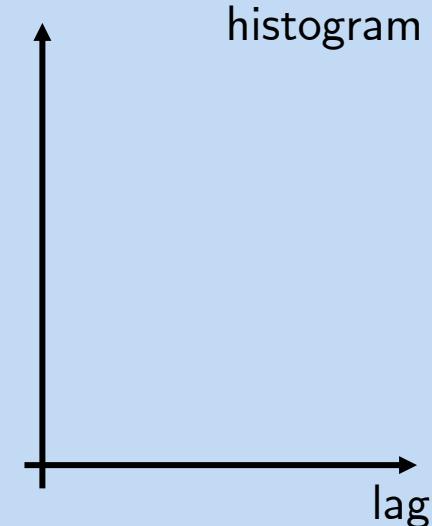
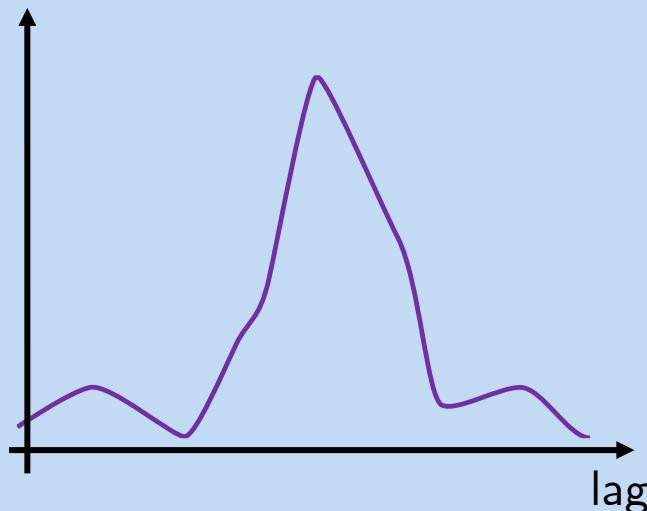
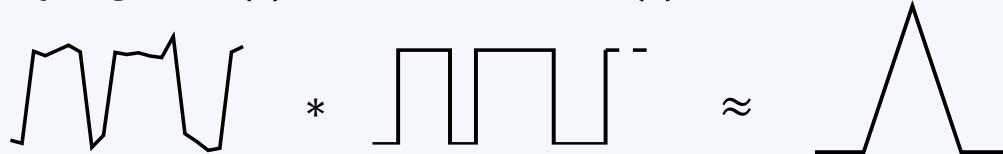
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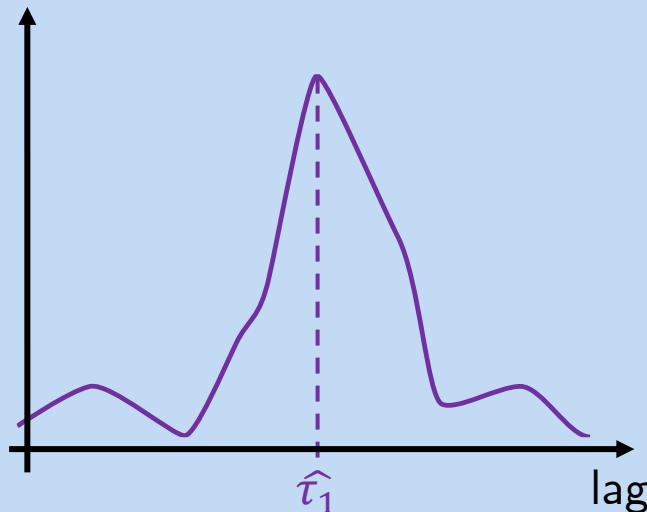
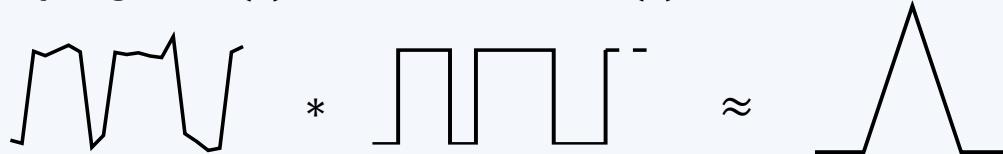
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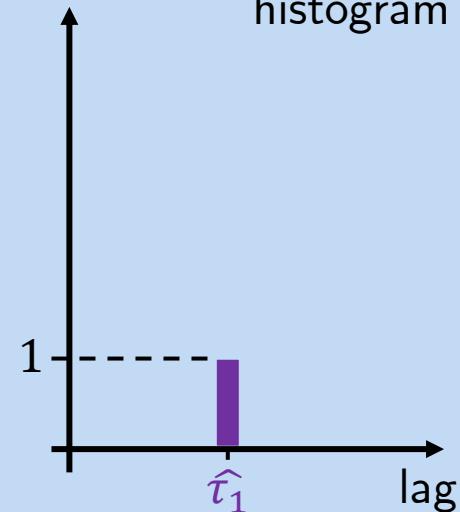
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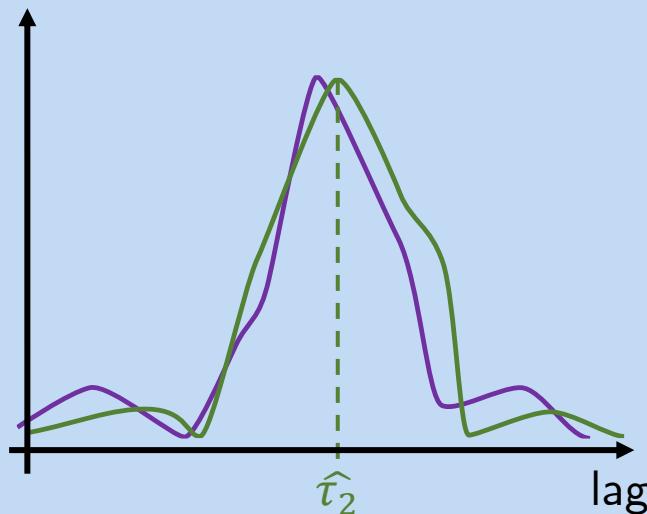
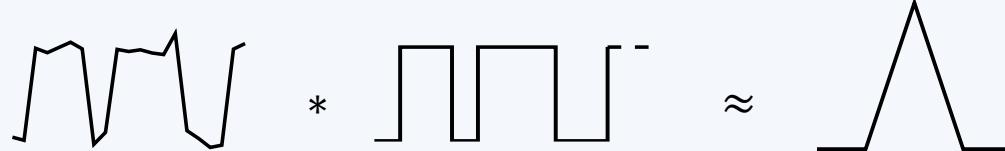
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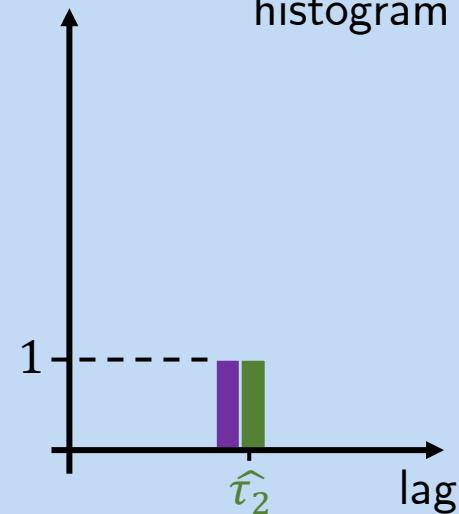
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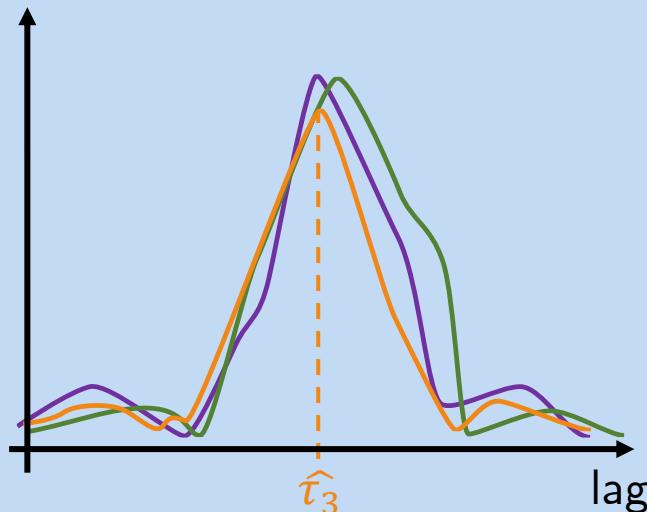
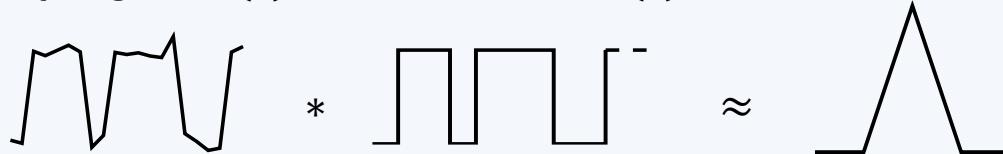
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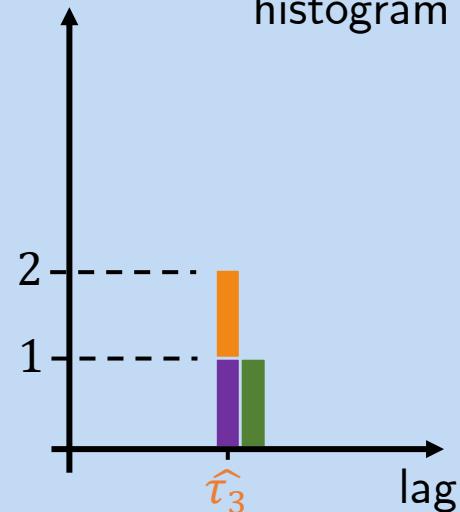
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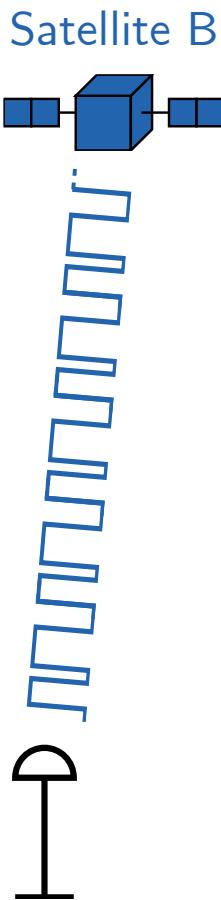


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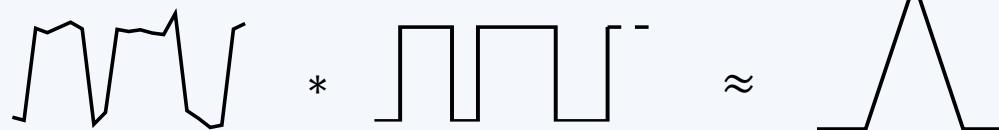
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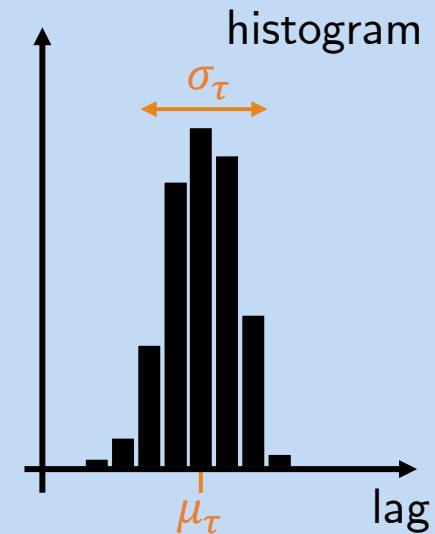
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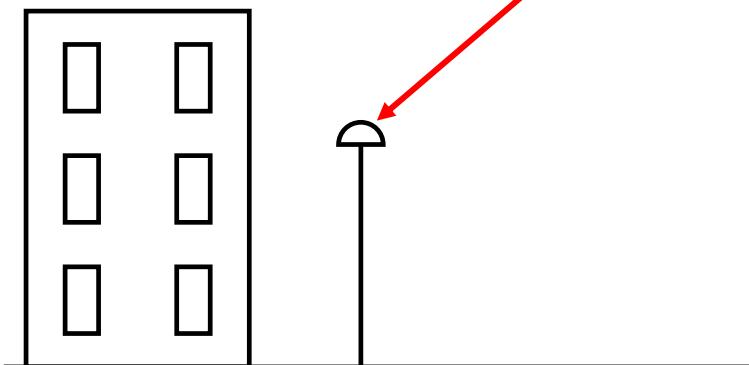


What one expects from an estimator:

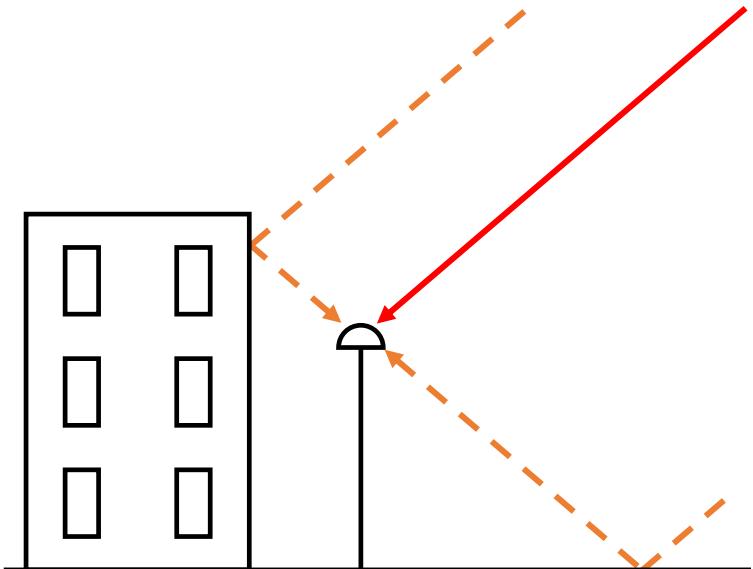
- unbiased:  $\mu_\tau = \tau_{true}$ ,
- minimum variance:  $\sigma_\tau = \text{CRB}(\tau)$ .

CRB: Cramér-Rao bound.

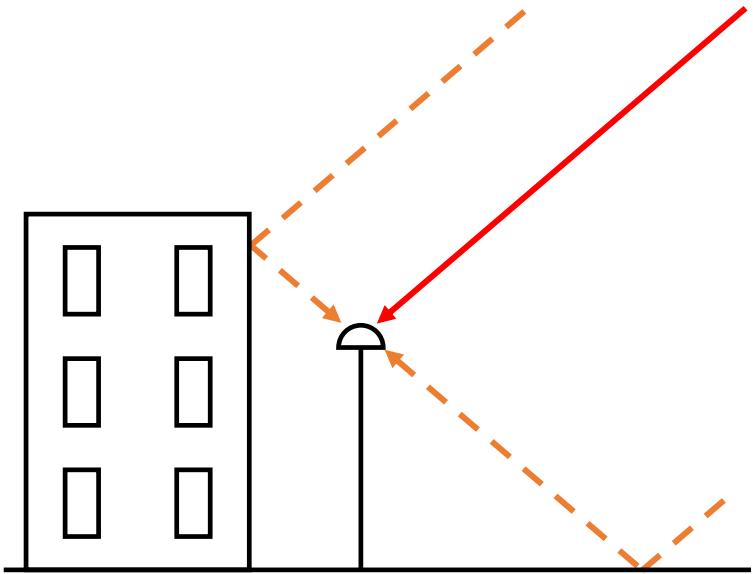




**Definition** [Kaplan and Hegarty, 2017]:  
*Multipath is the reception of multiple reflected and diffracted replicas of the desired signal, along with the direct path signal.*

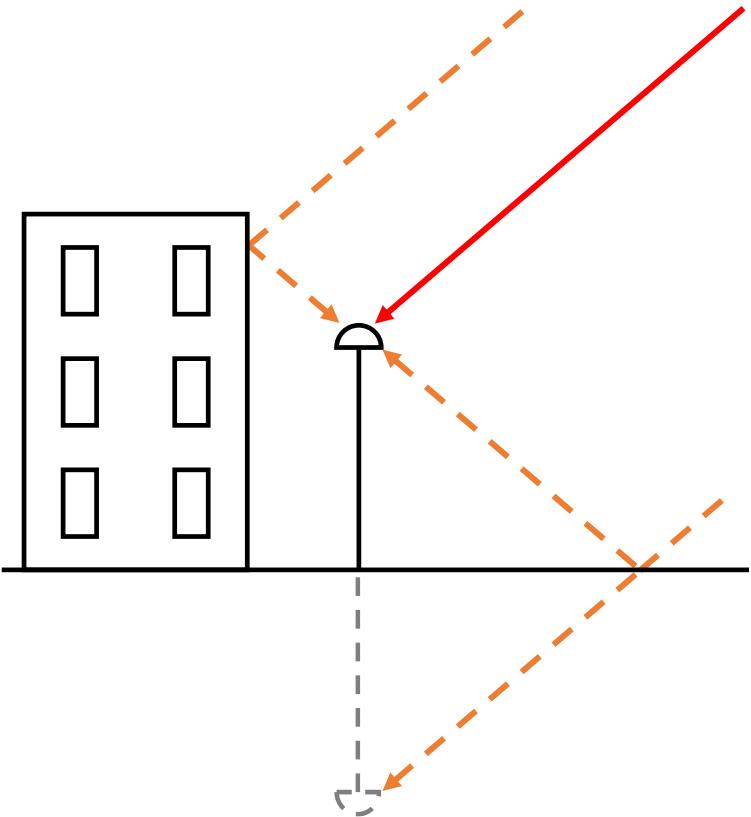


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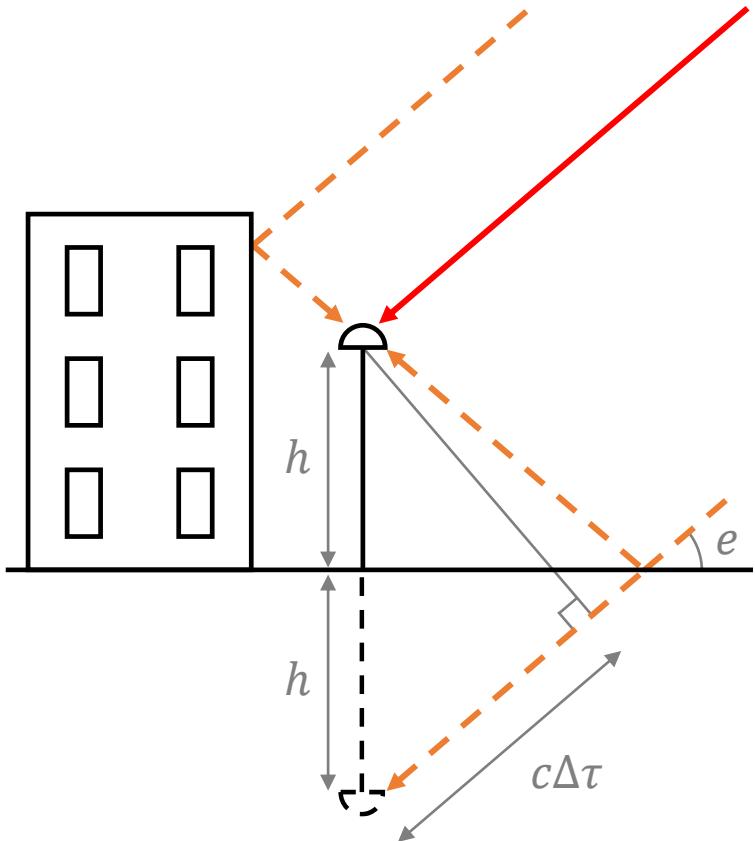


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- It contains information!
  - Geometric equation:

$$c\Delta\tau = 2h\sin(e)$$

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GNSS-R: study of GNSS signals reflected upon the Earth

- GNSS signals: L-band signals received 24/7 anywhere on Earth: signals of opportunity,
- altimetry and/or reflecting surfaces properties (e.g., reflectivity, roughness).

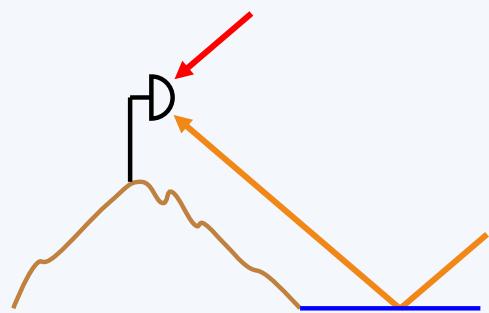
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ground-based



- local coverage
- coherent reflections
- one or two antennas

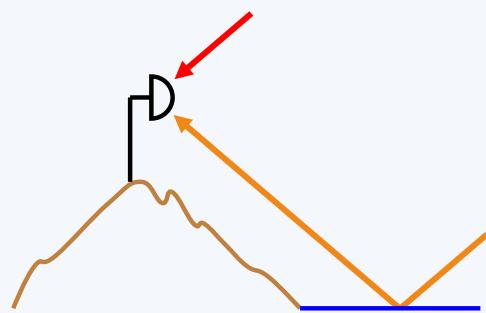
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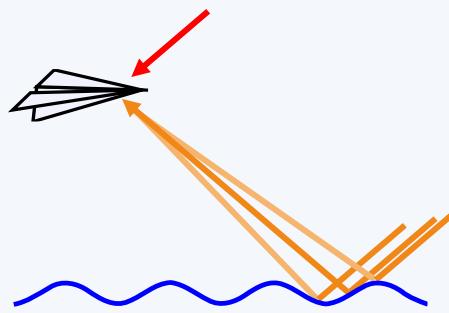
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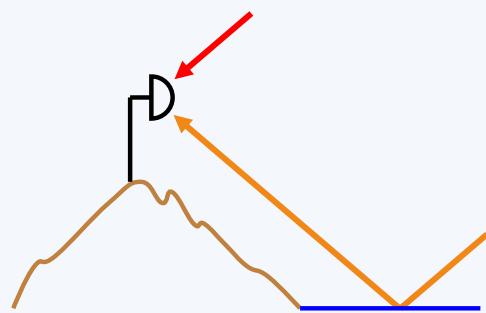
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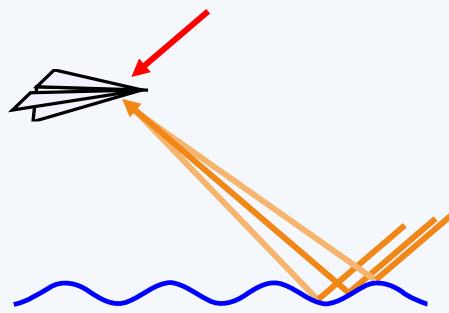
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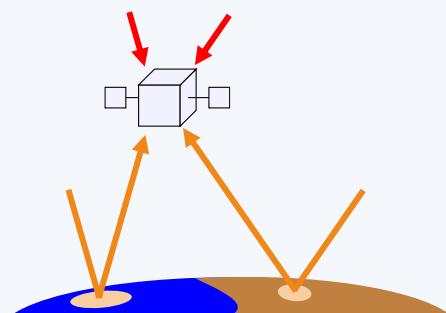
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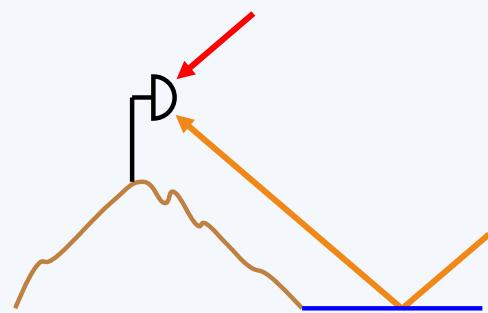
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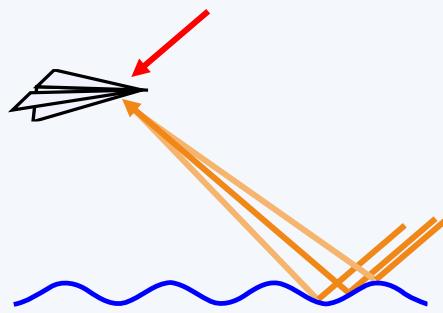
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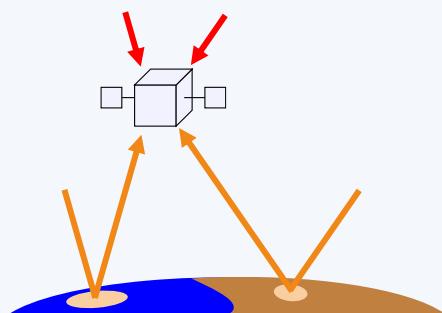
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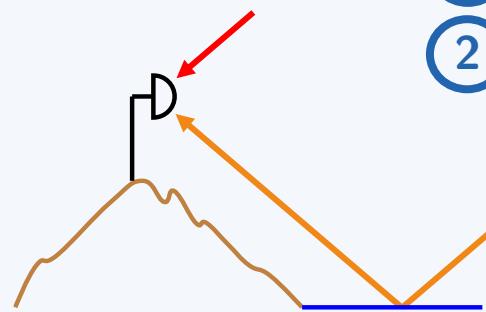
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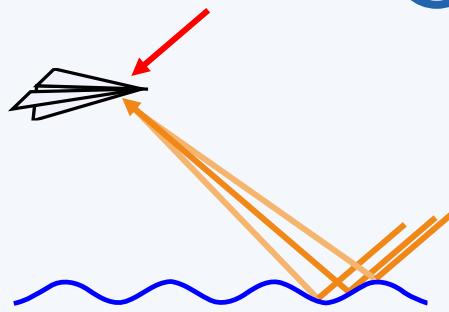
1  
2



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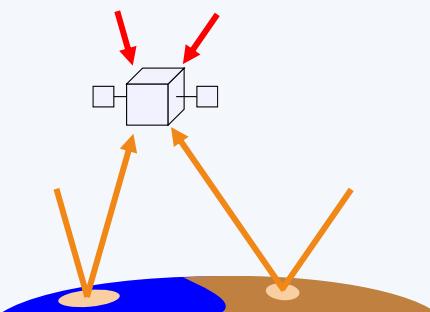
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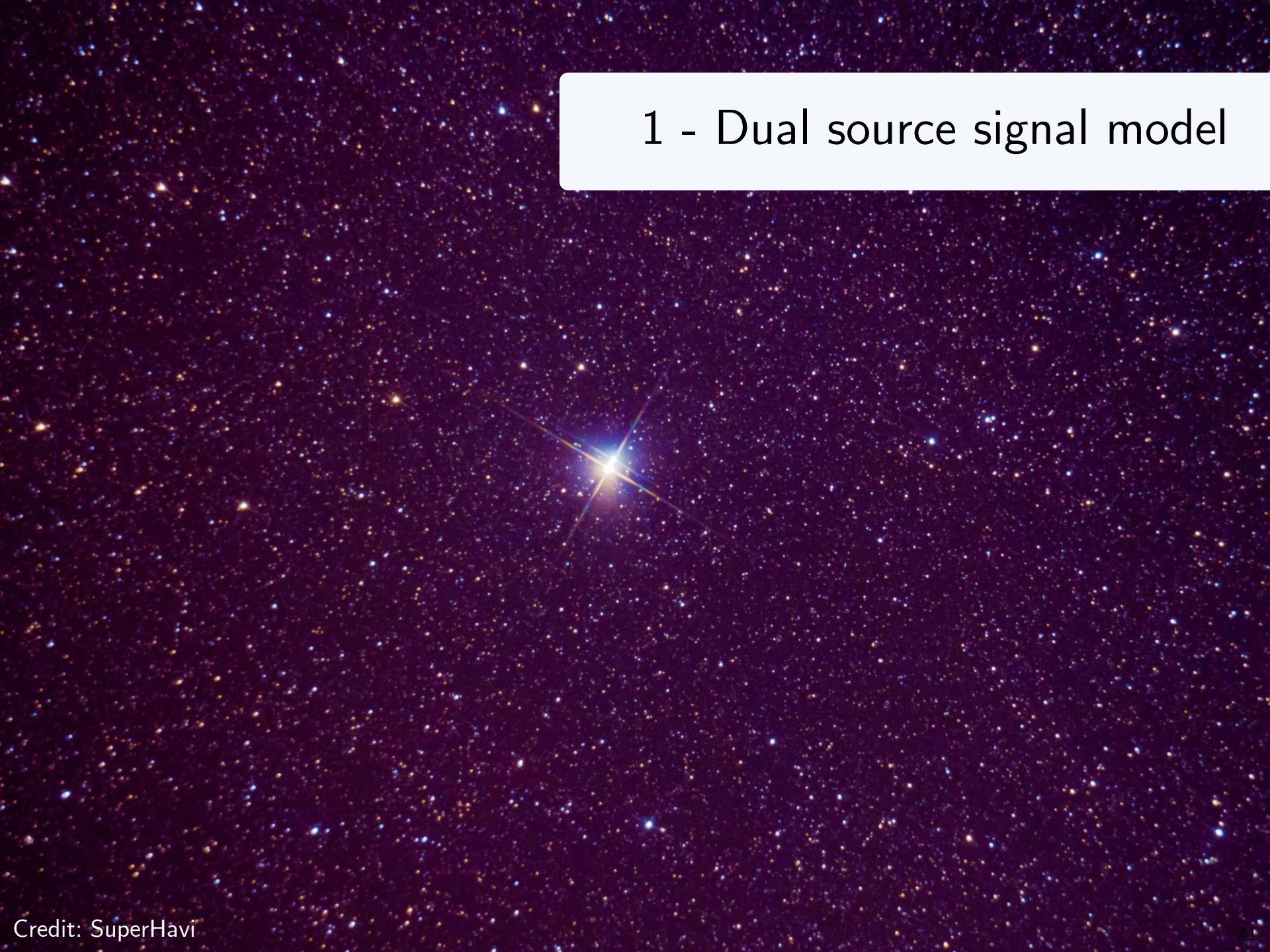
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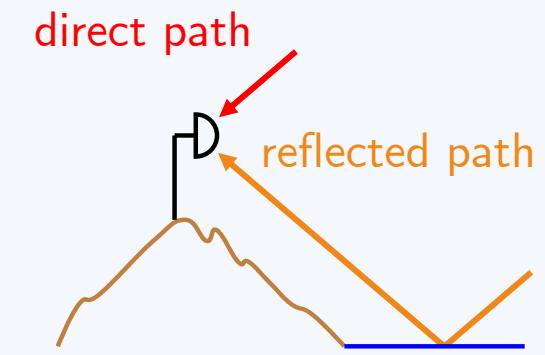
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- 
- The diagram consists of three blue circles numbered 1, 2, and 3, each followed by a list of bullet points. To the right of these lists are three orange curly braces. The first brace groups items 1 and 2, which are associated with the text "Theoretical approach". The second brace groups item 2, which is associated with the text "Experimental approach". The third brace groups item 3, which is associated with the text "Exploratory approach".
- Theoretical approach
- Experimental approach
- Exploratory approach



# 1 - Dual source signal model



# Signal model





# Signal model

- Dual source signal model with specular reflection:

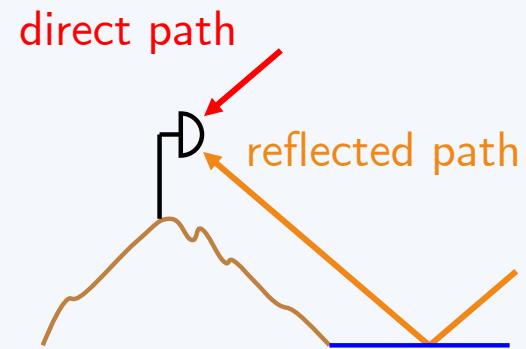
$$\mathbf{x} = \mathbf{A}(\boldsymbol{\eta}_0, \boldsymbol{\eta}_1) \boldsymbol{\alpha} + \mathbf{w}, \mathbf{w} \sim \mathcal{CN}(\mathbf{0}, \sigma_n^2 \mathbf{I}_N),$$

with  $N$  the number of samples and, for  $\boldsymbol{\eta}_i^T = (\tau_i, F_{d,i})$ ,

$$\mathbf{A}(\boldsymbol{\eta}_0, \boldsymbol{\eta}_1) = [\mathbf{s}(\boldsymbol{\eta}_0), \mathbf{s}(\boldsymbol{\eta}_1)],$$

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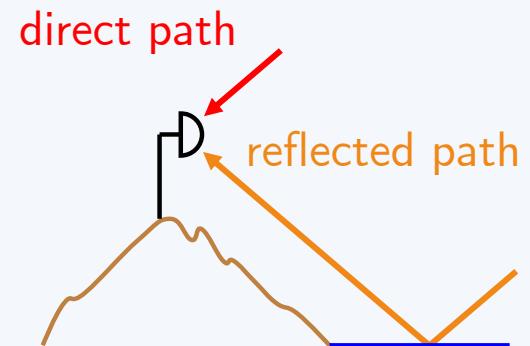
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- Deterministic parameters formulation with the following vector of unknowns:

$$\boldsymbol{\epsilon}^T = (\sigma_n^2, \underbrace{\tau_0, F_{d,0}, \rho_0, \phi_0}_{\boldsymbol{\theta}_0^T}, \underbrace{\tau_1, F_{d,1}, \rho_1, \phi_1}_{\boldsymbol{\theta}_1^T}).$$



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- Cramér-Rao bound: theoretical lower bound for the variance of any locally unbiased estimator.
- From the signal model, the Fisher Information Matrix (FIM) can be obtained using the Slepian-Bangs formula [Yau and Bresler, 1992]:

$$[\mathbf{F}_{\epsilon|\epsilon}(\epsilon)]_{k,l} = \frac{2}{\sigma_n^2} \operatorname{Re} \left\{ \left( \frac{\partial \mathbf{A}\boldsymbol{\alpha}}{\partial \epsilon_k} \right)^H \left( \frac{\partial \mathbf{A}\boldsymbol{\alpha}}{\partial \epsilon_l} \right) \right\} + \frac{N}{\sigma_n^4} \frac{\partial \sigma_n^2}{\partial \epsilon_k} \frac{\partial \sigma_n^2}{\partial \epsilon_l}.$$



# Cramér-Rao bound (CRB)

- Problem: estimate  $\epsilon$ . How good can we get?
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- The CRB for the estimation of  $\epsilon$  is obtained by inverting the FIM:

$$\mathbf{CRB}_{\epsilon|\epsilon}(\epsilon) = [\mathbf{F}_{\epsilon|\epsilon}(\epsilon)]^{-1}.$$



# Cramér-Rao bound (CRB)

$$\text{CRB}_{\epsilon|\epsilon}(\epsilon) = \begin{bmatrix} F_{\sigma_n^2|\epsilon} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{F}_{\theta_0|\epsilon} & \mathbf{F}_{\theta_0,\theta_1|\epsilon} \\ \mathbf{0} & \mathbf{F}_{\theta_1,\theta_0|\epsilon} & \mathbf{F}_{\theta_1|\epsilon} \end{bmatrix}^{-1}.$$

- Closed-form expression that depends on the signal baseband samples.
- $\mathbf{F}_{\theta_i|\epsilon}$ : known uncoupled contribution from each signal,
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  - Such an estimator does not exist for the non-linear problem at hand...
  - Estimator asymptotically efficient (when the number of observations [Stoica and Nehorai, 1990] or the signal to noise ratio [Renaux et al. 2006] become large): the maximum likelihood estimator!



# Dual source maximum likelihood estimator (2S-MLE)

- Signal model:  $\mathbf{x} = \mathbf{A}(\boldsymbol{\eta}_0, \boldsymbol{\eta}_1)\boldsymbol{\alpha} + \mathbf{w}, \mathbf{w} \sim \mathcal{CN}(\mathbf{0}, \sigma_n^2 \mathbf{I}_N) \Rightarrow \mathbf{x} \sim \mathcal{CN}(\mathbf{A}\boldsymbol{\alpha}, \sigma_n^2 \mathbf{I}_N).$



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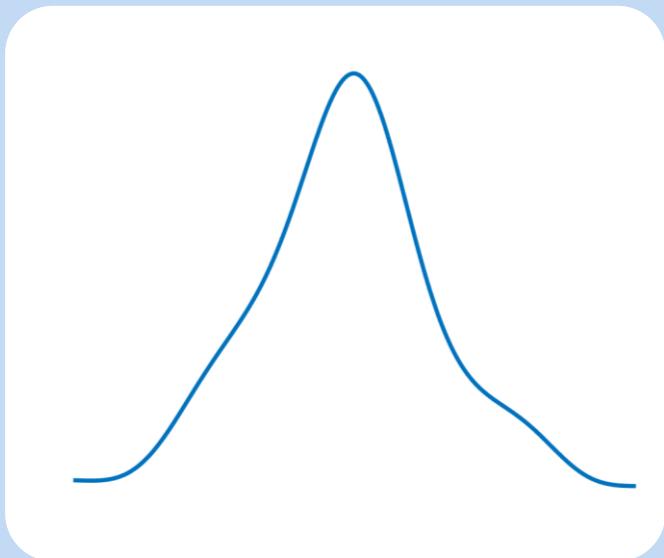
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- 9-dimensional grid search!
- Using linear algebra, this problem can be reduced to a 4-dimensional search.

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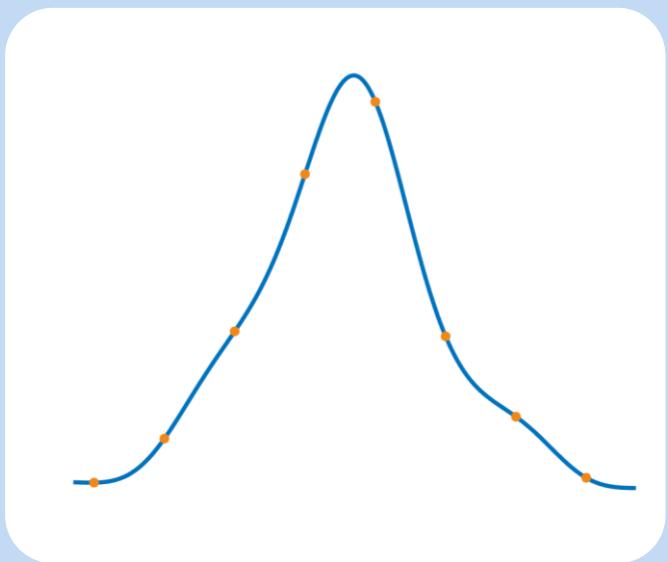
# 2S-MLE: search grid strategy



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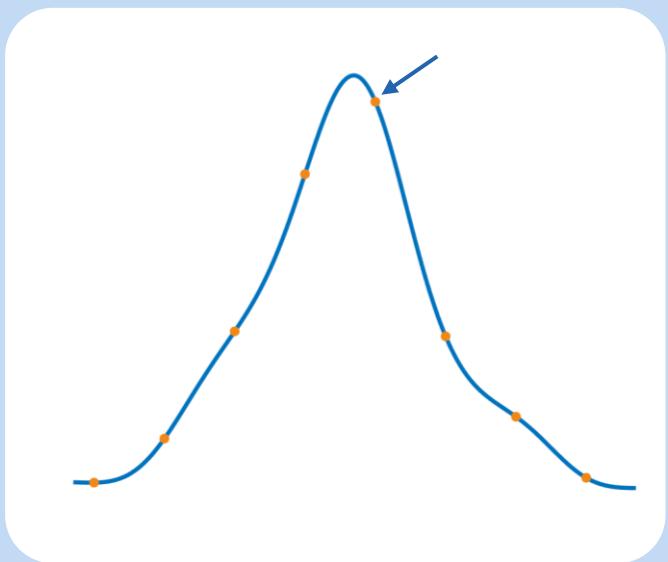
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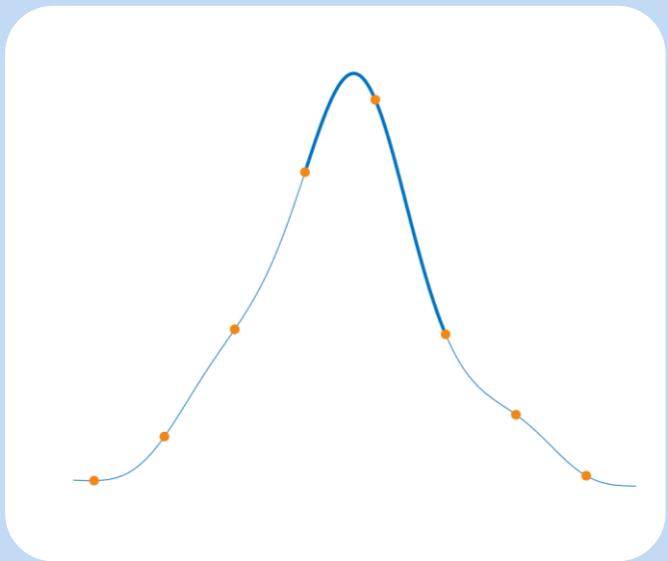
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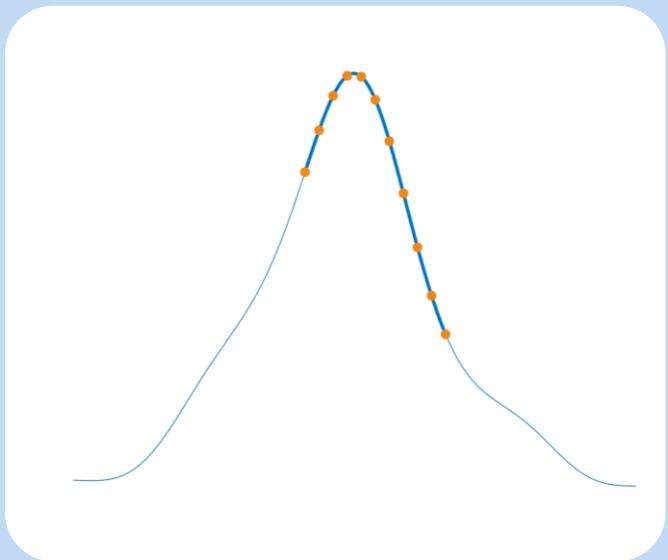
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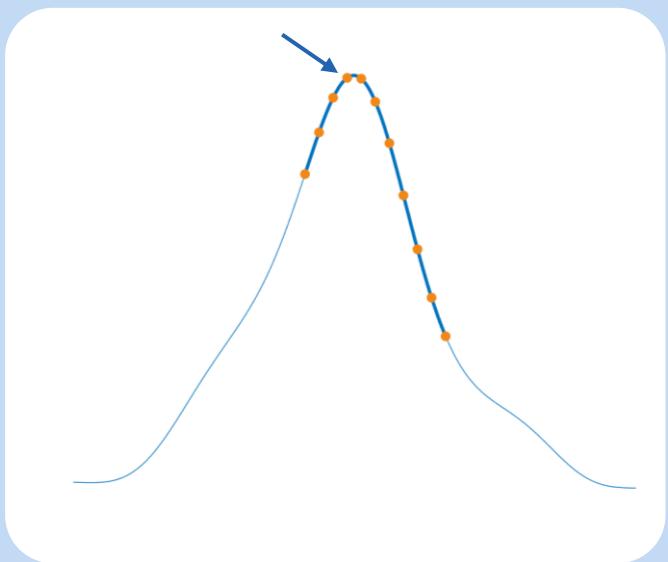
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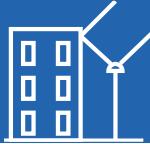
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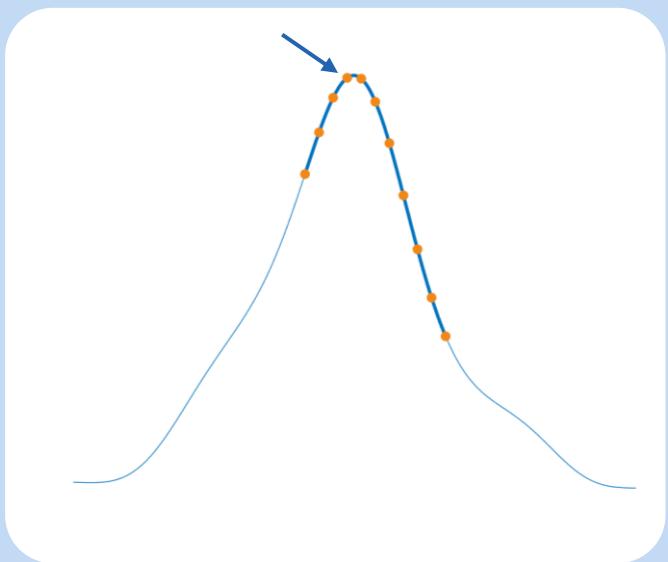
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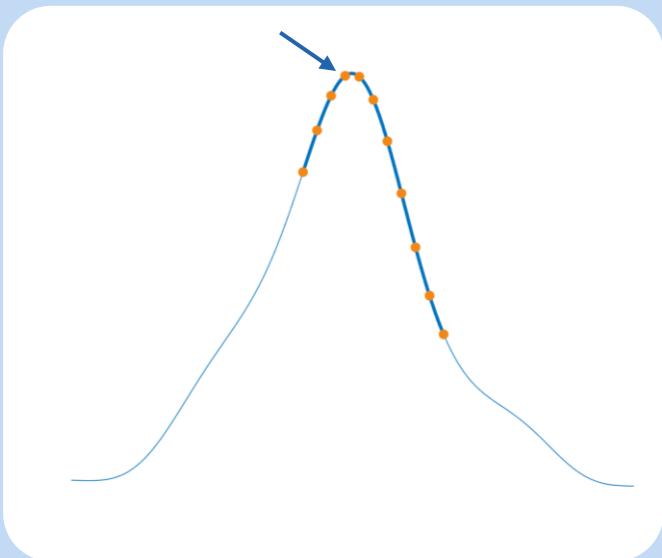
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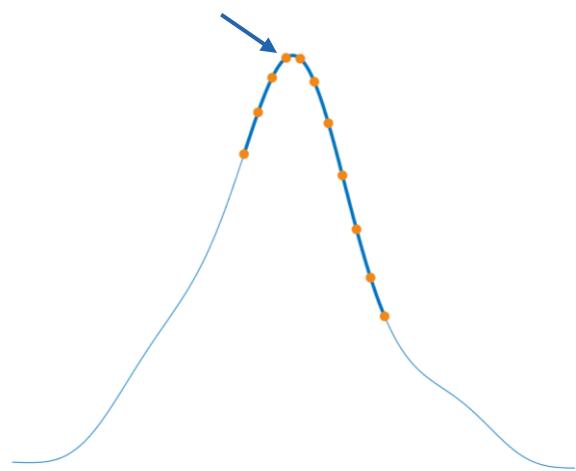


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  - $c\Delta\tau = 37$  m,
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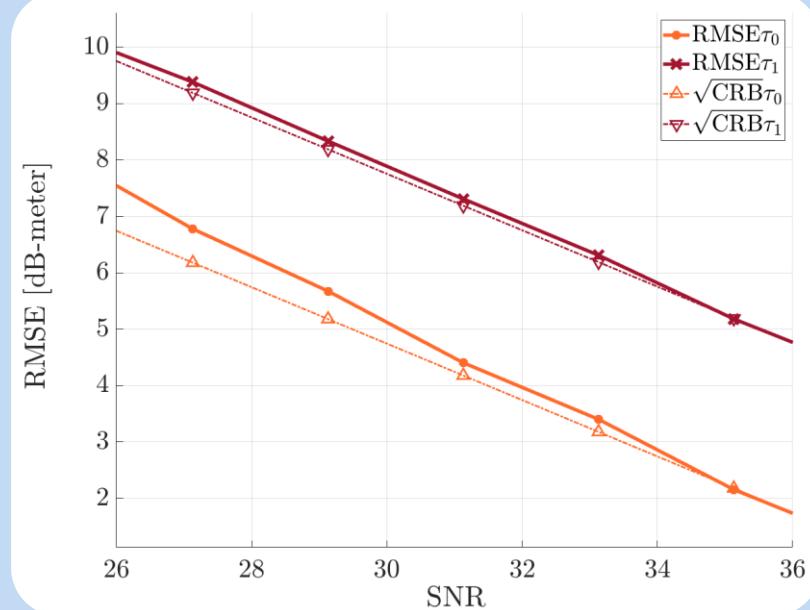


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# Wrap-up on 2S signal model

## In this presentation

- Dual source signal model adapted to the ground-based GNSS-R.
- Derivation of a closed-form CRB and validation using the 2S-MLE.

Lubeigt *et al.* 2020, *Remote Sensing*.



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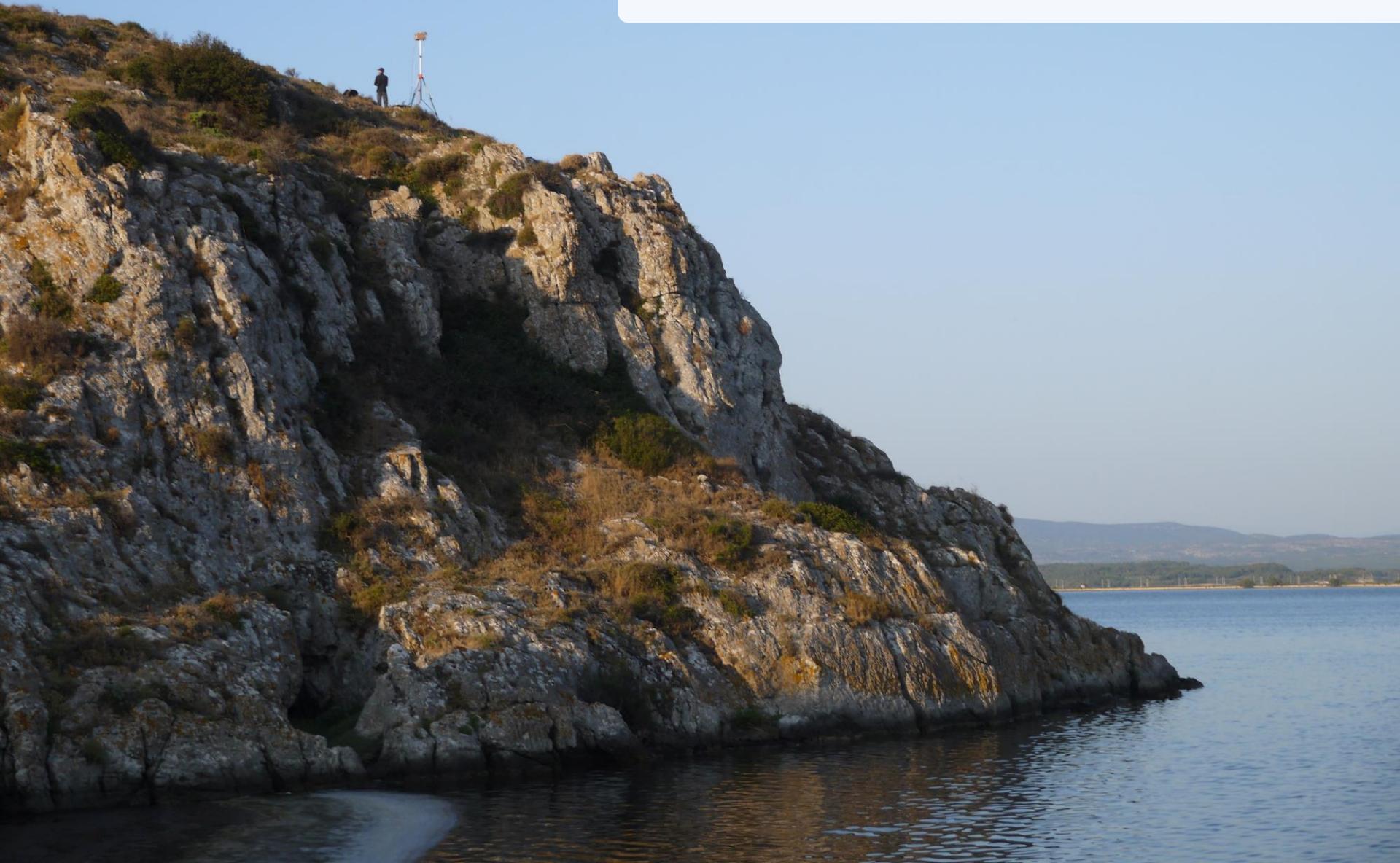
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## Related works

- Use of the CRB as a way to assess GNSS multipath effect.
  - ❑ Lubeigt *et al.* 2022, *IEEE Aerospace Conference*.
- Proposition of a metric for candidate GNSS signal design based on the CRB.
  - ❑ Lubeigt *et al.* 2022, *IEEE Trans. Aerosp. Electron. Syst.*
- Derivation of the Misspecified CRB (MCRB)
  - ❑ Lubeigt *et al.* 2023, *Signal Processing*.

## 2 - Ground-based GNSS-R





# Motivation

- Standard GNSS-R processing:
  - 1 channel for the direct path,
  - 1 channel for the reflected path.



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- Assumption: channels isolated from one another.

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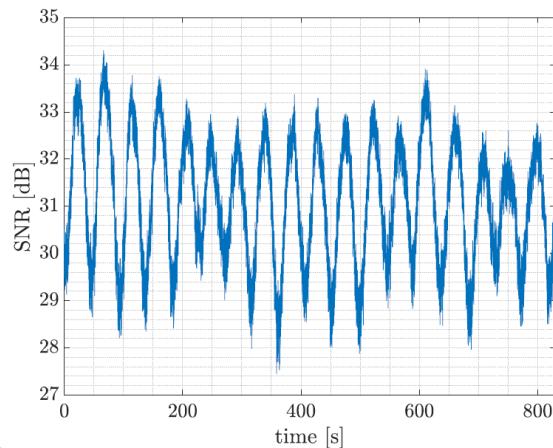


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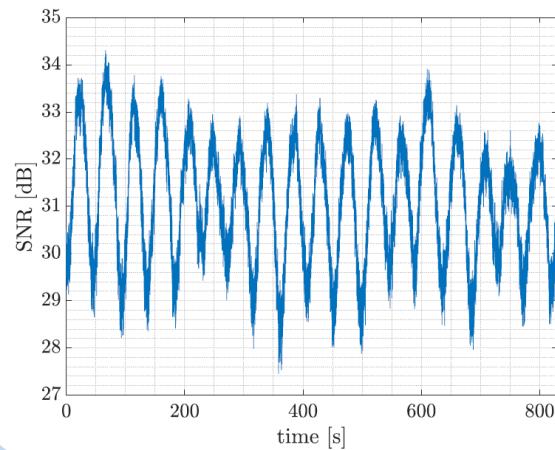


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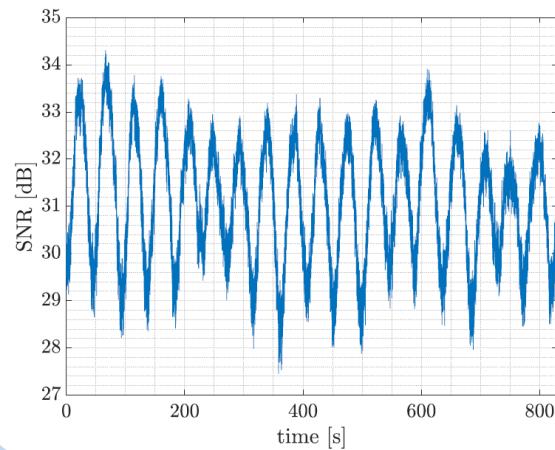
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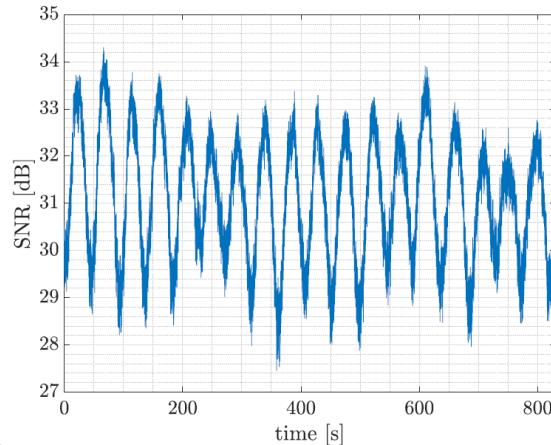
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- Ground-based GNSS-R is usually put aside because of the signal crosstalk.
- Challenge: change the signal processing approach to cope with the presence of crosstalk.

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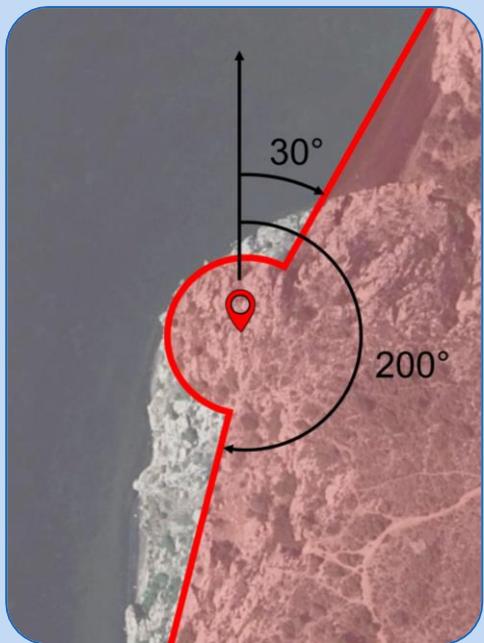
# Gruissan experiment





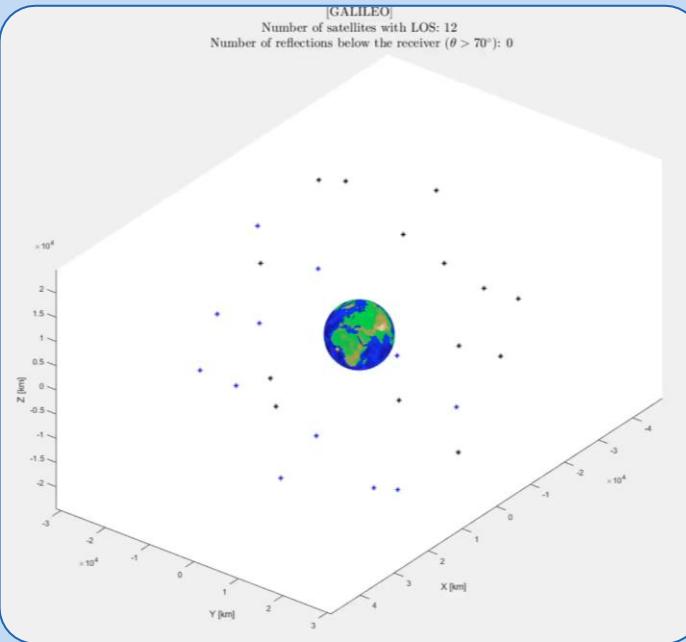
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- Site modeling: definition of a mask.



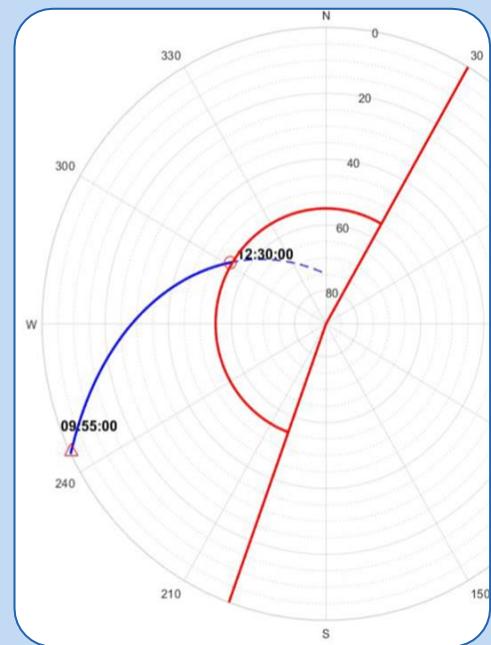
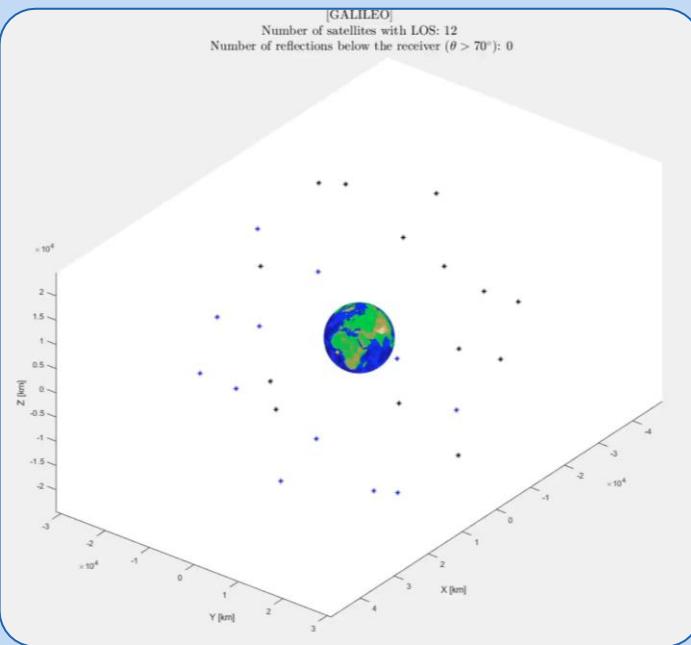
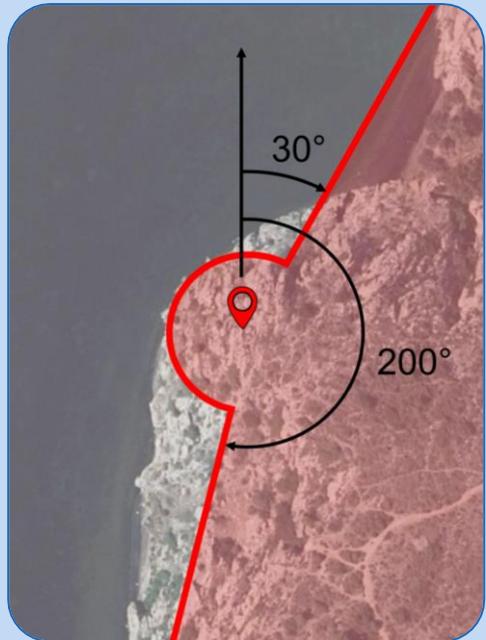
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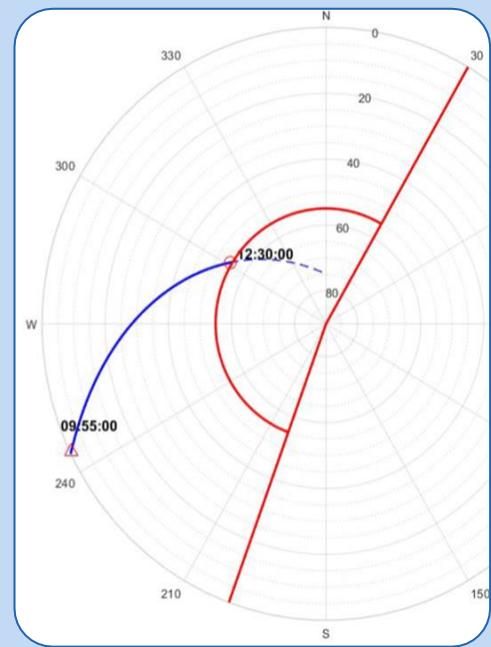
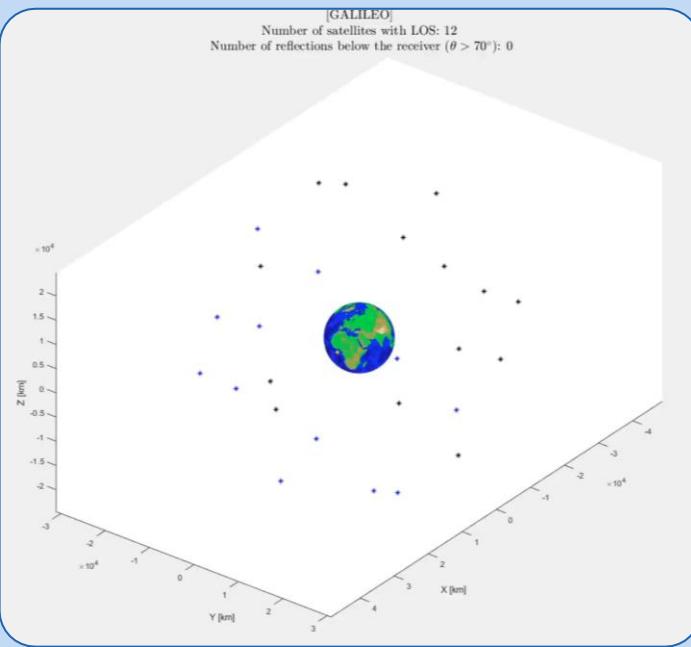
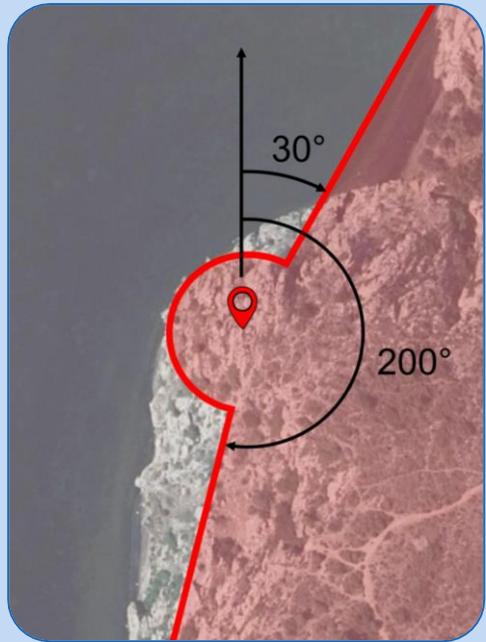
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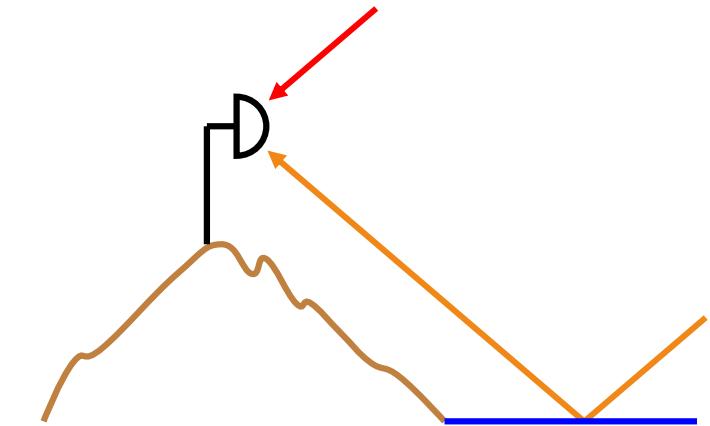
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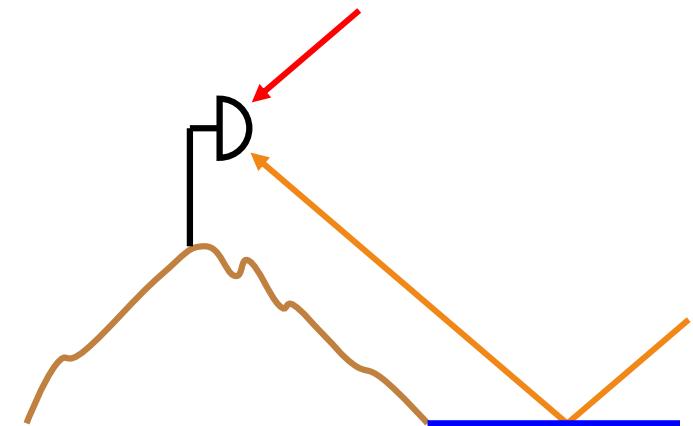
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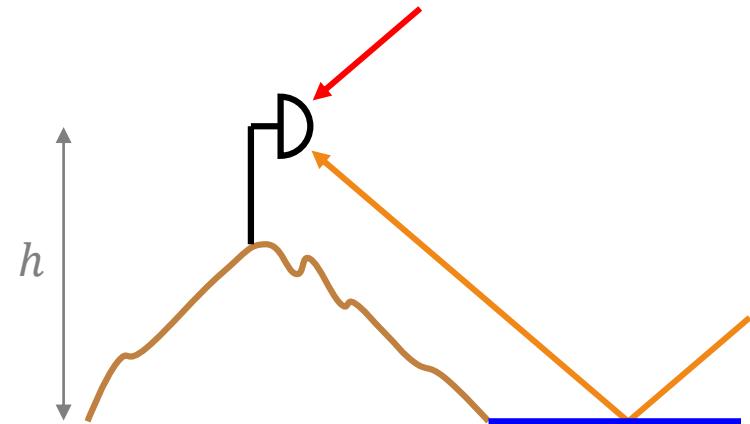
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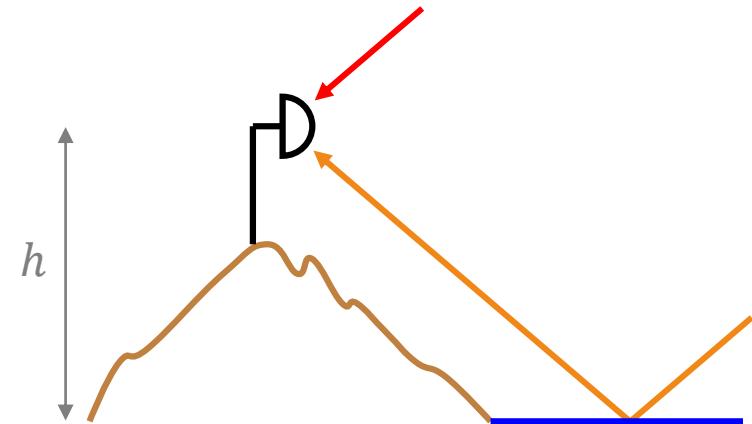
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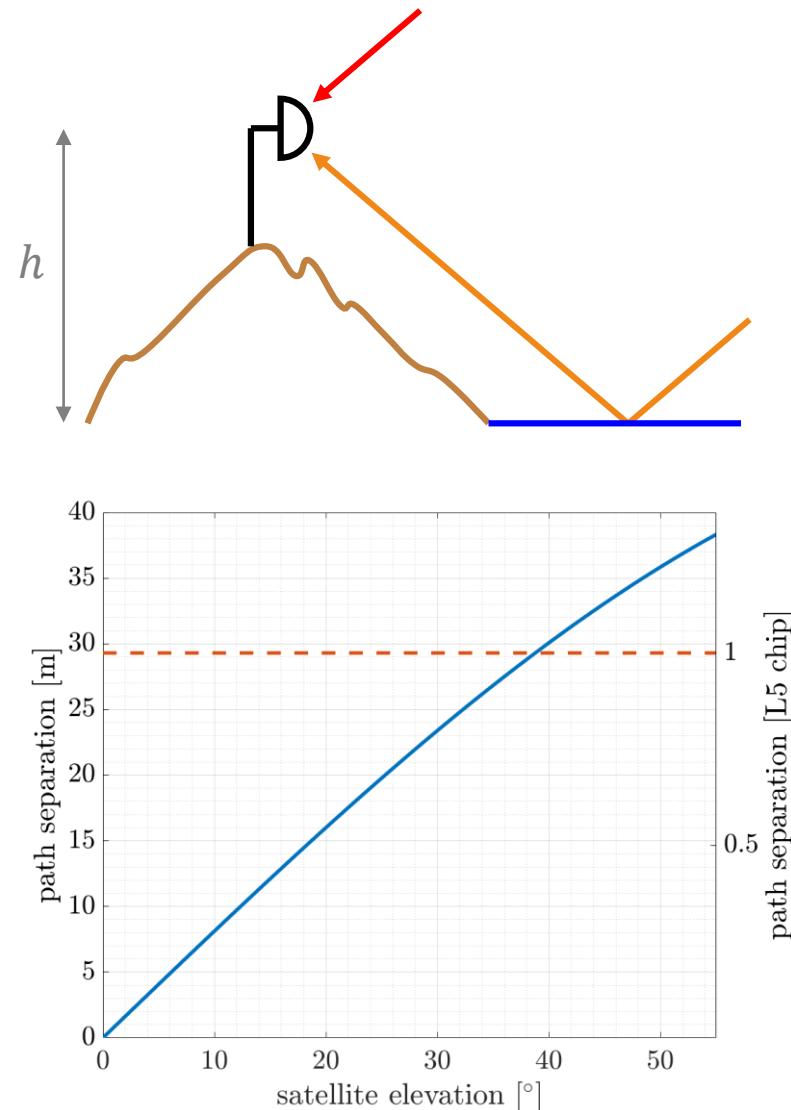
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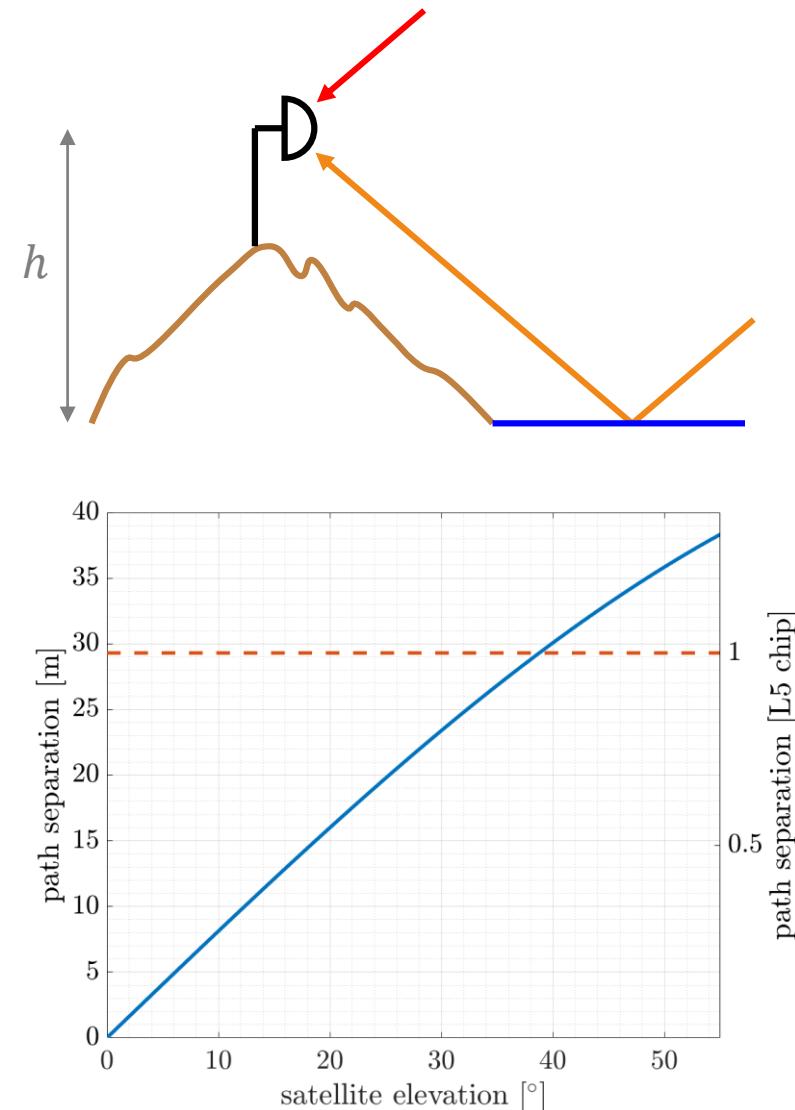


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Strong interference  
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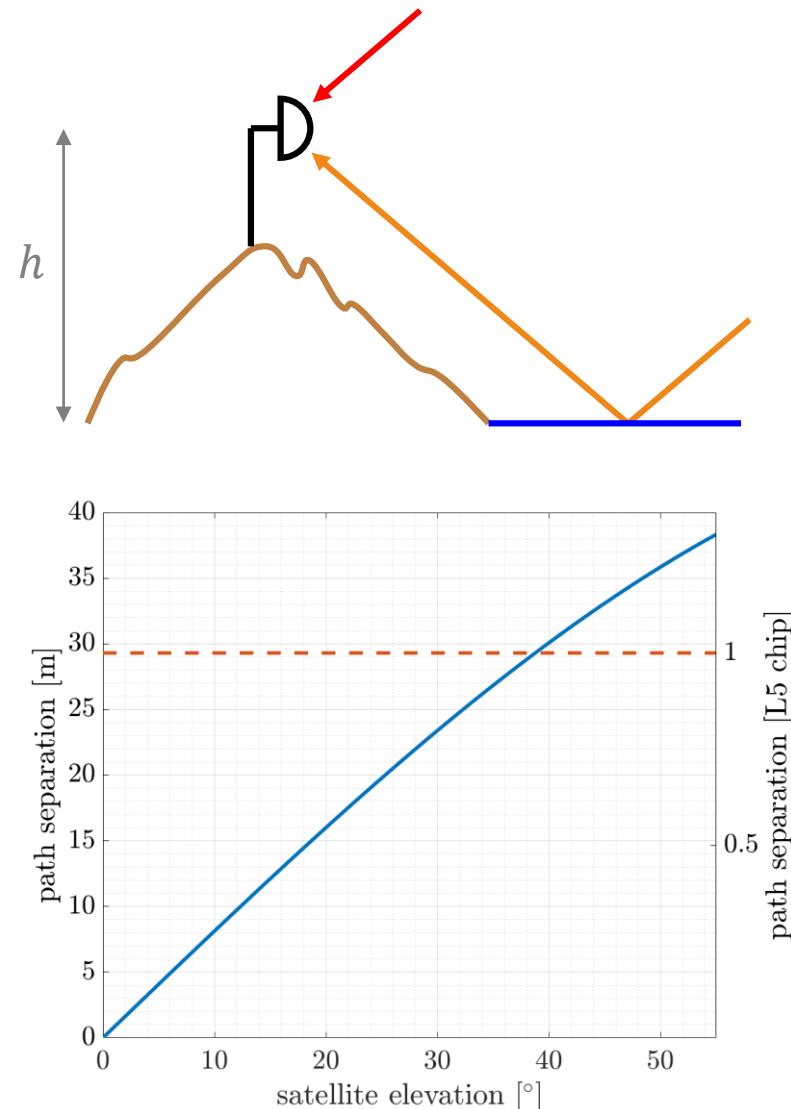
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Weak interference  
→ 2S processing



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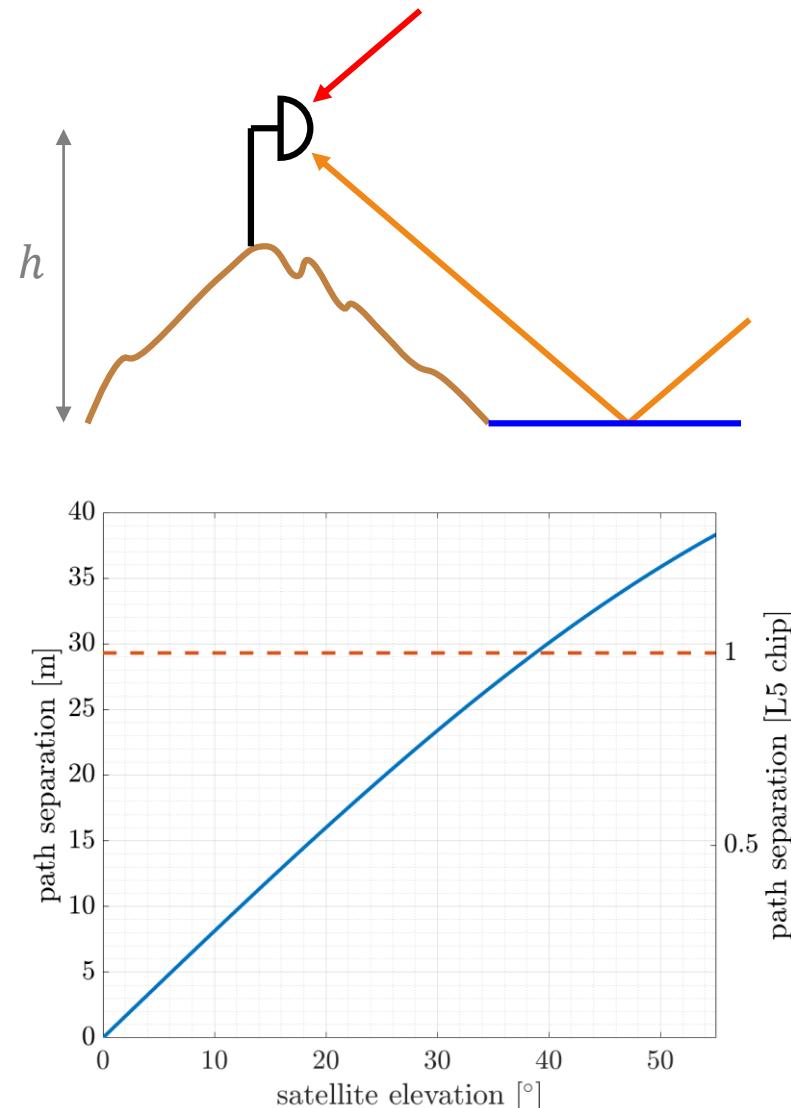
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(L5 chip  $\approx 30$  m)

Weak interference  
→ 2S processing

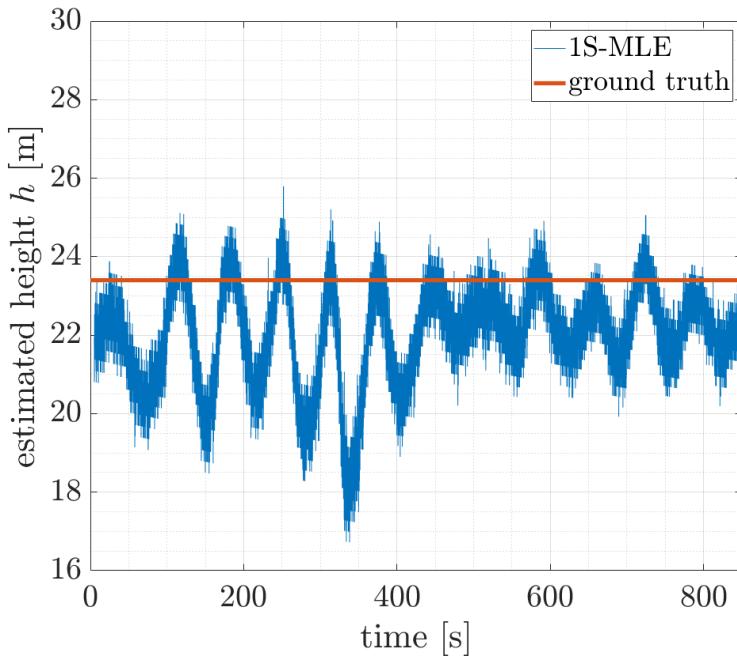


# Standard signal processing

Assuming no crosstalk: single source processing (Maximum Likelihood estimator):

- RHCP antenna:  $\hat{\tau}_0$ .
- LHCP antenna:  $\hat{\tau}_1$ .

$$\hat{h} = \frac{c(\hat{\tau}_1 - \hat{\tau}_0)}{2 \sin(e)}$$



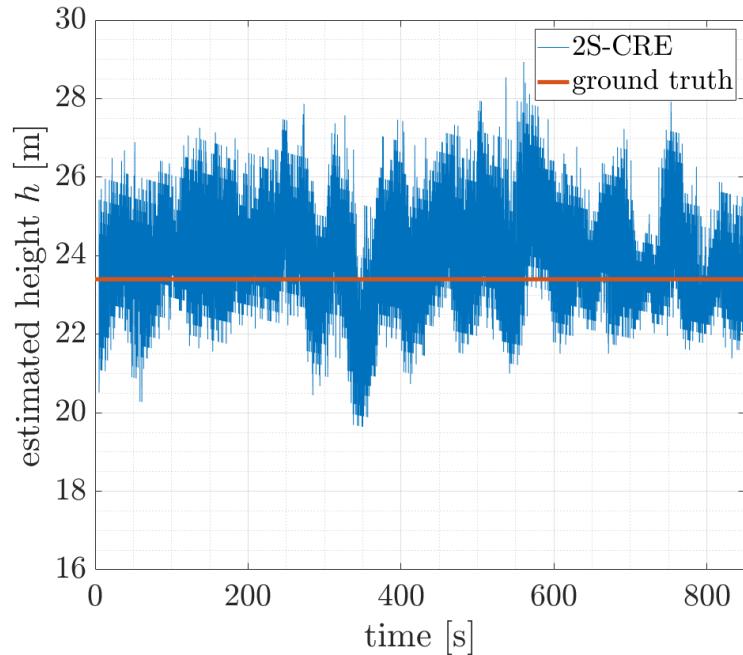
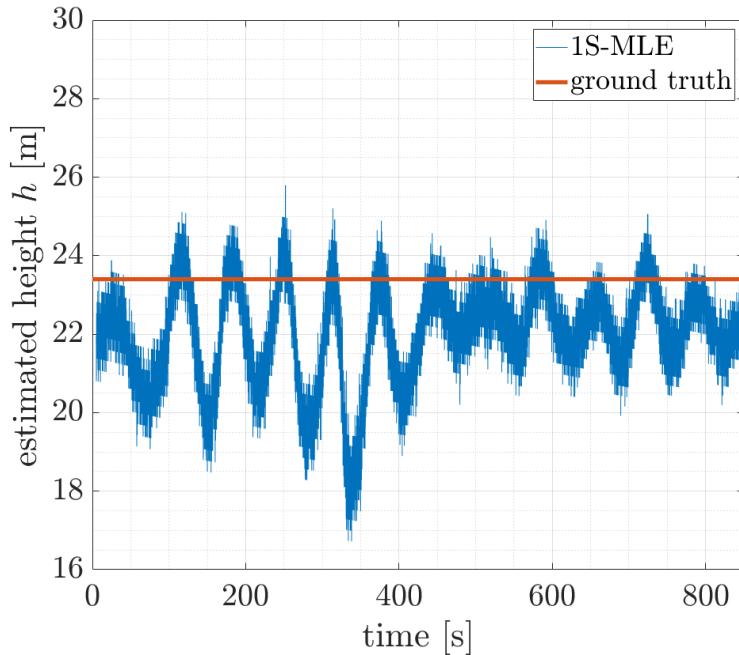


# Dual source signal processing

Assuming crosstalk: dual source processing (CLEAN-RELAX estimator):

- RHCP antenna:  $\hat{t}_0^{\text{RHCP}}, \hat{t}_1^{\text{RHCP}}$ .
- LHCP antenna:  $\hat{t}_0^{\text{LHCP}}, \hat{t}_1^{\text{LHCP}}$ .

$$\hat{h} = \frac{c(\hat{t}_1^{\text{LHCP}} - \hat{t}_0^{\text{RHCP}})}{2 \sin(e)}$$





# Wrap-up on ground-based GNSS-R

## In this presentation

- Presentation of the Gruissan experiment.
- First results using a simple dual source signal processing scheme.  
 Lubeigt *et al.* 2022, *GRETSL*.



# Wrap-up on ground-based GNSS-R

## In this presentation

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  - ❑ Lubeigt *et al.* 2022, *GRETISI*.

## Related works

- Use of the 2S-CRB to assess signal crosstalk impact on standard GNSS-R processings.
  - ❑ Lubeigt *et al.* 2021, *Remote Sensing*.
- Signal antenna close-to-ground GNSS-R:
  - Taylor approximation of the 2S-MLE to reduce its complexity.
  - Validation with simulations and comparison with 2S-MLE performance.
  - ❑ Lubeigt *et al.* 2022, *NAVITEC*.
  - ❑ Lubeigt *et al.* (under review after major revision), *Signal Processing*.

### 3 – Diffuse reflection





# Specular vs diffuse reflections



Specular reflection



# Specular vs diffuse reflections



## Specular reflection

- smooth surface (mirror-like),
- coherent reflection,

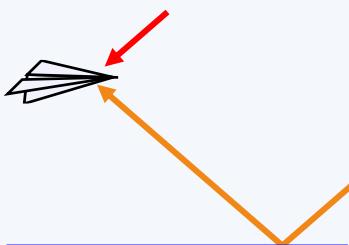


# Specular vs diffuse reflections



## Specular reflection

- smooth surface (mirror-like),
- coherent reflection,
- simple signal model.



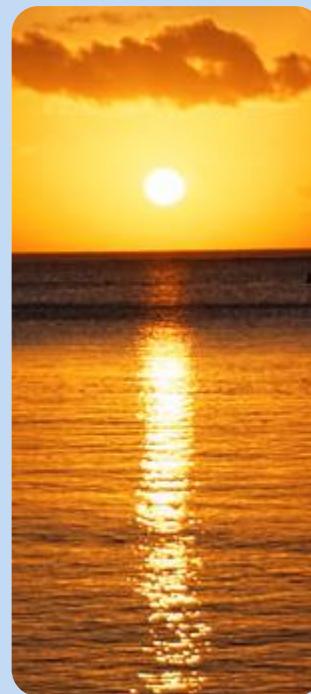
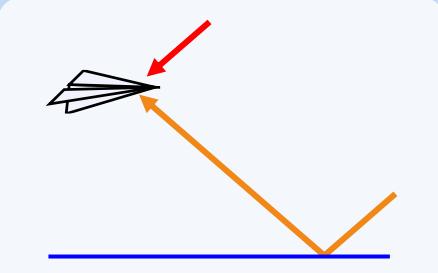


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Diffuse reflection

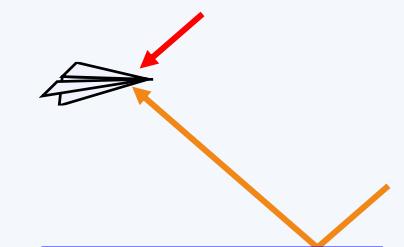


# Specular vs diffuse reflections



## Specular reflection

- smooth surface (mirror-like),
- coherent reflection,
- simple signal model.



## Diffuse reflection

- rough surface,
- coherent and non-coherent reflection,

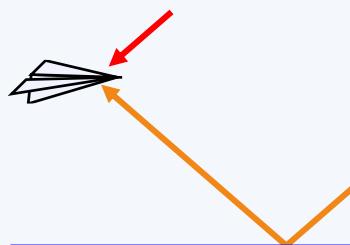


# Specular vs diffuse reflections



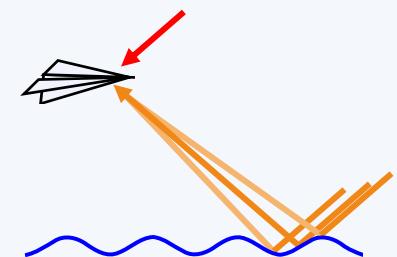
## Specular reflection

- smooth surface (mirror-like),
- coherent reflection,
- simple signal model.



## Diffuse reflection

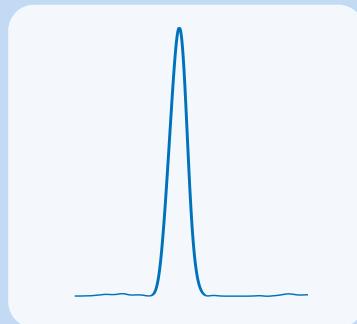
- rough surface,
- coherent and non-coherent reflection,
- signal model?





# Towards the impulse response signal model

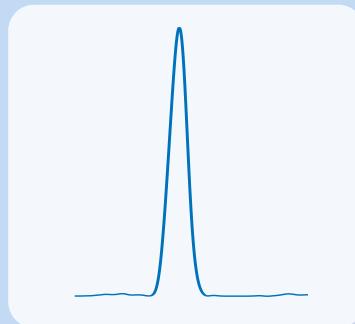
- Specular reflection:
  - symmetric cross-correlation function.



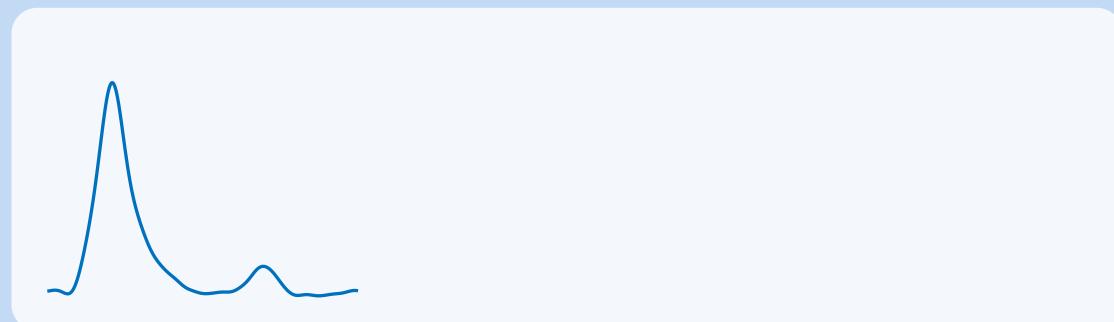


# Towards the impulse response signal model

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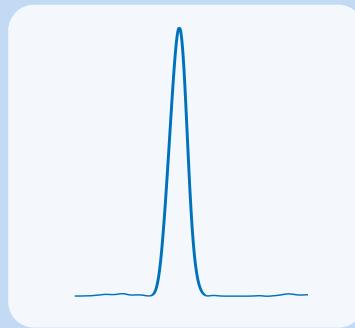
- Diffuse reflection:
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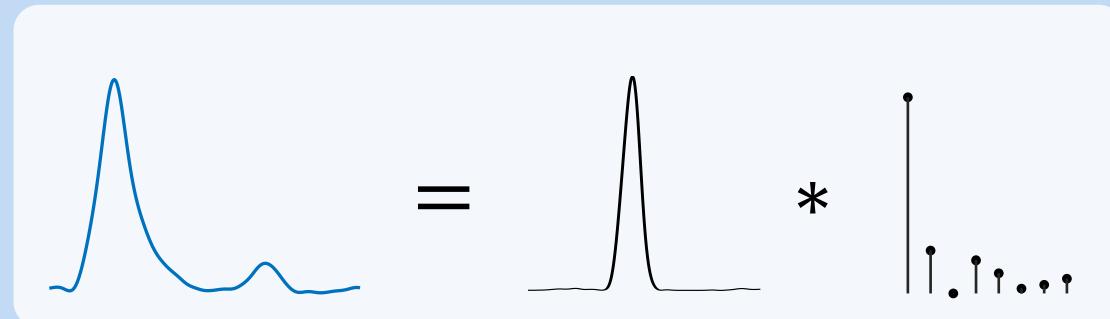


# Towards the impulse response signal model

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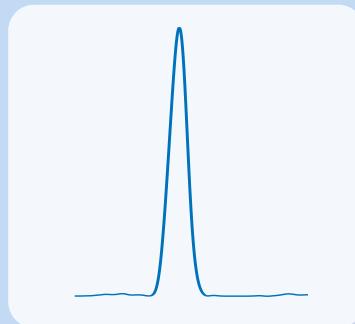
- Diffuse reflection:
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  - convolution product?



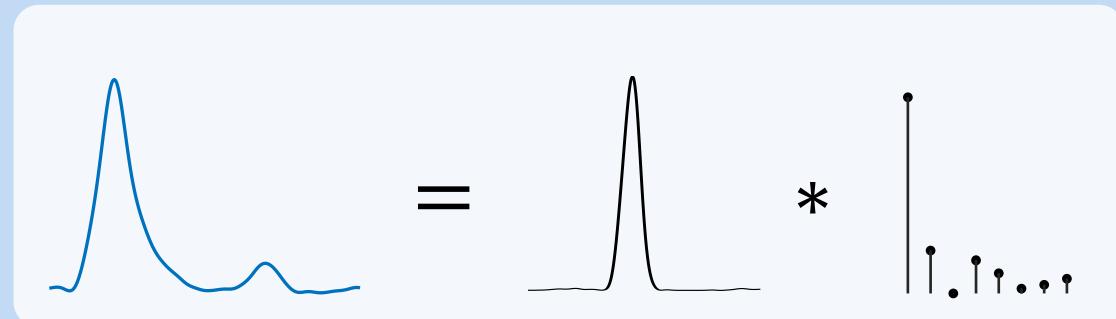


# Towards the impulse response signal model

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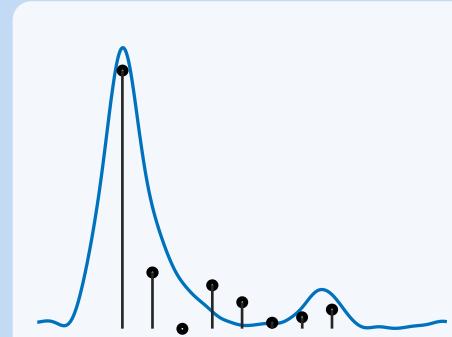
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Transmitted signal      Reflecting surface impulse response



# Reflecting surface IR estimation challenges





# Reflecting surface IR estimation challenges

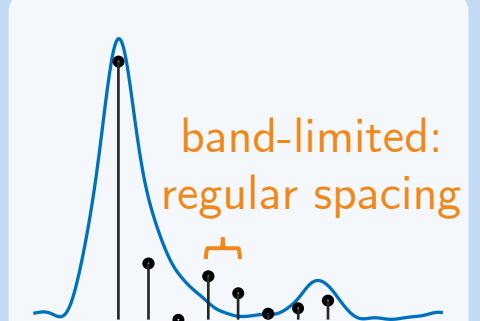
- Impulse response signal model (with  $P$  sources):

$$\mathbf{x} = \mathbf{h} * \mathbf{s}_0(\boldsymbol{\eta}) + \mathbf{w} = \mathbf{A}_P(\boldsymbol{\eta})\boldsymbol{\alpha} + \mathbf{w}, \mathbf{w} \sim \mathcal{CN}(\mathbf{0}, \sigma_n^2 \mathbf{I}_N),$$

with, for  $\boldsymbol{\eta}^T = (\tau, F_d)$ ,  $\mathbf{h} = \sum_{p=0}^{P-1} \alpha_p \delta_{pT_s}$ ,

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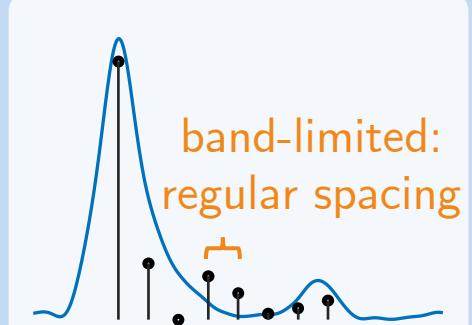
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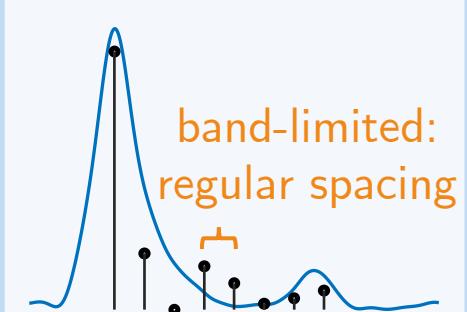
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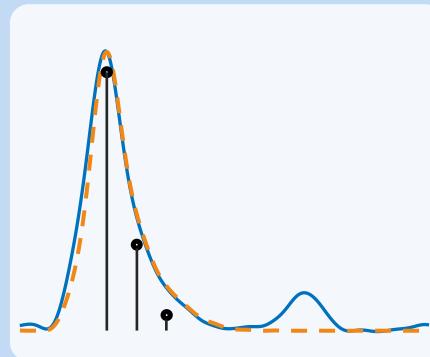
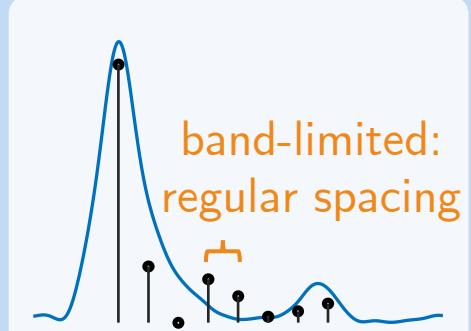
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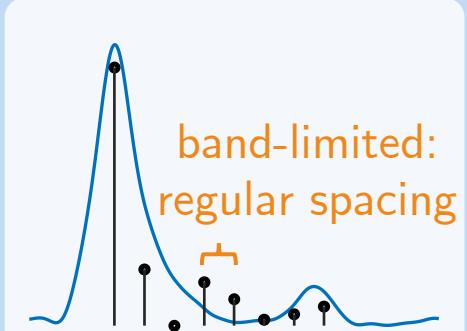
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- Undershoot:

- missed information,
  - bias estimates.





# Reflecting surface IR estimation challenges

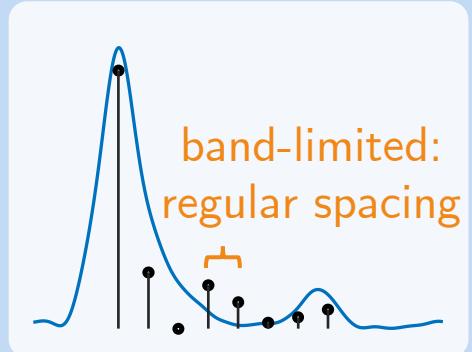
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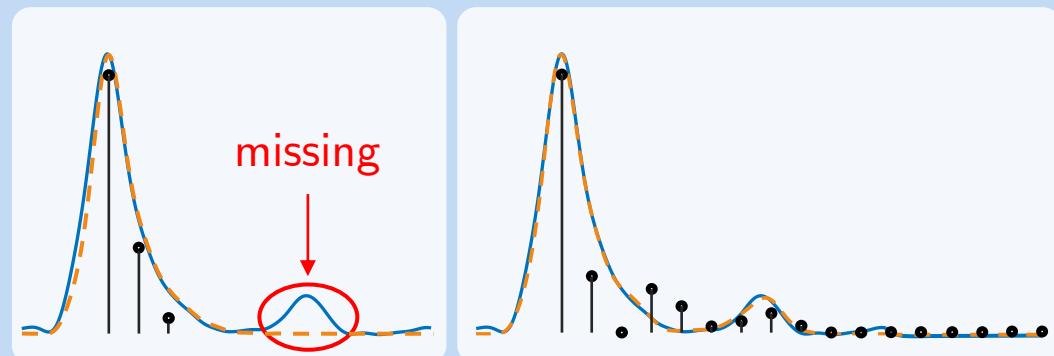
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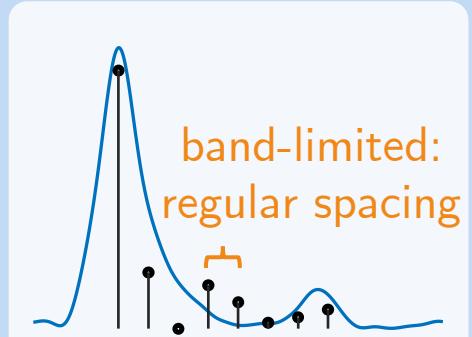
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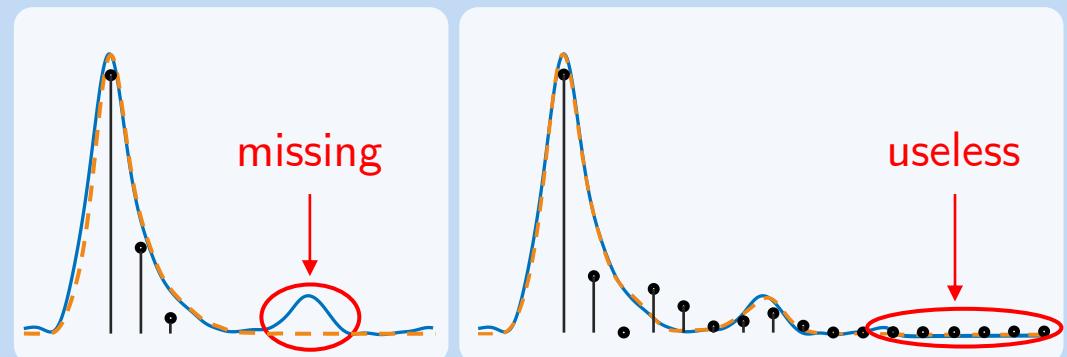
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- Challenge: determining the number of sources  $P$  to describe the impulse response.
- Undershoot:
  - missed information,
  - bias estimates.
- Overshoot:
  - correct but not optimal,
  - overkill...





# Reflecting surface IR size determination

Iterative procedure



# Reflecting surface IR size determination

## Iterative procedure

- Assume  $P$  sources,  $P < P_{\text{true}}$ ,
- test statistic for source  $P + 1$  based on the likelihood criterion:

$$T_{P+\text{next}} = \left| (\mathbf{P}_{\mathbf{A}_P}^\perp \mathbf{x})^H s_{P+1}(\hat{\tau}, \widehat{F_d}) \right|^2$$

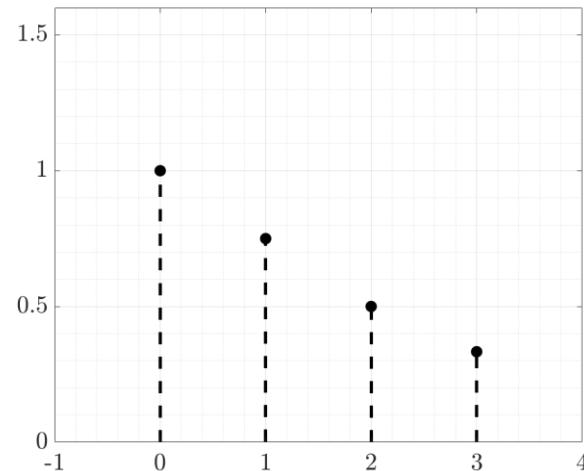


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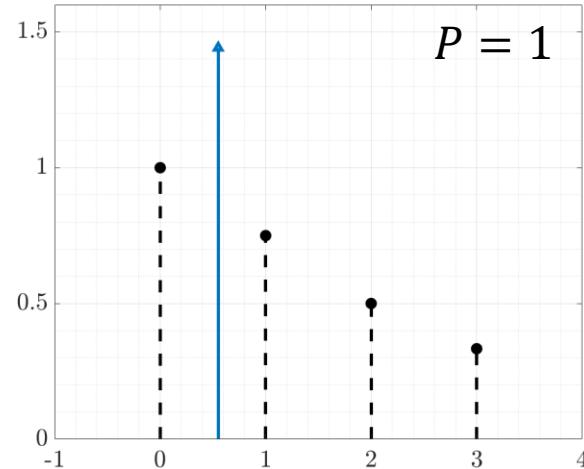


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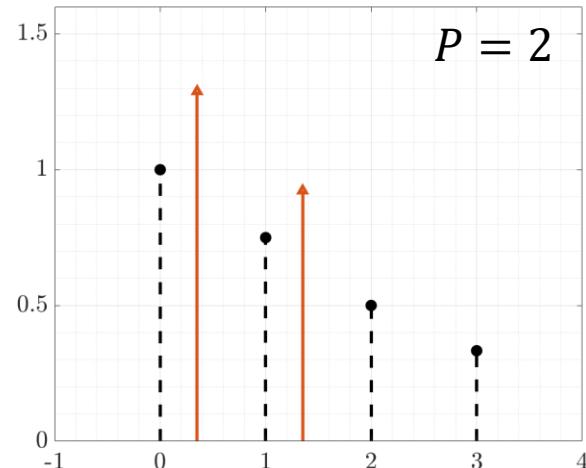


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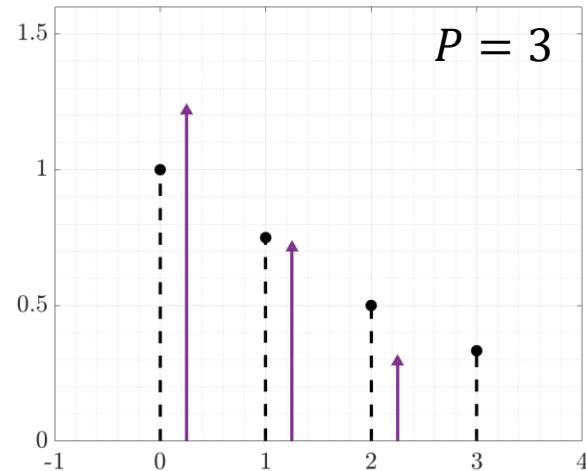


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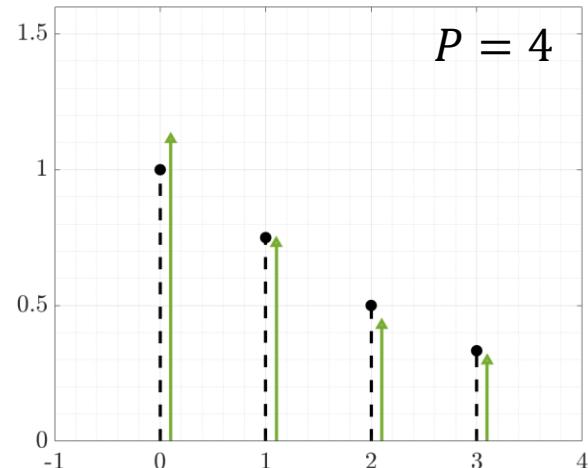


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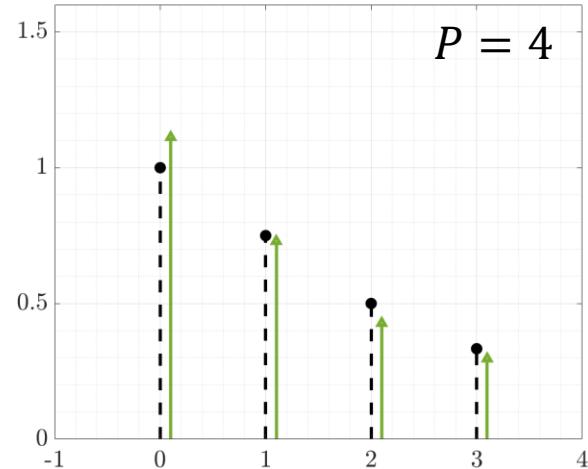


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## Overshoot-and-decimate procedure

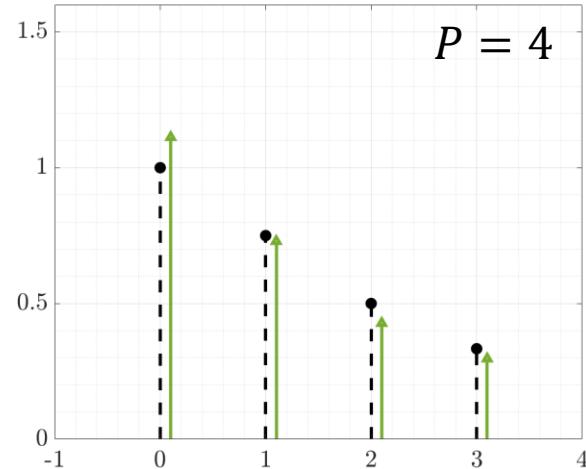


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## Overshoot-and-decimate procedure

- Assume  $M$  sources,  $M > P_{\text{true}}$ ,
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$$LR_m = \left\| \mathbf{P}_{\mathbf{A}_M}^\perp \mathbf{x} \right\|^2 / \left\| \mathbf{P}_{\mathbf{A}_{M-1,m}}^\perp \mathbf{x} \right\|^2$$

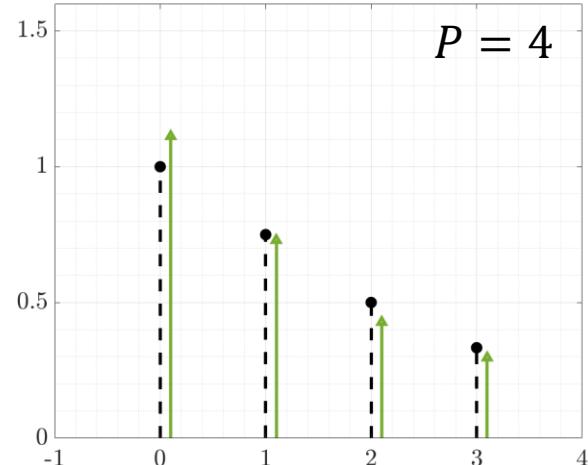


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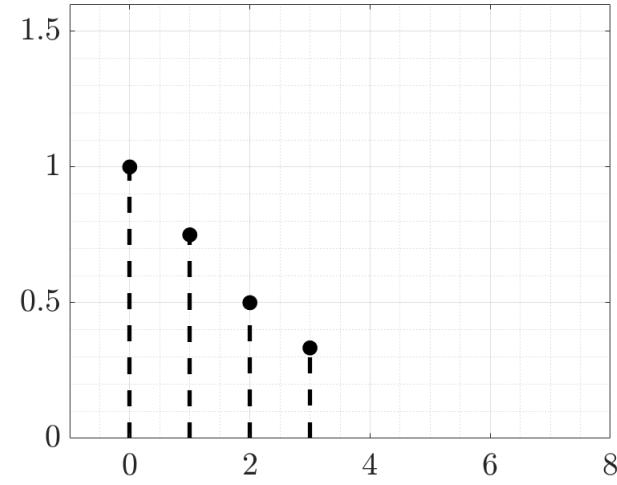
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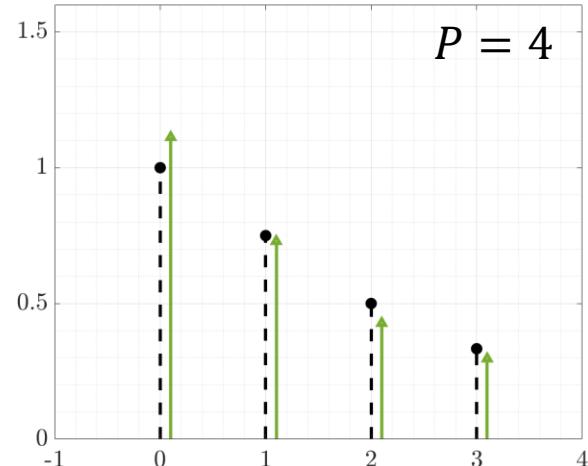


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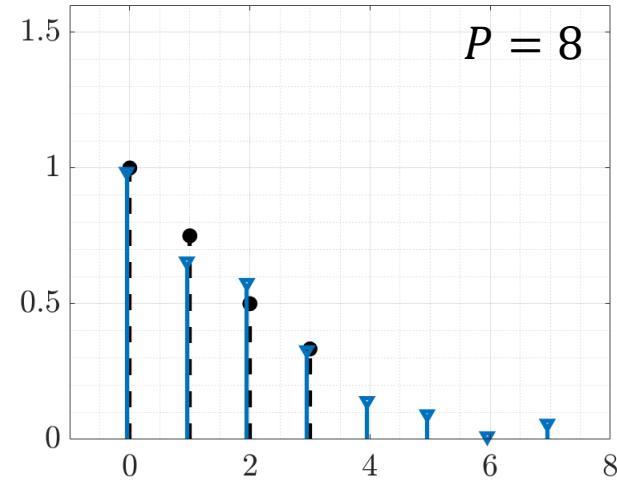
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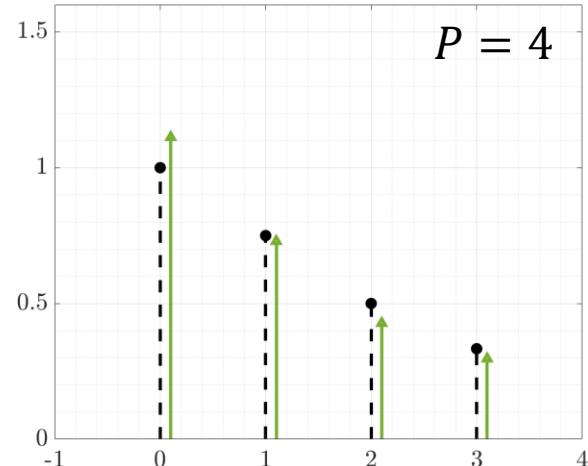


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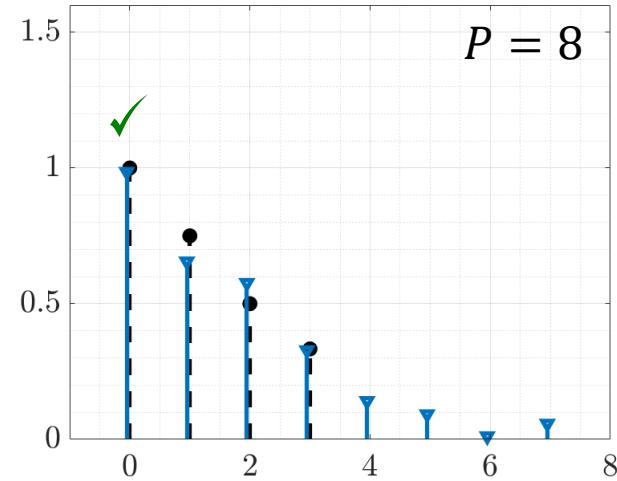
$$T_{P+\text{next}} = \left| (\mathbf{P}_{\mathbf{A}_P}^\perp \mathbf{x})^H s_{P+1}(\hat{\tau}, \widehat{F_d}) \right|^2$$



## Overshoot-and-decimate procedure

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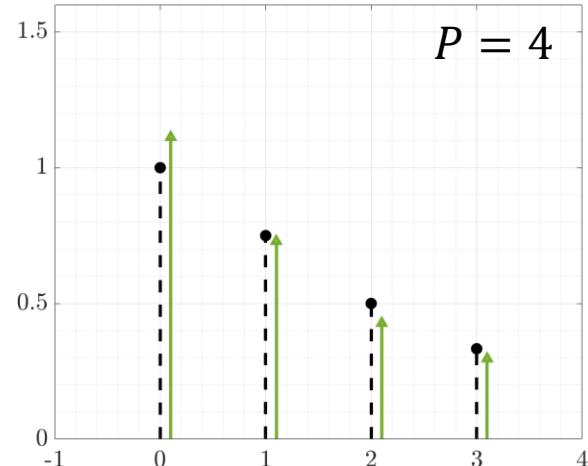


# Reflecting surface IR size determination

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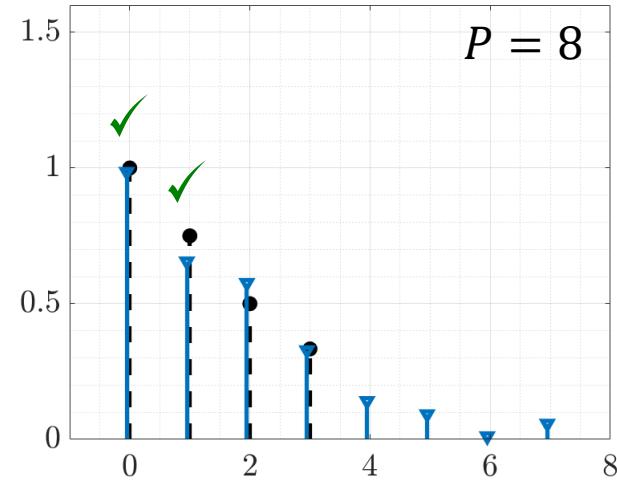
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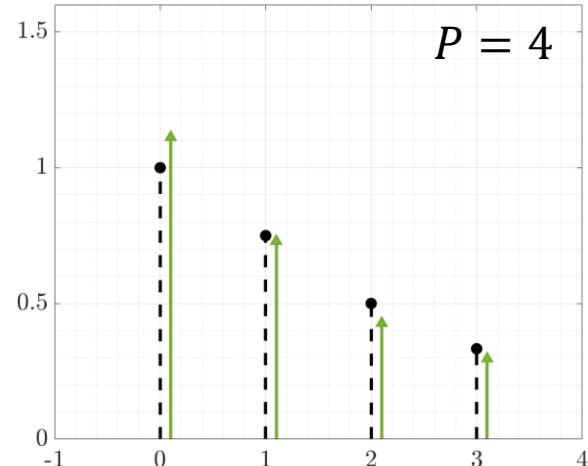


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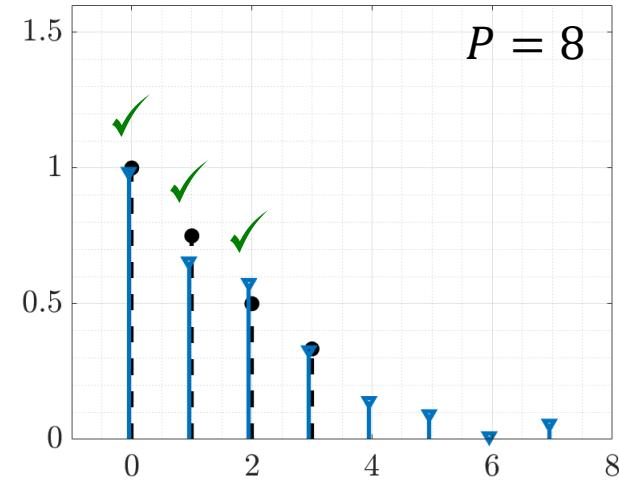
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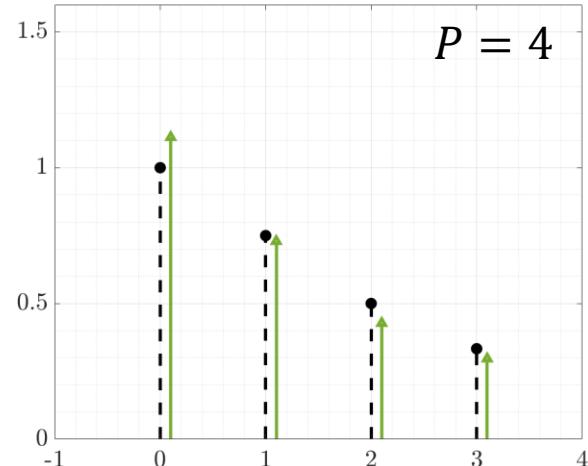


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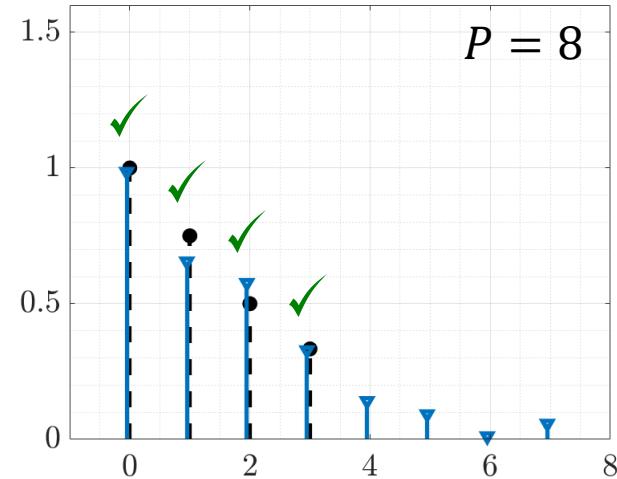
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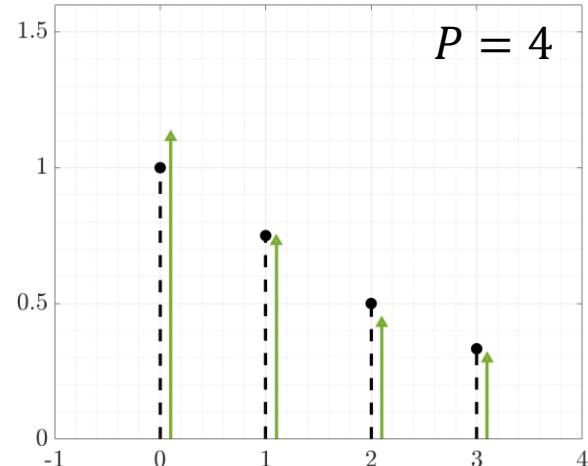


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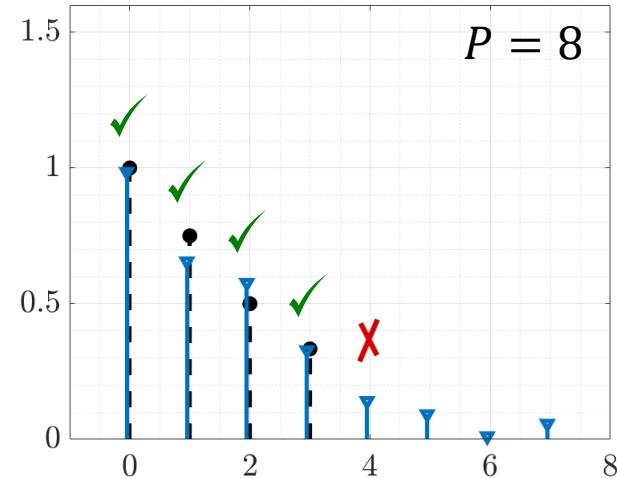
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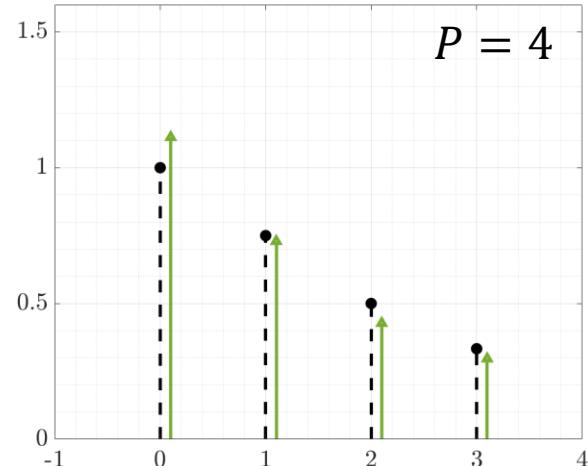


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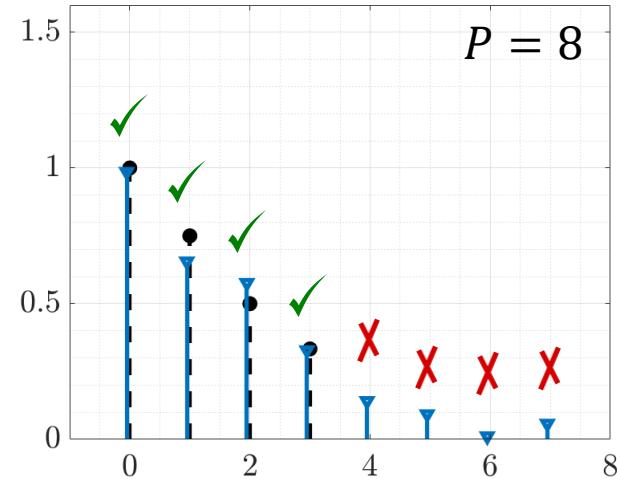
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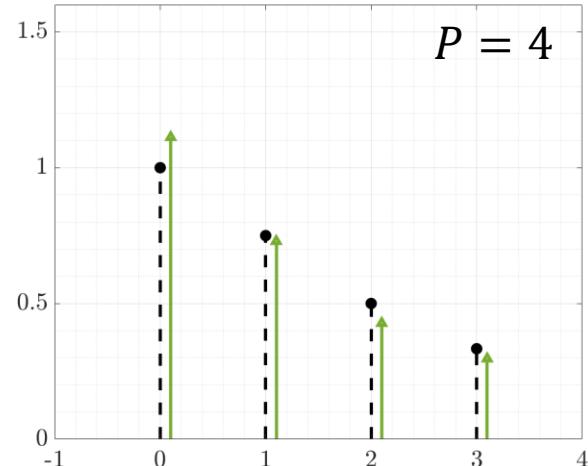


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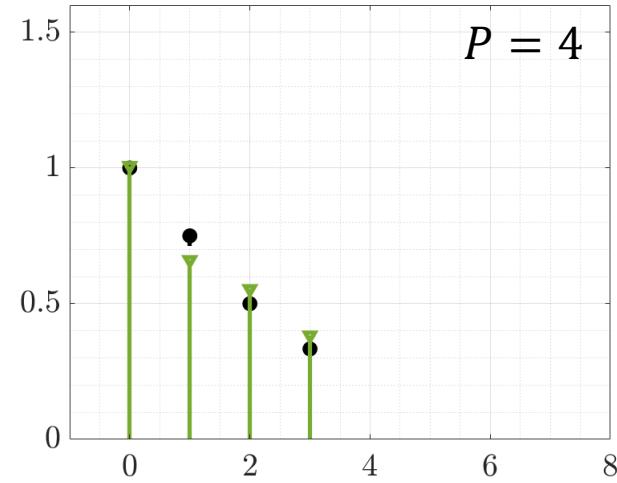
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## In this presentation

- Differences between specular and diffuse reflections.
- Introduction to reflecting surface impulse response signal model.
- Determination of the impulse response size.  
 Lubeigt *et al.* (under review after major revision), *Signal Processing*.



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## Related works

Signal coherence study with ICE in Barcelona:

- Mallorca's Puig Major experiment data.
- Detection of coherent-to-non-coherent transition based on the phase observation.
- Glistening zone size computation based on geometry.

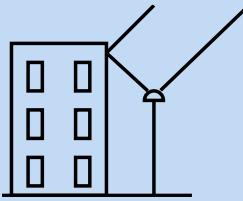
# Conclusion





# Conclusion

## GNSS Multipath



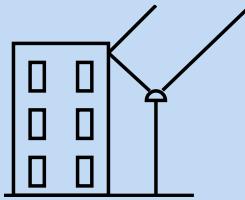
Theoretical approach:

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- Validation using the properties of the MLE.



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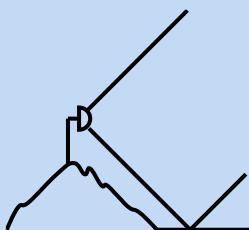
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## Ground-based GNSS-R



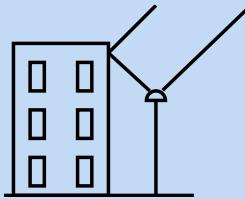
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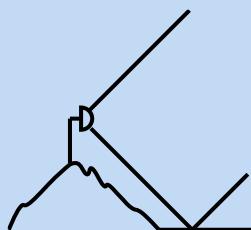
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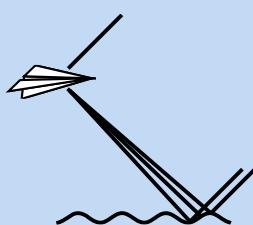
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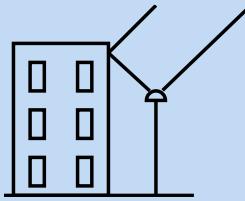


Exploratory approach:

- Specular / Diffuse reflection main differences.
- Reflecting surface impulse response signal model.
- Size of the reflecting surface impulse response.



## GNSS Multipath

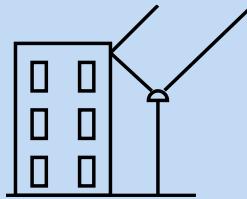


- Extension of MCRB to GNSS interferences (jamming, spoofing).  
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- Semiparametric signal models [[Fortunati \*et al.\* 2019](#)].



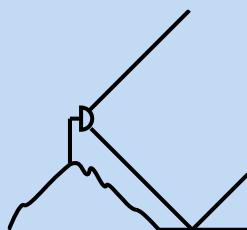
# Perspectives

## GNSS Multipath



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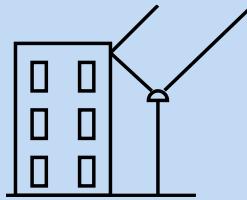


- Exploitation of wide bandwidth signals such as GALILEO E5 AltBOC or GNSS meta-signals [Ortega *et al.* 2020].
- Carrier phase [Lestarquit *et al.* 2016], [Medina *et al.* 2020].



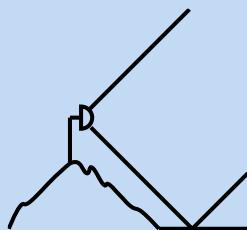
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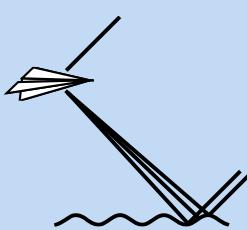
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## Diffuse reflection



- Reflecting surfaces are random objects:
  - unconditional signal models [Stoica and Nehorai, 1990],
  - sparsity-based models [Zhang *et al.* 2022].
- CNES SAFIRE experiment (airborne GNSS-R).



# Acknowledgements / Remerciements

## Encadrement de thèse



Eric, Jordi, Lorenzo, pour une équipe (trop) bien huilée.

## CNES



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tout le monde à TéSA, un environnement sain où il fait bon vivre.

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François pour ses idées géniales,  
Benoit pour son expérience et son précieux logiciel.

## ICE



Estel and Weiqiang for their (very) precious time and experience!



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- Corentin Lubeigt, et al. "Joint Delay-Doppler Estimation Performance in a Dual Source Context." *Remote Sensing*, vol. 12, no. 23, 3894, **2020**.
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- Corentin Lubeigt, et al. "Clean-to-Composite Bound Ratio: A Multipath Criterion for GNSS Signal Design and Analysis." *IEEE Transactions on Aerospace and Electronic Systems*, vol. 58, no. 6, pp. 5412–5424, **2022**.
- Corentin Lubeigt, et al. "Untangling First and Second Order Statistics Contributions in Multipath Scenarios." *Signal Processing*, vol. 205, 108868, **2023**.
- Corentin Lubeigt, et al. "Band-Limited Impulse Response Estimation Performance," submitted after major revision to *Signal Processing*.
- Corentin Lubeigt, et al. "Approximate Maximum Likelihood Time-Delay Estimation for Two Closely Spaced Sources," submitted after major revision to *Signal Processing*.
- Lorenzo Ortega, et al. "On the GNSS Synchronization Performance Degradation under Interference Scenarios: Bias and Misspecified CRB," submitted to *Navigation*.



# PhD contributions - Conferences

- Corentin Lubeigt, *et al.* "Multipath Estimating Techniques Performance Analysis." *IEEE Aerospace Conference* (March 2022): 1–6.
- Corentin Lubeigt, *et al.* "Close-to-Ground Single Antenna GNSS-R." *NAVITEC* (April 2022).
- Corentin Lubeigt, *et al.* "Les Signaux à Bande Large au Service de la Réflectométrie par GNSS à Site Bas." *GRETSI* (September 2022).
- Lorenzo Ortega, *et al.* "GNSS L5/E5 Maximum Likelihood Synchronization Performance Degradation Under DME Interferences." *IEEE/ION Position, Location and Navigation Symposium* (April 2023).



# Back-up: CRB calculation steps

- Slepian-Bangs formula:

$$[\mathbf{F}_{\epsilon|\epsilon}(\epsilon)]_{k,l} = \frac{2}{\sigma_n^2} \operatorname{Re} \left\{ \left( \frac{\partial \mathbf{A}\alpha}{\partial \epsilon_k} \right)^H \left( \frac{\partial \mathbf{A}\alpha}{\partial \epsilon_l} \right) \right\} + \frac{N}{\sigma_n^4} \frac{\partial \sigma_n^2}{\partial \epsilon_k} \frac{\partial \sigma_n^2}{\partial \epsilon_l}.$$

- $\mathbf{A}\alpha = \rho_0 e^{j\phi_0} \mathbf{s}(\tau_0, b_0) + \rho_1 e^{j\phi_1} \mathbf{s}(\tau_1, b_1)$ .
- After derivating and rearranging the terms:

$$\mathbf{F}_{\epsilon|\epsilon}(\epsilon) = \frac{2F_s}{\sigma_n^2} \operatorname{Re} \left\{ \mathbf{Q} \begin{bmatrix} \mathbf{W} & (\mathbf{W}^\Delta)^H \\ \mathbf{W}^\Delta & \mathbf{W} \end{bmatrix} \mathbf{Q}^H \right\} \text{ where } \mathbf{W}^\Delta = \begin{bmatrix} W_{1,1}^\Delta & W_{1,2}^\Delta & W_{1,3}^\Delta \\ W_{2,1}^\Delta & W_{2,2}^\Delta & W_{2,3}^\Delta \\ W_{3,1}^\Delta & W_{3,2}^\Delta & W_{3,3}^\Delta \end{bmatrix}.$$

$$\begin{aligned}
 \text{Example for } W_{1,1}^\Delta: \quad W_{1,1}^\Delta &= e^{j\omega_c \Delta b \tau_0} \int_R s(t - \tau_0) s(t - \tau_1)^* e^{-j2\pi f_c \Delta b t} dt \\
 &= \int_R s(u - \Delta\tau) (s(u) e^{j2\pi f_c \Delta b u})^* du \quad \begin{array}{l} u \leftarrow t - \tau_1 \\ \text{FT over an} \\ \text{hermitian product} \end{array} \\
 &= \int_{-\frac{F_s}{2}}^{\frac{F_s}{2}} (S(f) e^{-j2\pi f \Delta\tau}) S(f - f_c \Delta b)^* df
 \end{aligned}$$



# Back-up: CRB calculation steps

- Fourier transform of a band-limited signal of band  $B = F_s$ , for  $f \in \left[-\frac{F_s}{2}, \frac{F_s}{2}\right]$ :

$$S(f) = \frac{1}{F_s} \sum_{n=0}^{N-1} s(nT_s) e^{-j2\pi f n T_s} = \frac{1}{F_s} \mathbf{s}^T \mathbf{v}(f)^* \text{ where } \begin{cases} \mathbf{s} = (\dots, s(nT_s), \dots)^T, \\ \mathbf{v}(f) = (\dots, e^{j2\pi f n}, \dots)^T. \end{cases}$$

$$\begin{aligned} W_{1,1}^\Delta &= \int_{-\frac{F_s}{2}}^{\frac{F_s}{2}} S(f) e^{-j2\pi f \Delta\tau} S(f - f_c \Delta b)^* df \\ &= \frac{1}{F_s} \int_{-\frac{1}{2}}^{\frac{1}{2}} (\mathbf{s}^T \mathbf{v}(f)^*) e^{-j2\pi f \frac{\Delta\tau}{T_s}} \left( \mathbf{s}^H \mathbf{U} \left( \frac{\Delta b f_c}{F_s} \right) \mathbf{v}(f) \right) df \quad \leftarrow f \leftarrow \frac{f}{F_s} \\ &= \frac{1}{F_s} \mathbf{s}^H \mathbf{U} \left( \frac{\Delta b f_c}{F_s} \right) \underbrace{\left( \int_{-\frac{1}{2}}^{\frac{1}{2}} \mathbf{v}(f) \mathbf{v}(f)^H e^{-j2\pi f \frac{\Delta\tau}{T_s}} df \right)}_{\mathbf{V}^{\Delta,0} \left( \frac{\Delta\tau}{T_s} \right)} \mathbf{s} = \frac{1}{F_s} \mathbf{s}^H \mathbf{U} \left( \frac{\Delta b f_c}{F_s} \right) \mathbf{V}^{\Delta,0} \left( \frac{\Delta\tau}{T_s} \right) \mathbf{s}, \end{aligned}$$

where  $\mathbf{U}(q) = \text{diag}(\dots, e^{-j2\pi q n}, \dots)$ ,  $[\mathbf{V}^{\Delta,0}(p)]_{k,l} = \text{sinc}(k - l - p)$ .



# Back-up: Misspecified Cramér-Rao bounds (MCRB)

- True signal model: dual source signal model, with  $\boldsymbol{\theta}^T = (\boldsymbol{\eta}^T, \rho, \phi)$  and  $\boldsymbol{\eta}^T = (\tau, b)$ ,

$$p_{\mathbf{x}}(\mathbf{x}; \boldsymbol{\theta}_0, \boldsymbol{\theta}_1) = \mathcal{CN}(\alpha_0 \mathbf{a}(\boldsymbol{\eta}_0) + \alpha_1 \mathbf{a}(\boldsymbol{\eta}_1), \sigma_n^2 \mathbf{I}_N).$$

- Misspecified signal model: single source signal model,  $pt$ : pseudottrue,

$$f_{\mathbf{x}}(\mathbf{x}; \boldsymbol{\theta}_{pt}) = \mathcal{CN}(\alpha_{pt} \mathbf{a}(\boldsymbol{\eta}_{pt}), \sigma_n^2 \mathbf{I}_N).$$

- Misspecified Maximum Likelihood Estimator (MMLE): MLE of the misspecified model. The MMLE is biased but it is asymptotically misspecified-unbiased: it concentrates to a mean with a given variance that can be characterized:

- Mean: pseudottrue estimate that minimizes the Kullback-Leibler Divergence:

$$\boldsymbol{\theta}_{pt} = \arg \min_{\boldsymbol{\theta}} \{D(p_{\mathbf{x}} || f_{\mathbf{x}})\}.$$

- Variance: misspecified Cramér-Rao bound (MCRB):

$$\mathbf{MCRB}(\boldsymbol{\theta}_{pt}) = \mathbf{A}(\boldsymbol{\theta}_{pt})^{-1} \mathbf{B}(\boldsymbol{\theta}_{pt}) \mathbf{A}(\boldsymbol{\theta}_{pt})^{-1}.$$

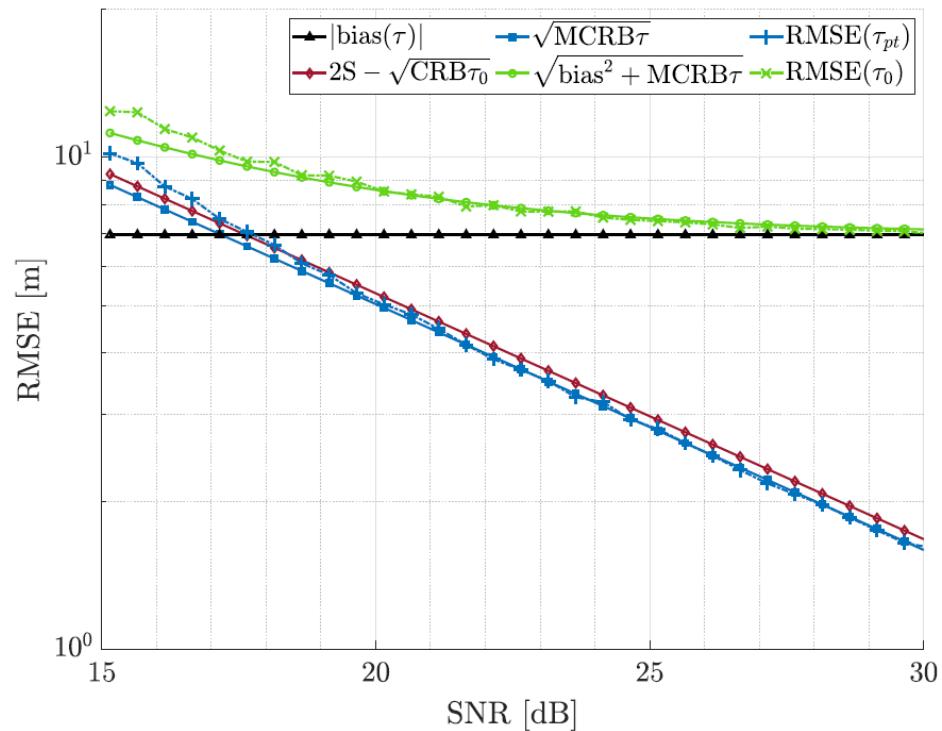
- $\mathbf{A}(\boldsymbol{\theta}_{pt})$  accounts for the model misspecification.
- $\mathbf{B}(\boldsymbol{\theta}_{pt})$  is the FIM of the single source signal model (known).



# Back-up: Misspecified Cramér-Rao bounds (MCRB)

- Simulation set-up:
  - signal: GPS L1 C/A,
  - 2000 Monte Carlo runs.

	$\theta_0$	$\theta_1$	$\theta_{pt}$
$\tau$ [m]	0	73.26	7
$F_d$ [Hz]	0	100	24
$\rho$ [-]	1	0.5	1.23
$\phi$ [deg]	0	15	2





# Back-up: 2S-MLE dimensionality reduction

- Signal model:  $\mathbf{x} = \mathbf{A}(\boldsymbol{\eta}_0, \boldsymbol{\eta}_1)\boldsymbol{\alpha} + \mathbf{w}, \mathbf{w} \sim \mathcal{CN}(\mathbf{0}, \sigma_n^2 \mathbf{I}_N) \Rightarrow \mathbf{x} \sim \mathcal{CN}(\mathbf{A}\boldsymbol{\alpha}, \sigma_n^2 \mathbf{I}_N).$

$$\hat{\boldsymbol{\epsilon}} = \arg \max_{\boldsymbol{\epsilon}} \{p(\mathbf{x}; \boldsymbol{\epsilon})\} \text{ where } p(\mathbf{x}; \boldsymbol{\epsilon}) = \frac{1}{(\pi \sigma_n^2)^N} e^{-\frac{1}{\sigma_n^2} \|\mathbf{x} - \mathbf{A}\boldsymbol{\alpha}\|^2}.$$

- Maximizing  $p(\mathbf{x}; \boldsymbol{\epsilon})$  is equivalent to minimizing  $\|\mathbf{x} - \mathbf{A}\boldsymbol{\alpha}\|^2$ :

$$\max_{\boldsymbol{\epsilon}} \{p(\mathbf{x}; \boldsymbol{\epsilon})\} = \min_{\boldsymbol{\epsilon}} \{\|\mathbf{x} - \mathbf{A}\boldsymbol{\alpha}\|^2\},$$

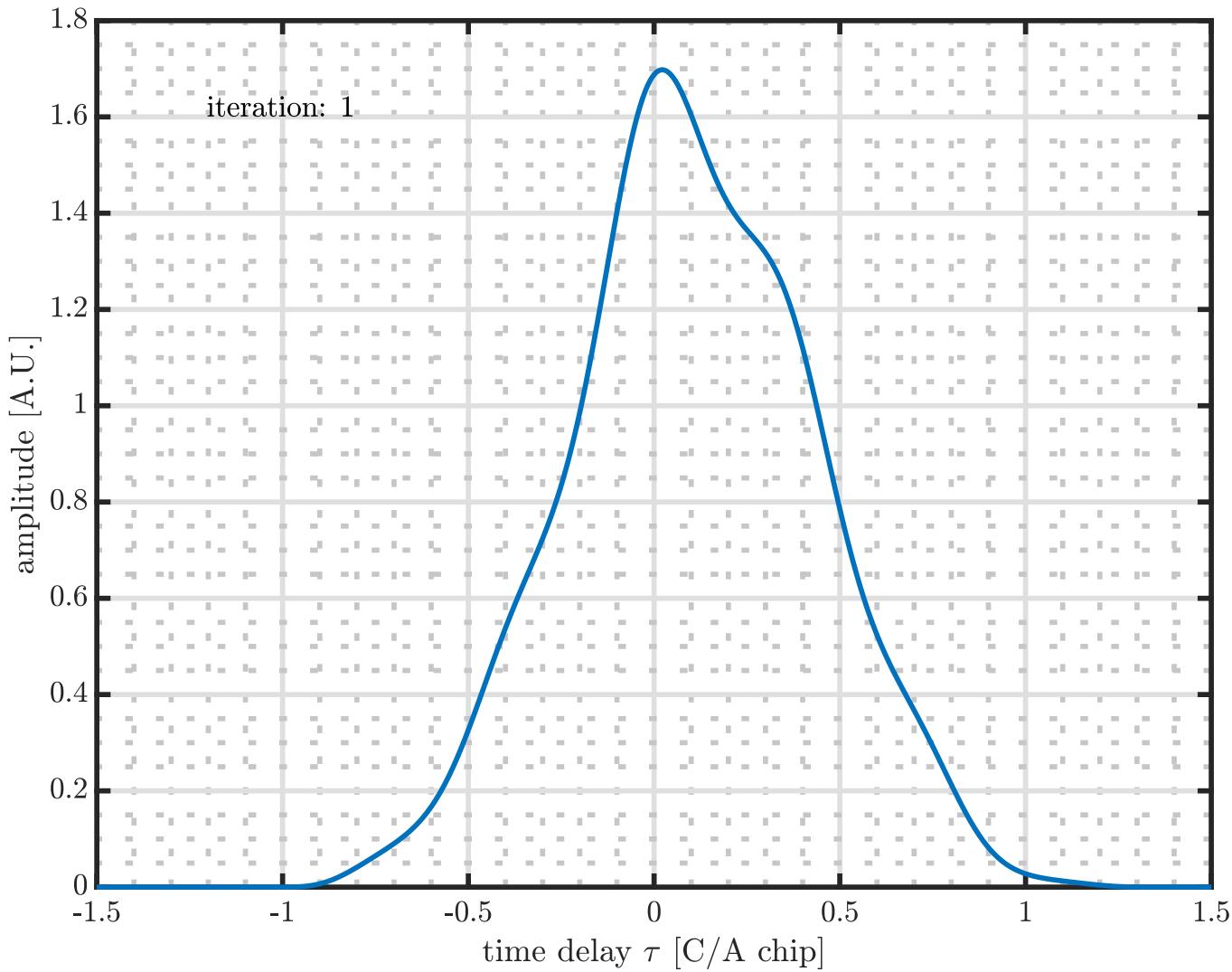
- and with the projector  $\mathbf{P}_A = \mathbf{A}(\mathbf{A}^H \mathbf{A})^{-1} \mathbf{A}^H$ ,

$$\begin{aligned} \|\mathbf{x} - \mathbf{A}\boldsymbol{\alpha}\|^2 &= \|\mathbf{P}_A(\mathbf{x} - \mathbf{A}\boldsymbol{\alpha})\|^2 + \|\mathbf{P}_A^\perp(\mathbf{x} - \mathbf{A}\boldsymbol{\alpha})\|^2 \\ &= \underbrace{\left\| \mathbf{A} \left( (\mathbf{A}^H \mathbf{A})^{-1} \mathbf{A}^H \mathbf{x} - \boldsymbol{\alpha} \right) \right\|^2}_{\text{null for } \boldsymbol{\alpha} \text{ well chosen}} + \|\mathbf{P}_A^\perp \mathbf{x}\|^2. \end{aligned}$$

$$\hat{\boldsymbol{\epsilon}} = \min_{\boldsymbol{\epsilon}} \{\|\mathbf{x} - \mathbf{A}\boldsymbol{\alpha}\|^2\} \Leftrightarrow \min_{\boldsymbol{\eta}_0, \boldsymbol{\eta}_1} \left\{ \|\mathbf{P}_A^\perp \mathbf{x}\|^2 \right\} \text{ and } \hat{\boldsymbol{\alpha}} = (\mathbf{A}^H \mathbf{A})^{-1} \mathbf{A}^H \mathbf{x}.$$

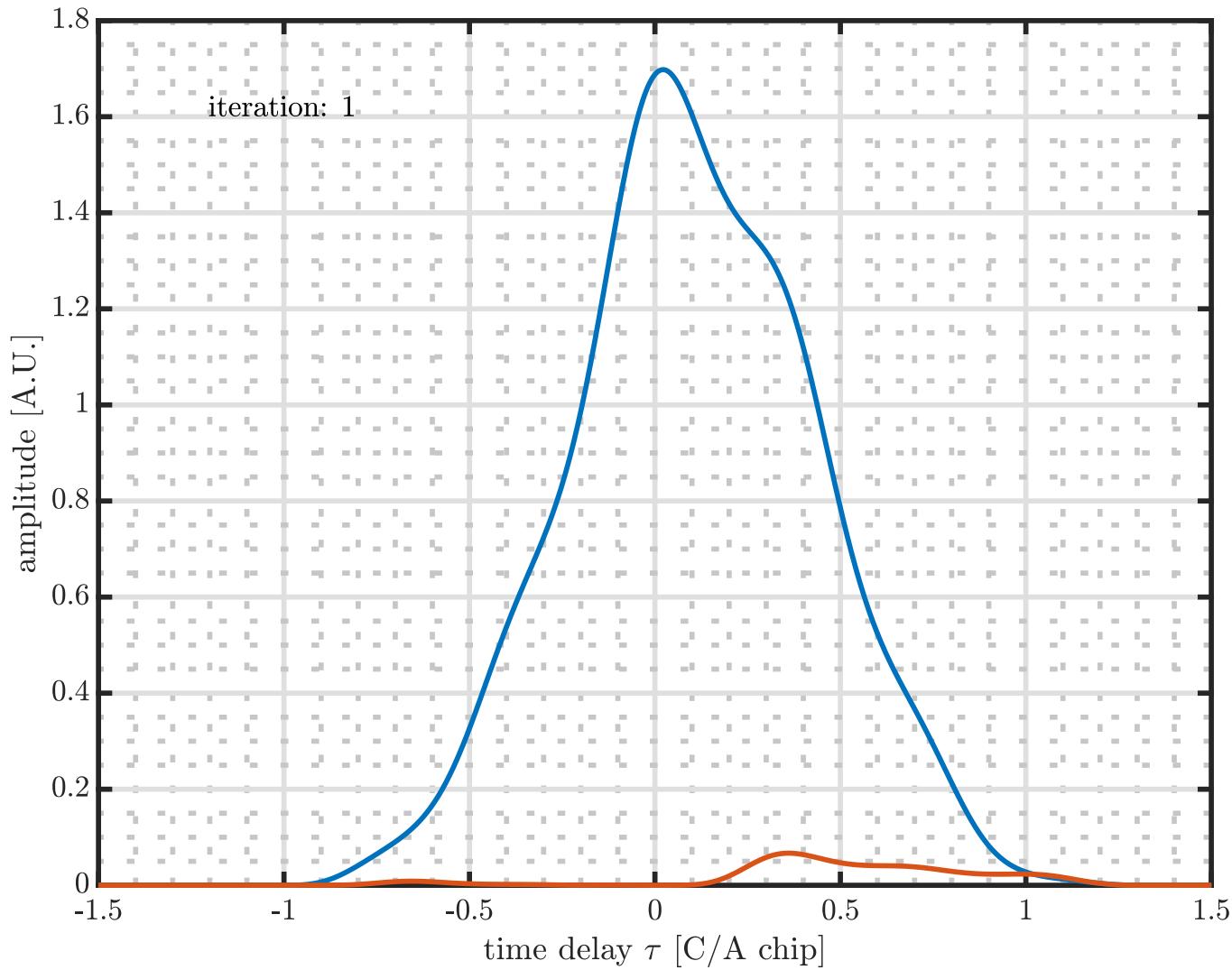


# Back-up: CLEAN-RELAX estimator



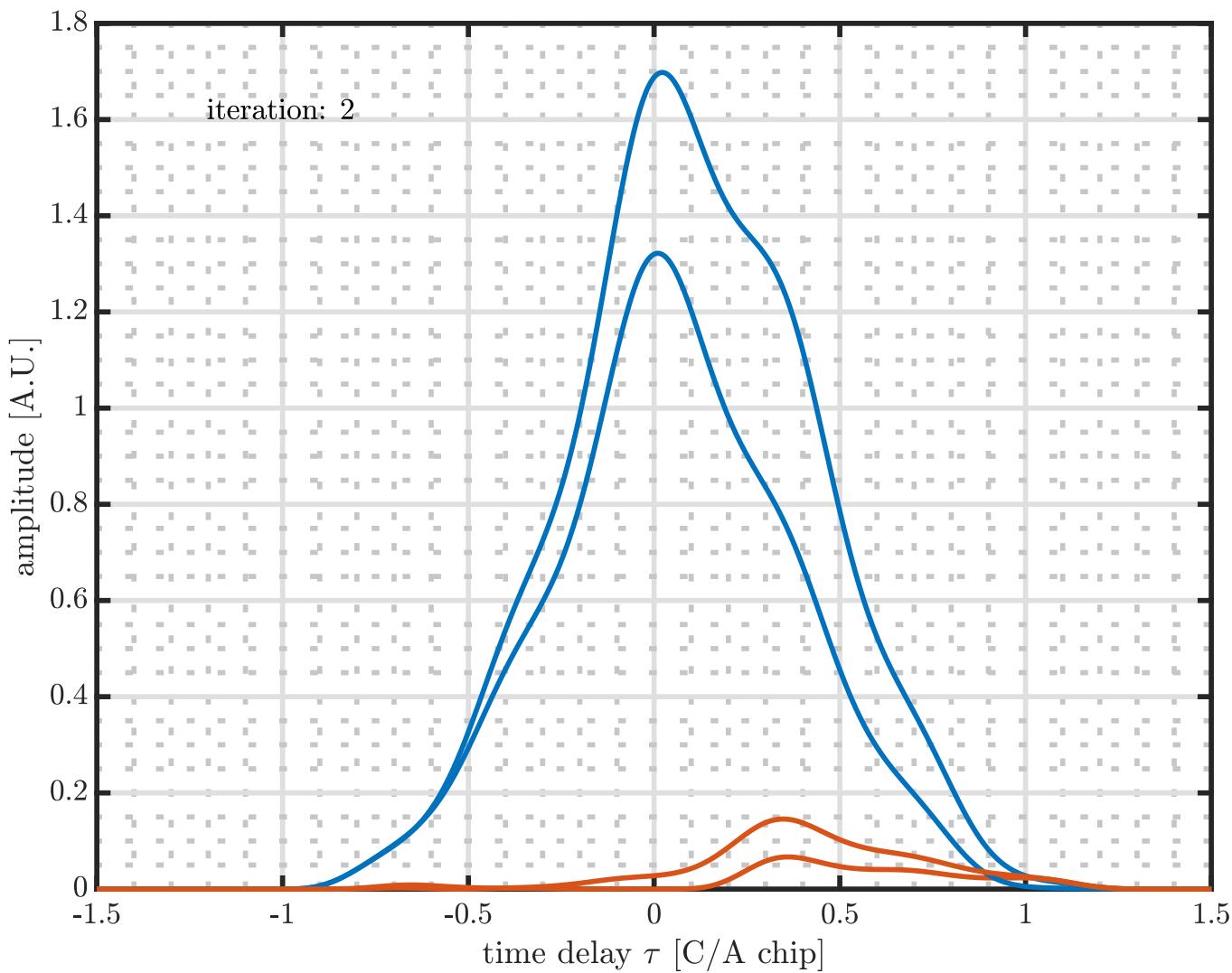


# Back-up: CLEAN-RELAX estimator



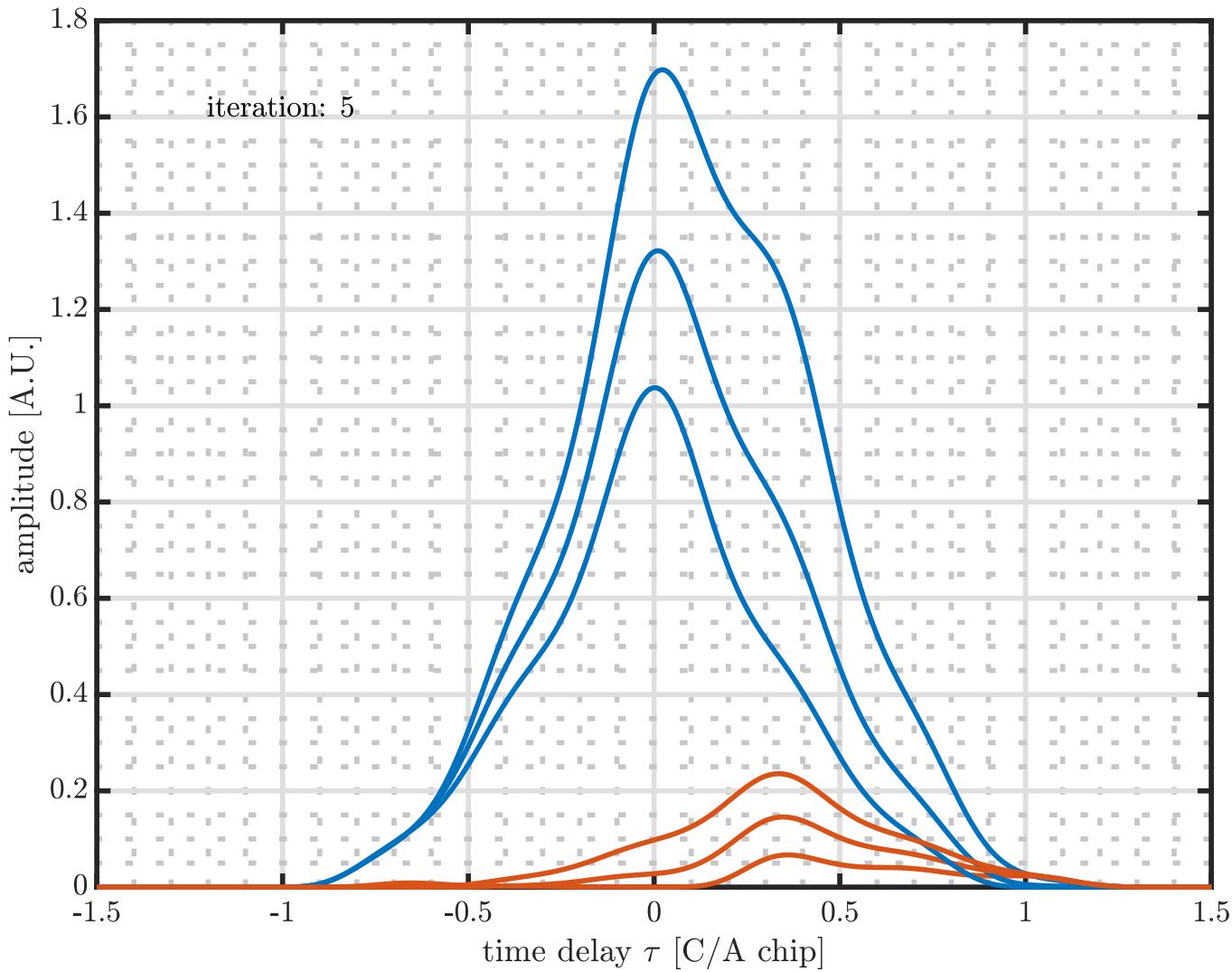


# Back-up: CLEAN-RELAX estimator



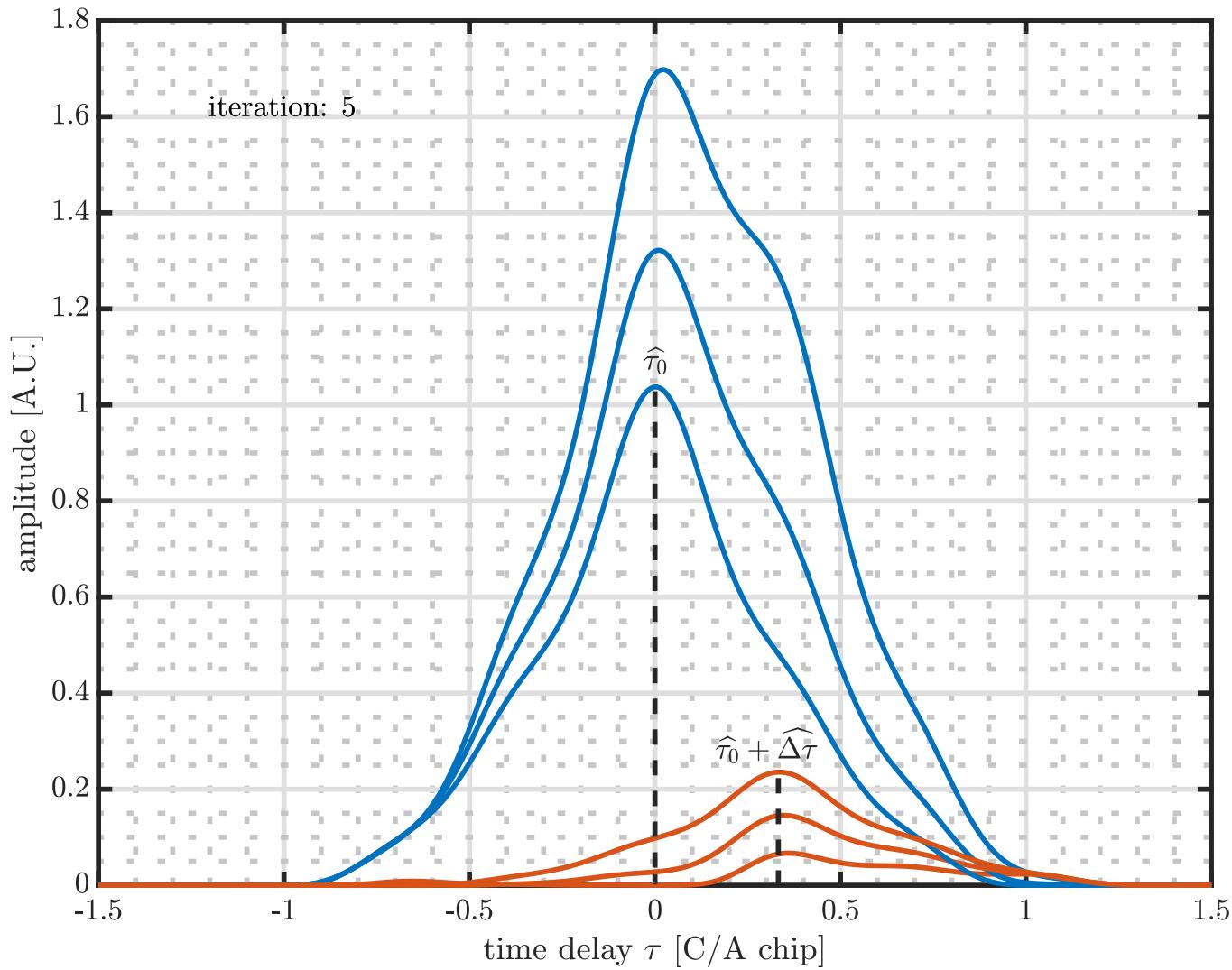


# Back-up: CLEAN-RELAX estimator



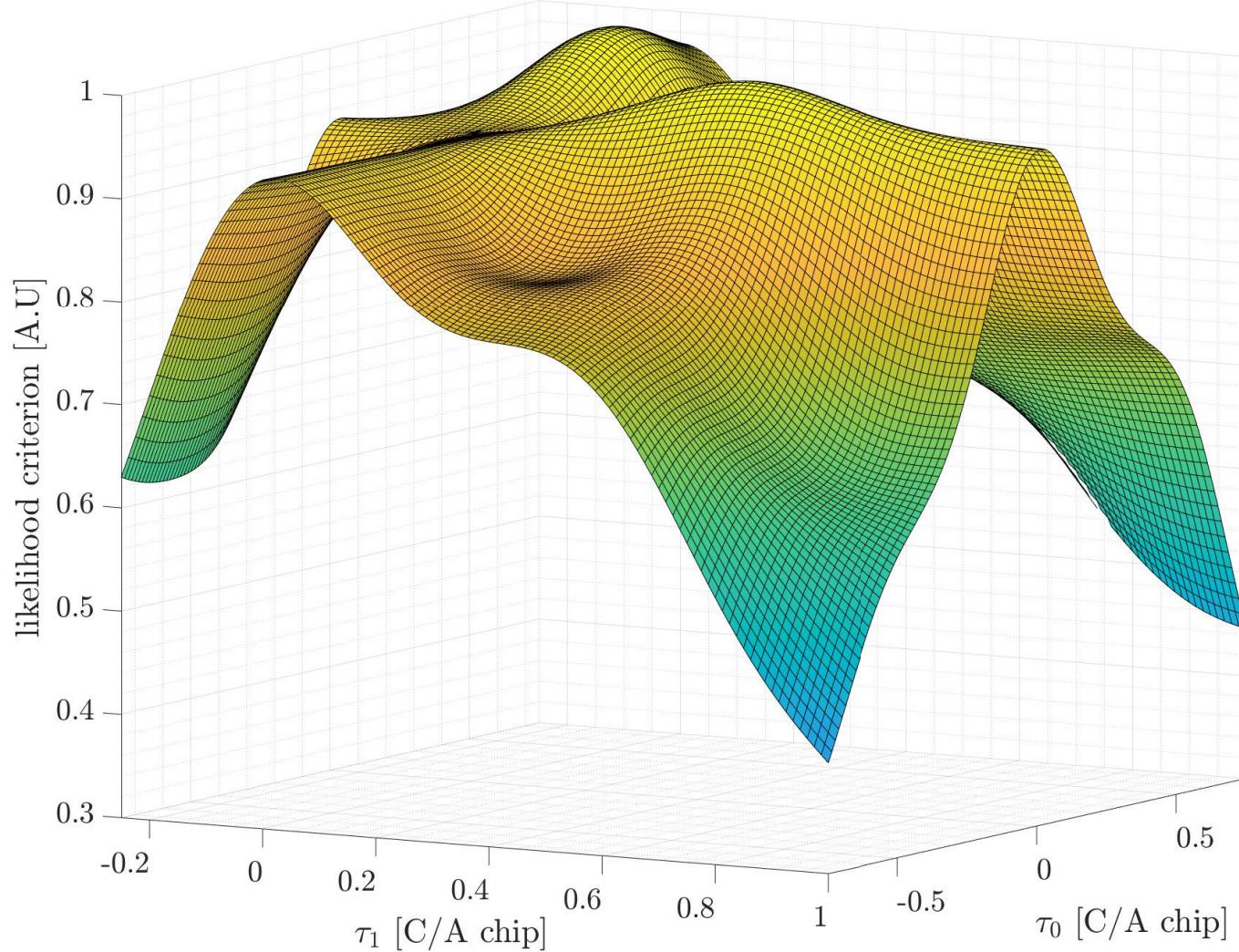


# Back-up: CLEAN-RELAX estimator



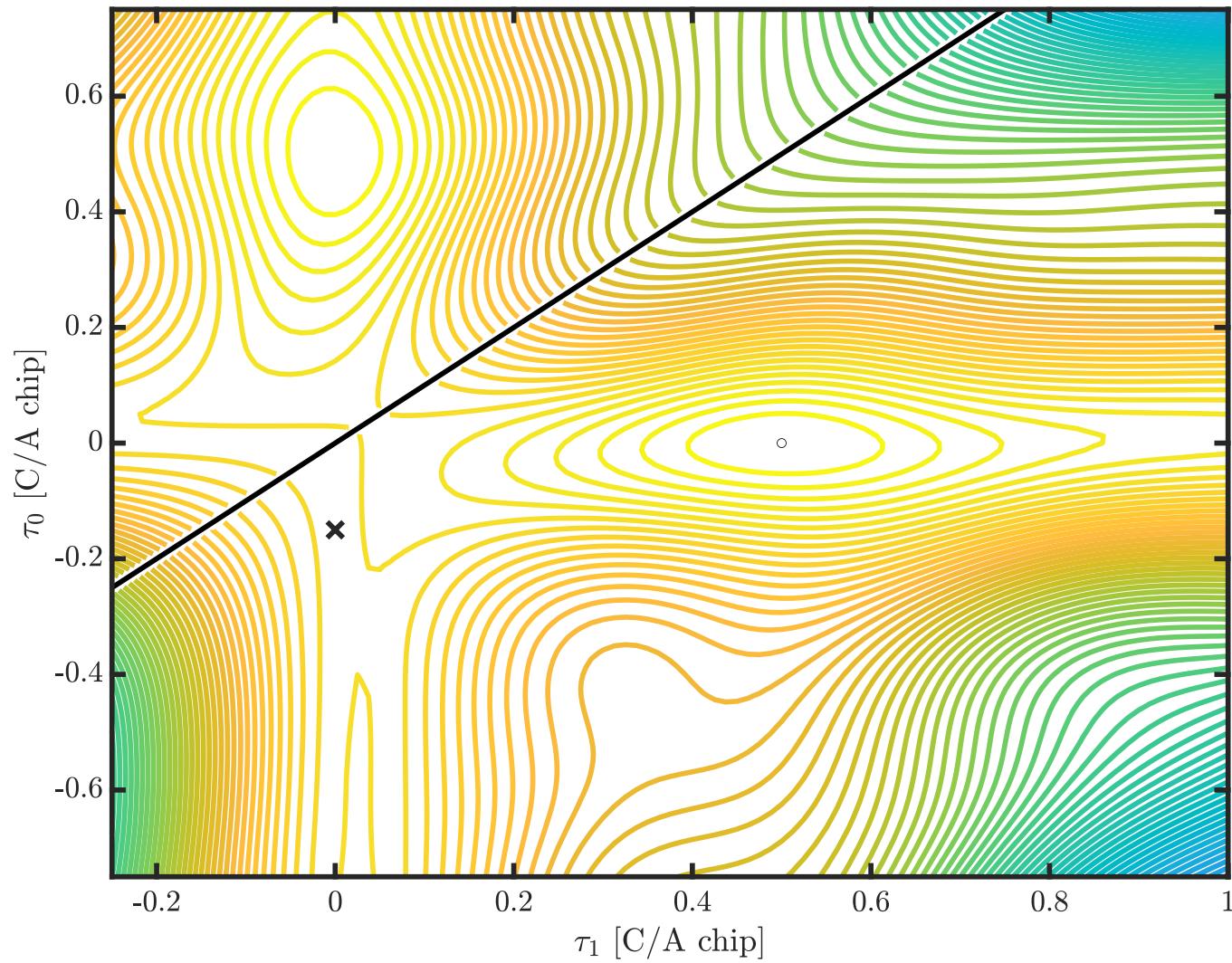


# Back-up: Alternate Projection estimator



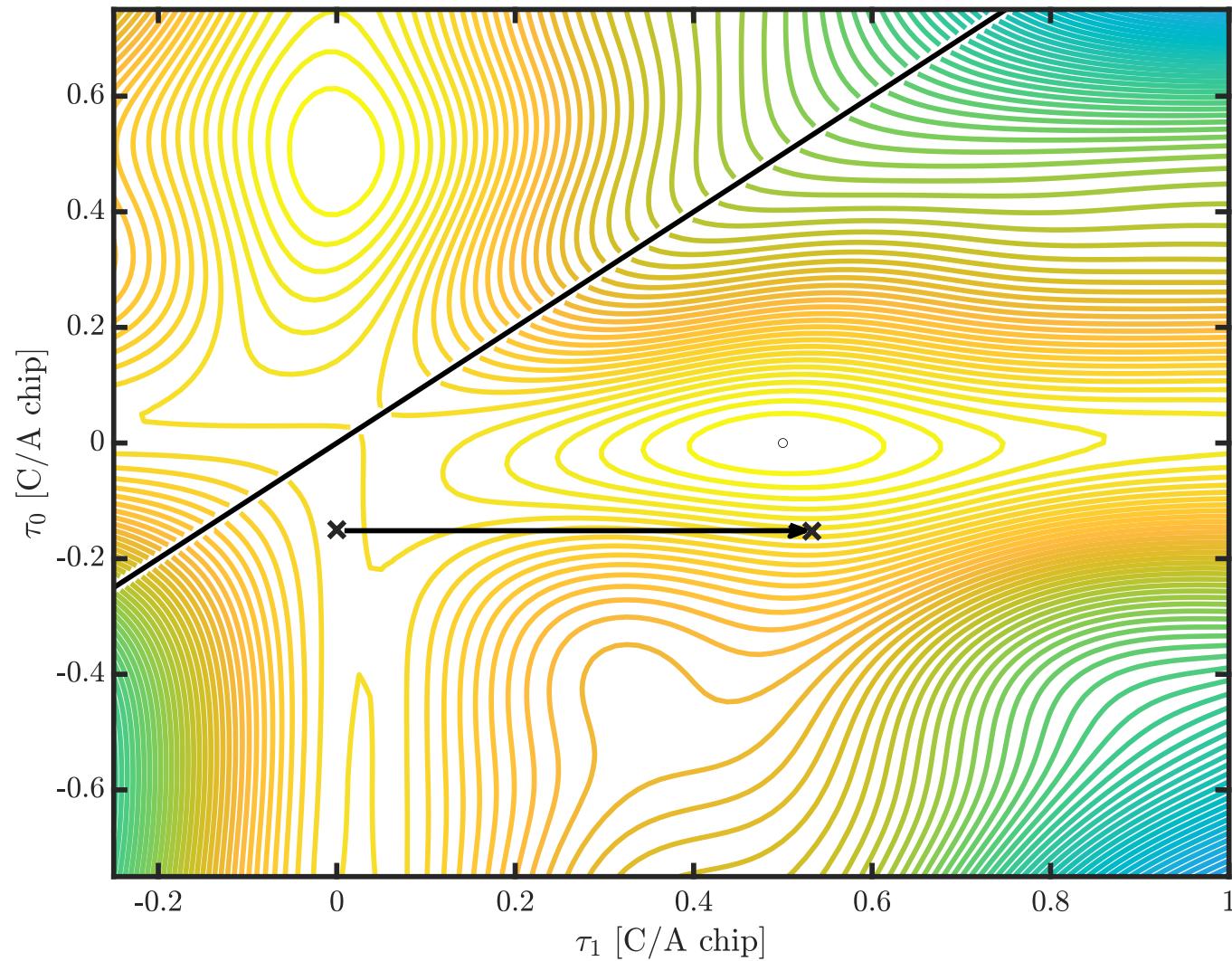


# Back-up: Alternate Projection estimator



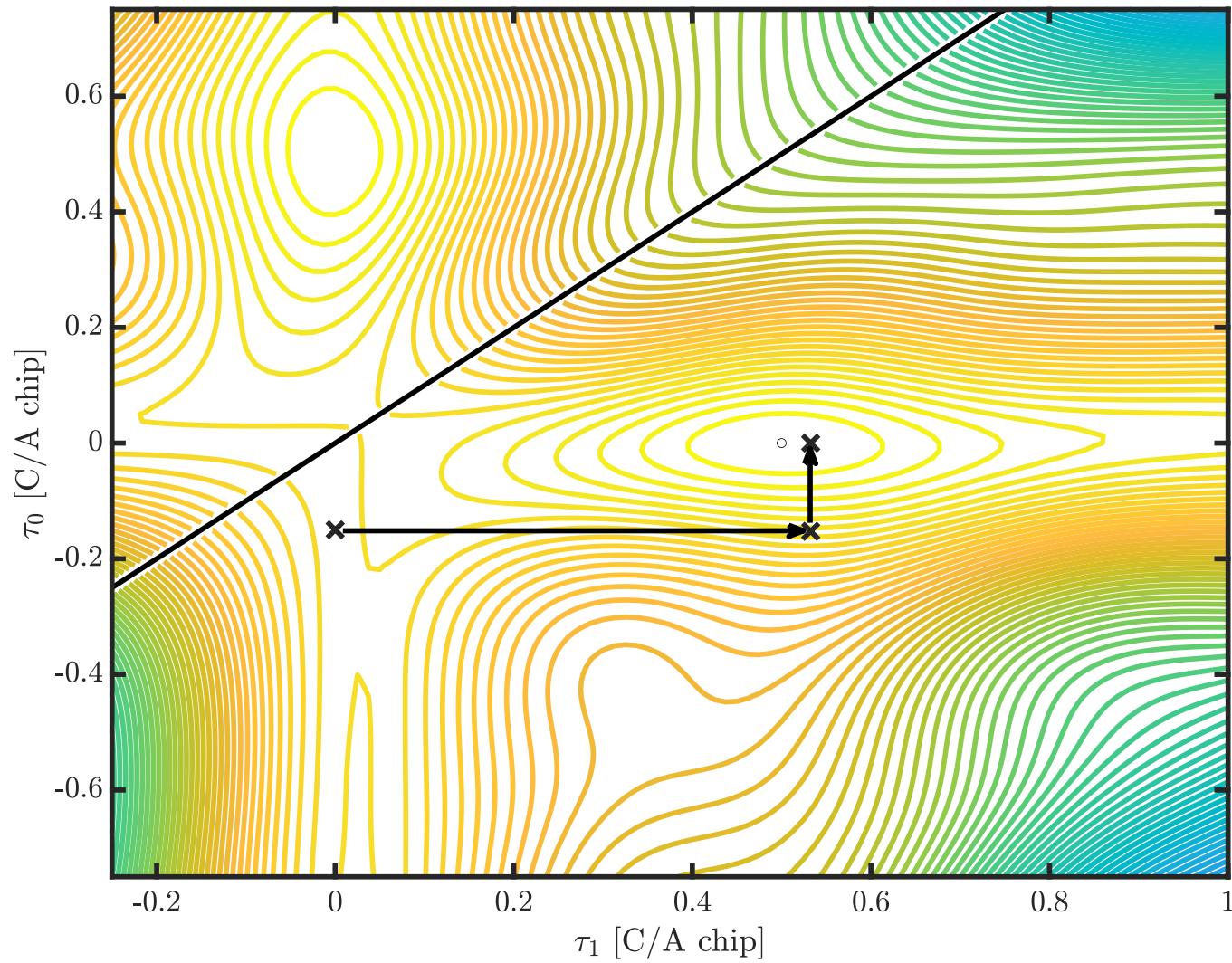


# Back-up: Alternate Projection estimator



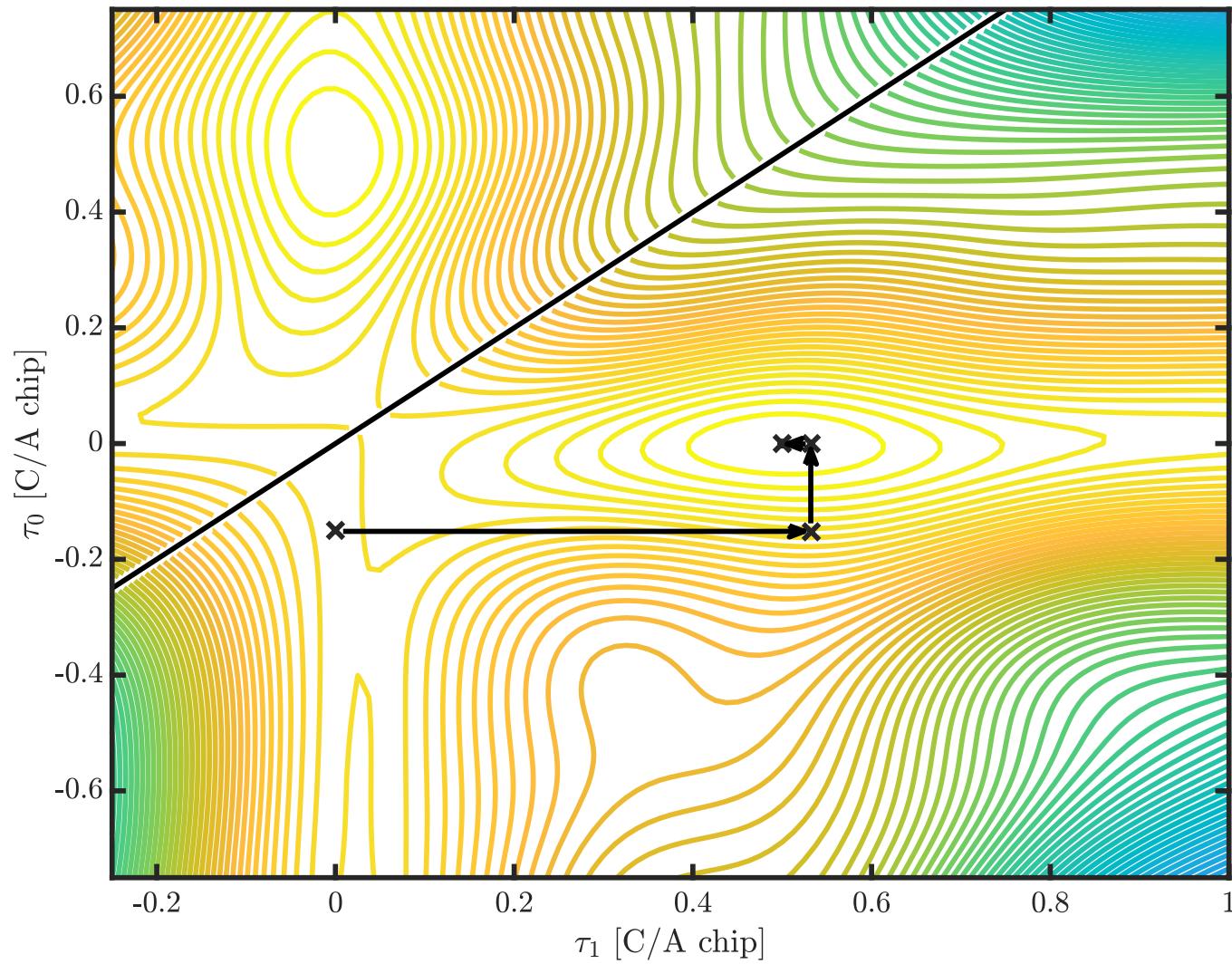


# Back-up: Alternate Projection estimator



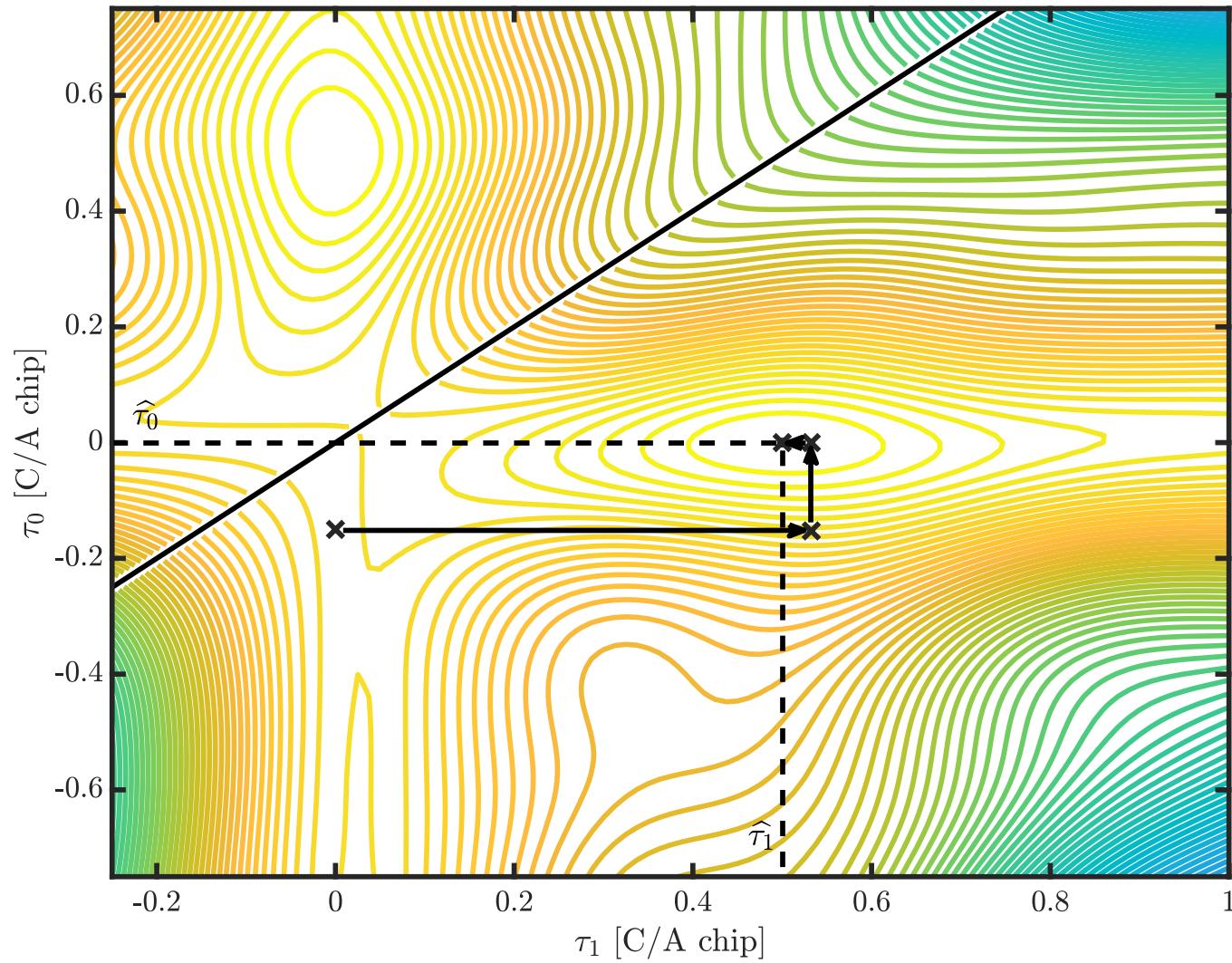


# Back-up: Alternate Projection estimator



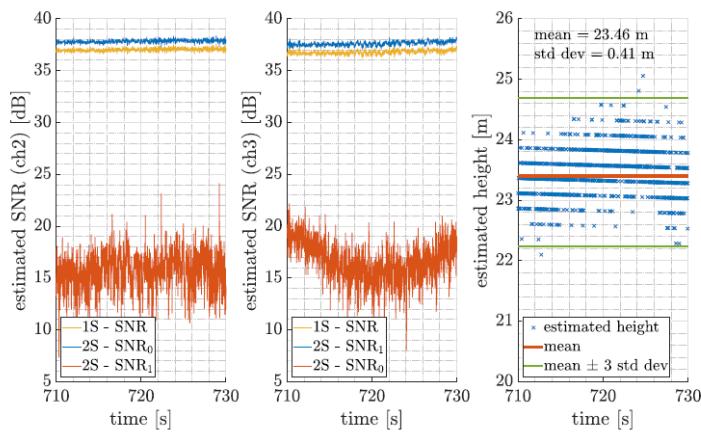
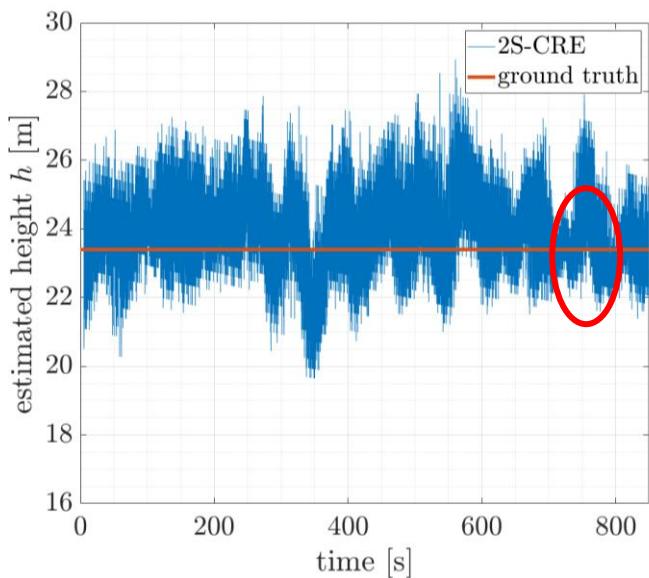


# Back-up: Alternate Projection estimator





# Back-up: Gruissan experiment 2S processing limits



- Gruissan experiment on GPS L5Q signal:
  - CRB prediction:  $\sqrt{CRB_h} = 0.27\text{m}$ .
  - Height std dev:  $\sigma_h = 0.41\text{m}$ , 2dB off.
- Possible explanations:
  - Implementation: quantization error.
  - CLEAN-RELAX is biased for the considered path separation (22m): signal crosstalk.
  - Local replica used (RF filters).
  - Unidentified events during recording.
  - Specular reflection assumption:

Rayleigh Criterion:  $\Delta h > \frac{\lambda}{8 \sin(e)} \approx 5\text{cm}$ .



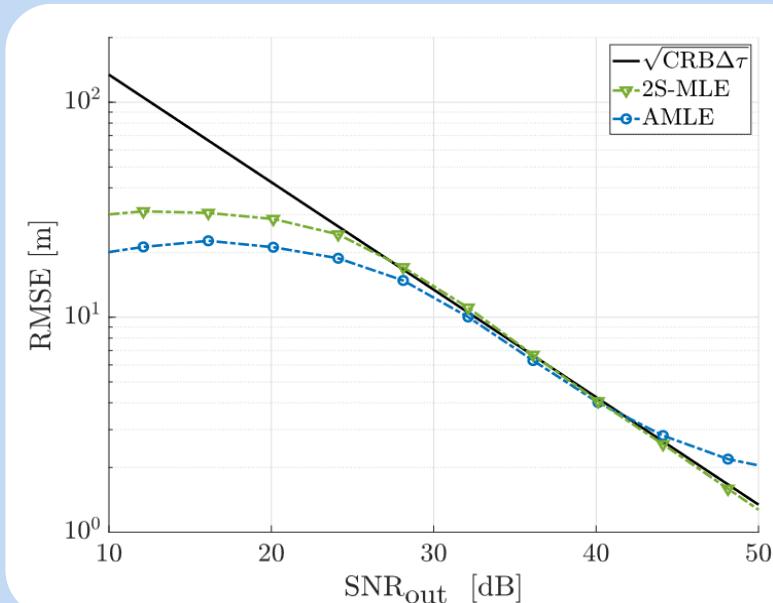
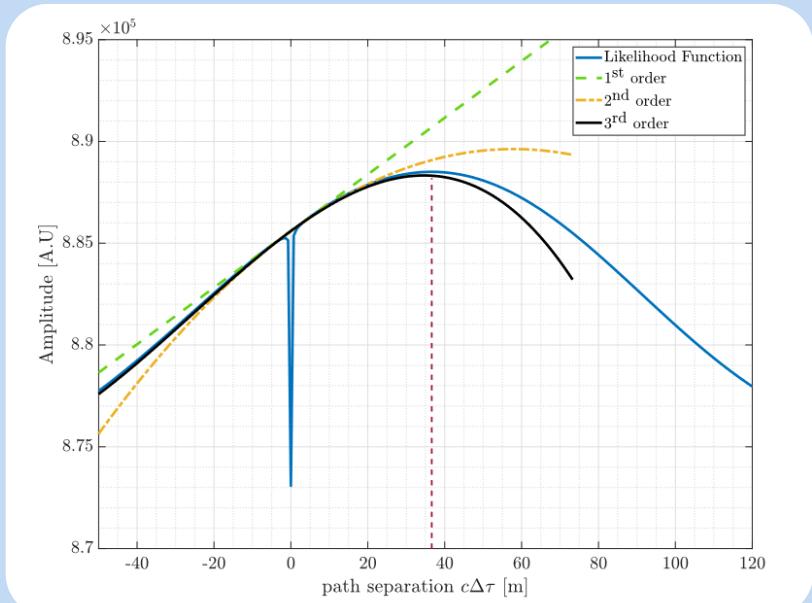


# Back-up: Approximate MLE

- Close-to-ground hypotheses: i)  $b_0 = b_1 = b$ , ii)  $\Delta\tau = \tau_1 - \tau_0$  very small compare to the width of the cross-correlation triangle.
- Dual source maximum likelihood estimation:

$$(\hat{\tau}_0, \hat{\Delta\tau}, \hat{b}) = \min_{\tau_0, \Delta\tau, b} \{L(\tau_0, \Delta\tau, b)\} \text{ and } \hat{\alpha} = (\mathbf{A}^H \mathbf{A})^{-1} \mathbf{A}^H \mathbf{x}.$$

- Third order Taylor approximation:  $L(\tau_0, \Delta\tau, b) = \|\mathbf{P}_{\mathbf{A}} \mathbf{x}\|^2 \approx \sum_n^3 L_n(\tau_0, \Delta\tau, b)$ .

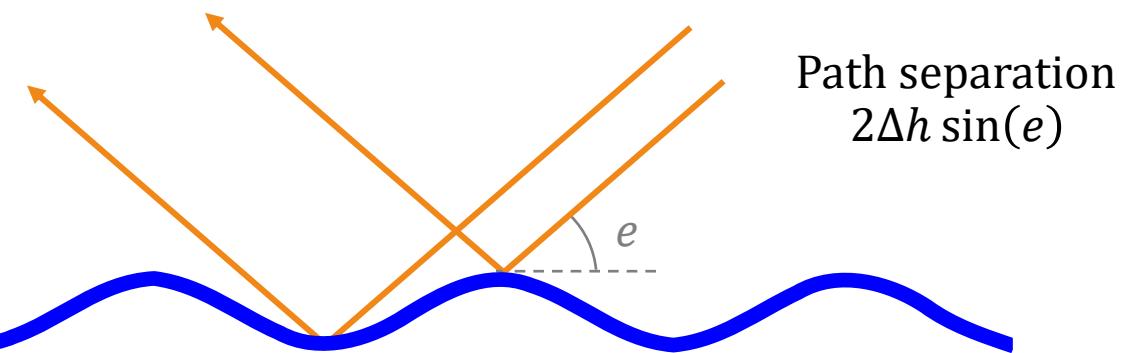




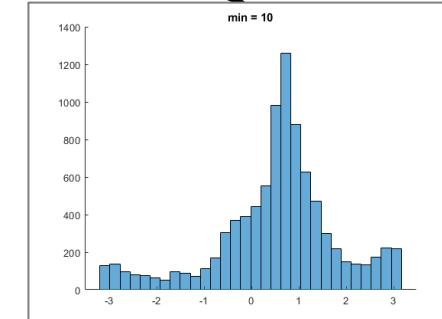
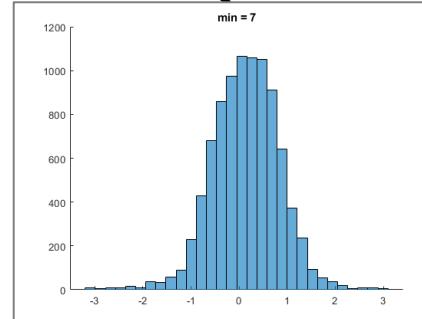
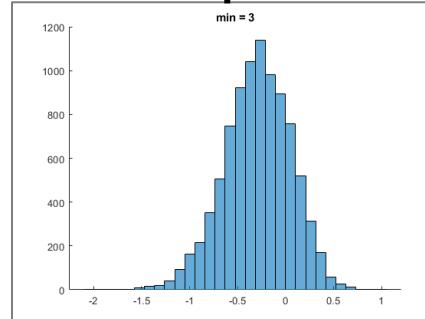
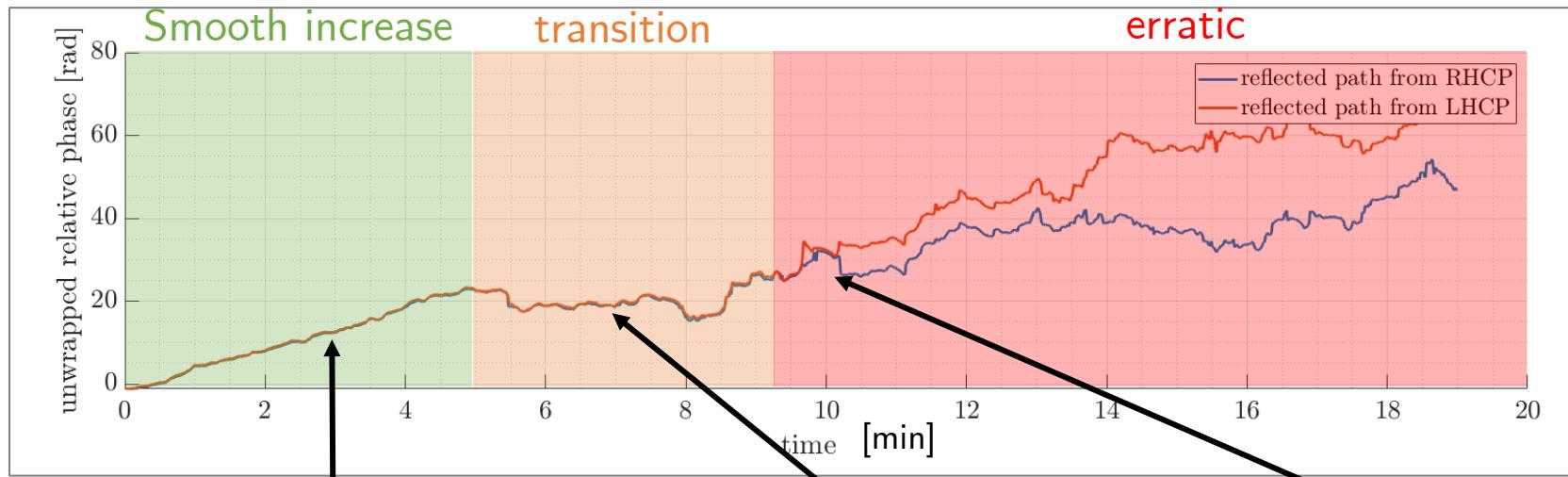
# Back-up: Rayleigh criterion and reflection coherence

Rayleigh Criterion (rough)

$$\Delta h > \frac{\lambda}{8 \sin(e)}$$



Path separation  
 $2\Delta h \sin(e)$





# Back-up: Impulse response detection tests results

- Monte Carlo simulation (2000 runs).
- PD: probability of detecting the correct number of sources.
- $P +$  next procedure:

SNR [dB]	PD	RMSE $_{\tau}$ [m]	$\sqrt{\text{CRB}_{\tau}}$ [m]
20	0.08	9.86	15.55
23	0.46	9.71	11.01
26	0.93	8.34	7.79

- Overshoot-and-decimate procedure:

SNR [dB]	PD	RMSE $_{\tau}$ [m]	$\sqrt{\text{CRB}_{\tau}}$ [m]
20	0.29	17.32	15.55
23	0.57	12.77	11.01
26	0.76	9.04	7.79

