- causal LTI systems and LCCDF
- response of systems with initial Conditions
- system stability and Transfer function
- Relationship & Japlace to CT Fourier Transform
- Inverse Systems,
- Recall from ECE 2714 the CT LCODE

$$\sum_{k=0}^{N} a_k D^k y(t) = \sum_{k=0}^{M} b_k D^k x(t) \qquad M \leq N$$

$$\sum_{k=0}^{N} a_k D^k y(t) = \sum_{k=0}^{M} b_k D^k x(t) + b_k D^k x(t) + \cdots \qquad A^k = \frac{d^k}{dt^k}$$

$$a_0 y(t) + a_1 D^k y(t) + \cdots + a_N D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) = b_0 x(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) + b_1 D^k x(t) + \cdots + a_k D^k y(t) + a_k D^k y(t$$

corresponds to an impulse response h(t).

AND That JEh(+) }= H(s) is transfer function.

- Using the derivative property of Japlace allows us to easily find H(s) without first finding h(t).
- Consider first case of zero-Initial conditions and caosal input x(t), so that y(o')=x(o')=Dy(o')=0x(o')=-··=0.

Then the derivative property is. JED"x(+)}=5"\(\mathbb{Z}(s)\).

This, plus linearity, and some algebra allows us to find the TF H(s).

Example: Dy(t) + ay(t) = bx(t) $a, b \in C$ $J \{D_{y}(t) + a_{y}(t)\} = J \{bx(t)\}$ SY(s) + aY(s) = bX(s) Y(s)(s+a) = bX(s)

- Another example: $D^2y(t) + \alpha Dy(t) + by(t) = c x(t) + d Dx(t)$ $a, b, c, d \in C$

$$(5^2 + as + b)Y(s) = (ds + c)S(s)$$

 $H(s) = Y(s) = ds + c$
 $\overline{S}(s) = \frac{ds + c}{s^2 + as + b}$

- Given an imput x(t) or X(s) (again causal) we can determine output in Japlace domain (s-domain) Y(s) = H(s) X(s) where X(s) = J {x(t)} and using inverse Laplace to get y(t)

Example:
$$D^2y(t) - 16y(t) = x(t)$$
 where $x(t) = e^{-4t}$
Find $y(t)(t \ge 0)$ $x(s) = \frac{1}{s+4}$

$$(s^{2}-16)Y(s)=X(s)=\frac{1}{s+4}$$

$$Y(s)=\frac{1}{(s+4)(s^{2}-16)}=\frac{1}{(s+4)^{2}(s-4)}$$

Then
$$Y(s) = H(s) \times S(s) = H(s) \times S_{\alpha}(s) + H(s) \times S_{\alpha}(s)$$

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The $X_{\alpha} = X_{\alpha} \times X_{\alpha} + X_{\alpha} \times$

For this reason it is combarsome to use Laplace for non-causal inputs even it system itself is causal.

- What if the initial conditions of LCCDE are not zero?

Then NOT a LTI system. However we can still analyze

the system to a

so we have LCCDE Dy + kcy = 0

This is called 240-tupot response. = x(t) = VU(-t)

- Stability.
 - -BIBO stability. Given LTI system with TF HGS)
 the system is stable if the real part of all poles
 of HGS) are in Left-hand side of the complex plane.
 - Example: $D^2y(t) y(t) = x(t)$ $y(0^-) = x(0^-) = 0$ (zero IC)

 Is the system BIBO stable?

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Taking transform
$$-5^24(5)-4(5)=8(5)$$

 $H(5)=\frac{4(5)}{8(5)}=\frac{1}{5-1}$

.. NOT Stable.

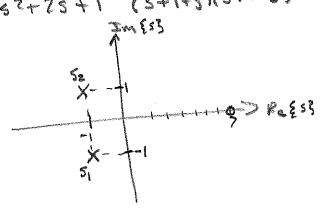
$$5^2 4(5) + 25 4(5) + 1 = -7 \Sigma(5) + 5 \Sigma(5)$$

$$H(s) = \frac{Y(s)}{Z(s)} = \frac{S+7}{s^2+2s+1} = \frac{s-7}{(s+1+3)(s+1-3)}$$

Re & Si3=-1 <0

both poles IN LHP

.. BIBO Stable



Note: Location of pole does not matter (in most but not all cases).

- A more nuanced look at stability.

Remark. I. In practice some care must be taken when cancelly common Factors in P(s) + Q(s) when $H(s) = \frac{P(s)}{Q(s)}$ (Pole-240 cancellation)

why? Suppose $H(s) = (s+h_0)(s+b_1)(s+b_2)\cdots(s+b_m)$ $(s+a_0)(s+a_1)(s+a_2)\cdots(s+a_n)$

AND $b_0 = a_0$ then $H(s) = \frac{(s+b_1)(s+b_2) - \cdots (s+b_m)}{(s+a_1)(s+a_2) - \cdots (s+a_n)}$

If $Re\{b_0\} = Re\{a_0\} > 0$ there is no issue. But if $Re\{b_0\} = Re\{a_0\} < 0$ and $a_0 \approx b_0$ e, g $a_0 = b_0 \pm e$ for $e \approx 0$

Then $\frac{(5+b_0)}{(5+a_0)} \neq 1 = \frac{5+b_0}{(5+b_0+6)}$ which is unstable.

Remark Z. What a bout poles on imaging axis, when Re \si\s = 0

- · If No poles in RIAP and one or more nonrepeated poles on imaginary Axis, system is marginally stable.
- If any poles in RHP or all poles in RHP but there is a repeated noot on imaginary Axis the system is unstable.

- relation ship between TF and Frequent Response.

· Note X(s) = \$\int \text{X(t)} \vec{e}^{st} dt for \(\mathbb{R}_e \vec{e}^{s\vec{s}} > \mathbb{T}. \)

· When we are considuring the TF H(s) and a stable system ROC includes s=jw and

H(s) = H(sw) = Frequency Response & system,

This is often how systems analysis proceeds with non-causal System description - TF => FR => Fourier Analysis, next time we will look at Block Diagrams & CHOUTS.

Inverse Systems, Recall from 2714 that an inverse System 52 of another system 5, is one where when placed In series the input = output

In terms of impulse responses this implies that h(t) = h, (+) * h2(+) = S(+)

Inverse systems are hard to construct in this form, hower taking the Laplace transform we see

This implies that Hz(s) = Hi(s)