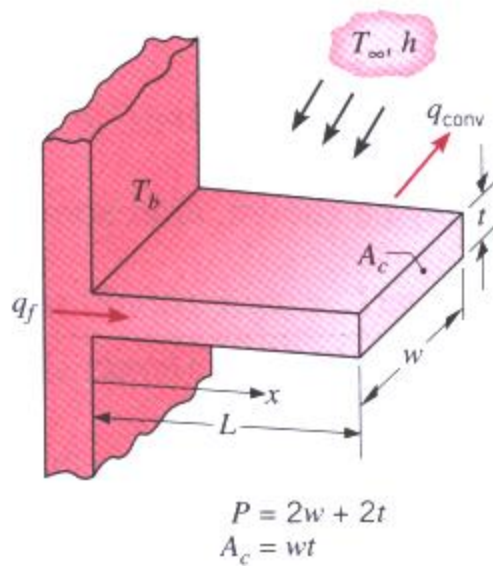


Finite Differences & Matrix Math Example: Temperature Distribution in a Rectangular Fin

Fins are extended surfaces used to enhance heat transfer, like those on an automotive radiator assembly, or on high-power computer chips. Consider the rectangular fin shown in the figure below, described by the geometric dimensions of length L , width w , thickness t , perimeter P , and cross-sectional area A_c ; made of a material with thermal conductivity k ; subjected to convective heat transfer from the surface characterized by a heat transfer coefficient h and ambient temperature T_∞ ; and maintained at a base temperature (at $x=0$) T_b and tip temperature (at $x=L$) of T_L . Following a one-dimensional heat transfer assumption, the temperature distribution in the fin is governed by the following ordinary differential equation (ODE):

$$\frac{d^2 T}{dx^2} - \frac{hP}{kA_c} (T - T_\infty) = 0 \quad (1)$$



Because the fin is subjected to known temperatures at each end, this comprises a **boundary value problem** for solution. To simplify matters, consider the following substitutions:

$$\theta(x) \equiv T(x) - T_\infty, \quad m^2 \equiv \frac{hP}{kA_c} \quad (2)$$

With these in hand, the governing ODE (1) becomes one for $\theta(x)$ instead:

$$\frac{d^2 \theta}{dx^2} - m^2 \theta = 0 \quad (3)$$

The boundary conditions established by T_b and T_L must also be transformed into

values for θ_b and θ_L as well. By appropriate methods, the exact solution to (3) and the specified boundary conditions becomes:

$$\theta(x) = \frac{\theta_L \sinh(mx) + \theta_b \sinh(m(L-x))}{\sinh(mL)} \quad (4)$$

Alternatively, a finite difference approach can be used to **approximate** a solution for $\theta(x)$. Consider setting up a series of N+1 equally-spaced nodal points x_i which span the entire length of the fin from x_0 at $x=0$ to x_N at $x=L$, separated by the distance Δx . At each x_i , (3) can be approximated with a 3-point finite difference equation as (refer to the handout [Survey of Difference Approximations](#) for more details):

$$\frac{\theta(x_{i+1}) - 2\theta(x_i) + \theta(x_{i-1}))}{(\Delta x)^2} - m^2 \cdot \theta(x_i) = 0 \quad (5)$$

Note that the approximation in (5) is **not** applied at x_0 nor x_N , since in this case the values of θ are already known there. Thus, by applying (5) to all $N-1$ **interior** nodes yields $N-1$ linear simultaneous equations in the $N-1$ unknown values of θ .

Consider a rectangular fin with the following conditions:

$$\begin{aligned} L &= 500 \text{ mm} \\ w &= 62 \text{ mm} \\ t &= 4 \text{ mm} \\ h &= 65 \text{ W/m}^2 \cdot \text{K} \\ k &= 35 \text{ W/m} \cdot \text{K} \\ T_\infty &= 20^\circ \text{C} \\ T_b &= 98^\circ \text{C} \\ T_L &= 35^\circ \text{C} \end{aligned}$$

Using the approach outlined above, set up and solve for the approximate temperature distribution $\theta(x)$ with 50 divisions ($N=50$) in x . Compare the results with those given by the exact solution in (4).