

Spacecraft Dynamics + Simulation

* "Dynamics"

$$\dot{x} = f(t, x, u)$$

↑ time ↑ state vector ↑ control inputs vector

- Can get this from e.g. Newton
- Can always write as 1st order vector ODE:

$$F = ma \quad , \quad x = \begin{bmatrix} r \\ v \end{bmatrix} \Rightarrow a = \dot{v}$$

↑ position ↓ velocity

$$\dot{x} = \begin{bmatrix} \dot{r} \\ \dot{v} \end{bmatrix} = \begin{bmatrix} v \\ \frac{1}{m} F \end{bmatrix}$$

* "Simulation"

- Usually we can't solve these ODEs for $x(t)$ analytically:

$$x(t) = x(0) + \underbrace{\int_0^t f(t, x, u) dt}_{\text{this is a nasty integral}}$$

- We use numerical methods to approximate the solution
- Many options, but most common are Runge-Kutta
- These fit a polynomial to $x(t)$ over a (short) time step by evaluating f

- "Order" = order of polynomial
- "Stages" = number of f evals
- Classic 4th-order Runge-Kutta Method ("Runy")

$$\begin{aligned} k_1 &= f(t_n, x_n) \\ k_2 &= f(t_n + \frac{1}{2}\Delta t, x_n + \frac{1}{2}\Delta t \cdot k_1) \\ k_3 &= f(t_n + \frac{1}{2}\Delta t, x_n + \frac{1}{2}\Delta t \cdot k_2) \\ k_4 &= f(t_n + \Delta t, x_n + \Delta t \cdot k_3) \end{aligned} \quad \left. \begin{array}{l} \\ \\ \\ \end{array} \right\} 4 \text{ stages}$$

$$x_{n+1} = x_n + \frac{1}{6}\Delta t(k_1 + 2k_2 + 2k_3 + k_4)$$

- Lots of extensions (e.g. adaptive step size) that you can find in libraries (e.g. ode45 in Matlab)

* Spacecraft Dynamics

- Spacecraft can mostly be modeled as rigid bodies
- Rigid body \Rightarrow ignore flexible dynamics
- For a cubesat:
 - Orbit dynamics $\approx 1/\text{hour}$
 - Attitude dynamics $\approx 1 \text{ Hz}$
 - Flexible dynamics $\approx 1 \text{ kHz}$
- This is less true for larger spacecraft

* Orbit Dynamics

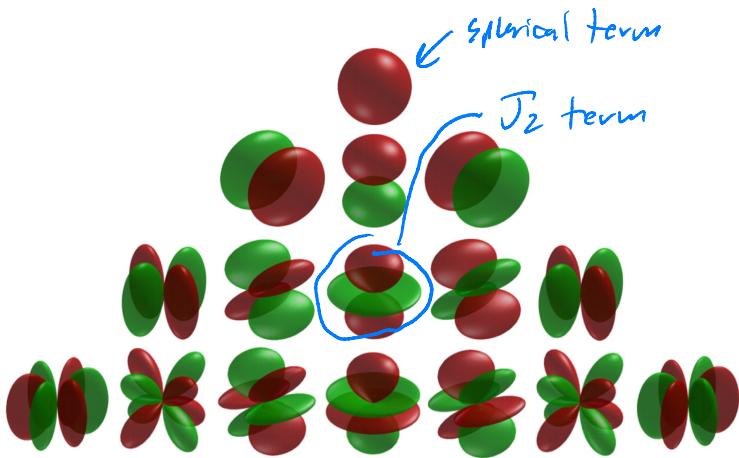
- What forces act on a satellite in LEO?
- Gravity (not just spherical)
- Atmospheric drag
- Solar radiation pressure

- Gravity

$$d_g = \frac{-Mr}{\|r\|^3} + J_2(r)$$

"Spherical term" J_2 "doughnut" term

"Standard gravitational parameter" = GM



- In LEO $\|J_2\| \approx \|F_{drag}\|$. Next term is $\approx 1000\times$ smaller.

- Drag:

$$F_{drag} = -\frac{1}{2} C_D \rho A v \|v\|$$

\downarrow Atm. Density \downarrow velocity vector
 \uparrow Drag coefficient \nwarrow surface area

$C_D \approx 2.2$ for spacecraft in LEO

$\rho \approx 10^{-15} - 10^{-11}$ kg/m³ (use a model like Harris - Priestley)

- Add up all forces to get the dynamics:

$$\begin{bmatrix} \dot{r} \\ \dot{v} \\ \dot{x} \end{bmatrix} = \begin{bmatrix} v \\ \alpha_g(r) + \frac{1}{m} F_{\text{dmg}}(r, v) \end{bmatrix}$$

$\alpha_g(r) + \frac{1}{m} F_{\text{dmg}}(r, v)$

$f(x)$

* Attitude

- What is attitude?
 - Rotation from some body-fixed frame to some inertial frame (e.g. ECI)
 - We can parameterize this many ways
 - Euler angles (roll, pitch, yaw etc.) (bad)
 - Quaternion (4D unit vector) (good)
 - Axis-angle vectors (OKish)
 - Rotation matrices (good)
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* Rotation Matrices:

- Rotates components of a vector from body to inertial frame:

$${}^N X = {}^N Q {}^B X$$

- Rows are n_i basis vectors expressed in B components

$$\begin{bmatrix} {}^N X_1 \\ {}^N X_2 \\ {}^N X_3 \end{bmatrix} = \begin{bmatrix} {}^B n_1^T \\ {}^B n_2^T \\ {}^B n_3^T \end{bmatrix} {}^B X$$

- Columns are b_i basis vectors in N components

$${}^N X = [{}^N b_1 \ {}^N b_2 \ {}^N b_3] \begin{bmatrix} {}^B X_1 \\ {}^B X_2 \\ {}^B X_3 \end{bmatrix}$$

$$\Rightarrow Q Q^T = Q^T Q = I \Rightarrow Q^+ = Q^{-1}$$

$\Rightarrow Q$ is an orthogonal matrix ($Q \in O(3)$)

- $\det(Q) = 1$ called "special"

$$\Rightarrow Q \in SO(3)$$

↳ Rotation Kinematics

- How do we integrate a gyro?

$$\omega(t) \longrightarrow \dot{\tilde{Q}}(t) \longrightarrow Q(t)$$

?

- Velocities in a rotating frame



$${}^N \dot{r} = {}^N Q ({}^B \dot{r} + {}^B \omega \times {}^B r)$$

$${}^B \dot{r} = Q^T {}^N \dot{r} - {}^B \omega \times {}^B r$$

"Kinematic transport theorem"

- Think about a vector fixed in the body frame!

$${}^n\dot{r} = \overset{\circ}{Q} {}^B\dot{r} \Rightarrow {}^n\ddot{r} = \overset{\circ}{Q} {}^B\ddot{r} + \overset{\circ}{Q} \overset{\circ}{\omega} {}^B\dot{r}$$

$$= \overset{\circ}{Q} (\overset{\circ}{\omega} {}^B\dot{r})$$

* Define skew-symmetric "hat" operator

$$\omega \times r = \hat{\omega} r \Rightarrow \hat{\omega} = \begin{bmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix}$$

$$\Rightarrow \boxed{\dot{\overset{\circ}{Q}} = \overset{\circ}{Q} \hat{\omega}}$$

* This a linear 1st order ODE. For constant ω :

$$\overset{\circ}{Q}(t) = \overset{\circ}{Q}_0 e^{t \hat{\omega}}$$

Matrix exponential (expm in matlab)

* We can also define axis-angle vectors:

$$\hat{\phi} = \log(\overset{\circ}{Q}), \quad \phi = r\theta$$

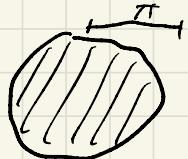
angle in radians
unit vector axis of rotation

Quaternions:

- Naive integration $\dot{\overset{\circ}{Q}} = \overset{\circ}{Q} \hat{\omega}$ will lead to $\overset{\circ}{Q} \notin SO(3)$ due to numerical error
- Projecting back onto $SO(3)$ is a pain (need SVD)
- Quaternions are nicer for simulation

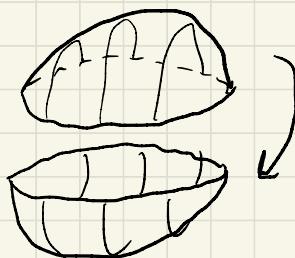
* Geometry:

- Set of all possible axis-angle vectors $-\pi \leq \|\phi\| \leq \pi$
is a ball in \mathbb{R}^3
- Visualize as a disk in \mathbb{R}^2 :



- Discontinuities jump when we cross $\pm\pi$ that causes "Recurrent singularity"
- We want to get rid of the jump:

1) Stretch disk up out of plane into hemisphere:



2) Make a copy

3) Rotate the copy and glue it on underneath
to make a sphere

- Now instead of jumping, we can continue smoothly onto the "Southern Hemisphere"
- There are 2 quaternions for every rotation matrix ("double cover of $SO(3)$ ")

* Useful Quaternion Stuff:

* Points on the unit sphere in 4D are given by:

$$q = \begin{bmatrix} r \sin(\theta/2) \\ \cos(\theta/2) \end{bmatrix}, \quad r = \text{axis (unit vector)} \\ \theta = \text{angle (radians)}$$

$$= \begin{bmatrix} v \\ s \end{bmatrix} \leftarrow \text{"vector part"} \\ \leftarrow \text{"scalar part"}$$

- turns out this is the quaternion exponential

* Identity quaternion

$$q_I = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

* Quaternion "Conjugate" (\sim transpose/inverse)

$$q^+ = \begin{bmatrix} r \sin(-\theta/2) \\ \cos(-\theta/2) \end{bmatrix} = \begin{bmatrix} -v \\ s \end{bmatrix}$$

* Quaternion Multiplication

$$q_1 * q_2 = \begin{bmatrix} v_1 \\ s_1 \end{bmatrix} * \begin{bmatrix} v_2 \\ s_2 \end{bmatrix} = \begin{bmatrix} s_1 v_2 + s_2 v_1 + v_1 \times v_2 \\ s_1 s_2 - v_1 \cdot v_2 \end{bmatrix}$$

$$= \underbrace{\begin{bmatrix} s_1 I + \hat{v}_1 & v_1 \\ v_1^\top & s_1 \end{bmatrix}}_{L(q_1)} \begin{bmatrix} v_2 \\ s_2 \end{bmatrix} = \underbrace{\begin{bmatrix} s_2 I - \hat{v}_2^\top & v_2 \\ -v_2^\top & s_2 \end{bmatrix}}_{R(q_2)} \begin{bmatrix} v_1 \\ s_1 \end{bmatrix}$$

- $L(q^+) = L^T(q), \quad R(q^+) = R^T(q)$

* How to rotate vectors?

$$\begin{bmatrix} \hat{x} \\ 0 \end{bmatrix} = q^* \begin{bmatrix} x \\ 0 \end{bmatrix} * q^+$$

* Quaternions Work just like rotation Matrices:

$$Q_3 = Q_2 Q_1 \Leftrightarrow q_3 = q_2 * q_1$$

$$Q_1 = Q_2^T Q_3 \Leftrightarrow q_1 = q_2^+ * q_3$$

$$\hat{x} = Q \hat{x} Q^T \Leftrightarrow \begin{bmatrix} \hat{x} \\ 0 \end{bmatrix} = q^* \begin{bmatrix} x \\ 0 \end{bmatrix} * q^+$$

* Quaternion Kinematics:

$$\dot{q} = \frac{1}{2} q^* \begin{bmatrix} \omega \\ 0 \end{bmatrix}$$