

**GEORGIA INSTITUTE OF TECHNOLOGY**

**School of Civil & Environmental Engineering**

**CEE 2300 – Environmental Engineering Principles**

**Instructor: S. G. Pavlostathis**

**Spring 2013**

**EXAM 2 – Closed Book & Notes**

**DATE: Wednesday, March 13, 2013**

**TIME: 1:35 to 2:55 PM**

**NAME:** \_\_\_\_\_

**Student ID #:** \_\_\_\_\_

1. \_\_\_\_\_/25

2. \_\_\_\_\_/25

3. \_\_\_\_\_/25

4. \_\_\_\_\_/25

**TOTAL:** \_\_\_\_\_/100

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1. **(25 points)** Briefly define/explain/answer the following:

1-a **(5 pts)** Priority Pollutants

1-b **(5 pts)** Plot the normalized concentration of a pollutant ( $C/C_0$  on the y-axis) versus time ( $t$  on the x-axis) for a batch reactor achieving 80% pollutant destruction in 5 hours assuming that pollutant destruction follows first-order kinetics.

1-c **(5 pts)** First Law of Thermodynamics.

1-d **(5 pts)** Second Law of Thermodynamics.

1-e **(5 pts)** Convective Heat Transfer (give an example)

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- 2. (25 points)** For a continuous-flow, completely mixed reactor (i.e., CSTR), do the following:
- 2-a.** Set up a mass balance equation for a zero-order contaminant removal rate and then solve it for the steady-state detention time ( $\theta$ ).
- 2-b.** For a CSTR system with a flow rate ( $Q$ ) equal to 1,000 m<sup>3</sup>/day, an influent contaminant concentration ( $C_o$ ) equal to 200 mg/L, and a zero-order reaction rate constant ( $k$ ) equal to 20 mg/L · day, calculate the steady-state detention time ( $\theta$ , days) and the reactor volume ( $V$ , m<sup>3</sup>) necessary to achieve a contaminant removal efficiency equal to 90%.

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3. **(25 points)** A homeowner is considering buying a new natural gas furnace. Assume natural gas is 100% methane delivered at 25°C and 1 atm pressure. The methane lower heating value (LHV or net heat of combustion) at 25°C is -802.2 kJ/mol of methane, whereas its higher heating value (HHV or gross heat of combustion) at 25°C is -890.2 kJ/mol of methane. For a typical home in Georgia with an annual gas consumption equivalent to 20,000 kWh and the price of 1 m<sup>3</sup> of natural gas at \$0.26, calculate the annual savings in dollars related to natural gas consumption if the homeowner buys a condensing as opposed to a non-condensing furnace.

Note: 1 kWh = 3,600 kJ

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4. **(25 points)** An uncovered swimming pool loses 1 inch of water off of its 1,000 ft<sup>2</sup> surface per week due to evaporation. The heat of vaporization for water at the pool temperature is 1,050 BTU/lb. The cost of energy to heat the pool is \$10 per million BTU. A salesman claims that a \$500 pool cover that reduces evaporative water losses by two-thirds will pay for itself in one 15-week swimming season. Can it be true?

Note: 1 ft = 12 in; water specific weight = 62.4 lb/ft<sup>3</sup>

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## APPENDIX – USEFULL EQUATIONS & DATA

Atomic weights: H = 1, O = 16, C = 12, N = 14, S = 32, P = 31, Ca = 40, F = 19, Al = 27, Na = 23  
Mg = 24.3

Ideal gas law:  $P V = n R T$   $R = 0.082 \text{ L atm/(mol K)}$

Absolute temperature:  $K = ^\circ\text{C} + 273.15$   
 $^{\circ}\text{R} = ^\circ\text{F} + 459.67$

Henry's law:  $P_{A,g} = k_H [A]$   $P_{A,g}$  = partial pressure of A gas, atm  
 $k_H$  = Henry's law constant, L · atm/mol  
 $[A]$  = aqueous-phase concentration of A, mol/L

Water:  $[H^+][OH^-] = K_w = 10^{-14} \text{ (mol/L)}^2$  @ 298 K

pH:  $\text{pH} = -\log [H^+]$   $[H^+]$  in units of mol/L

Acetic acid:  $\text{AcH} \rightleftharpoons \text{Ac}^- + \text{H}^+$   $\text{pK}_a = 4.7$

Carbonate system (@ 298 K):  $[\text{CO}_2]_{\text{aq}} = K_H P_{\text{CO}_2} P_{\text{total}}$   $K_H = 0.0334 \text{ mol/L} \cdot \text{atm}$   
 $\text{CO}_{2,\text{aq}} + \text{H}_2\text{O} \rightleftharpoons \text{H}^+ + \text{HCO}_3^-$   $K_1 = 4.47 \times 10^{-7} \text{ mol/L}$   
 $\text{HCO}_3^- \rightleftharpoons \text{H}^+ + \text{CO}_3^{2-}$   $K_2 = 4.68 \times 10^{-11} \text{ mol/L}$

Gibbsite (@ 298 K):  $\text{Al}(\text{OH})_3(\text{s}) \rightleftharpoons \text{Al}^{3+} + 3 \text{OH}^-$   $K_{\text{sp}} = 1 \times 10^{-32} \text{ mol}^4/\text{L}^4$

Kinetics (Removal or destruction)

Rate Order	Rate Expression	Batch Reactor	CSTR	PFR
		Time (t)	Detention time ( $\theta$ )	Detention time ( $\theta$ )
Zero	$dC/dt = -k$	$t = (C_o - C_t)/k$	$\theta = (C_o - C_t)/k$	$\theta = (C_o - C_t)/k$
First	$dC/dt = -k C$	$t = (\ln C_o - \ln C_t)/k$	$\theta = [(C_o/C_t) - 1]/k$	$\theta = (\ln C_o - \ln C_t)/k$
Second	$dC/dt = -k C^2$	$t = [(1/C_t) - (1/C_o)]/k$	$\theta = [1/(k C_t)] [(C_o/C_t) - 1]$	$\theta = [(1/C_t) - (1/C_o)]/k$

CSTR–Step Function Response:  $C_t = C_\infty + (C_o - C_\infty) \exp [-(k + \theta^{-1})t]$   
 $k$  = first-order rate constant ( $\text{d}^{-1}$ )  
 $\theta$  = hydraulic retention time (d)

$\Delta H^\circ$  = heat of reaction =  $\sum_{\text{products}} H^\circ - \sum_{\text{reactants}} H^\circ$  where  $H^\circ$  = standard enthalpy at 298 K

Rate of change in stored energy (Heat):  $\Delta H = \dot{m} c \Delta T$   $\dot{m}$  = mass flow rate  
 $c$  = specific heat capacity  
 $\Delta T$  = temperature change

Heat transfer rate:  $q = A (T_2 - T_1)/R$   $q$  = heat transfer rate through a surface (W or BTU/h)  
 $A$  = surface area ( $\text{m}^2$  or  $\text{ft}^2$ )  
 $T_2, T_1$  = high, low temper. on each side of the surface ( $^\circ\text{C}$  or  $^\circ\text{F}$ )  
 $R$  = overall thermal resistance ( $\text{m}^2 \text{ }^\circ\text{C/W}$  or  $\text{ft}^2 \text{ }^\circ\text{F h/BTU}$ )