Forms of the Euler Equations

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1 Conservative Variables to Primitive Variables

We begin with the Euler equations in the conservative form.

$$\frac{\partial \mathbf{U}}{\partial t} + \frac{\partial \mathbf{F}}{\partial x} + \frac{\partial \mathbf{G}}{\partial x} = 0 \tag{1}$$

where

$$\mathbf{U} = \begin{bmatrix} \rho \\ \rho u \\ \rho v \\ \rho E \end{bmatrix}, \quad \mathbf{F} = \begin{bmatrix} \rho u \\ \rho u^2 + p \\ \rho u v \\ \rho u H \end{bmatrix}, \quad \mathbf{G} = \begin{bmatrix} \rho v \\ \rho u v \\ \rho v^2 + p \\ \rho v H \end{bmatrix}$$
(2)

where ρ is the density, u and v are the velocity components in the x and y direction, respectively, and p is the static pressure. The specific energy and enthalpy are given by

$$E = \frac{1}{\gamma - 1} \frac{p}{\rho} + \frac{1}{2} (u^2 + v^2) \tag{3}$$

$$H = \frac{\gamma}{\gamma - 1} \frac{p}{\rho} + \frac{1}{2} (u^2 + v^2). \tag{4}$$

The vector of primitive variables is given by

$$\mathbf{W} = \begin{bmatrix} \rho \\ u \\ v \\ p \end{bmatrix} \tag{5}$$

which is linked with the consistent and conservative variables through the transformations

$$\partial \mathbf{U} = \mathbf{T}^{-1} \partial \mathbf{W} \tag{6}$$

where

$$\mathbf{T}^{-1} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ u & \rho & 0 & 0 \\ v & 0 & \rho & 0 \\ \frac{1}{2} q^2 & \rho u & \rho v & \frac{1}{\gamma - 1} \end{bmatrix}.$$
 (7)

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Its inverse is given by

$$\mathbf{T} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\frac{u}{\rho} & \frac{1}{\rho} & 0 & 0 \\ -\frac{v}{\rho} & 0 & \frac{1}{\rho} & 0 \\ \frac{\gamma - 1}{2} q^2 & u(\gamma - 1) & v(\gamma - 1) & \gamma - 1 \end{bmatrix}.$$
 (8)

Now, we can transform the conservation form into the primitive variable form by multiplying (1) by $\mathbf{T_{uw}}^{-1}$ from the left.

$$\mathbf{T}\frac{\partial \mathbf{U}}{\partial t} + \mathbf{T}\left(\frac{\partial \mathbf{F}}{\partial x} + \frac{\partial \mathbf{G}}{\partial x}\right) = 0 \tag{9}$$

$$\mathbf{T}\frac{\partial \mathbf{U}}{\partial t} + \mathbf{T}\left(\mathbf{A}\frac{\partial \mathbf{U}}{\partial x} + \mathbf{B}\frac{\partial \mathbf{U}}{\partial x}\right) = 0 \tag{10}$$

$$\mathbf{T}\frac{\partial \mathbf{U}}{\partial t} + \mathbf{T}\left(\mathbf{A}\mathbf{T}^{-1}\mathbf{T}\frac{\partial \mathbf{U}}{\partial x} + \mathbf{B}\mathbf{T}^{-1}\mathbf{T}\frac{\partial \mathbf{U}}{\partial x}\right) = 0$$
(11)

$$\frac{\partial \mathbf{W}}{\partial t} + \mathbf{T} \mathbf{A} \mathbf{T}^{-1} \frac{\partial \mathbf{W}}{\partial x} + \mathbf{T} \mathbf{B} \mathbf{T}^{-1} \frac{\partial \mathbf{W}}{\partial x} = 0$$
 (12)

where $\mathbf{A} = \frac{\partial \mathbf{F}}{\partial \mathbf{U}}$, $\mathbf{B} = \frac{\partial \mathbf{G}}{\partial \mathbf{U}}$, and we thus find

$$\mathbf{A_{w}} \equiv \mathbf{T}\mathbf{A}\mathbf{T}^{-1} = \begin{bmatrix} u & \rho & 0 & 0 \\ 0 & u & 0 & \frac{1}{\rho} \\ 0 & 0 & u & 0 \\ 0 & \gamma p & 0 & u \end{bmatrix}$$

$$\mathbf{B_{w}} \equiv \mathbf{T}\mathbf{B}\mathbf{T}^{-1} = \begin{bmatrix} v & 0 & p & 0 \\ 0 & v & 0 & 0 \\ 0 & 0 & v & \frac{1}{\rho} \\ 0 & 0 & v & \frac{1}{\rho} \end{bmatrix}$$
(13)

$$\mathbf{B_{w}} \equiv \mathbf{T}\mathbf{B}\mathbf{T}^{-1} = \begin{bmatrix} v & 0 & p & 0 \\ 0 & v & 0 & 0 \\ 0 & 0 & v & \frac{1}{\rho} \\ 0 & 0 & \gamma p & v \end{bmatrix}$$
(14)

where M = q/a is the Mach number. For simplicity, we write the Euler equations in terms of the natural coordinates: the streamline and its normal.

$$\frac{\partial \mathbf{W}}{\partial t} + \mathbf{A_{ws}} \frac{\partial \mathbf{W}}{\partial s} + \mathbf{B_{wn}} \frac{\partial \mathbf{W}}{\partial n} = 0 \tag{15}$$

where

$$\mathbf{A_{ws}} = \mathbf{A_{w}} \cos\theta + \mathbf{B_{w}} \sin\theta = \begin{bmatrix} q & \frac{\rho u}{q} & \frac{\rho v}{q} & 0\\ 0 & q & 0 & \frac{u}{\rho q}\\ 0 & 0 & q & \frac{v}{\rho q}\\ 0 & \frac{\gamma u p}{q} & \frac{\gamma v p}{q} & q \end{bmatrix}$$

$$\mathbf{B_{wn}} = \mathbf{B_{w}} \cos\theta - \mathbf{A_{w}} \sin\theta = \begin{bmatrix} 0 & -\frac{\rho v}{q} & \frac{\rho u}{q} & 0\\ 0 & 0 & 0 & -\frac{v}{\rho q}\\ 0 & 0 & 0 & \frac{u}{\rho q}\\ 0 & -\frac{\gamma v p}{q} & \frac{\gamma u p}{q} & 0 \end{bmatrix}.$$

$$(16)$$

$$\mathbf{B_{wn}} = \mathbf{B_{w}} \cos\theta - \mathbf{A_{w}} \sin\theta = \begin{bmatrix} 0 & -\frac{\rho}{q} & \frac{\rho}{q} & 0\\ 0 & 0 & 0 & -\frac{v}{\rho q}\\ 0 & 0 & 0 & \frac{u}{\rho q}\\ 0 & -\frac{\gamma vp}{q} & \frac{\gamma up}{q} & 0 \end{bmatrix}.$$
(17)

2 Symmetrizing Variables

The vector of the symmetrizing variables is

$$\partial \mathbf{U_m} = \begin{bmatrix} \frac{\partial p}{\rho a} \\ \partial q \\ q \partial \theta \\ \partial s \end{bmatrix}$$
 (18)

which is linked with the primitive variables through the transformations

$$\partial \mathbf{U_m} = \mathbf{T_m} \partial \mathbf{W} \tag{19}$$

where

$$\mathbf{T_m} = \begin{bmatrix} 0 & 0 & 0 & \frac{1}{\rho a} \\ 0 & \frac{u}{q} & \frac{v}{q} & 0 \\ 0 & -\frac{v}{q} & \frac{u}{q} & 0 \\ -a^2 & 0 & 0 & 1 \end{bmatrix}.$$
 (20)

Its inverse is

$$\mathbf{T_{m}}^{-1} = \begin{bmatrix} \frac{\rho}{a} & 0 & 0 & -\frac{1}{a^{2}} \\ 0 & \frac{u}{q} & -\frac{v}{q} & 0 \\ 0 & \frac{v}{q} & \frac{u}{q} & 0 \\ \rho a & 0 & 0 & 0 \end{bmatrix}.$$
 (21)

Now, we can transform the conservation form into the primitive variable form by multiplying (1) by T_m from the left.

$$\mathbf{T_m} \frac{\partial \mathbf{W}}{\partial t} + \mathbf{T_m} \left(\mathbf{A_{ws}} \frac{\partial \mathbf{W}}{\partial s} + \mathbf{B_{wn}} \frac{\partial \mathbf{W}}{\partial n} \right) = 0$$
 (22)

$$\mathbf{T_{m}} \frac{\partial \mathbf{W}}{\partial t} + \mathbf{T_{m}} \left(\mathbf{A_{ws}} \mathbf{T_{m}}^{-1} \mathbf{T_{m}} \frac{\partial \mathbf{W}}{\partial s} + \mathbf{B_{wn}} \mathbf{T_{m}}^{-1} \mathbf{T_{m}} \frac{\partial \mathbf{W}}{\partial n} \right) = 0$$
 (23)

$$\frac{\partial \mathbf{U_m}}{\partial t} + \mathbf{T_m} \mathbf{A_{ws}} \mathbf{T_m}^{-1} \frac{\partial \mathbf{U_m}}{\partial s} + \mathbf{T_m} \mathbf{B_{wn}} \mathbf{T_m}^{-1} \frac{\partial \mathbf{U_m}}{\partial n} = 0$$
 (24)

where

$$\mathbf{A_{ms}} = \mathbf{T_{m}} \mathbf{A_{ws}} \mathbf{T_{m}}^{-1} = \begin{bmatrix} q & a & 0 & 0 \\ a & q & 0 & 0 \\ 0 & 0 & q & 0 \\ 0 & 0 & 0 & q \end{bmatrix}$$
(25)

$$\mathbf{B_{mn}} = \mathbf{T_m} \mathbf{B_{wn}} \mathbf{T_m}^{-1} = \begin{bmatrix} 0 & 0 & a & 0 \\ 0 & 0 & 0 & 0 \\ a & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}.$$
 (26)

In Cartesian coordinates, we obtain

$$\mathbf{T_{m}} \frac{\partial \mathbf{W}}{\partial t} + \mathbf{T_{m}} \left(\mathbf{A_{w}} \frac{\partial \mathbf{W}}{\partial x} + \mathbf{B_{w}} \frac{\partial \mathbf{W}}{\partial y} \right) = 0$$
 (27)

$$\mathbf{T_{m}} \frac{\partial \mathbf{W}}{\partial t} + \mathbf{T_{m}} \left(\mathbf{A_{w}} \mathbf{T_{m}}^{-1} \mathbf{T_{m}} \frac{\partial \mathbf{W}}{\partial x} + \mathbf{B_{w}} \mathbf{T_{m}}^{-1} \mathbf{T_{m}} \frac{\partial \mathbf{W}}{\partial y} \right) = 0$$
 (28)

$$\frac{\partial \mathbf{U_m}}{\partial t} + \mathbf{T_m} \mathbf{A_w} \mathbf{T_m}^{-1} \frac{\partial \mathbf{U_m}}{\partial x} + \mathbf{T_m} \mathbf{B_w} \mathbf{T_m}^{-1} \frac{\partial \mathbf{U_m}}{\partial y} = 0$$
 (29)

where

$$\mathbf{A_{m}} = \mathbf{T_{m}} \mathbf{A_{w}} \mathbf{T_{m}}^{-1} = \begin{bmatrix} u & u/M & -v/M & 0 \\ u/M & u & 0 & 0 \\ -v/M & 0 & u & 0 \\ 0 & 0 & 0 & u \end{bmatrix}$$

$$\mathbf{B_{m}} = \mathbf{T_{m}} \mathbf{B_{w}} \mathbf{T_{m}}^{-1} = \begin{bmatrix} v & v/M & u/M & 0 \\ v/M & v & 0 & 0 \\ u/M & 0 & v & 0 \\ 0 & 0 & 0 & v \end{bmatrix} .$$
(30)

$$\mathbf{B_{m}} = \mathbf{T_{m}} \mathbf{B_{w}} \mathbf{T_{m}}^{-1} = \begin{bmatrix} v & v/M & u/M & 0 \\ v/M & v & 0 & 0 \\ u/M & 0 & v & 0 \\ 0 & 0 & 0 & v \end{bmatrix}.$$
(31)

3 Another Symmetrizing Variables

The state vector

$$\partial \mathbf{U_c} = \begin{bmatrix} \frac{\partial p}{\rho a} \\ \partial u \\ \partial v \\ \partial s \end{bmatrix}$$
 (32)

also symmetrizes the Euler equations. The transformation matrix is given by

$$\mathbf{T_c} = \begin{bmatrix} 0 & 0 & 0 & \frac{1}{\rho a} \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ -a^2 & 0 & 0 & 1 \end{bmatrix}. \tag{33}$$

where

$$\partial \mathbf{U_c} = \mathbf{T_c} \partial \mathbf{W} \tag{34}$$

Its inverse is

$$\mathbf{T_c}^{-1} = \begin{bmatrix} \frac{\rho}{a} & 0 & 0 & -\frac{1}{a^2} \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ \rho a & 0 & 0 & 0 \end{bmatrix}.$$
 (35)

Now, we can transform the primitive form into the primitive variable form by multiplying (1) by $\mathbf{T_c}$ from the left.

$$\mathbf{T_c} \frac{\partial \mathbf{W}}{\partial t} + \mathbf{T_c} \left(\mathbf{A_{ws}} \frac{\partial \mathbf{W}}{\partial s} + \mathbf{B_{wn}} \frac{\partial \mathbf{W}}{\partial n} \right) = 0$$
 (36)

$$\mathbf{T_c} \frac{\partial \mathbf{W}}{\partial t} + \mathbf{T_c} \left(\mathbf{A_{ws}} \mathbf{T_c}^{-1} \mathbf{T_c} \frac{\partial \mathbf{W}}{\partial s} + \mathbf{B_{wn}} \mathbf{T_c}^{-1} \mathbf{T_c} \frac{\partial \mathbf{W}}{\partial n} \right) = 0$$
 (37)

$$\frac{\partial \mathbf{U_c}}{\partial t} + \mathbf{T_c} \mathbf{A_{ws}} \mathbf{T_c}^{-1} \frac{\partial \mathbf{U_c}}{\partial s} + \mathbf{T_c} \mathbf{B_{wn}} \mathbf{T_c}^{-1} \frac{\partial \mathbf{U_c}}{\partial n} = 0$$
 (38)

where

$$\mathbf{A_{cs}} = \mathbf{T_{c}} \mathbf{A_{ws}} \mathbf{T_{c}}^{-1} = \begin{bmatrix} q & u/M & v/M & 0 \\ u/M & q & 0 & 0 \\ v/M & 0 & q & 0 \\ 0 & 0 & 0 & q \end{bmatrix}$$
(39)

$$\mathbf{B_{cn}} = \mathbf{T_c} \mathbf{B_{wn}} \mathbf{T_c}^{-1} = \begin{bmatrix} 0 & -v/M & u/M & 0 \\ -v/M & 0 & 0 & 0 \\ u/M & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}.$$
(40)

Similarly, in Cartesian coordinates, we obtain

$$\mathbf{T_c} \frac{\partial \mathbf{W}}{\partial t} + \mathbf{T_c} \left(\mathbf{A_w} \frac{\partial \mathbf{W}}{\partial x} + \mathbf{B_w} \frac{\partial \mathbf{W}}{\partial y} \right) = 0$$
 (41)

$$\mathbf{T_c} \frac{\partial \mathbf{W}}{\partial t} + \mathbf{T_c} \left(\mathbf{A_w} \mathbf{T_c}^{-1} \mathbf{T_c} \frac{\partial \mathbf{W}}{\partial x} + \mathbf{B_w} \mathbf{T_c}^{-1} \mathbf{T_c} \frac{\partial \mathbf{W}}{\partial y} \right) = 0$$
 (42)

$$\frac{\partial \mathbf{U_c}}{\partial t} + \mathbf{T_c} \mathbf{A_w} \mathbf{T_c}^{-1} \frac{\partial \mathbf{U_c}}{\partial x} + \mathbf{T_c} \mathbf{B_w} \mathbf{T_c}^{-1} \frac{\partial \mathbf{U_c}}{\partial y} = 0$$
 (43)

where

$$\mathbf{A_{c}} = \mathbf{T_{c}} \mathbf{A_{w}} \mathbf{T_{c}}^{-1} = \begin{bmatrix} u & a & 0 & 0 \\ a & u & 0 & 0 \\ 0 & 0 & u & 0 \\ 0 & 0 & 0 & u \end{bmatrix}$$

$$\mathbf{B_{c}} = \mathbf{T_{c}} \mathbf{B_{w}} \mathbf{T_{c}}^{-1} = \begin{bmatrix} v & 0 & a & 0 \\ 0 & v & 0 & 0 \\ a & 0 & v & 0 \\ 0 & 0 & 0 & v \end{bmatrix}.$$

$$(44)$$

$$\mathbf{B_c} = \mathbf{T_c} \mathbf{B_w} \mathbf{T_c}^{-1} = \begin{bmatrix} v & 0 & a & 0 \\ 0 & v & 0 & 0 \\ a & 0 & v & 0 \\ 0 & 0 & 0 & v \end{bmatrix}.$$
 (45)

Dimensionally Consistent Variables 4

The state vector

$$\partial \mathbf{U_p} = \begin{bmatrix} \partial p \\ \rho q \partial q \\ \rho q^2 \partial \theta \\ \partial s \end{bmatrix}$$

$$\tag{46}$$

also symmetrizes the Euler equations. The transformation matrix is given by

$$\mathbf{T}_{\mathbf{p}} = \begin{bmatrix} 0 & 0 & 0 & 1\\ 0 & \rho u & \rho v & 0\\ 0 & -\rho v & \rho u & 0\\ -a^2 & 0 & 0 & 1 \end{bmatrix}. \tag{47}$$

where

$$\partial \mathbf{U_p} = \mathbf{T_p} \partial \mathbf{W} \tag{48}$$

Its inverse is

$$\mathbf{T}_{\mathbf{p}}^{-1} = \begin{bmatrix} \frac{1}{a^2} & 0 & 0 & -\frac{\rho}{a^2} \\ 0 & \frac{u}{\rho q^2} & -\frac{v}{\rho q^2} & 0 \\ 0 & \frac{v}{\rho q^2} & \frac{u}{\rho q^2} & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}. \tag{49}$$

Now, we can transform the primitive form into the primitive variable form by multiplying (1) by $\mathbf{T_c}$ from the left.

$$\frac{\partial \mathbf{U_p}}{\partial t} + \mathbf{T_p} \mathbf{A_{ws}} \mathbf{T_p}^{-1} \frac{\partial \mathbf{U_p}}{\partial s} + \mathbf{T_p} \mathbf{B_{wn}} \mathbf{T_p}^{-1} \frac{\partial \mathbf{U_p}}{\partial n} = 0$$
 (50)

where

$$\mathbf{A_{ps}} = \mathbf{T_{p}} \mathbf{A_{ws}} \mathbf{T_{p}}^{-1} = \begin{bmatrix} q & a^{2}/q & 0 & 0 \\ q & q & 0 & 0 \\ 0 & 0 & q & 0 \\ 0 & 0 & 0 & q \end{bmatrix}$$

$$\mathbf{B_{pn}} = \mathbf{T_{p}} \mathbf{B_{wn}} \mathbf{T_{p}}^{-1} = \begin{bmatrix} 0 & 0 & a^{2}/q & 0 \\ 0 & 0 & 0 & 0 \\ q & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}.$$
(51)

$$\mathbf{B_{pn}} = \mathbf{T_p} \mathbf{B_{wn}} \mathbf{T_p}^{-1} = \begin{bmatrix} 0 & 0 & a^2/q & 0 \\ 0 & 0 & 0 & 0 \\ q & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}.$$
 (52)

Similarly, in Cartesian coordinates, we obtain

$$\mathbf{A_{p}} = \mathbf{T_{p}} \mathbf{A_{w}} \mathbf{T_{p}}^{-1} = \begin{bmatrix} u & u/M^{2} & -v/M^{2} & 0 \\ u & u & 0 & 0 \\ -v & 0 & u & 0 \\ 0 & 0 & 0 & u \end{bmatrix}$$

$$\mathbf{B_{p}} = \mathbf{T_{p}} \mathbf{B_{w}} \mathbf{T_{p}}^{-1} = \begin{bmatrix} v & v/M^{2} & u/M^{2} & 0 \\ v & v & 0 & 0 \\ u & 0 & v & 0 \\ 0 & 0 & 0 & v \end{bmatrix} .$$
(53)

$$\mathbf{B}_{\mathbf{p}} = \mathbf{T}_{\mathbf{p}} \mathbf{B}_{\mathbf{w}} \mathbf{T}_{\mathbf{p}}^{-1} = \begin{bmatrix} v & v/M^2 & u/M^2 & 0 \\ v & v & 0 & 0 \\ u & 0 & v & 0 \\ 0 & 0 & 0 & v \end{bmatrix}.$$
 (54)

References

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- [2] NISHIKAWA, H., RAD, M., ROE, P. L., Grids and Solutions from Residual Minimization, ICCFD Proceedings, Kyoto. Springer-Verlag, 2000.