

Electrical Engineering

HW 6– Chapter 7 Solution

<1>

(a) The power factor is

$$pf = \cos \theta = \frac{P}{V_{rms} I_{rms}} = \frac{800}{12 \times 120} = 0.56$$

(b) The phase angle θ is

$$\theta = \arccos(0.56) = 56.25^\circ$$

(c) The impedance Z is

$$Z = |Z| \angle \theta = \frac{\mathbf{V}}{\mathbf{I}} = \frac{120 \angle 0^\circ}{12 \angle -56.25^\circ} = 10 \angle 56.25^\circ = 5.56 + j8.31 \quad \Omega$$

(d) Obviously, the resistance is 5.56Ω

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$$a) \quad P = \frac{650}{\sqrt{2}} \times \frac{20}{\sqrt{2}} \times \cos(10^\circ) = 6401.25 \text{ W}$$

$$Q = \frac{650}{\sqrt{2}} \times \frac{20}{\sqrt{2}} \times \sin(10^\circ) = 1128.7 \text{ VAR} \quad S = \frac{650}{\sqrt{2}} \times \frac{20}{\sqrt{2}} \angle 10^\circ = 6500 \angle 10^\circ \text{ VA}$$

b) Use the same calculation as shown above, we can have

$$P = 4599.3 \text{ W} \quad Q = 4599.3 \text{ VAR} \quad S = 6504.4 \angle 45^\circ \text{ VA}$$

$$c) \quad P = 60 \text{ W} \quad Q = 857.91 \text{ VAR} \quad S = 860 \angle 86^\circ \text{ VA}$$

$$d) \quad P = 401.22 \text{ W} \quad Q = 260.56 \text{ VAR} \quad S = 478.4 \angle 33^\circ \text{ VA}$$

<3>

$$(a) \quad jX_L = j\omega L = j377 \times 25.55 \times 10^{-3} = j9.63 \quad \Omega$$

$$jX_C = \frac{1}{j\omega C} = \frac{1}{j377 \times 265 \times 10^{-6}} = -j10.01 \, \Omega$$

$$jX_L || jX_C = j255.64 \, \Omega$$

The equivalent impedance Z is

$$Z = jX_L || jX_C + R = 10 + j255.64 = 255.83 \angle 87.76^\circ$$

The current in the circuit is

$$I = \frac{V_S}{Z} = \frac{120 \angle 0^\circ}{255.5 \angle 87.8^\circ} = 0.47 \angle -87.76^\circ$$

The real power P is

$$P = I^2 R = 0.47^2 \times 10 = 2.20 \, \text{W}$$

The reactive power Q is

$$Q = I^2 X = 0.47^2 \times 255.64 = 56.24 \, \text{VAR}$$

$$(b) \quad jX_L = j\omega L = j314 \times 25.55 \times 10^{-3} = j8.02 \, \Omega$$

$$jX_C = \frac{1}{j\omega C} = \frac{1}{j314 \times 265 \times 10^{-6}} = -j12.02 \, \Omega$$

$$jX_L || jX_C = j24.13 \, \Omega$$

The equivalent impedance Z is

$$Z = jX_L || jX_C + R = 10 + j24.13 = 26.12 \angle 67.49^\circ$$

The current in the circuit is

$$I = \frac{V_S}{Z} = \frac{120 \angle 0^\circ}{26 \angle 67.38^\circ} = 4.59 \angle -67.49^\circ$$

The real power P is

$$P = I^2 R = 4.59^2 \times 10 = 211.01 \, \text{W}$$

The reactive power Q is

$$Q = I^2 X = 4.59^2 \times 24.13 = 509.25 \, \text{VAR}$$

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The current is

$$I = \frac{120}{12 + j377 \times 20 \times 10^{-3}} = \frac{120}{14.17 \angle 32.14^\circ} = 8.47 \angle -32.14^\circ \text{ A}$$

(a) The average power dissipated in the load is $P_{av} = I^2 R = 8.47^2 \times 10 = 717.4 \text{ W}$

(b) The power factor of the motor is $pf = \cos 32.14^\circ = 0.847$ lagging

(c) $\theta = \cos^{-1} 0.9 = 25.84^\circ$

$$S_{NEW} \angle 25.84^\circ = 717.4 \text{ W} + j(Q_L - Q_C) \quad S_{NEW} = 797.1 \quad Q_{NEW} = 347.4$$

$$Q_L = 450.7 \text{ VAR} \quad Q_C = 103.3 \text{ VAR}$$

$$Q_C = \frac{V^2}{X_C} = \frac{120^2}{X_C} = 103.3$$

$$X_C = 139.4 \text{ } \Omega \quad C = \frac{1}{\omega X_C} = 19 \mu\text{F}$$

<5>

$$\text{a) } \omega = 5, Z_T = R \parallel Z_{L2} + Z_C + Z_{L1} = 4 + j5 \Omega, \tilde{I} = \frac{15}{\sqrt{2} \cdot 4} = 2.6517 \text{ A}$$

$$P = \tilde{I}^2 R = 28.12 \text{ W}, Q = \tilde{I}^2 X = 35.15 \text{ VAR}$$

$$\text{b) } \omega = 15, Z_T = R \parallel Z_{L2} + Z_C + Z_{L1} = 60 + j44.33 \Omega, \tilde{I} = \frac{15}{\sqrt{2} \cdot 60} = 0.1768 \text{ A}$$

$$P = \tilde{I}^2 R = 1.8755 \text{ W}, Q = \tilde{I}^2 X = 1.3857 \text{ VAR}$$

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First, we compute the load impedance:

$$Z_L = (R + jX_L) \parallel jX_C = 0.38 - j8.88$$

Then, we compute the load current

$$\tilde{I}_L = \frac{\tilde{V}_L}{Z_L} = 0.4 + j10.1 \text{ A}$$

and the complex power:

$$S = \tilde{V}_L \cdot \tilde{I}_L^* = 36 - j909 \text{ W}$$

Therefore

$$P_{av} = 36W$$

$$Q = -909VAR$$

For computing the reactance needed for the power factor correction, we compute the complex power without capacitor. First, we compute the load impedance:

$$Z_L = (R + jX_L) = 25 + j70$$

Then, we compute the load current

$$\tilde{I}_L = \frac{\tilde{V}_L}{Z_L} = 0.4 - j1.14 \text{ A}$$

and the complex power:

$$S = \tilde{V}_L \cdot \tilde{I}_L^* = 36.64 + j102.63 \text{ W}$$

Therefore

$$Q = 102.63VAR$$

So, we need to contribute a negative reactive power equal to -102.63. This requires a negative reactance and then a capacitor with $Q_C = -102.63VAR$

$$X_C = \frac{|\tilde{V}_L|^2}{Q_C} = -\frac{90^2}{-102.63} = -78.92\Omega$$

$$C = -\frac{1}{\omega X_C} = 3.36 \cdot 10^{-5} F$$

<7>

(a) The equivalent resistance seen by the voltage source:

To find the equivalent resistance seen by the voltage source, use equation 7.32:

$$Z_1 = \frac{1}{N^2} Z_2$$

In this case, the load impedance, Z_2 , is the output resistance R_O , which has the impedance:

$$Z_2 = R_O = 12 \Omega = 12\angle 0$$

Plug Z_2 into equation 7.32:

$$Z_1 = \frac{1}{5^2} * 12\angle 0$$

$$= 0.48\angle 0 \Omega$$

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| Final answer: $Z_1 = 0.48\angle 0 \Omega$ |
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(b) The power P_{source} supplied by the voltage source:

From equation 7.31, we know that ideal transformers conserve power. Therefore:

$$S_1 = S_2$$

Using this property, we may solve for the source power by computing the real power at the primary terminal using equation 7.12:

$$P_{source} = P_{avg} = \frac{\tilde{V}^2}{|Z|} \cos(\theta_Z)$$

where $\tilde{V} = \tilde{V}_g$ and $Z = Z_S + Z_1$. Plug these values into equation 7.12:

$$\begin{aligned} P_{source} &= \frac{80}{(0.48 + 2)} * \cos(0) \\ &= 168.67 \text{ W} \end{aligned}$$

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| Final answer: $P_{source} = 168.67 \text{ W}$ |
|---|

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$$R_{Seq} = R_0$$

Assume R_{Seq} is load impedance seen by the source and $R_{Seq} = n^2 R_0$

For maximum power delivery $R_{Seq} = R_{in}$

$$n = \sqrt{\frac{R_{in}}{R_0}} = \sqrt{12} = 3.46$$

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$$\begin{aligned}\tilde{\mathbf{I}}_n &= \tilde{\mathbf{I}}_{an} + \tilde{\mathbf{I}}_{bn} + \tilde{\mathbf{I}}_{cn} = 22\angle 0^\circ + 10\angle 120^\circ + 15\angle 45^\circ = 22 + 5 + j8.66 + 10.6 + 10.6j = \\ &= 37.6 + j19.26 = 42.24\angle 27.12^\circ \text{ A}\end{aligned}$$

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Current in each wire:

Note that the phase voltages of the wye network are balanced by equations 7.49 and 7.47. Therefore:

$$\tilde{\mathbf{V}}_{an} = \tilde{\mathbf{V}}_R = 110\angle 0^\circ \text{ V rms}$$

$$\tilde{\mathbf{V}}_{bn} = \tilde{\mathbf{V}}_B = 110\angle 4\pi/3 \text{ V rms}$$

$$\tilde{\mathbf{V}}_{cn} = \tilde{\mathbf{V}}_W = 110\angle 2\pi/3 \text{ V rms}$$

However, the wye load configuration is not balanced, so the current in the neutral line will be non-zero. Refer to Figure 7.49 for a simplified representation of the circuit. Using KCL, we can write the neutral line current as:

$$\tilde{\mathbf{I}}_N = \tilde{\mathbf{I}}_R + \tilde{\mathbf{I}}_W + \tilde{\mathbf{I}}_B$$

Now, calculate each of these currents using superposition:

$$\tilde{\mathbf{I}}_R = \frac{\tilde{\mathbf{V}}_{an}}{\mathbf{Z}_a}$$

where \mathbf{Z}_a is R . Plug in known values:

$$\begin{aligned}\tilde{\mathbf{I}}_R &= \frac{110\angle 0}{50\angle 0} \\ &= 2\text{ A}\end{aligned}$$

Solve for $\tilde{\mathbf{I}}_B$:

$$\begin{aligned}\tilde{\mathbf{I}}_B &= \frac{\tilde{\mathbf{V}}_{bn}}{\mathbf{Z}_b} \\ &= \frac{110\angle 4\pi/3}{45.24\angle \pi/2} \\ &= 2.43\angle \frac{5\pi}{6} \\ &= -2.10 + j1.22\text{ A}\end{aligned}$$

Solve for $\tilde{\mathbf{I}}_W$:

$$\begin{aligned}
 \tilde{I}_W &= \frac{\tilde{V}_{cn}}{Z_c} \\
 &= \frac{110 \angle 2\pi/3}{19.94 \angle (-\pi/2)} \\
 &= 5.52 \angle 7\pi/6 \\
 &= -4.78 - j2.76 \text{ A}
 \end{aligned}$$

Add up the components to solve to the neutral line current:

$$\begin{aligned}
 \tilde{I}_N &= 2 - 2.10 + j1.22 - 4.78 - j2.76 \\
 &= -4.88 - j1.54 \text{ A}
 \end{aligned}$$

Final answer: $\tilde{I}_R = 2 \text{ A}$, $\tilde{I}_B = -2.10 + j1.22 \text{ A}$, $\tilde{I}_W = -4.78 - j2.76 \text{ A}$, $\tilde{I}_N = -4.88 - j1.54 \text{ A}$

Real power:

The real power consumed will be the power in branch R , because it is the only branch with a real load. Furthermore, the voltage and load in this branch have only real components. Therefore, the real power is:

$$\begin{aligned}
 P &= 110 * 2 \\
 &= 220 \text{ W}
 \end{aligned}$$

Final answer: $P = 220 \text{ W}$