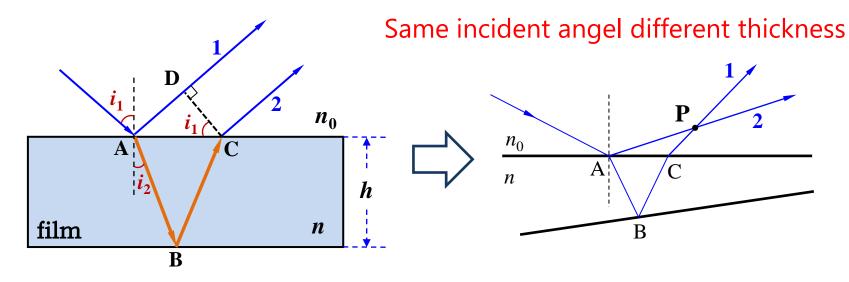
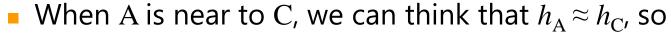


For a film with unequal thickness, the reflected (or refracted) light will interfere near the surface. The OPL difference is determined mainly by the thickness and is called equal thickness interference.



$$\Delta = 2h\sqrt{n^2 - n_0^2 \sin^2 i_1} + \frac{\lambda}{2}$$
 Deter

Determined by h

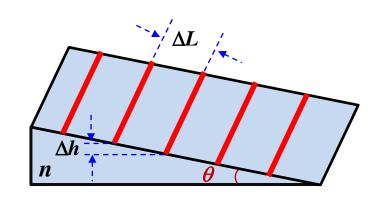


$$\Delta = 2nh\cos i_2 + \frac{\lambda}{2}$$

When is normally incident:

$$i_1 \approx i_2 \approx 0$$

$$\Delta \approx 2nh + \frac{\lambda}{2}$$



*m*<sup>th</sup> order bright fringes

$$2nh_m + \frac{\lambda}{2} = m\lambda$$
  $\Longrightarrow$   $h_m = (m-1/2)\frac{\lambda}{2n} = \text{Const}$ 

The trajectory equation is a straight line parallel to the edge



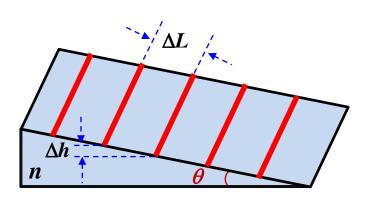
$$h_{m} = (m-1/2)\frac{\lambda}{2n}$$

$$h_{m+1} = (m+1-1/2)\frac{\lambda}{2n}$$

$$\implies \Delta h = \frac{\lambda}{2n}$$

Fringes spacing

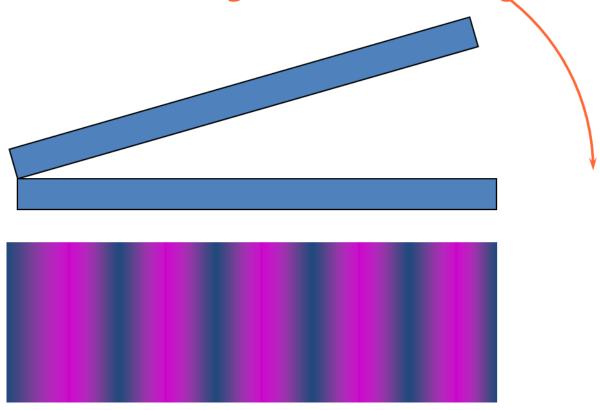
$$\Delta L = \frac{\Delta h}{\tan \theta} \approx \frac{\Delta h}{\theta} = \frac{\lambda}{2n\theta}$$

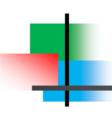


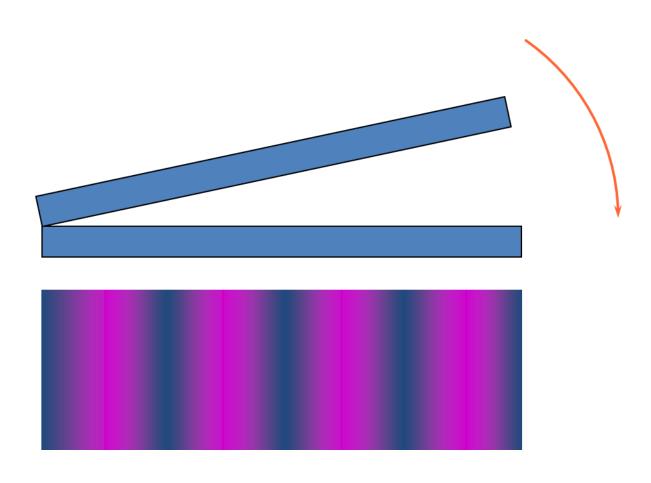
- The change in the density (spacing) of the fringes reflects the change in the wedge angle.
- It can be used to measure changes in small angles.

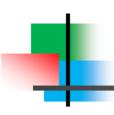


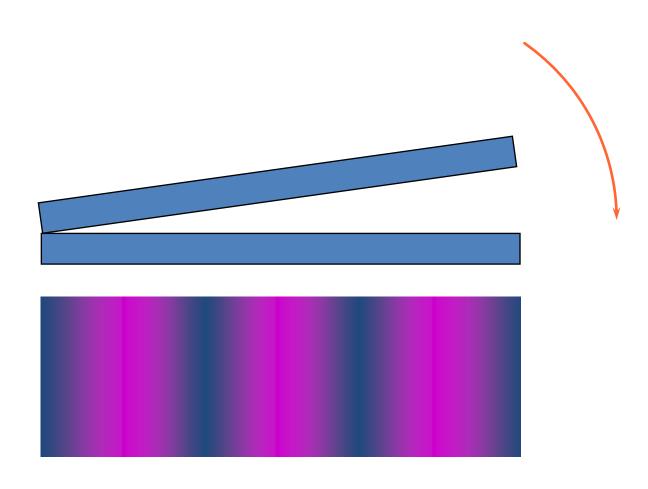
The angle becomes smaller, the fringes become wider, and the fringes move to the right

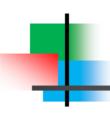


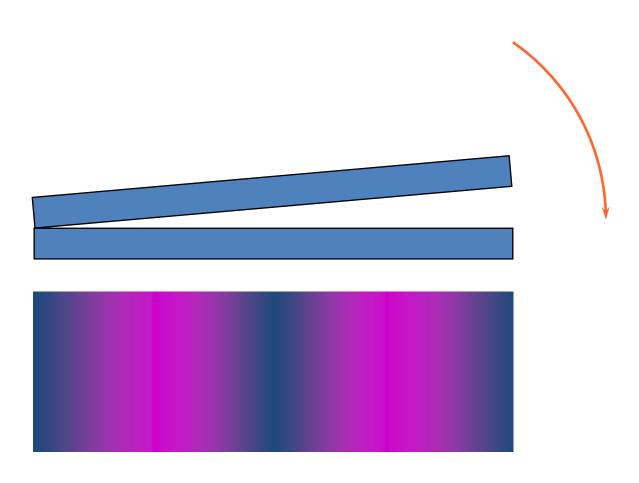




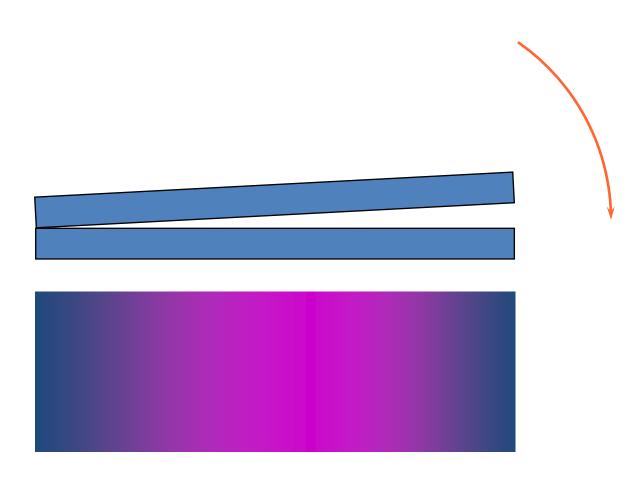




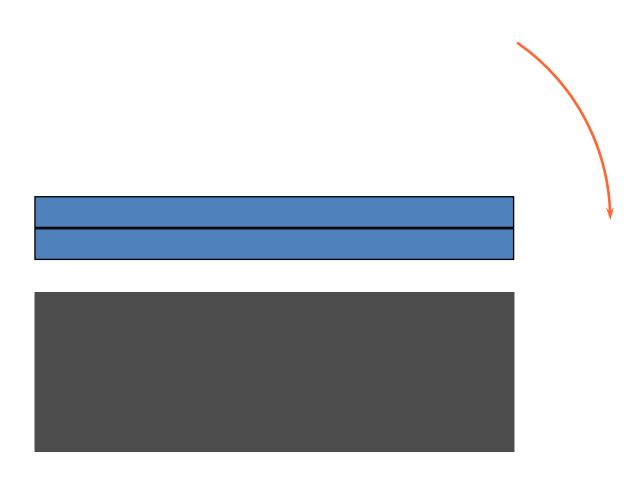














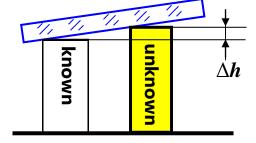
### Applications:

- Measure wavelength
- Measure refractive index
- Measuring small changes

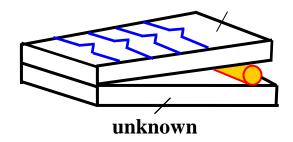




	Λ <i>L</i> ≈	$\frac{\lambda}{\lambda}$
$2n\theta$	$\Delta L \sim$	$2n\theta$



■ Measuring surface irregularity





### Interference fringes

■ When white light is illuminated,>>Colorful fringes.

$$\Delta L \approx \frac{\lambda}{2n\theta}$$

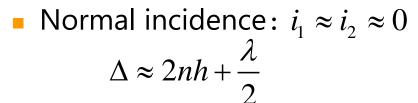




- For same region, uniform thickness, different colors when viewed from different angles: equal inclination interference;
- Unequal thickness: equal thickness interference.

# **Newton's ring**

If a large *R* plane-convex lens is placed on a flat plate, the reflected light from the two interfaces of an air wedge can interference. The fringes are concentric rings called **Newton's rings**.

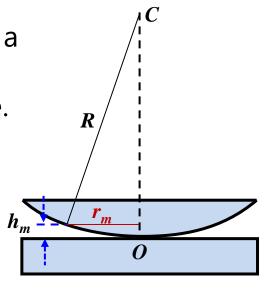




$$2h_m + \frac{\lambda}{2} = (2m+1)\frac{\lambda}{2} \qquad \Longrightarrow \qquad h_m = \frac{m\lambda}{2}$$

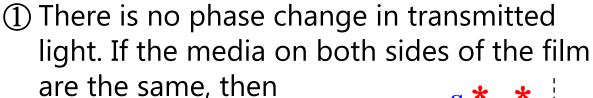


■ At center point, 
$$h = 0$$
  $(m = 0)$ ,  $\Delta = \frac{\lambda}{2}$   $\Longrightarrow$  dark



Newton's ring

# Interference of transmitted light

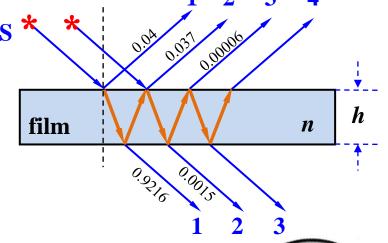


$$\Delta = 2nh\cos i_2$$

- ② The interference pattern of transmitted and reflected is complementary.
- ③ Low visibility. ???

The amplitude of the two beams of coherent light differs too much

☐ The interference fringes are observed from the transmitted light, and the center of the Newton's ring is a bright spot, as shown in the right figure.





### **Localized or Nonlocalized**

- Localization of interference fringes: Studying where in the two lightwaves overlapping areas, clear interference fringes can be produced.
- Nonlocalized interference fringes: Clear interference fringes can be formed anywhere in the overlapped area;
   E.g.: Young's Experiment, Fresnel Double Mirror, Lloyd Mirror
- Localized interference fringes: The interference fringes are only visible at certain positions in the overlapped region.

E.g: thin film interference—Extended light source: a collection of many point sources at different locations

00:29



# § 6.5 Michelson interferometer

- In 1887, Michelson-Morey experiment;
- Spectral fine structure analysis by visibility curve;
- The Cd red line spectrum is 643.84696 nm to represent international unit of meter, which becomes the international standard during 1927-1960.



Albert A. Michelson 1852-1931, Poland

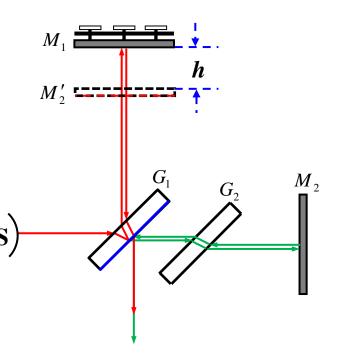
The first American to receive a Nobel Prize in physics, 1907. Because of precise optic instruments and spectroscopy and metrology studies with these instruments.



### Michelson interferometer

 $G_1$  and  $G_2$  are optical flat plate with the same thickness and uniform geometry and identical geometry.

The  $G_I$  side is coated with a thin silver layer that is transflective. Placed at an angle of  $45^{\circ}$  with respect to the horizontal direction;  $G_2$  is called a compensation plate.



 $M_1$  can move back and forth,  $M'_2$  is fixed, fringe changes.

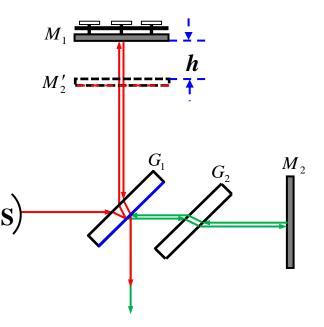
The interference is equivalently from the virtual image  $M'_2$  and  $M_1$ .



### Interference fringes

The OPL difference between the two beams is

$$\Delta = 2h$$
  $\Delta = 2\underline{n}h\cos i_2 + \frac{\lambda}{2}$ 



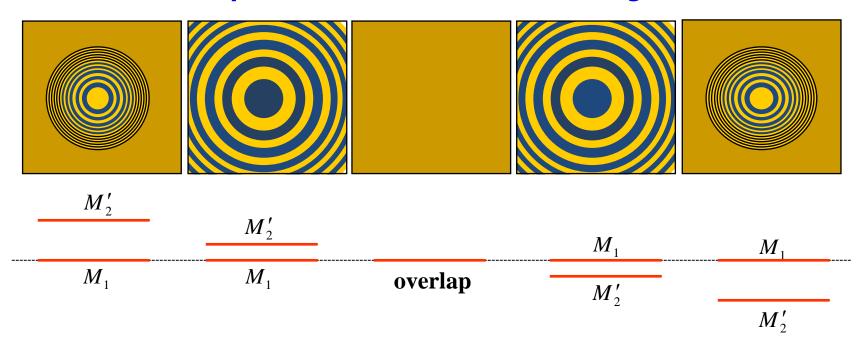
Change the angle of  $M_2$  we can get h = 0, h = constants (Equal inclination interference),  $h \neq constants$  (Equal thickness interference) (wedge-shaped film).

If  $M_1$  is shifted back and forth by  $\Delta h$ , the interference fringes move N, then:  $\Delta h = N \frac{\lambda}{2}$ 



### Interference fringes

### **Equal inclination interference fringes**



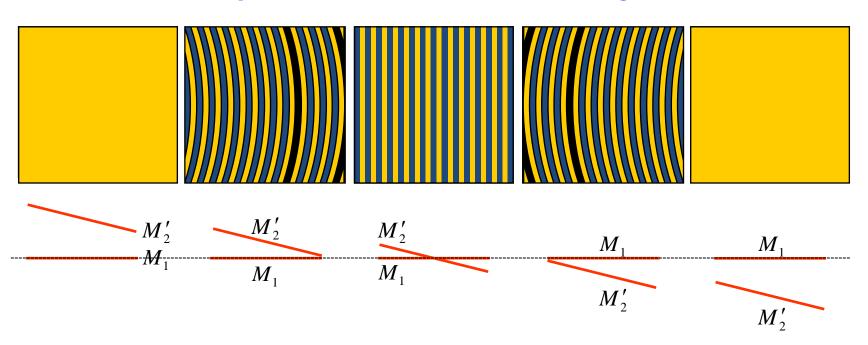
If  $M_1$  moves to  $M_2$ , the air film thickness decreases, the interference fringes shrink toward the center and disappear, and when  $M_1$  moves over  $\lambda/2$ , a fringe disappears.

If move in the opposite direction, a fringe emerges;

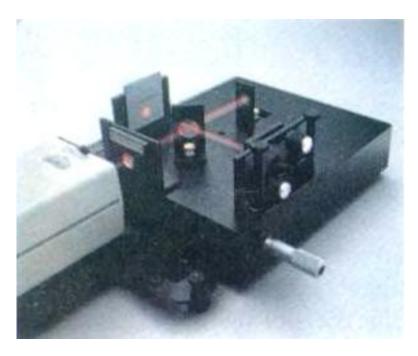


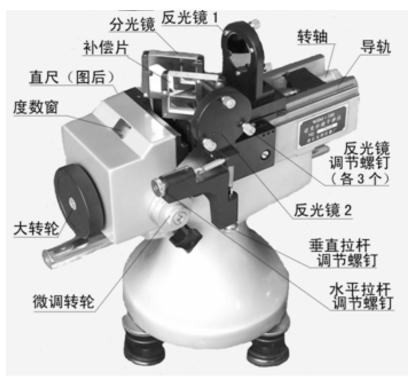
### Interference fringes

### **Equal thickness interference fringes**



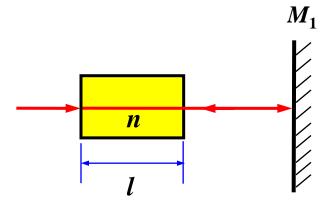
### Michelson interferometer





### Application

- > Measuring small displacements, measuring wavelengths  $(\lambda/20)$
- Measured refractive index:



The medium to be tested is inserted into the optical path 1 to generate an additional OPL difference:

 $\Delta h = N \frac{\lambda}{-}$ 

$$\delta = 2(n-1)l$$

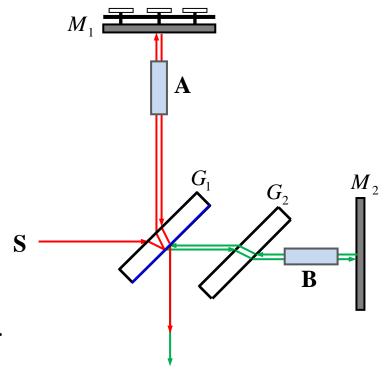
> Measuring coherence length:  $\Delta_{\text{max}} = L_0 = \frac{\lambda^2}{\Delta \lambda}$ 



**Example:** In the arms of the Michelson interferometer, insert two 10 cm long glass tubes A and B. Both of the tubes are vacuumed. It is observed that 107.2 fringes move during the filling of tube A with air.  $\lambda = 546$  nm. Determine the refractive index of air.

Assume that the refractive index of air is *n*:

$$\delta = 2(n-1)l = 107.2\lambda$$
$$n = \frac{107.2 \times \lambda}{2l} + 1 = 1.0002927$$

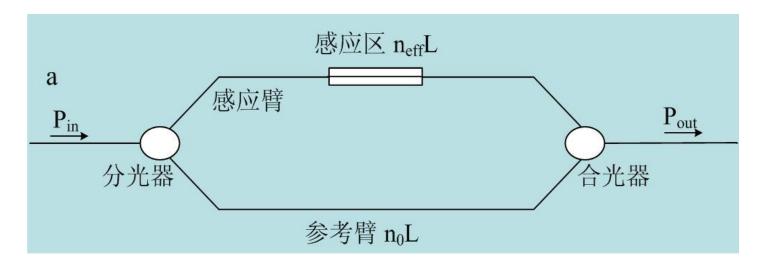


### **High precision**



### **Mach-Zehnder interferometer**

### Mach-Zehnder interferometer



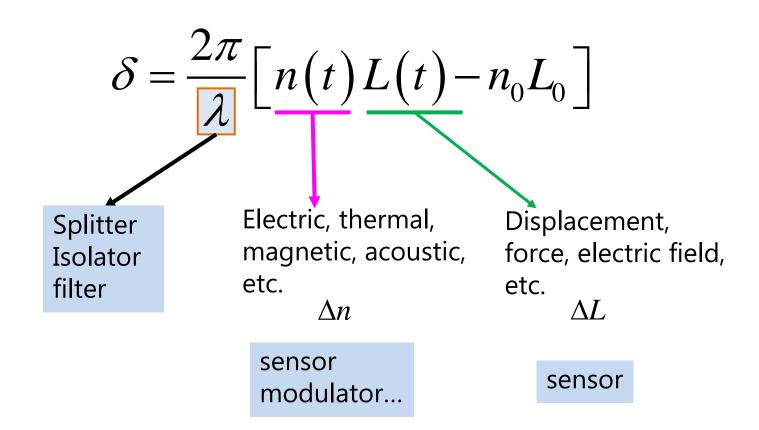
Output intensity: 
$$I_{out} = I_S + I_R + 2\sqrt{I_S I_R} \cos \delta$$

Phase difference between the two arms

$$\delta = \frac{2\pi}{\lambda} \left[ n(t) L(t) - n_0 L_0 \right]$$



### **Mach-Zehnder interferometer**

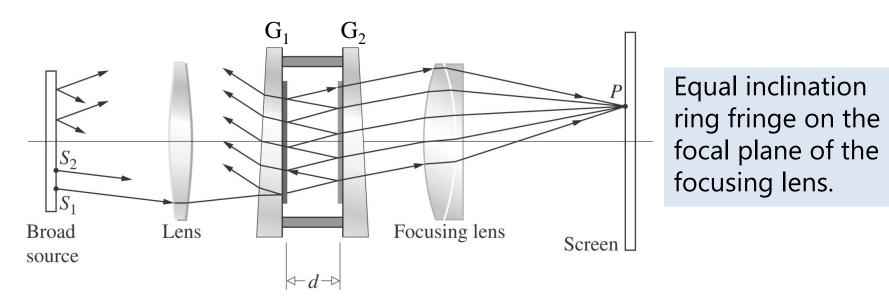


MZ Interferometers are widely used in the fields of modulation and sensing.



# § 6.6 Fabry-Pèrot Interferometer

Fabry-Pèrot interferometer:



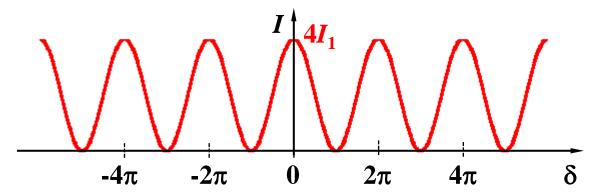
High reflection at inner surfaces

The distance d between  $G_1$  and  $G_2$  is adjustable
—Fabry-Pèrot interferometer

The distance d between  $G_1$  and  $G_2$  is fixed
—Fabry-Pèrot etalon



Intensity of double beam interference:  $I = 4I_1 \cos^2 \frac{\delta}{2} = 2I_1 (1 + \cos \delta)$ 



 $I \sim \delta$  change slowly>>fringe is not sharp>> low resolution. In multi-beam interference,  $I \sim \delta$  change quickly >> fringe is sharp >> high resolution.

Multi-beam | Amplitude splitting | interference | Wavefront splitting

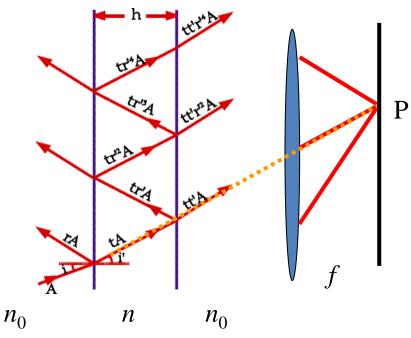
F-P interference

Grating diffraction



### Determine multi-beam interference intensity

Denote  $n_0 \rightarrow n$ : amplitude-reflection coefficient r, amplitude-transmission coefficient t.  $n \rightarrow n_0$ : amplitude-reflection coefficient r, amplitude-transmission coefficient t.



Phase shift caused by reflection is included in r' = -r.

Multi-beam interference requires (i) the film to be long enough, (ii) the incident angle i is not too large.

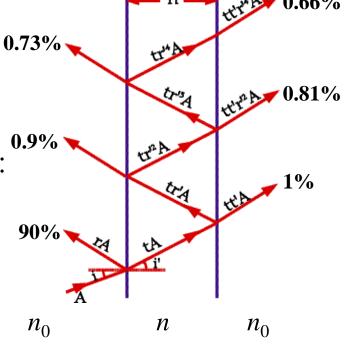
If the incident light amplitude A, wavelength  $\lambda$ , first beam transmitted light  $\varphi_0 = 0$ .

Phase difference between adjacent two transmitted light:

$$\delta = \frac{2\pi}{\lambda} \Delta = \frac{2\pi}{\lambda} 2h \cos i_2$$

Amplitude of each transmitted beam:

$$ilde{E}_1 = tt'Ae^{i0}$$
 $ilde{E}_2 = tt'r'^2Ae^{i\delta}$ 
 $ilde{E}_3 = tt'r'^4Ae^{i2\delta}$ 
 $ilde{E}_4 = tt'r'^6Ae^{i3\delta}$ 



As can be seen from the above expressions, they are infinitely series with a common ratio of  $r'^2e^{i\delta}$ .



Complex amplitude of transmitted beam:

$$\begin{split} \tilde{E}_{T} &= \tilde{E}_{1} + \tilde{E}_{2} + \dots = \sum_{j=1}^{\infty} \tilde{E}_{j} = Att' \left( 1 + r'^{2} e^{i\delta} + r'^{4} e^{i2\delta} + \dots \right) \\ &= A \frac{tt'}{1 - r'^{2} e^{i\delta}} = A \frac{1 - r^{2}}{1 - r^{2} e^{i\delta}} \end{split}$$

The last step uses the Fresnel reflection/refraction amplitude coefficients:

$$r = -r'$$
,  $1 - r^2 = tt'$  (You&Yu's Book: Page 54)

Transmission intensity:

$$I_{T} = \tilde{E}_{T} \cdot \tilde{E}_{T}^{*} = A^{2} \frac{\left(1 - r^{2}\right)^{2}}{\left(1 - r^{2}e^{i\delta}\right)\left(1 - r^{2}e^{-i\delta}\right)} = A^{2} \frac{\left(1 - r^{2}\right)^{2}}{1 - 2r^{2}\cos\delta + r^{4}}$$



It is known that  $A^2 = I_0$  and  $r^2 = R$ , so

$$I_T = A^2 \frac{\left(1 - r^2\right)^2}{1 - 2r^2 \cos \delta + r^4} = I_0 \frac{\left(1 - R\right)^2}{1 - 2R \cos \delta + R^2}$$

Use the equation:  $\cos \delta = 1 - 2\sin^2 \frac{\delta}{2}$ 

$$I_{T} = I_{0} \frac{(1-R)^{2}}{(1-R)^{2} + 4R\sin^{2}\frac{\delta}{2}} = \frac{I_{0}}{1+F\sin^{2}\frac{\delta}{2}}$$

$$F \equiv \frac{4R}{(1-R)^2}$$
 is called **coefficient of finesse**.

### Characteristics of interference fringes

$$I_{T} = I_{0} \frac{(1-R)^{2}}{(1-R)^{2} + 4R\sin^{2}\frac{\delta}{2}}$$

- (1) The intensity extremum is determined by  $\delta_i$  not R.
- ① When  $\delta = 2m\pi$ ,  $\sin \delta/2 = 0$ ;

$$I_{T \max} = I_0 \qquad I_{R \min} = 0$$

② When  $\delta = (2m+1)\pi$ ,  $\sin \delta/2 = 1$ 

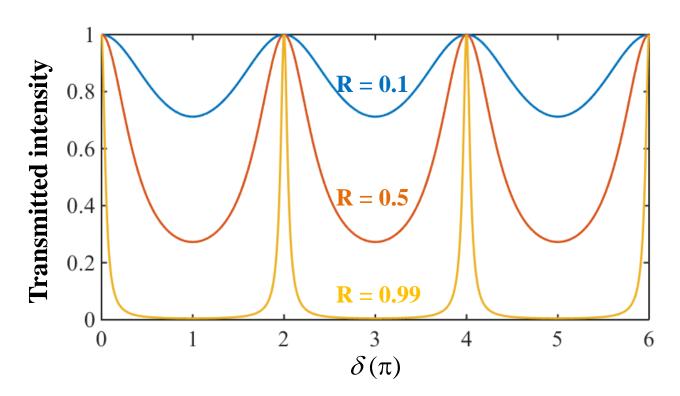
$$I_{T \min} = I_0 \frac{(1-R)^2}{(1+R)^2}$$
  $I_{R \max} = I_0 - I_{T \min} = I_0 \frac{4R}{(1+R)^2}$ 

$$R \uparrow \implies I_{T \min} \downarrow I_{R \max} \uparrow$$

### (2) Coefficient of finesse is determined by R.

$$\frac{I_T}{I_0} = \frac{1}{1 + F \sin^2 \frac{\delta}{2}}$$

$$\frac{I_T}{I_0} = \frac{1}{1 + F \sin^2 \frac{\delta}{2}} \qquad F = \frac{4R}{\left(1 - R\right)^2} \qquad R \uparrow, \text{ sharpness } \uparrow$$





### (二) 参数估算:透过峰的半峰宽 (FWHM)。

**习题4.23** 设法布里-珀罗干涉仪腔长3 cm,反射率R = 0.98,采用扩展光源照明。求 $\lambda$  = 0.5  $\mu$ m的谱线宽度?

$$\frac{I_T}{I_0} = \frac{1}{1+F\sin^2\frac{\delta}{2}}$$

$$\frac{I_T}{I_0} = \frac{1}{1+F\sin^2\frac{\delta}{2}}$$

$$F\sin^2\frac{\delta'}{2} = 1 \quad \Longrightarrow \quad \frac{1}{2}(1-\cos\delta') = \frac{1}{F} \quad F = \frac{4R}{(1-R)^2}$$

$$\cos \delta' = \frac{F - 2}{F} = 0.9798$$

$$\Rightarrow \Delta \lambda = 2 |\lambda' - \lambda| = 2.6 \times 10^{-4} \text{ nm}$$

$$\arccos 0.9798 = \frac{4\pi h}{\lambda'} - \frac{4\pi h}{\lambda}$$



- (3) The shape of the interference fringes: the interference pattern is an equal inclination fringes.
- Reflected light interference pattern: very thin dark lines on a bright background.
- ☐ Transmitted light interference pattern: very fine bright lines appear on a wide dark background.

  - \*\* The bright fringes of the F-P interferometer are sharper and brighter than the rings of the Michelson interferometer.



The ring fringes formed by different wavelengths of light have different sizes (interference splitting), and the fringes are sharp.

$$\Delta = 2h\cos i_2 = m\lambda$$

The F-P interferometer is a high-resolution spectroscopic instrument that is commonly used to study the (hyper)fine structure of the spectrum.

F-P interferometer is very important in modern optics:

- (1) **Spectrometer**
- (2) Resonant cavity
- (3) Wavelength division multiplexing components
- (4) comparison method measures the wavelength of light

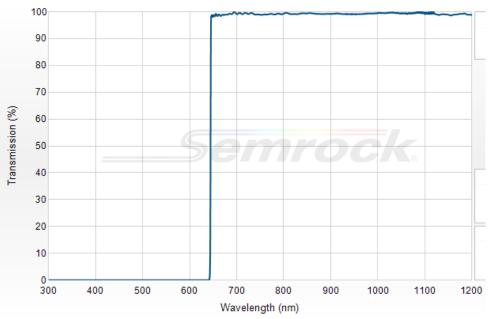


# § 6.7 Optical thin film

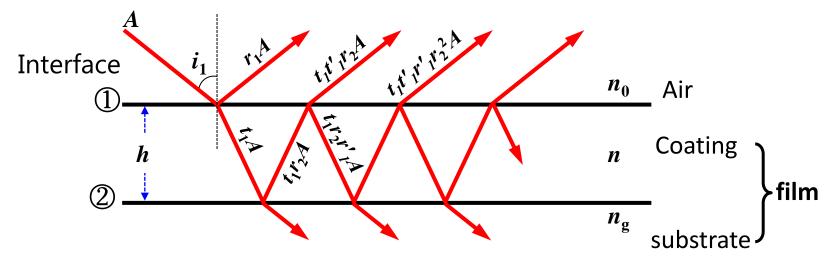
**Coating technology:** A thin layer of transparent or metallic film is coated to the glass or smooth metal surface by evaporation, deposition or spin-coating.

### Single / multilayer films









Interface ①: 
$$n_0 \rightarrow n$$
, reflectivity  $r_1$ , transmittance  $t_1$ ;  $n \rightarrow n_0$ ,  $r'_1$ ,  $t'_1$ 
Interface ②:  $n \rightarrow n_g$ ,  $r_2$ ,  $t_2$ ;

Appropriate choice of n and h causes multi-beam interference of light that is sequentially reflected and transmitted on interface ① ②, so that the reflected light is strengthened or attenuated.

# -

# Single layer film

For the sake of simplicity, only the normal incidence of light waves is discussed.

The multi-beam interference problem is fixed at  $(n_0 \cdot n \cdot n_g \cdot h)$  i = 0, determine the R of the single-layer film.

The solution is the same as the reflectivity calculation of the F-P interferometer, except that the amplitudereflection and amplitude-transmission coefficient of the upper and lower interfaces are different.

(1) Amplitude and intensity expression of the reflected light:

$$ilde{E}_R = \sum_{j=1}^{\infty} ilde{E}_j \qquad I_T = ilde{E}_R \cdot ilde{E}_R^*$$

2) Write a single layer film reflectance expression:

$$R = \frac{I_R}{I_0}$$



Amplitude of reflected wave:  $\tilde{E}_R = A \frac{r_1 + r_2 e^{i\delta}}{1 + r_1 r_2 e^{i\delta}}$ 

Membrane reflectivity: 
$$R = \frac{\tilde{E}_R \tilde{E}_R^*}{A^2} = \frac{r_1^2 + 2r_1r_2\cos\delta + r_2^2}{1 + 2r_1r_2\cos\delta + r_1^2r_2^2}$$

when 
$$i = 0$$
  $\delta = \frac{2\pi}{\lambda} \Delta = \frac{4\pi}{\lambda} nh$   $r_1 = \frac{n_0 - n}{n_0 + n}$   $r_2 = \frac{n - n_g}{n + n_g}$ 

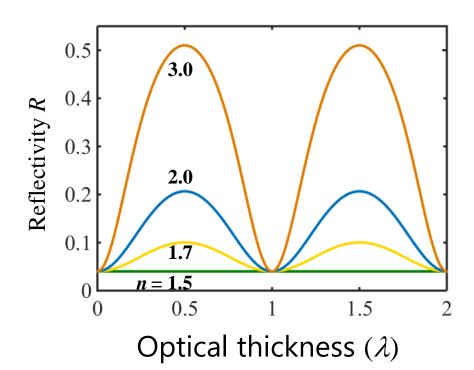
$$\Rightarrow$$

$$R = \frac{(n_0 - n_g)^2 \cos^2 \frac{\delta}{2} + (\frac{n_0 n_g}{n} - n)^2 \sin^2 \frac{\delta}{2}}{(n_0 + n_g)^2 \cos^2 \frac{\delta}{2} + (\frac{n_0 n_g}{n} + n)^2 \sin^2 \frac{\delta}{2}}$$



If: 
$$n_0 = 1.0$$
,  $n_g = 1.5$ ,  $i = 0$   
 $R \sim nh$  curve is shown:

$$R = \frac{(n_0 - n_g)^2 \cos^2 \frac{\delta}{2} + (\frac{n_0 n_g}{n} - n)^2 \sin^2 \frac{\delta}{2}}{(n_0 + n_g)^2 \cos^2 \frac{\delta}{2} + (\frac{n_0 n_g}{n} + n)^2 \sin^2 \frac{\delta}{2}}$$



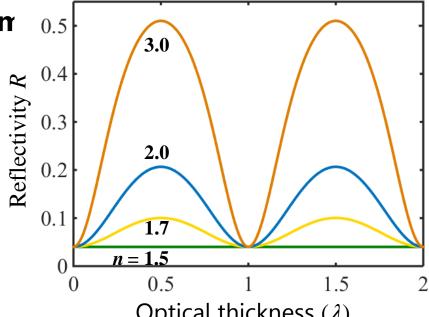
### (1) reflection increasing film

### **Requirement:** $n > n_{\sigma}$

When  $\delta = (2m+1)\pi$ , R is max.

$$\delta = \frac{4\pi}{\lambda} nh$$

$$nh = (2m+1)\lambda/4$$



Optical thickness ( $\lambda$ )

When the optical thickness is the odd times of

 $\lambda/4$ , R is the max, **reflection increasing film**.

$$R = R_{\text{max}} = \frac{\left(n_0 n_g - n^2\right)^2}{\left(n_0 n_g + n^2\right)^2}$$

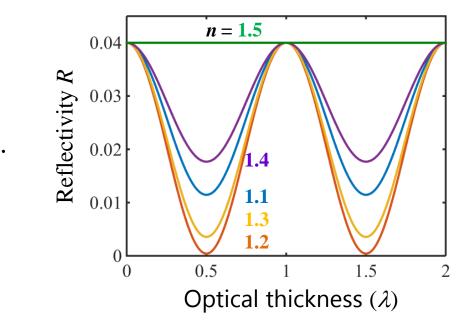
$$R = \frac{(n_0 - n_g)^2 \cos^2 \frac{\delta}{2} + (\frac{n_0 n_g}{n} - n)^2 \sin^2 \frac{\delta}{2}}{(n_0 + n_g)^2 \cos^2 \frac{\delta}{2} + (\frac{n_0 n_g}{n} + n)^2 \sin^2 \frac{\delta}{2}}$$

### (2) Antireflection film

### Requirement: $n < n_g$

When  $\delta = (2m+1)\pi$ , *R* is min.

$$\delta = \frac{4\pi}{\lambda} nh$$



When the optical thickness is the odd times

of  $\lambda/4$ , R is the min, **antireflection**.

$$R = R_{\min} = \frac{\left(n_0 n_g - n^2\right)^2}{\left(n_0 n_g + n^2\right)^2}$$

$$R = \frac{(n_0 - n_g)^2 \cos^2 \frac{\delta}{2} + (\frac{n_0 n_g}{n} - n)^2 \sin^2 \frac{\delta}{2}}{(n_0 + n_g)^2 \cos^2 \frac{\delta}{2} + (\frac{n_0 n_g}{n} + n)^2 \sin^2 \frac{\delta}{2}}$$

When 
$$n = \sqrt{n_0 n_g}$$
  $R_{\min} = 0$ 



(3) when  $\delta = 2m\pi$ ,  $nh = m\lambda/2$ .

Whatever  $n < n_g$ , or  $n > n_g$  the r is same as un-coating.

$$R = \frac{\left(n_0 - n_g\right)^2}{\left(n_0 + n_g\right)^2} \qquad R = \frac{\left(n_0 - n_g\right)^2 \cos^2\frac{\delta}{2} + \left(\frac{n_0 n_g}{n} - n\right)^2 \sin^2\frac{\delta}{2}}{\left(n_0 + n_g\right)^2 \cos^2\frac{\delta}{2} + \left(\frac{n_0 n_g}{n} + n\right)^2 \sin^2\frac{\delta}{2}}$$



When  $nh = (2m+1)\lambda/4$ , R is extremum.

 $n > n_{\rm g}$  reflection increasing film

 $n < n_{\rm g}$  Antireflection film

How do we understand these films in physics? ?

$$\Delta = 2nh = \left(2m+1\right)\frac{\lambda}{2}$$

	Interface	Incidence	Reflection	Phase change	film
$n > n_{\rm g}$	1	$n_0 \rightarrow n$	External	Υ	Reflection
	2	$n \rightarrow n_g$	Internal	N	increasing
$n < n_{\rm g}$	1	$n_0 \rightarrow n$	External	Υ	Antireflection
	2	$n \rightarrow n_g$	External	Υ	

# -

# Multilayer film

Reflection increasing film:  $R\uparrow$ 

Antireflection film:  $T\uparrow$ 

Interference filter: Extracting light of a certain

wavelength or band from complex light.

Multi-layer medium high-reflection film: The film system is composed of H and L films alternately, and the total number of layers N is odd.

Each layer  $nh = \lambda/4$  The number of layer  $\uparrow \rightarrow R \uparrow \circ$ 

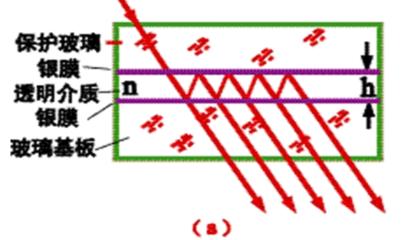
For example: Full reflection mirror of He-Ne laser cavity  $N = 15 \sim 19$ , n(ZnS - MgF), for  $\lambda = 632.8$  nm,  $R \sim 99.6\%$ .

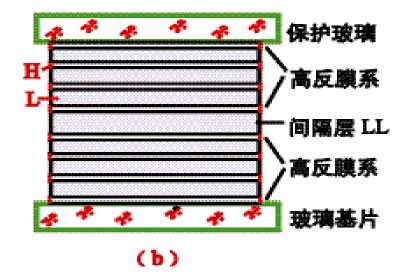
**Thin Film Optics**: Studying the relationship between n, h and R, T



### Interference filter

Structure: Minimal F-P etalon





Metal-coated interference filter

### All-dielectric interference filter

Interference filter: The narrowband filter is formed by the frequency selection principle of the F-P cavity.



### Homework

Problem 9.8, 9.13, 9.45 and 9.51.

### Homework\*

Find a text book of Quantum optics, and find out what's the first-order correlation and its relationship with out text.

### **Next week**

Huygen's Principle, Fraunhofer and Fresnel Diffraction

Sections 4.4.2, 10.1 and 10.2