# Chapter 5: Part C Simple applications of macroscopic thermodynamics

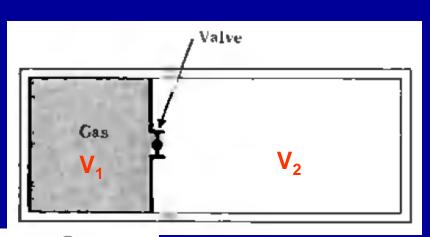
Zhi-Jie Tan Wuhan University

2019 spring semester

- > free expansion
- > Throttling process
- heat engine

### Free energy expansion and throttling process 5.9 free expansion

Open valve and the gas is free to expand to fill the volume  $V_2$  from  $V_1$ 



container is adiabatically insulated,

$$Q = 0$$

does no work in the process

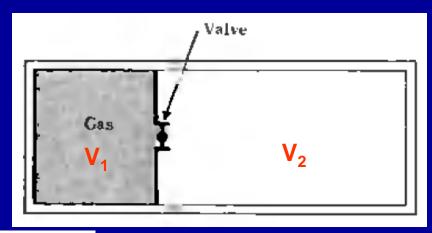
$$W = 0$$

$$\Delta E = 0$$

#### Free energy expansion and throttling process 5.9 free expansion

**First law** 

 $\Delta E = 0$ 



**Then** 

$$E(T_2, V_2) = E(T_1, V_1)$$

Specially, for ideal gas 
$$E(T_2) = E(T_1)$$
  $T_2 = T_1$ 

Generally,

$$E(T_2, V_2) = E(T_1, V_1)$$

$$\Omega \propto V^{N} \chi(E)$$

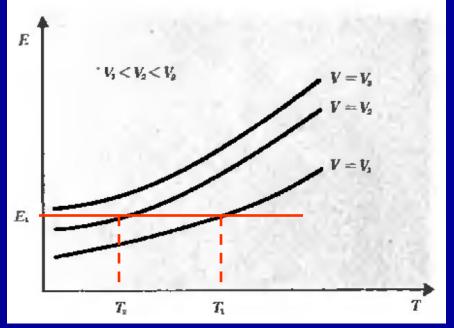
$$\beta = \frac{\partial \ln \chi(E)}{\partial E}$$

$$\beta = \beta(E)$$

Free energy expansion and throttling process

5.9 free expansion

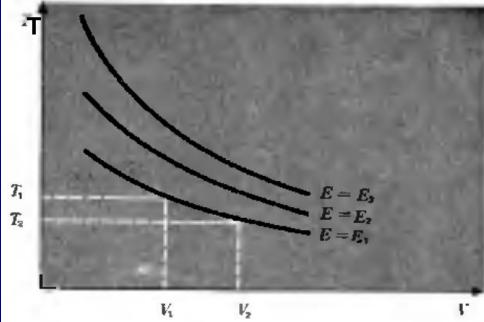




V-T curvo

Cas

Valve



#### Free energy expansion and throttling process 5.9 free expansion: example

#### Van de Waals gas

$$\epsilon(T_2,v_2) = \epsilon(T_1,v_1)$$

$$dE = C_V dT + \left[ T \left( \frac{\partial p}{\partial T} \right)_V - p \right] dV$$

$$\int_{T_1}^{T_2} c_V(T') \ dT' - \frac{a}{v_2} = \int_{T_2}^{T_2} c_V(T') \ dT' - \frac{a}{v_1}$$

$$\int_{T_1}^{T_2} c_V(T') dT' - \int_{T_0}^{T_1} c_V(T') dT' = a \left( \frac{1}{v_2} - \frac{1}{v_1} \right)$$
$$\int_{T_1}^{T_2} c_V(T') dT' = a \left( \frac{1}{v_2} - \frac{1}{v_1} \right)$$

#### Free energy expansion and throttling process

5.9 free expansion: example

 $\epsilon(T_2,v_2) = \epsilon(T_1,v_1)$ 

Van de Waals gas

Ignore  $c_V$  change in  $[T_1, T_2]$ 

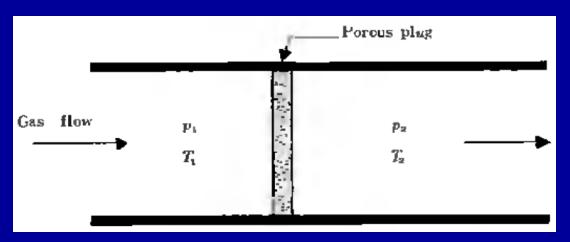
$$c_{V}(T_{2}-T_{1})=a\left(\frac{1}{v_{2}}-\frac{1}{v_{1}}\right)$$

$$T_{2}-T_{1}=-\frac{a}{c_{V}}\left(\frac{1}{v_{1}}-\frac{1}{v_{2}}\right)$$

For an expansion where  $v_2 > v_1$ ,

$$T_2 < T_1$$

**Steady-state**experiment by J-T



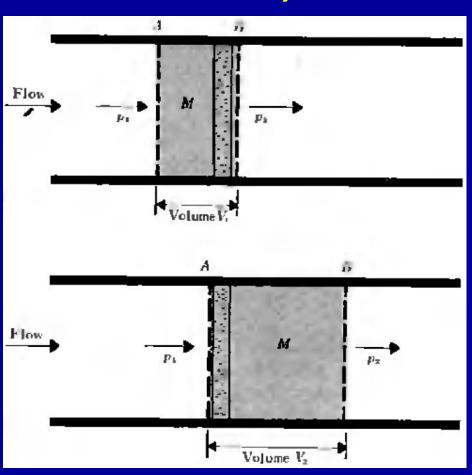
A porous plug provide a constriction to the flow of gas;

A continuous steam of gas flow from left to right;  $p_1$  in the left >  $p_2$  in the right;

T<sub>1</sub> is the temperature in left, what is T<sub>2</sub> in right?

Initial: Left, p<sub>1</sub>, V<sub>1</sub>

Final: right, p<sub>2</sub>, V<sub>2</sub>



$$\Delta E = E_2 - E_1 = E(T_2, p_2) - E(T_1, p_1)$$

$$W = p_2 V_2 - p_1 V_1$$

To external and by external

adiabatically insulated

$$Q = 0$$

Then,

$$\Delta E + W = Q = 0$$

$$(E_2 - E_1) + (p_2V_2 - p_1V_1) = 0$$

$$E_2 + p_2V_2 \approx E_1 + p_1V_1$$

Already define 
$$H \equiv E + pV$$

$$(E_2 - E_1) + (p_2V_2 - p_1V_1) = 0$$

$$E_2 + p_2V_2 = E_1 + p_1V_1$$

$$H(T_2,p_2) = H(T_1,p_1)$$

$$H = H(T)$$

For ideal gas,

$$H = E + pV = E(T) + \nu RT$$

$$H(T_2) = H(T_1) \qquad T_2 = T_1$$

in throttling process

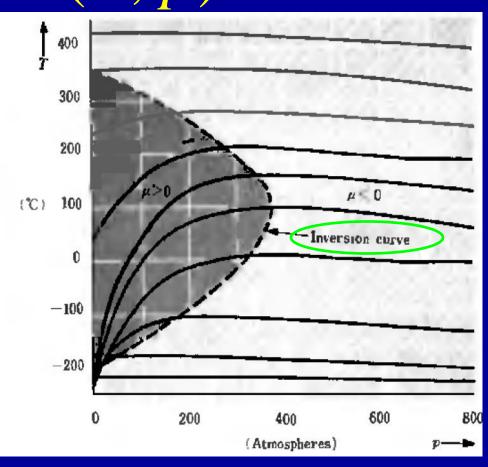
More generally, H = H(T, p)

$$\mu \equiv \left(\frac{\partial T}{\partial p}\right)_{\! H}$$

μ>0, T increases with p μ<0, T decreases with p

**Inversion curve** 

$$\mu == ??$$



1st law 2nd law

$$dE = T dS - p dV$$

$$dH \equiv d(E + pV) = T dS + V dp$$

$$dH = 0.$$

$$C_p = T(\partial S/\partial T)_p$$
.

$$0 = T \left[ \left( \frac{\partial S}{\partial T} \right)_p dT + \left( \frac{\partial S}{\partial p} \right)_T dp \right] + V dp$$

$$C_p dT + \left[ T \left( \frac{\partial S}{\partial p} \right)_T + V \right] dp = 0$$

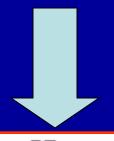
$$\mu \equiv \left(\frac{\partial T}{\partial p}\right)_{H}$$

$$\mu \equiv \left(\!\frac{\partial T}{\partial p}\!\right)_{\! H}$$

$$\mu \equiv \left(\frac{\partial T}{\partial p}\right)_{H} = -\frac{T(\partial S/\partial p)_{T} + V}{C_{p}}$$

$$\alpha \equiv \frac{1}{V}\left(\frac{\partial V}{\partial T}\right)_{p}$$
Maxwell

$$\alpha \equiv \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_{v}$$

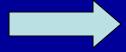


$$\left(\frac{\partial S}{\partial p}\right)_{T} = -\left(\frac{\partial V}{\partial T}\right)_{p} = -V\alpha$$

$$\mu = \frac{V}{C_p} (T\alpha - 1)$$

For ideal gas,  $\alpha = T^{-1}$ 

$$\alpha = T^{-1}$$

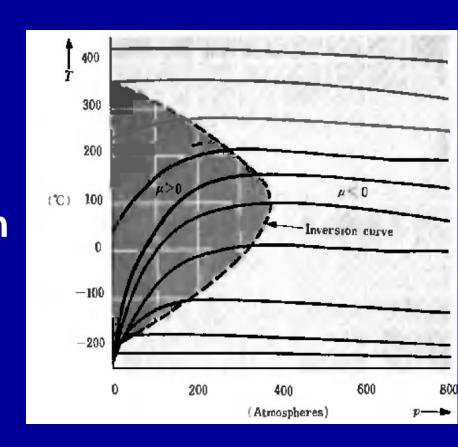


$$\mu = 0$$

J-T effect constitute a practical method for cooling gas.

1, It is necessary to work in the region of pressure and T where  $\mu > 0$ .

2, The initial T < T maximum on the inversion curve



Free energy expansion and throttling process 5.10 throttling process (Joule-Thomson ..)

Joule-Thomson effect and molecular force

```
For ideal gas,

T does not change for free expansion

for throttling process
```

These process becomes interesting for realistic gas virial expansion

For any gas,  $n \equiv N/V$ .

$$p = kT[n + B_2(T)n^2 + B_3(T)n^3 \cdot \cdot \cdot]$$
virial coefficent
$$p = \frac{N}{V}kT\left(1 + \frac{N}{V}B_2\right)$$

Free energy expansion and throttling process 5.10 throttling process (Joule-Thomson ...)

Joule-Thomson effect and molecular force

$$p = \frac{N}{V} kT \left( 1 + \frac{N}{V} B_2 \right)$$

At low T, attractive force play dom. role,  $B_2<0$ ; At high T, (exclusion) collision play dom. role,  $B_2>0$  $B_2$  increases with T

$$\mu == ??$$

#### Free energy expansion and throttling process 5.10 throttling process (Joule-Thomson ..) Joule-Thomson effect and molecular force

$$p = \frac{N}{V} kT \left( 1 + \frac{N}{V} B_2 \right)$$

$$p = \frac{NkT}{V}\left(1 + \frac{p}{kT}B_2\right) = \frac{N}{V}(kT + pB_2)$$

$$V = N\left(\frac{kT}{p} + B_2\right)$$

$$\mu = \frac{V}{C_p} \left( T\alpha - 1 \right)$$

$$\alpha \equiv \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_p$$

$$\alpha \equiv \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_{p}$$

$$\mu = \frac{1}{C_p} \left[ T \left( \frac{\partial V}{\partial T} \right)_p - V \right] = \frac{N}{C_p} \left( T \frac{\partial B_2}{\partial T} - B_2 \right)$$

## Free energy expansion and throttling process 5.10 throttling process (Joule-Thomson ..) Joule-Thomson effect & molecular force: discussion

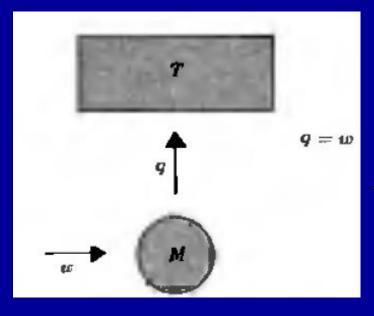
$$\mu = \frac{1}{C_p} \left[ T \left( \frac{\partial V}{\partial T} \right)_p - V \right] = \frac{N}{C_p} \left( T \frac{\partial B_2}{\partial T} - B_2 \right)$$

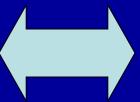
At low T,  $B_2<0$ ,  $\mu>0$ At high T,  $B_2>0$ ,  $\mu$  can <0

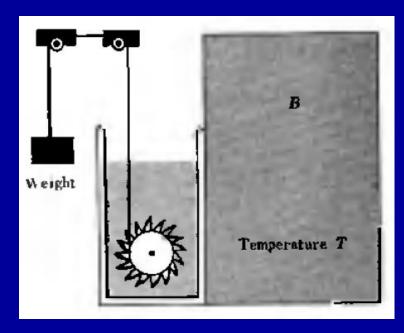
The inversion curve  $(\mu=0)$  indicates the competition between attraction and repulsion.

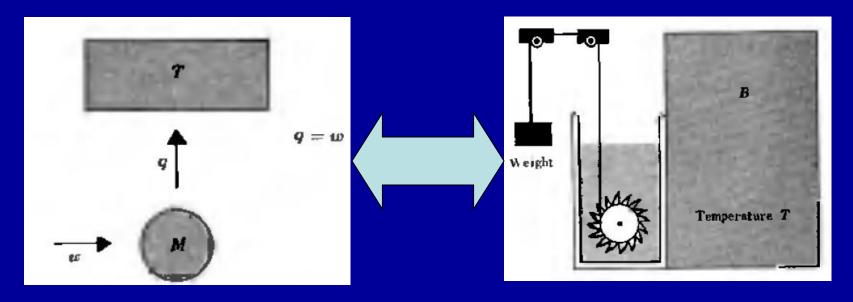
Historically, the subject of thermodynamics began with the study of engines:

- 1, great technological important
- 2, intrinsic physical interests





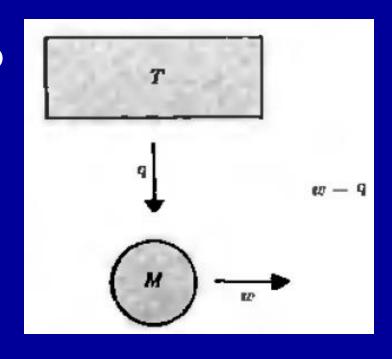




It is easy to do mechanical work w upon a device, and then extract from it heat q (q=w)

To what extent is it possible to proceed in the reversal way?

To build a device to extract internal energy from a heat reservoir in form of heat, and convert it to work?



The device is called heat engine!

Heat engine--- key point:

The work cannot be provided by the engine itself; or the heat-to-work process cannot be continued. Thus one wish the heat engine keeps the same macro-state at the end of process (cycle);

**Heat engine--- Question?** 

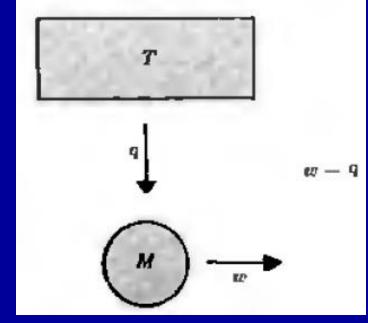
To what extent is it possible to exact a net amount of energy from heat reservoir?

In reservoir, energy is randomly distributed over many degree of freedom.

To energy associated the single freedom connected with the external parameter.

**Heat engine--- Question?** 

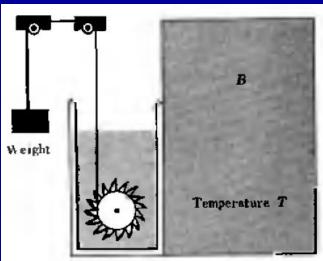
First law since E of M does not change







not realizable.

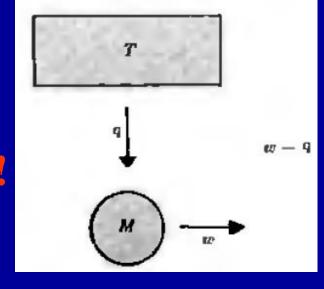


Work→ heat is an irreversible process

Since accessible states more random and entropy increases

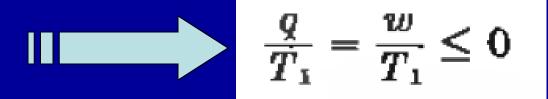
Ideal heat engine violates 2nd law!

$$\Delta S \geq 0$$



Heat reservoir, absorbed heat == (-q)The entropy change  $-q/T_{1}$ 





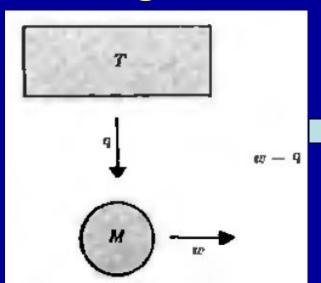
Wish w>0,
So it cannot be satisfied!!!

$$\frac{q}{T_1} = \frac{w}{T_1} \le 0$$

Wish w>0, So it cannot be satisfied!!!

It is impossible to construct a perfect heat engine.

Kelvin's formulation of the second law



#### **First law**

$$q_1=w+q_2$$

#### 2nd law

$$\Delta S = \frac{(-q_1)}{T_1} + \frac{q_2}{T_2} \ge 0$$



$$\frac{-q_1}{T_1} + \frac{q_1 - w}{T_2} \ge 0$$

#### First law \_\_ 2n

#### 2nd law

$$\frac{-q_1}{T_1} + \frac{q_1 - w}{T_2} \ge 0$$

$$\frac{w}{T_2} \leq q_1 \left( \frac{1}{T_2} - \frac{1}{T_1} \right)$$

$$\eta = \frac{T_1 - T_2}{T_1}$$

$$\begin{array}{c|c}
T_1 \\
\downarrow \\
M \\
\downarrow \\
q_2
\end{array}$$

$$\begin{array}{c|c}
T_2 \\
\end{array}$$

$$\begin{array}{c|c}
T_2 \\
\end{array}$$

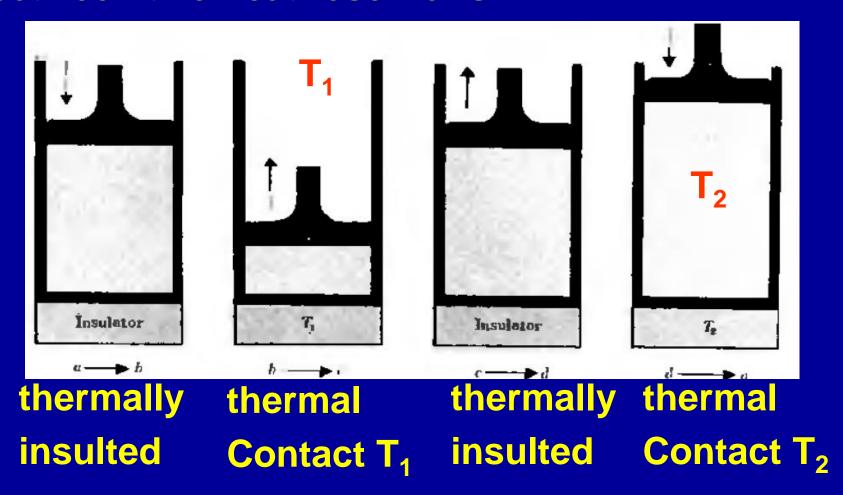
Define 
$$\eta \equiv \frac{w}{q_1} \le 1 - \frac{T_2}{T_1} = \frac{T_1 - T_2}{T_1}$$

**Efficiency of heat engine** 

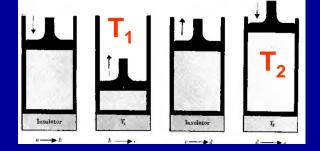
if quasi-static,

$$\eta = \frac{T_1 - T_2}{T_1}$$

# Heat engine and refrigerator 5.11 Carnot engines How does such a engine operate quasi-statically between two heat reservoirs ?



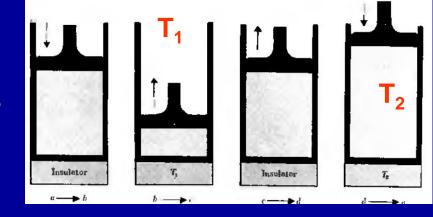
### Heat engine and refrigerator 5.11 Carnot engines: process



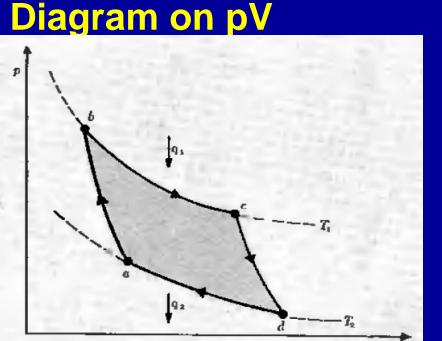
- 1.  $a \to b$ : The engine is thermally insulated Its external parameter is changed slowly until the engine temperature reaches  $T_1$ . Thus  $x_a \to x_b$  such that  $T_2 \to T_1$ .
- 2.  $b \to c$ : The engine is now placed in thermal contact with the heat reservoir at temperature  $T_1$ . Its external parameter is changed further, the engine remaining at temperature  $T_1$  and absorbing some heat  $q_1$  from the reservoir. Thus  $x_b \to x_c$  such that heat  $q_1$  is absorbed by the engine.
- 3.  $c \to d$ : The engine is again thermally insulated. Its external parameter is changed in such a direction that its temperature goes hack to  $T_2$ . Thus  $x_c \to x_d$  such that  $T_1 \to T_2$ .
- 4.  $d \rightarrow a$ : The engine is now placed in thermal contact with the heat reservoir at temperature  $T_2$ . Its external parameter is then changed until it returns to its initial value  $x_a$ , the engine remaining at temperature  $T_2$  and rejecting some heat  $q_2$  to this reservoir. Thus  $x_d \rightarrow x_a$  and heat  $q_2$  is given off by the engine.

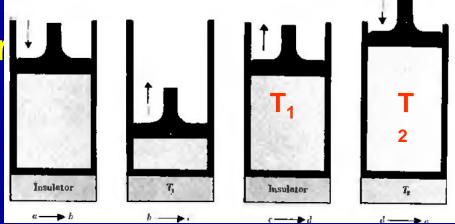
The engine is now back in its initial state and the cycle is completed.

### Heat engine and refrigerator 5.11 Carnot engines: process



- $a \rightarrow b$ ; thermally insulted; compression;  $T_2 \rightarrow T_1; q = 0$
- $b \rightarrow c$ ; thermal contact with  $T_1$ ; expansion;  $q_1$
- $c \rightarrow d$ ; thermally insulted; expansion;  $T_1 \rightarrow T_2$ ; q = 0
- $d \rightarrow a$ ; thermal contact with  $T_2$ ; compression;  $-q_2$





$$w = \int_{a}^{b} p \, dV + \int_{b}^{c} p \, dV + \int_{c}^{d} p \, dV + \int_{d}^{a} p \, dV$$

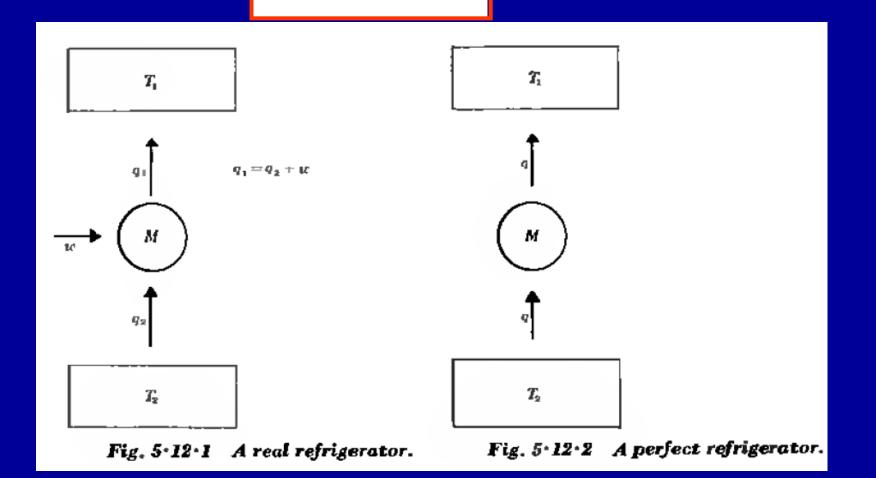
$$\eta \equiv \frac{w}{q_1} \le 1 - \frac{T_2}{T_1} = \frac{T_1 - T_2}{T_1}$$

### Heat engine and refrigerator 5.11 Refrigerator

Remove heat from reservoir at low T to that at high T

**First law** 

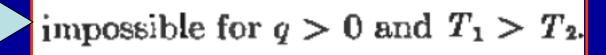
$$w+q_2=q_1$$



#### Heat engine and refrigerator **5.11 Refrigerator**

Remove heat from reservoir at low T to that at high T

Perfect refrigerator 
$$\Delta S = \frac{q}{T_1} + \frac{(-q)}{T_2} \ge 0$$
$$q\left(\frac{1}{T_1} - \frac{1}{T_2}\right) \ge 0$$



It is impossible to construct a perfect refrigerator.

the Clausius formulation of the second law

### Heat engine and refrigerator 5.11 Refrigerator: real

First law

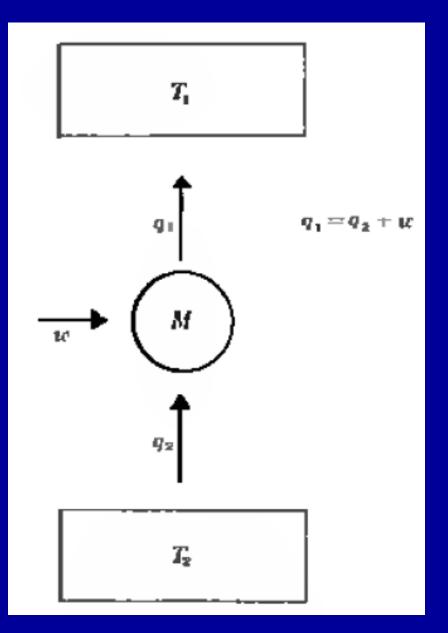
$$q_2 = q_1 - w$$

2nd law

$$\Delta S = \frac{q_1}{T_1} + \frac{(-q_2)}{T_2} \ge 0$$
 $\frac{q_2}{q_1} \le \frac{T_2}{T_1}$ 

$$\varepsilon = \frac{q_2}{w} = \frac{q_2}{q_1 - q_2} = \frac{1}{q_1/q_2 - 1}$$

$$\leq \frac{1}{T_1/T_2 - 1} = \frac{T_2}{T_1 - T_2}$$



#### Class-work

P 198 5.26

#### Homework

P 192 5.18,5.20,5.23,5.24