

电动力学-第八次作业

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Problem 8.4

Answer:

(a)

$$(\vec{\mathbf{T}} \cdot d\mathbf{a})_z = T_{zx}da_x + T_{zy}da_y + T_{zz}da_z \quad (1.1)$$

For x-y plane:

$$(\vec{\mathbf{T}} \cdot d\mathbf{a})_z = \epsilon_0 \left(E_z E_z - \frac{1}{2} E^2 \right) (-r dr d\phi) \quad (1.2)$$

Now:

$$\begin{cases} \mathbf{E} = \frac{1}{4\pi\epsilon_n} 2 \frac{q}{r^2} \cos \theta \hat{\mathbf{r}} \\ \cos \theta = \frac{r}{s} \end{cases} \quad (1.3)$$

So:

$$E_z = 0 \quad (1.4)$$

$$E^2 = \left(\frac{q}{2\pi\epsilon_0} \right)^2 \frac{r^2}{(r^2 + a^2)^3} \quad (1.5)$$

Then:

$$F_z = \frac{1}{2} \epsilon_0 \left(\frac{q}{2\pi\epsilon_0} \right)^2 2\pi \int_0^{\pi} \frac{r^3 dr}{(r^2 + a^2)^3} = \frac{q^2}{4\pi\epsilon_0} \frac{1}{(2a)^2} \quad (1.6)$$

(b)

In this case:

$$\begin{cases} \mathbf{E} = -\frac{1}{4\pi\epsilon_0} 2 \frac{q}{s^2} \sin \theta \hat{\mathbf{z}} \\ \sin \theta = \frac{a}{s} \end{cases} \quad (1.7)$$

So:

$$E^2 = E_z^2 = \left(\frac{qa}{2\pi\epsilon_0} \right)^2 \frac{1}{(r^2 + a^2)^3} \quad (1.8)$$

So:

$$F_z = -\frac{\epsilon_0}{2} \left(\frac{qa}{2\pi\epsilon_0} \right)^2 2\pi \int_0^\infty \frac{rdr}{(r^2 + a^2)^3} = -\frac{q^2}{4\pi\epsilon_0} \frac{1}{(2a)^2} \quad (1.9)$$

Problem 8.7

Answer:

(a)

$E_x = E_y = 0, E_z = -\sigma/\epsilon_0$, Then:

$$\left\{ \begin{array}{l} T_{xy} = T_{xz} = T_{yz} = \dots = 0 \\ T_{xx} = T_{yy} = -\frac{\epsilon_0}{2} E^2 = -\frac{\sigma^2}{2\epsilon_0} \\ T_{zz} = \epsilon_0 \left(E_z^2 - \frac{1}{2} E^2 \right) = \frac{\epsilon_0}{2} E^2 = \frac{\sigma^2}{2\epsilon_0} \end{array} \right. \quad (2.1)$$

So:

$$\vec{\mathbf{T}} = \frac{\sigma^2}{2\epsilon_0} \begin{pmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & +1 \end{pmatrix} \quad (2.2)$$

(b)

$$\mathbf{F} = \oint \vec{\mathbf{T}} \cdot d\mathbf{a} \quad (2.3)$$

Do integrata over the xy plane;

$$F_z = \int T_{zz} da_z = -\frac{\sigma^2}{2\epsilon_0} A \quad (2.4)$$

So, the force per unit area is:

$$f = \frac{\mathbf{F}}{A} = -\frac{\sigma^2}{2\epsilon_0} \hat{\mathbf{z}} \quad (2.5)$$

(c)

$$-T_{zz} = \frac{\sigma^2}{2\epsilon_0} \quad (2.6)$$

(d)

The recoil force is the momentum delivered per unit time, so the force per unit area on the top plate is:

$$f = -\frac{\sigma^2}{2\epsilon_0} \hat{\mathbf{z}} \quad (2.7)$$

This result is same as (b)

Problem 8.9

Answer:

(a)

The angular momentum stored in the fields is:

$$\vec{l} = \vec{r} \times \epsilon_0 \vec{E} \times \vec{B} = \frac{QB_0}{4\pi r} \hat{r} \times (\hat{r} \times \hat{z}) \quad (3.1)$$

We have:

$$\hat{r} \times (\hat{r} \times \hat{z}) = \hat{r}(\hat{r} \cdot \hat{z}) - \hat{z}(\hat{r} \cdot \hat{r}) = \hat{r} \cos \theta - \hat{z} \quad (3.2)$$

Over the sphere, only the z-component of the angular momentum will survive the integration so:

$$(\hat{r} \times (\hat{r} \times \hat{z}))_z = (\hat{r} \cos \theta - \hat{z}) \cdot \hat{z} = \cos^2 \theta - 1 = -\sin^2 \theta \quad (3.3)$$

Then:

$$L_z = \int_V l_z dV = \int_a^b \int_0^\pi \int_0^{2\pi} \frac{QB_0}{4\pi r} (-\sin^2 \theta) r^2 dr \sin \theta d\theta d\phi = -\frac{QB_0}{4\pi} 2\pi \int_a^b r dr \int_0^\pi \sin^3 \theta d\theta \quad (3.4)$$

We have:

$$x = \cos \theta \quad dx = -\sin \theta d\theta \quad (3.5)$$

Then:

$$L_z = -\frac{\pi QB_0}{2} \frac{1}{2} (b^2 - a^2) \int_1^{-1} \sin^3 \theta \frac{dx}{-\sin \theta} = -\frac{\pi QB_0}{3} (b^2 - a^2) \quad (3.6)$$

So:

$$\vec{L} = -\frac{\pi QB_0}{3} (b^2 - a^2) \hat{z} \quad (3.7)$$

(b)

When the magnetic field is turning off an electric field is induced. By Faraday's law:

$$2E\pi s = -s^2\pi\dot{B} \implies \vec{E} = -\frac{s}{2}\dot{B}\hat{\phi} \quad (3.8)$$

Torque on the patch of surface on a sphere is with (on the sphere) $s = a \sin \theta$:

$$d\vec{N} = \vec{a} \times d\vec{F} = \vec{a} \times \sigma dS \vec{E} = -\vec{a} \times \sigma dS \frac{a \sin \theta}{2} \dot{B} \hat{\phi} = -\sigma a^2 \sin^2 \theta d\theta d\phi \vec{a} \times \frac{a}{2} \dot{B} \hat{\phi} \quad (3.9)$$

Now, again only the z-component will survive, so the projection of vector $\vec{a} \times \hat{\phi}$ on the z-axis is:

$$(\vec{a} \times \hat{\phi})_z = (\vec{a} \times \hat{\phi}) \cdot \hat{z} = a \cos \left(\pi - \frac{\pi}{2} - \theta \right) = a \sin \theta \quad (3.10)$$

With this:

$$dN_z = -\sigma a^4 \frac{1}{2} \dot{B} \sin^3 \theta d\theta d\phi \quad (3.11)$$

$$N_z = -\frac{1}{2} \dot{B} \sigma a^4 \int_0^\pi \sin^3 \theta d\theta \int_0^{2\pi} d\phi = -\pi \dot{B} \sigma a^4 \frac{4}{3} \quad (3.12)$$

where we solved the same integral ($\sin^3 \theta$) in the (a) part of the problem. Now this is valid for both spheres, so for the bigger sphere just replace a with b . Using $\sigma = Q/4\pi a^2$ (small sphere) and $\sigma = -Q/4\pi b^2$ the torques are:

$$N_{z,a} = -\frac{\pi}{3} \dot{B} Q a^2 \quad N_{z,b} = \frac{\pi}{3} \dot{B} Q b^2 \quad (3.13)$$

The total angular momentum of the system is then:

$$\begin{aligned} L_z &= \int_0^{t_f} (N_{z,a} + N_{z,b}) dt = \frac{\pi}{3} Q (b^2 - a^2) \int_0^{t_f} \dot{B} dt = \frac{\pi}{3} Q (b^2 - a^2) \int_{B_0}^0 dB \\ &= -\frac{\pi}{3} Q B_0 (b^2 - a^2) \end{aligned} \quad (3.14)$$

So:

$$\vec{L} = -\frac{\pi}{3} Q B_0 (b^2 - a^2) \hat{z} \quad (3.15)$$

Problem 8.14

Answer:

(a)

$$\begin{aligned}
\frac{U}{l} &= \int_0^{2\pi} \int_a^b u s ds d\phi \\
&= \int_0^{2\pi} \int_a^b \left[\frac{\epsilon_0}{2} \left(\frac{\lambda}{2\pi\epsilon_0 s} \right)^2 + \frac{1}{2\mu_0} \left(\frac{\mu_0 \lambda v}{2\pi s} \right)^2 \right] s ds d\phi \\
&= 2\pi \frac{1}{2\epsilon_0} \left(\frac{\lambda}{2\pi} \right)^2 \int_a^b \left(\frac{1}{s^2} + \frac{1}{s^2} \frac{v^2}{c^2} \right) s ds \\
&= \frac{\lambda^2}{4\pi\epsilon_0} (1 + \beta^2) \int_a^b \frac{ds}{s} = \frac{\lambda^2}{4\pi\epsilon_0} (1 + \beta^2) \ln \frac{b}{a}
\end{aligned} \tag{4.1}$$

(b)

Now, for the momentum per unit length stored in the fields just integrate the momentum density over a unit length of the system:

$$\begin{aligned}
\frac{\vec{p}}{l} &= \int_0^{2\pi} \int_a^b \vec{g} s ds d\phi = \int_0^{2\pi} \int_a^b \epsilon_0 \vec{E} \times \vec{B} s ds d\phi \\
&= \int_0^{2\pi} \int_a^b \epsilon_0 \frac{\lambda}{2\pi\epsilon_0 s} \hat{s} \times \frac{\mu_0 \lambda v}{2\pi s} \hat{\phi} s ds d\phi \\
&= \frac{\mu_0 \lambda^2 v}{4\pi^2} \int_a^b \frac{ds}{s} \int_0^{2\pi} d\phi \hat{s} \times \hat{\phi} = \frac{\mu_0 \lambda^2 v}{2\pi} \ln \frac{b}{a} \hat{z}
\end{aligned} \tag{4.2}$$

(c)

For the power transported down the wires integrate the Poynting vector over the annular surface in between the cylinders, with the positive orientation in the z-direction:

$$\begin{aligned}
P &= \int_a^b \int_0^{2\pi} \vec{S} \cdot d\vec{A} = \frac{1}{\mu_0} \int_a^b \int_0^{2\pi} (\vec{E} \times \vec{B}) \cdot s ds d\phi \hat{z} \\
&= \frac{1}{\mu_0} \int_a^b \int_0^{2\pi} \left(\frac{\lambda}{2\pi\epsilon_0 s} \hat{s} \times \frac{\mu_0 \lambda v}{2\pi s} \hat{\phi} \right) \cdot s ds d\phi \\
&= \frac{\lambda^2 v}{4\pi^2 \epsilon_0} \int_a^b \frac{ds}{s} \int_0^{2\pi} d\phi \\
&= \frac{\lambda^2 v}{2\pi \epsilon_0} \ln \frac{b}{a}
\end{aligned} \tag{4.3}$$