

HINT & SOLUTIONS : IDEAL GAS

EXERCISE # S-I

1. $2\text{NaN}_3 \longrightarrow 2\text{Na} + 3\text{N}_2$
Mole : 2 3
Volume of N_2 formed = $\frac{3 \times 0.0821 \times 300}{1} = 73.9$ lits.

2. Case-I : $P.V. = \frac{3.6}{36} \times 0.0821 \times T \quad \dots(1)$

Case-II : $P.V. = \frac{3}{36} \times 0.0821 \times (T + 15) \quad \dots(2)$

Equating (1) & (2),

We get, $T = 75\text{K}$

From equation (1)

$P \times 8.21 = \frac{3.6}{36} \times 0.0821 \times 75$

$\Rightarrow P = 0.075 \text{ atm}$

3. $P.V_1 = \frac{1}{4} RT \quad \dots(1)$

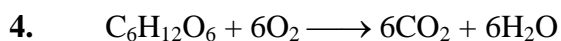
$P.V_2 = \frac{0.125}{4} RT \quad \dots(2)$

Now, (1) \div (2),

$\frac{V_1}{V_2} = 8 \Rightarrow V_2 = \frac{1}{8} V_1$
or $\frac{4}{3} \pi r_2^3 = \frac{1}{8} \times \frac{4}{3} \pi r_1^3$

$\Rightarrow r_2^3 = \left(\frac{10}{2}\right)^3$

$\Rightarrow r_1 = 5 \text{ cm}$



$n_{\text{O}_2} = \frac{1 \times 0.2 \times 10^{-3}}{0.08 \times 300}$

$\approx 8.3 \times 10^{-6} \text{ mole}$

\therefore mass of glucose required for hour by a resting mole having mass 60 kg

$\approx \frac{8.3 \times 10^{-6}}{6} \times 180 \times 60$

$\approx 15 \text{ gm.}$

Also, volume of CO_2 product = $\frac{8.3 \times 10^{-6} \times 0.08 \times 300}{1} \times 60$
 $\approx 12 \text{ dm}^3.$

5. $n^2 = \left(\frac{P}{RT} \right)^2 \times V^2$

$$\Rightarrow \text{slope} = \left(\frac{P}{RT} \right)^2$$

$$\Rightarrow \text{slope} = \frac{(8 \cdot 21)^2}{(0 \cdot 0821 \times 200)^2}$$

$$\approx 0 \cdot 25$$

or $\frac{1}{4}$

6. As, $M = \frac{dRT}{P}$

$$\Rightarrow M = \frac{0 \cdot 8 \times 0 \cdot 082 \times 300}{2 \cdot 46}$$

$$\Rightarrow M = 8 \text{ gm/mole}$$

7. By using equation of state,

$$\frac{P_1 V_1}{T_1} = \frac{P_2 V_2}{T_2}$$

$$\Rightarrow \frac{P \cdot V}{T_1} = \frac{4P \times 2V}{T_2}$$

$$\Rightarrow \boxed{T_2 = 8T_1}$$

8. As, $P^2 = (nRT)^2 \times \frac{1}{V^2}$

$$\Rightarrow \text{slope} = (nRT)^2$$

$$\Rightarrow \text{slope} = (1 \times 0 \cdot 08 \times 400)^2$$

$$= (32)^2$$

$$= (1024)$$

9. $P_f (100 + V) = (n_1 + n_2)RT \quad \dots(1)$

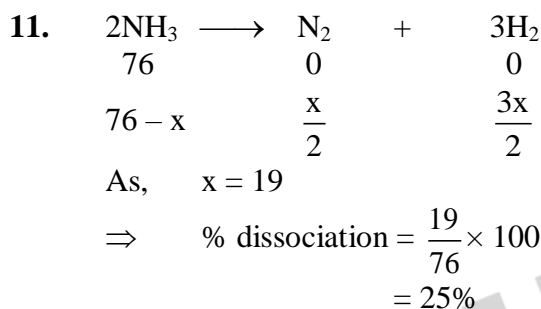
$$P_A (100) = n_3 \cdot RT \quad \dots(2)$$

Now, (1) \div (2),

$$\frac{P_f}{P_A} \times \frac{100 + V}{100} = \frac{(n_1 + n_2)RT}{n_3 RT} \left(\frac{P_f}{P_A} = \frac{40}{100} \& n_1 + n_2 = n_3 \right)$$

$$\Rightarrow V = 150 \text{ ml}$$

$$\begin{aligned}
 10. \quad n_{\text{He}} &= \frac{0.3 \times 1}{0.0821 \times 300} \\
 &= 0.012 \\
 \text{Now, } \frac{0.4 \times 3}{0.0821 \times 300} &= n_{\text{T}} \\
 \Rightarrow n_{\text{T}} &= 0.048 \\
 \Rightarrow n_{\text{Ne}} &= 0.048 - 0.012 \\
 &= 0.036 \\
 \Rightarrow \frac{n_{\text{He}}}{n_{\text{Ne}}} &= \frac{0.036}{0.012} \\
 &\approx 3
 \end{aligned}$$



$$\begin{aligned}
 12. \quad (i) \quad P &= \frac{nRT}{V} \\
 &= \frac{16 \times 0.0821 \times 300}{32 \times 8.21} \\
 &= 1.5 \\
 (ii) \quad & \begin{array}{ccc} 3\text{O}_2 & \longrightarrow & 2\text{O}_3 \\ \text{mole : } .5 & & 0 \\ & & 0.5 - .25 \quad 0.25 \times \frac{2}{3} \end{array} \\
 \text{Now, } P_{\text{O}_2} &= x_{\text{O}_2} \times P_{\text{T}} \\
 &= \frac{0.25}{.5} \times 1.5 \\
 &\approx 0.75 \\
 \& \quad P_{\text{O}_3} &= \frac{0.16}{.5} \times 1.5 \\
 &\approx 0.50 \\
 (iii) \quad P_{\text{T}} &= \frac{n_{\text{T}} \times RT}{V} \\
 &= \frac{0.42 \times 0.0821 \times 50}{8.21} \\
 &\approx 0.208 \text{ atm.}
 \end{aligned}$$

13. Total pressure of mixture = $P_{H_2} + P_{O_2}$

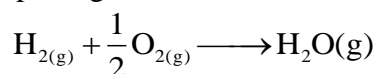
$$\Rightarrow P_T = \frac{10^{-2} \times 10^3 \times 0.0821 \times 473}{2 \times 10} + \frac{6.4 \times 10^{-2} \times 10^3 \times 0.0821 \times 473}{32 \times 10}$$

$$\Rightarrow P_T \approx 27.17 \text{ atm}$$

or

$$27.54 \times 10^5 \text{ N/m}^2$$

Where spark ignites the mixture,



$$\text{mole : } \begin{array}{ccc} 5 & 2 & 0 \\ 1 & 0 & 4 \end{array}$$

$$\Rightarrow \text{moles total} \approx 5$$

$$\Rightarrow P_{(\text{final})} = \left(\frac{5 \times 0.0821 \times 473}{10} \times 1.013 \times 10^5 \right)$$

$$= 19.66 \times 10^5 \text{ N/m}^2$$

14. $P_T = P_{N_2} + P_{O_2}$

$$\Rightarrow P_{N_2} = 90 - 63$$

i.e. $P_{N_2} = 27 \text{ mm of Hg}$

Now, $P_{N_2} = x_{N_2} \times P_T$

$$\Rightarrow x_{N_2} = \frac{27}{90} \Rightarrow x_{N_2} = 0.3$$

$$\Rightarrow \text{Answer is } (0.3 \times 10) \text{ i.e. } 3$$

15. $\frac{r_{H_2}}{r_{O_2}} = \frac{P_{H_2}}{P_{O_2}} \sqrt{\frac{M_{O_2}}{M_{H_2}}}$

$$= \frac{1 \times 32}{2 \times 8} \sqrt{\frac{32}{2}}$$

$$= 8$$

16. $\frac{r_{\text{mix}}}{r_x} = \sqrt{\frac{M_x}{M_{\text{mix}}}}$

$$\frac{600}{200} = \sqrt{\frac{M_x}{20/3}}$$

$$9 = \frac{M_x}{20/3}$$

$$M_x = 9 \times \frac{20}{3}$$

$$M_x = 60g$$

$$17. \quad (i) \quad \frac{r_{\text{SO}_2}}{r_{\text{CH}_4}} = \sqrt{\frac{M_{\text{CH}_4}}{M_{\text{SO}_2}}} = \sqrt{\frac{16}{64}}$$

$$\Rightarrow \frac{r_{\text{SO}_2}}{r_{\text{CH}_4}} = \frac{1}{2}$$

$$(ii) \quad \frac{r_{\text{SO}_2}}{r_{\text{CH}_4}} = \frac{3 \times 16}{64 \times 2} \sqrt{\frac{1}{4}}$$

$$= \frac{3}{16}$$

$$(iii) \quad \frac{r_{\text{SO}_2}}{r_{\text{CH}_4}} = 1 \times \sqrt{\frac{1}{4}}$$

$$\Rightarrow \frac{r_{\text{SO}_2}}{r_{\text{CH}_4}} = \frac{1}{2}$$

$$18. \quad \frac{r_{\text{N}_2}}{r_{\text{SF}_6}} = \sqrt{\frac{M_{\text{SF}_6}}{M_{\text{N}_2}}}$$

$$(\text{dn})_{\text{N}_2} = \sqrt{\frac{146}{28}} \times (\text{dn})_{\text{SF}_6}$$

$$= 2.28 \times 100$$

$$= 228$$

No. of molecules of N_2 present in the product gas for every 100 molecules of SF_6 is 228.

$$19. \quad \text{No} \rightarrow \begin{array}{|c|c|} \hline \leftarrow x \rightarrow & \leftarrow 100-x \rightarrow \\ \hline \end{array} \leftarrow \text{O}_2$$

$$\frac{r_{\text{NO}_2}}{r_{\text{O}_2}} = \sqrt{\frac{M_{\text{O}_2}}{M_{\text{NO}}}}$$

$$\frac{x}{100-x} = \sqrt{\frac{32}{30}}$$

$$\Rightarrow x = 50.8 \text{ cm}$$

20. At constant volume & temperature

$$P \propto W$$

Thus, for N_2 : $P_1 = 2 \text{ atm}$, $P_2 = 1/2 \text{ atm}$. at $t = 1 \text{ hr}$.

$$\frac{P_1}{P_2} = \frac{W_1}{W_2}$$

$$\Rightarrow W_2 = \frac{14 \times 1/2}{2}$$

$$\Rightarrow W_2 = \frac{14}{4}$$

$$\therefore \text{wt. of N}_2 \text{ diffused} = 14 - \frac{14}{4}$$

$$= \frac{21}{4} \text{ kg.}$$

For H₂ : P₁ = 2 atm, P₂ = $\frac{1}{2}$ at t = t hrs.

$$w_1 = 1 \text{ kg} \quad w_2 \rightarrow ?$$

$$\Rightarrow w_2 = \frac{1}{4} \text{ kg}$$

Hence, wt. of H₂ diffused = $1 - \frac{1}{4} = \frac{3}{4} \text{ kg.}$

Now, $\frac{r_A}{r_B} = \frac{\rho_B}{\rho_A}$

or, $\frac{V_A \times t_B}{V_B \times t_A} = \frac{\rho_B}{\rho_A} \sqrt{\frac{\rho_A}{\rho_B}}$

$$\frac{W_A \times t_B}{W_B \times t_A} = \frac{\rho_B}{\rho_A} \sqrt{\frac{\rho_A}{\rho_B}}$$

For our problem,

$$\frac{W_{H_2} \times t_{N_2}}{W_{N_2} \times t_{H_2}} = \sqrt{\frac{M_{H_2}}{M_{N_2}}}$$

$$\frac{\frac{3}{4} \times 1}{\frac{21}{2} \times t} = \sqrt{\frac{2}{28}}$$

$$\Rightarrow t = \frac{60}{14} \text{ mins}$$

$$\Rightarrow t = 16 \text{ mins}$$

21. $\frac{r_{O_2}}{r_{\text{mix}}} = \sqrt{\frac{M_{\text{mix}}}{M_{O_2}}}$

$$\frac{336}{224} = \sqrt{\frac{M_{\text{mix}}}{32}} \Rightarrow M_{\text{mix.}} = 72$$

Now, Let molecular weight of unknown gas be x g

$$\Rightarrow 72 = \frac{3}{4} \times 32 + \frac{1}{4} \times x$$

$$\Rightarrow x = 192 \text{ gm}$$

22. using, $Pv = nRT$

$$n_T = \frac{24.6 \times 3}{0.0821 \times 300}$$

$$\Rightarrow n_T = 3$$

$$\Rightarrow n_{H_2} = 2 \quad \& \quad n_{D_2} = 1$$

Now,

$$\frac{\left(\frac{n_{H_2}}{n_{D_2}}\right)_f}{\left(\frac{n_{H_2}}{n_{D_2}}\right)_i} = \left(\frac{M_{D_2}}{M_{H_2}}\right)^{\frac{n}{2}} \Rightarrow \frac{\left(\frac{1 \times 4}{4 \times 2}\right)}{\left(\frac{2}{1}\right)} = \left(\frac{1}{2}\right)^{\frac{n}{2}}$$

$$\Rightarrow \frac{1}{4} = \left(\frac{1}{2}\right)^{\frac{n}{2}} \Rightarrow \frac{1}{16} = \left(\frac{1}{2}\right)^n$$

$$\Rightarrow \left(\frac{1}{2}\right)^4 = \left(\frac{1}{2}\right)^n \Rightarrow n = 4$$

23. $P_f \cdot V_f = n_T \cdot R \times T$

$$\Rightarrow \frac{7}{6} \times 10 \times 2.4 = n_T \times 25$$

$$\Rightarrow n_T = 1.12$$

Now, $n_T = n_1 + n_2$

As, $n_2 = \frac{20 \times 4}{25} = \frac{8}{25}$

$$\Rightarrow n_1 = 1.12 - \frac{8}{25} = 0.8$$

Now, $n_1 = \frac{P_1 V_1}{RT}$

$$\Rightarrow P_1 = \frac{.8 \times 25}{2}$$

$$\Rightarrow P_1 = 10 \text{ atm or } 1 \text{ MPa}$$

24. As, $n_i = n_f$

$$\Rightarrow \frac{(P \cdot V) \times n}{RT} = \frac{P_f \times V(1 + 2 + 3 + \dots + n)}{RT}$$

$$\Rightarrow P = \frac{P_f (n+1)}{2}$$

$$\Rightarrow P_f = \left(\frac{2P}{n+1}\right)$$

25. As, $\frac{P_1}{T_1} = \frac{P_2}{T_2}$

$$\Rightarrow \frac{250 \times 10^3}{300} = \frac{10^6}{T_2}$$

$$\Rightarrow T_2 = 1200 \text{ K}$$

Yes, the cylinder will blow up.

26. $n_1 = \frac{2.463 \times 2}{25}$ & $n_2 = \frac{4.926 \times 1}{25}$

$$\Rightarrow P_f \times 3 = \frac{9.852}{25} \times 25$$

$$\Rightarrow P_f = 3.284 \text{ atm}$$

27. $(U_{\text{r.m.s}})_{\text{SO}_2}$ at TK = $(U_{\text{Arg.}})_{\text{O}_2}$ at 300K

$$\left(\sqrt{\frac{3RT}{M}} \right)_{\text{SO}_2} = \left(\sqrt{\frac{8RT}{\pi M}} \right)_{\text{O}_2} \text{ at } 300 \text{ K}$$

$$\Rightarrow \frac{3 \times T}{64} = \frac{8 \times 300}{\pi \times 32}$$

$$\Rightarrow T = 509.554 \text{ K} \quad \text{Or} \quad 236.3^\circ\text{C}.$$

28. $U_{\text{r.m.s}} = \sqrt{\frac{3P}{P}}$

$$= \sqrt{\frac{3 \times 10^5 \times 10^{-6}}{3 \times 10^{-4} \times 10^{-3}}}$$

$$= \sqrt{10^6} = 1000 \text{ m/s}$$

29. As, $\text{K.E} = \frac{3}{2} \text{ KT}$

$$= \frac{3}{2} \times \frac{1.38 \times 10^{-23} \times 300}{1.6 \times 10^{-19}} \text{ eV}$$

$$= 3.88 \times 10^{-2} \text{ eV}$$

$$\Rightarrow x = 2$$

$$30. \quad \lambda = \frac{1}{\sqrt{2\pi r^2 N^+}} \quad \text{or} \quad \frac{1 \times KT}{\sqrt{2\pi r^2} \times P}$$

$$\Rightarrow \quad \frac{\lambda_2}{\lambda_1} = \frac{1}{5}$$

$$\Rightarrow \quad \lambda_2 = \frac{1}{5} \times \lambda_1 \quad \text{or} \quad \frac{1}{5} \times 10$$

$$\Rightarrow \quad \lambda_2 = 2 \text{ cm}$$

$$31. \quad \lambda = \frac{KT}{\sqrt{2\pi r^2} \times P}$$

on substituting the values, we get

$$\lambda = 3.3 \times 10^3 \text{ cm.}$$

$$32. \quad \text{As,} \quad Z_1 = \sqrt{2\pi r^2} U_{\text{avg}} N^*$$

$$(U_{\text{Avg.}})_{\text{Ne}} < (U_{\text{Avg.}})_{\text{H}_2}$$

$$\Rightarrow \quad N_{\text{He}}^* > N_{\text{H}_2}^*$$

$$\Rightarrow \quad \text{He has higher concentration.}$$

EXERCISE # S-II

1. $P_{\text{(glycerine)}} = \frac{2.75 \times 5}{13.6} + 76 = 176 \text{ cm of Hg}$

$$\Rightarrow n_{\text{gas}} = \frac{\frac{176}{76} \times 10}{0.0821 \times 300} \Rightarrow n_{\text{gas}} = 0.94$$

2. $10 \times 4 = P_1 \times 8$

$$P_1 = 5$$

$$\frac{V_1}{T_1} = \frac{V_2}{T_2}$$

$$\frac{8}{300} = \frac{V_1}{600}$$

$$V_1 = 16\text{L}$$

$$\frac{P_1}{T_1} = \frac{P_2}{T_2}$$

$$\frac{5}{600} = \frac{3}{T_3}$$

$$T_3 = \frac{600 \times 3}{5} = 360 \text{ K}$$

$$\frac{5}{300} = \frac{P_2}{T_4}$$

3. $P \propto d$

So $P = kd$

it $P_1 = 1 \text{ atm} \quad d_1 = 1 \text{ m} \quad \Rightarrow \quad K = 1 \text{ atm m}^{-1}$

(a) $\frac{P_1 V_1}{n_1} = \frac{P_2 V_2}{n_2}$

$$\frac{P_1 \times \frac{4}{3} \pi r_1^3}{n_1} = \frac{P_2 \times \frac{4}{3} \pi r_2^3}{n_2}$$

$$\frac{1 \times 1}{1} = \frac{3 \times (3)^3}{n_2}$$

$$n_2 = 81$$

So moles of gas added = $81 - 1 = 80$

(b) at 7 atm pressure $d = 7 \text{ m}$

$$V_{\text{balloon}} = 57.1 \pi \text{ m}^3$$

So balloon will burst is its volume becomes $36 \pi \text{ m}^3$

$$\frac{4}{3}\pi r^3 = 36\pi \Rightarrow r = 3 \text{ m}$$

$$D = 6 \text{ m}$$

$$P = 6 \text{ atm}$$

$$\frac{P_1 V_1}{n_1} = \frac{P_2 V_2}{n_2}$$

$$\frac{1 \times \frac{4}{3}\pi \times \frac{1}{8}}{1} = \frac{6 \times 36\pi}{n_2}$$

$$n_2 = 1296$$

$$\text{moles added} = 1296 - 1 = 1295$$

$$4. \quad \frac{r_{\text{mix}}}{r_{\text{kr}}} = \sqrt{\frac{M_{\text{kr}}}{M_{\text{mix}}}}$$

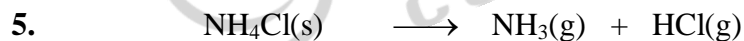
$$1.16 = \sqrt{\frac{84}{M_{\text{mix}}}}$$

$$M_{\text{mix}} = 62.42$$

$$62.42 = \frac{71}{1 + \alpha}$$

$$1 + \alpha = \frac{71}{62.42} = 1.137$$

$$\alpha = 0.137$$



| | | | |
|-------|---|---|---|
| n_i | 1 | 0 | 0 |
| n_f | 0 | 1 | 1 |

$$P_{\text{gas}} = \frac{2 \times 0.0821 \times 600}{24.63} = 4 \text{ atm}$$

$$6. \quad T_{\text{max}} \text{ at } P_{\text{max}}$$

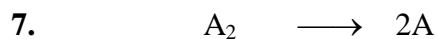
$$PV = nRT$$

$$\frac{1}{8.21} P \times 8.21 \times P = 1 \times 0.0821 \times T$$

$$\text{At } P = 10 \text{ atm}$$

$$100 \times 8.21 = 1 \times 0.0821 \times T$$

$$T = 10000 \text{ K}$$



$$n_i \quad 1 \quad 0$$

$$n_f \quad 0.5 \quad 1$$

$$PV = nRT$$

$$P \times 33.6 = 1.5 \times 0.0821 \times 546$$

$$P = 2 \text{ atm}$$

8. (a) $m_{\text{rms}} = \sqrt{\frac{3RT}{M}}$

$$= \sqrt{\frac{3 \times 8.314 \times 300}{2 \times 10^{-3}}} = 1934.24 \text{ ms}^{-1}$$

(b) $\mu_{\text{rms}} = \sqrt{\frac{3RT}{M}} = \sqrt{\frac{3PV}{nM}}$

$$= \sqrt{\frac{3 \times 10^5 \times 5 \times 10^{-3}}{3 \times 2 \times 10^{-3}}} = 500 \text{ m/sec}$$

(c) $\mu_{\text{rms}} = \sqrt{\frac{3RT}{M}} = \sqrt{\frac{3P}{d}}$

$$= \sqrt{\frac{3 \times 10^5}{10^3}} = \sqrt{300} = 17.32 \text{ m/sec}$$

9. (i) $P = \frac{nRT}{V}$

$$= \frac{10^{-3} \times 0.08 \times 300}{2} = 0.012 \text{ atm}$$

(ii) $\frac{P_1}{n_1 T_1} = \frac{P_2}{n_2 T_2}$

$$\frac{0.012}{10^{-3} \times 300} = \frac{1}{n_2 \times 600}$$

$$n_2 = \frac{1}{24}$$

$$N = \frac{6 \times 10^{23}}{24} = 2.5 \times 10^{22}$$

$$(iii) \quad KE_{total} = \frac{3}{2} RT \times n$$

$$= \frac{3}{2} \times 8 \times 300 \times 10^{-3}$$

$$(vi) \quad KE_{total} = \frac{3}{2} \times 8 \times 6000 \times \frac{1}{24}$$

$$= 300 \text{ J}$$

$$(v) \quad \frac{\mu_{mps,A}}{m_{mps,B}} = \sqrt{\frac{T_A}{T_B}} = \frac{1}{\sqrt{2}}$$

$$(vi) \quad Z_{11} = \frac{1}{\sqrt{2}} \pi \sigma^2 \mu_{avg} (N)^2$$

$$Z_{11} \propto \frac{P^2}{T^{\frac{3}{2}}}$$

$$\frac{Z_{11,A}}{Z_{11,B}} = \left(\frac{12 \times 10^{-3}}{1} \right)^2 \times \left(\frac{600}{300} \right)^{3/2} = 0.4 \times 10^{-3} : 1$$

$$10. (a) \quad \lambda = \frac{1}{\sqrt{2} \pi \sigma^2 N^*}$$

$$N^* = \frac{1}{\sqrt{2} \times 3.14 \times (0.26 \times 10^{-9})^2 \times 2.6 \times 10^{-5}}$$

$$N^* = 1281 \times 10^{20} \text{ M}^{-3}$$

$$(b) \quad N^* = \frac{P}{KT}$$

$$1281 \times 10^{20} = \frac{P \times 6 \times 10^{23}}{8.314 \times 300}$$

$$P = 530.6 \text{ Pa}$$

EXERCISE # O-I

1. (C)

Sol. By equation of state, $\frac{P_1 V_1}{T_1} = \frac{P_2 V_2}{T_2}$

$$\Rightarrow \frac{P \cdot V_1}{273} = \frac{P \cdot 2V_1}{T_2}$$

$$\Rightarrow T_2 = 546 \text{ K} \quad \text{or} \quad 273^\circ\text{C}$$

2. (B)

Sol. At constant temperature, $P \propto \frac{1}{V}$

$$\Rightarrow P_1 < P_2$$

3. (D)

Sol. Mass of liquid = 50 gm

$$\Rightarrow \text{volume of container} = \frac{50}{25} = 2 \text{ dm}^3$$

4. (C)

Sol. $d_A = 2d_B$ & $M_B = 3M_A$

As, $P = \frac{dRT}{M}$

$$\Rightarrow P_A = \frac{d_A RT}{M_A} \quad \dots(1)$$

& $P_B = \frac{d_B RT}{M_B} \quad \dots(2)$

(1) \div (2)

$$\frac{P_A}{P_B} = \frac{d_A}{d_B} \times \frac{M_B}{M_A}$$

$$= \frac{2d_B}{d_B} \times \frac{3M_A}{M_A} = 6 \quad \Rightarrow \quad P_A : P_B = 6 : 1$$

5. (C)

Sol. $(nRT)_1 = (nRT)_2$

$$\frac{4}{18} \times R \times T = \frac{3.2}{18} \times R \times (T + 50)$$

$$\Rightarrow T = 200\text{K}$$

6. (C)

Sol. V.D = 70 \Rightarrow molar mass = 140

$$\Rightarrow 12x + 16x = 140$$

$$\Rightarrow 28x = 140$$

$$\Rightarrow x = \frac{140}{28} \Rightarrow x = 5$$

7. (C)

Sol. Vapour pressure depends on temperature only, so, as the temperature remains constant, V.P. will remain unchanged.

8. (C)

Sol. Assuming volume remaining constant

$$\frac{W_1 T_1}{P_1} = \frac{W_2 T_2}{P_2}$$

$$\Rightarrow \frac{10 \times T}{P} = \frac{W_2 \times 2T \times 2}{3 \times P}$$

$$\Rightarrow W_2 = 7.5 \text{ gm}$$

$$\Rightarrow \text{mass of gas escaped} = W_1 - W_2 \\ = 10 - 7.5 = 2.5 \text{ gm}$$

9. (D)

Sol. This statement is in accordance to Dalton's Law.

10. (B)

Sol. $\text{NH}_3 + \text{HCl} \longrightarrow \text{NH}_4\text{Cl}$

Dalton's Law is applicable for non-reacting gas.

11. (C)

Sol.

| | | | |
|----------------------------|-----------------|---|------------------|
| | He | : | 0 |
| Number of ratio of atoms | 1 | : | 1 |
| Ratio of mole of atoms | $\frac{1}{N_A}$ | : | $\frac{1}{N_A}$ |
| Ratio of mole of molecules | $\frac{1}{N_A}$ | : | $\frac{1}{3N_A}$ |

$$\text{Now, } \frac{1}{N_A} + \frac{1}{3N_A} = P$$

$$\Rightarrow \frac{4}{3N_A} = P \Rightarrow \frac{1}{N_A} = \frac{3P}{4}$$

If Helium is removed from the vessel,

Let pressure of system be P'

$$\Rightarrow P' = \frac{1}{3N_A} = \frac{1}{3} \times \frac{3P}{4}$$

$$\Rightarrow P' = \frac{P}{4} \text{ or } 0.25 P$$

12. (D)

Sol. Rate of diffusion of gas is inversely proportional to the square root of its molecular weight.

13. (A)

Sol. $\text{rate} \propto \frac{1}{\sqrt{M}}$

14. (C)

Sol. $r \propto \frac{1}{\sqrt{M}}$

15. (D)

Sol. $\text{rate} \propto \frac{1}{\sqrt{M}}$

Increasing order of effusion is ($\text{CO}_2 < \text{O}_2 < \text{NH}_3 < \text{H}_2$)

16. (B)

Sol. As, $\frac{r_1}{r_2} = \sqrt{\frac{M_2}{M_1}}$

\Rightarrow Relative rates of effusion are, $a < c < b$.

17. (B)

Sol. Rate of diffusion of Hydrogen is about

$$\frac{r_{\text{H}_2}}{r_{\text{He}}} = \sqrt{\frac{M_{\text{He}}}{M_{\text{H}_2}}} = \sqrt{2} = 1.4$$

$$\Rightarrow r_{\text{H}_2} = 1.4 \times r_{\text{He}}$$

18. (A)

Sol. $\frac{W_{\text{H}_2}}{W_{\text{O}_2}} = \sqrt{\frac{M_{\text{H}_2}}{M_{\text{O}_2}}}$

$$= \sqrt{\frac{2}{32}} = \sqrt{\frac{1}{16}} = \frac{1}{4}$$

19. (A)

Sol. $\frac{r_{\text{CH}_4}}{r_X} = \sqrt{\frac{M_X}{M_{\text{CH}_4}}}$

$$1 = \sqrt{\frac{M_X}{16}}$$

$$4 \times 16 = M_X$$

$$\Rightarrow M_X = 64 \text{ gm}$$

20. (A)

Sol. $\frac{n'_{\text{He}}}{n'_{\text{CH}_4}} = \frac{4}{1} \times \sqrt{\frac{16}{4}} = 8 : 1$

21. (B)

Sol. $\frac{r_x}{r_y} = 3 = \sqrt{\frac{D_y}{D_x}}$

$$\frac{D_y}{D_x} = \frac{9}{1}$$

$$\Rightarrow D_x : D_y = 1 : 9$$

22. (A)

Sol. $\frac{r_{\text{O}_2}}{r_{\text{H}_2}} = \frac{16 \times 2}{32 \times 2} \sqrt{\frac{2}{32}}$

$$= \frac{1}{2} \times \frac{1}{4} = \frac{1}{8}$$

23. (C)

Sol. $\frac{\left(\frac{n_A}{n_B}\right)_f}{\left(\frac{n_B}{n_B}\right)_i} = \left(\frac{M_B}{M_A}\right)^{n/2}$

$$\frac{3072}{20} \times \frac{1600}{240} = \left(\frac{32}{2}\right)^{n/2}$$

$$(4)^5 = (4)^n$$

$$\Rightarrow n = 5$$

24. (D)

Sol. $P_{\text{(final)}} = \frac{P_1 V_1 + P_2 V_2}{V_T}$

$$= \left(\frac{720 \times 200 + 750 \times 400}{1000} \right) = \left(\frac{444000}{1000} \right)$$

$$= 444 \text{ mm}$$

25. (C)

Sol. $\frac{r_{\text{mix}}}{r_{\text{SO}_2}} = \sqrt{\frac{M_{\text{SO}_2}}{M_{\text{mix}}}}$

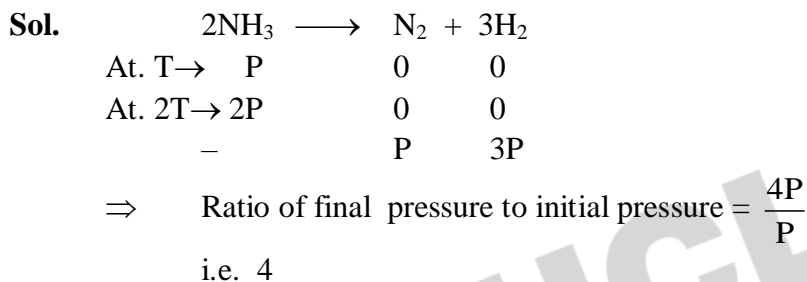
$$2 = \sqrt{\frac{64}{M_{\text{mix}}}}$$

$$\Rightarrow M_{\text{max.}} = 16$$

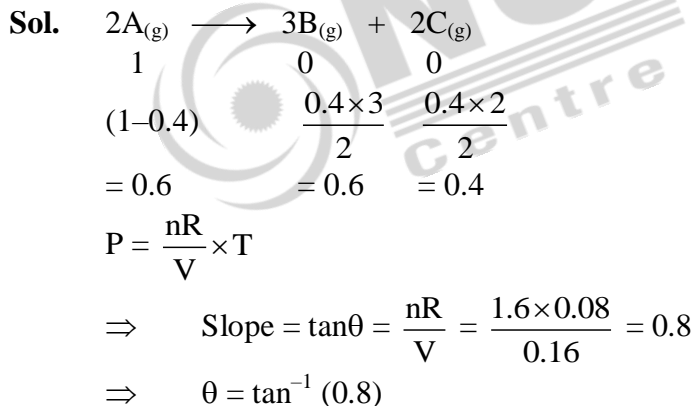
Now, $16 = \frac{17}{1 + \infty}$

$$\Rightarrow \infty = 6.25\%$$

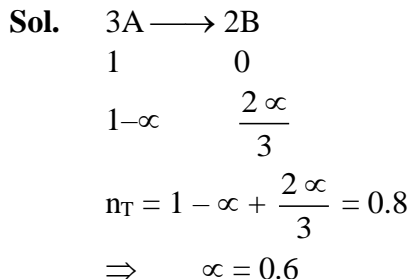
26. (A)



27. (B)



28. (B)



29. (A)

Sol. As $M_{\text{Avg.}}$ remains same

\Rightarrow Total pressure will remain same

30. (A)

Sol.

$$\begin{aligned} U_{\text{m.p.s}} &: U_{\text{Avg}} : U_{\text{r.m.s}} \\ \sqrt{\frac{2RT}{M}} &: \sqrt{\frac{8RT}{\pi M}} : \sqrt{\frac{3RT}{M}} \\ \sqrt{2} &: \sqrt{\frac{8}{\pi}} : \sqrt{3} \\ \text{OR, } 1 &: 1.128 : 1.224 \end{aligned}$$

31. (D)

Sol.

$$\begin{aligned} (U_{\text{avg.}})_X &= 2(U_{\text{avg.}})_Y \\ \left(\sqrt{\frac{8PV}{\pi M}} \right)_X &= 2 \left(\sqrt{\frac{8PV}{\pi M}} \right)_Y \\ \Rightarrow P_X V_X &= 4 \times P_Y V_Y \\ \Rightarrow \frac{P_X}{P_Y} &= \frac{4 \times 2}{1} \\ \Rightarrow P_X &= 8P_Y \end{aligned}$$

32. (A)

Sol. $U_{\text{r.m.s}} \propto \frac{1}{\sqrt{M}}$

33. (D)

Sol.

$$\begin{aligned} U_{\text{r.m.s}} &= \sqrt{\frac{V_1^2 + V_2^2 + V_3^2 + V_4^2}{4}} \\ &= \sqrt{\frac{4 + 9 + 16 + 25}{4}} = \frac{\sqrt{54}}{2} \text{ cm/s} \end{aligned}$$

34. (B)

Sol.

$$\begin{aligned} S &= \sqrt{\frac{(7)^2 \times 4 + 6 \times x^2}{10}} \\ 2S &= \frac{49 \times 4 + 6x^2}{10} \Rightarrow x = 3 \end{aligned}$$

35. (D)

Sol. $\frac{1}{N} \left(\frac{dN}{dU} \right) \propto M$

36. (D)

Sol. $(V_{\text{Avg}})_{\text{N}_2} = 0.3 \text{ m/s}$ at 27°C

$$\sqrt{\frac{8RT}{\pi M}} = 0.3$$

$$\Rightarrow \frac{8R}{\pi M} = \frac{(0.3)^2}{300} \quad \dots(1)$$

$$\text{Now, } \sqrt{\frac{8RT}{\pi M}} = 0.6$$

$$\frac{8R}{\pi M} \times T = 0.6 \times 0.6$$

$$\Rightarrow T = \frac{0.6 \times 0.6 \times 300}{(0.3)^2}$$

$$\Rightarrow T = 1200 \text{ K}$$

37. (B)

$$\text{Sol. } U_{\text{r.m.s}} = \sqrt{\frac{3RT}{M}} = \sqrt{\frac{3PV}{nM}} = \sqrt{\frac{3P}{D}}$$

38. (D)

$$\text{Sol. } U_{\text{r.m.s}} \propto \frac{1}{\sqrt{M}}$$

39. (B)

$$\text{Sol. } (U_{\text{r.m.s}})_T = 2 \times (U_{\text{r.m.s}})_{373\text{K}}$$

$$\Rightarrow \frac{3RT}{M} = 4 \times \frac{3R \times 373}{M}$$

$$\Rightarrow T = 4 \times 373$$

$$\Rightarrow T = 1492 \text{ K}$$

40. (A)

$$\text{Sol. K.E} = \frac{3}{2} RT$$

$$= \frac{3}{2} \times 2 \times 300$$

$$= 900 \text{ cal/mole}$$

41. (B)

$$\text{Sol. K.E} = \frac{3}{2} KT$$

$$= \frac{3}{2} \times 1.3807 \times 10^{-23} \times 298$$

$$= 6.17 \times 10^{-21} \text{ J}$$

42. (C)

Sol. $(K.E.)_{He \text{ at } TK} = (K.E.)_{Ar \text{ at } 400 K}$
 $\Rightarrow \frac{3}{2} \times 0.30 \times R \times T = \frac{3}{2} \times 0.40 \times R \times 400$
 $\Rightarrow T = \frac{1600}{3} = 533 K$

43. (A)

Sol. As, K.E depends on T only
 \Rightarrow It will remain same

44. (B)

Sol. $(U_{m.p.s})_{O_2} = (U_{r.m.s})_{N_2}$
 $\left(\sqrt{\frac{2RT}{M}} \right)_{O_2} = \left(\sqrt{\frac{3RT}{M}} \right)_{N_2}$
 $\frac{2 \times T}{32} = \frac{3 \times 700}{28}$
 $\Rightarrow T = 1200 K$

45. (C)

Sol. K.E depends on Temperature only
 So, K.E. remain same

46. (A)

Sol. As, $N^* = \frac{P}{KT}$
 $= \frac{10^5}{1.38 \times 10^{-23} \times 300}$
 $\Rightarrow N^* = 2.4 \times 10^{25} m^{-3}$

47. (A)

Sol. At. Constant volume,
 $Z_{11} \propto \sqrt{P}$
 \Rightarrow Correct option is (A)

EXERCISE # O-II

1. (A, B)

Sol. Slope of P-T curve gives volume.

2. (A, B)

3. (C, D)

Sol. $K.E \propto T$

4. (D)

5. (A, B, D)

Sol. $r \propto \frac{1}{\sqrt{M}}$

6. (A, B, C, D)

7. (A, C)

Sol. $U_{rms} \propto \sqrt{\frac{T}{M}}$

8. For untainer-1 before opening the value,

$$P = \frac{nRT}{V} = \frac{2 \times 0.082 \times 300}{16.42} = 3 \text{ atm.}$$

Pressure in each compartment is same after opening the value, as total moles remains conserved.

9. $2A(g) \longrightarrow 3B(g) + 2C(g)$

$$P_i \rightarrow \quad 1 \quad \quad 0 \quad \quad 0$$

$$P_f \rightarrow \quad 0.8 \quad \quad \left(\frac{3}{2} \times .2\right) \quad 0.2$$

$$\text{Total final pressure} = (0.8 + 0.3 + 0.2) = 1.3 \text{ atm}$$

\Rightarrow Total pressure increases by 0.3 atm

As, $P_{\text{gas}} > P_{\text{atm.}}$

\Rightarrow difference in mercury level is 22.8 cm or 228 mm.

10. $y = \frac{1}{V^2}$ or $\sqrt{y} = \frac{1}{V}$
 $P = X$ & $P = \text{constant}/V$
 $A \longrightarrow R$ ($X = K\sqrt{y} \Rightarrow y = K^1 x^2$)
 $B \longrightarrow S$ ($V = KT, y = V$ & $\frac{1}{T} = x \therefore y = \frac{K}{x}$)
 $C \longrightarrow P$ ($P = RT; PT = RT^2$ or $y = kx$)
 $D \longrightarrow Q$ ($V = \frac{C}{P} \Rightarrow y = c\sqrt{x}; y^2 = cx$)

11. (B)

Sol. $P.e^{v/2} = nCT$

At $P = 1 \text{ atm}, V = 0$

$$\Rightarrow i.e^0 = 2 \times C \times 500$$

$$\Rightarrow C = \frac{1}{1000}$$

$$\Rightarrow C = 10^{-3} \quad \text{or} \quad 0.001$$

12. (D)

Sol. For P.T. curve, slope = $\frac{nc}{e^{v/2}}$
 $= \frac{2 \times 0.001}{e} = \frac{2}{1000e}$

13. (A)

Sol. $n = \frac{PV}{RT}$
 $= \frac{1 \times 200}{0.0821 \times 200} = 12.18$

As, $P = \frac{nCT}{e^{v/2}}$
 $= \frac{12.18 \times 0.001 \times 821}{e^{200/2}}$
 $= \frac{10}{e^{100}}$

14. $\frac{r_1}{r_2} = \frac{P_1}{P_2} \sqrt{\frac{M_2}{M_1}} = \frac{\ell_1/t}{\ell_2/t}$

$$\frac{\ell_1}{\ell_2} = \frac{1}{x} = \frac{1}{2} \sqrt{\frac{64}{4}}$$

$$x = \frac{1}{2} \text{ m} = 50 \text{ cm}$$

$$15. \quad \frac{r_1}{r_2} = \frac{n_1}{n_2} = \sqrt{\frac{M_2}{M_1}}$$

$$\frac{4/2}{x/32} = \sqrt{\frac{32}{2}}$$

$$\frac{64}{x} = 4$$

$$x = 16$$

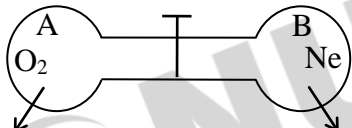
$$16. \quad P V = n R T$$

$$\frac{4.1 \times 3}{300 \times 0.0821} = n_x = 0.5 = n_{He} + n_x$$

$$n_x = 0.1$$

$$\frac{r_1}{r_2} = \frac{n_1}{n_2} = \sqrt{\frac{M_2}{M_1}}$$

$$\frac{0.4}{0.1} = \sqrt{\frac{M}{4}} \quad M = 64$$

$$17. \quad \begin{array}{c} \text{A} \quad \text{B} \\ \text{O}_2 \quad \text{Ne} \end{array}$$


$$P_1 = 950 \text{ mm} \quad P_2 = 900 \text{ mm}$$

$$n_T = n_1 + n_2$$

$$\frac{\frac{910}{760} \times (V_A + V_B)}{R T} = \frac{\frac{950}{760} V_A}{R T} = \frac{\frac{900}{760} V_B}{R T}$$

$$V_B = 4V_A$$

$$18. \quad n_T = \frac{\frac{910}{760} \times \left(\frac{5}{4} \times 304 \right)}{0.08 \times 300}$$

$$= 18.95$$

$$\frac{n_A}{n_B} = \frac{V_A}{V_B} = \frac{1}{4}$$

$$n_B = \frac{4}{5} \times n_T$$

$$n_B = 15.16$$

$$n_A = \frac{1}{5} \times n_T$$

$$= 3.790$$

EXERCISE # JEE-MAINS

1. (1)

Sol. Factual

2. (4)

Sol. $2\text{BCl}_3 + 3\text{H}_2 \longrightarrow 2\text{B} + 6\text{HCl}$

$$\text{mole : } \left(\frac{21.6}{10.8} \right) = 2$$

$$n_{\text{H}_2} = 3$$

$$\begin{aligned} \Rightarrow \text{Volume of H}_2 \text{ at 273K \& 1 atm} \\ = 3 \times 22.4 \\ = 67.2 \text{ L} \end{aligned}$$

3. (3)

Sol. $K.E \propto T$

$$\Rightarrow \frac{(K.E)_{40^\circ\text{C}}}{(L.E)_{20^\circ\text{C}}} = \frac{313}{293}$$

4. (3)

Sol. $P \propto n$

$$\Rightarrow \frac{P_{\text{CH}_4}}{P_{\text{O}_2}} = \frac{w \times 32}{16 \times w} = \frac{2}{1}$$

 Fraction of total pressure exerted by O_2 is $\frac{1}{3}$

5. (4)

Sol. $u \propto \sqrt{T}$

6. (3)

Sol. $u > v > a$

7. (3)

Sol. As, V remains constant

$$n \propto \frac{1}{T}$$

$$\text{i.e. } n_1 T_1 = n_2 T_2$$

$$\Rightarrow n_1 \times 300 = \frac{3}{5} n_1 \times T_2$$

$$\Rightarrow T_2 = \frac{300 \times 5}{3}$$

$$\Rightarrow T_2 = 500 \text{ K}$$

8. (3)

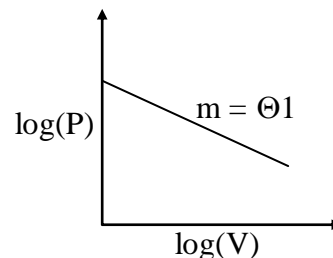
Sol. As $P = \frac{nRT}{V}$

$$\Rightarrow \log(P) = \log(nRT) + \log\left(\frac{1}{V}\right)$$

or, $\log(P) = \log(nRT) - \log(V)$

For, 1 mole ideal gas,

$$\log(P) = \log(RT) - \log(V)$$



9. (1)

Sol. $\sqrt{2} : \sqrt{\frac{8}{\pi}} : \sqrt{3}$

10. (1)

Sol. Factual

11. (1)

Sol. $U_{rms} = \sqrt{\frac{3RT}{m}}$

i.e. $U_{rms} \propto \sqrt{T}$

$$\frac{5 \times 10^4}{10 \times 10^4} = \sqrt{\frac{T_1}{T_2}}$$

$$\frac{1}{4} = \frac{T_1}{T_2}$$

$$\Rightarrow (T_2 = 4T_1)$$

12. (3)

Sol. $U_{mps} = C = \sqrt{\frac{2RT}{m}}$

$$V_{Avg} = \bar{C} = \sqrt{\frac{8RT}{\pi m}} \quad \& \quad U_{rms} = C = \sqrt{\frac{3RT}{m}}$$

$$\Rightarrow C : \bar{C} : C = 1 : 1.128 : 1.225$$

13. (4)

| Sol. | Element | % (by mass) | relation no. of moles | Simplest atomic ratio |
|------|---------|-------------|--------------------------|-------------------------|
| | N | 87.5 | $\frac{87.5}{14} = 6.25$ | $\frac{6.25}{6.25} = 1$ |
| | H | 12.5 | $\frac{12.5}{1} = 12.5$ | $\frac{12.5}{6.25} = 2$ |

Empirical formula = NH_2

Molar mass of compound = 32

As, molecular formula = $n \times$ empirical formula

$$\Rightarrow n = \frac{32}{16} = 2$$

$$\Rightarrow (\text{m.f} = \text{N}_2\text{H}_4)$$

14. (1)

Sol. $P_1V_1 = P_2V_2$

$$840 \times 750 = 360 \times V_2$$

$$\Rightarrow V_2 = \frac{840 \times 750}{360}$$

$$\Rightarrow V_2 = 1750 \text{ ml} \quad \text{or} \quad 1.750 \text{ L}$$

15. (4)

Sol. $(U_{\text{rms}})_{\text{O}_2} = (U_{\text{rms}})_{\text{He}}$

$$\sqrt{\frac{3R \times T}{32}} = \sqrt{\frac{3R \times 300}{4}}$$

$$\Rightarrow \frac{T}{32} = \frac{300}{4}$$

$$\Rightarrow T = \frac{32 \times 300}{4}$$

$$\Rightarrow T = 2400 \text{ K}$$

16. (3) Factual

17. $V_{\text{rms}} \times \sqrt{\frac{T}{M}}$

T is doubled

M is lalfed

$$V'_{\text{rms}} = \sqrt{4} V_{\text{rms}}$$

$$V'_{\text{rms}} = 2 V_{\text{rms}}$$

$$= 2 \mu$$

18. (4)

Sol. $(n_i)_T = (n_f)_T$

$$\frac{P_1 V}{RT_1} + \frac{P_1 V}{RT_1} = \frac{P_f V}{RT_1} + \frac{P_f V}{RT_2}$$

$$\frac{2P_1 V}{RT_1} = \frac{P_f V}{R} \left(\frac{1}{T_1} + \frac{1}{T_2} \right)$$

$$\Rightarrow P_f = 2P_1 \left(\frac{T_2}{T_1 + T_2} \right)$$

19. (2)

Sol. $V_1 = V_2$, $n_2 = \frac{3}{5} n_1$

$$n_1 T_1 = n_2 T_2$$

$$n_1 (300) = n_2 (T_2)$$

$$300 = \frac{3}{5} T_2$$

$$T_2 = 500 \text{ K}$$

20. (3)

Sol. $V_A = 2V_B$

$$Z_A = 3Z_B$$

$$\frac{Z_A}{Z_B} = \frac{P_A V_A}{P_B V_B}$$

$$3 = \frac{P_A}{P_B} \times 2 \Rightarrow 2P_A = 3P_B$$

21. (3)

Sol. $n_A = 0.5$ $n_B = x$ mole

For the container

$$P = 200 \text{ Pa}$$

$$V = 10 \text{ m}^3$$

$$T = 1000 \text{ K}$$

$$P V = n R T$$

$$200 \times 10 = (0.5 + x) R \times 1000$$

$$0.5 + x = \frac{2}{R}$$

$$x = \frac{2}{R} - 0.5 \Rightarrow \frac{4 - R}{2R}$$

22. (4)

Sol. V_{MPS} is proportional to $\sqrt{\frac{T}{M}}$

EXERCISE # JEE-ADVANCED

1. $n_{\text{He}} = \frac{.4}{4} = 0.1$

$n_{\text{O}_2} = \frac{1.6}{32} = 0.05$

$n_{\text{N}_2} = \frac{1.4}{28} = 0.05$

$P_T = \frac{0.2 \times 0.0821 \times 300}{10}$

$P_T = 0.492 \text{ atm}$

$P_{\text{He}} = \frac{0.1}{0.2} \times 0.492$

$\Rightarrow P_{\text{He}} = 0.246 \text{ atm}$

2. (C)

Sol. According to Graham's Law,

$$\frac{r_A}{r_B} \propto \frac{P_A}{P_B} \left(\frac{M_B}{M_A} \right)^{1/2}$$

3. Mass of liquid = 148 – 50 = 98g

Volume of liquid = $\frac{98}{0.98} = 100 \text{ ml} = \text{volume of flask}$

Mass of gas = 50.5 – 50 = 0.50 g

Using, $PV = nRT$, we get

$M = \frac{wRT}{PV} = \frac{0.5 \times 0.082 \times 300}{1 \times 0.1}$

$\Rightarrow M = 123 \text{ g mol}^{-1}$

4. For a fixed amount of gas at constant volume,

$P \propto T$

$\frac{1}{1.1} = \frac{T}{T+10}$

$\Rightarrow T = 100 \text{ K} \quad \text{or} \quad \ominus 173^\circ\text{C}$

Also, $V = \frac{nRT}{P} = \frac{12}{120} \times \frac{0.0821 \times 100}{1}$

$\Rightarrow V = 0.82 \text{ L}$

5. For the same amount of gas being diffused,

$\frac{r_1}{r_2} = \frac{t_2}{t_1} = \frac{P_1}{P_2} \sqrt{\frac{M_2}{M_1}}$

$$\frac{57}{38} = \frac{0.8}{1.6} \sqrt{\frac{M_2}{28}}$$

$$\Rightarrow M_2 = 252 \text{ g mol}^{-1}$$

The formula of compound can be considered to be XeF_n

$$\Rightarrow 131 + 19n = 252$$

$$\Rightarrow n = 6$$

\Rightarrow The unknown gas is XeF_6 .

6. (C)

Sol. $(U_{\text{rms}})_{\text{H}_2} = \sqrt{7} (U_{\text{rms}})_{\text{N}_2}$

$$\frac{T_{(\text{H}_2)}}{2} = 7 \times \frac{T_{(\text{N}_2)}}{28}$$

$$\Rightarrow T_{(\text{H}_2)} = \frac{T_{(\text{N}_2)}}{2}$$

$$\Rightarrow T_{(\text{H}_2)} < T_{(\text{N}_2)}$$

7. **Statement-1:** False, Besides amount, pressure also depends on volume.

Statement-2: True as $u_{\text{rms}} \propto \sqrt{T}$

8. (D)

Sol. $U_{\text{rms}} = \sqrt{\frac{3RT}{m}} = \sqrt{\frac{3P}{d}}$

$$\Rightarrow U_{\text{rms}} \propto \left(\frac{1}{d}\right)^{1/2}$$

9. For an ideal gas, $V_m = 22.4$ lit at 273 K & 1 atm.

In option (C), at the initial point, the volume is 22.4 lit. as required by the ideal gas equation &

$\left(\frac{V}{T}\right)$ have the same value at both initial & final points.

10. $\frac{V_{\text{Avg}}}{U_{\text{rms}}} = \sqrt{\frac{8RT}{\pi m}} \div \sqrt{\frac{3RT}{m}}$

$$= \sqrt{\frac{8}{3\pi}}$$

$$\Rightarrow U_{\text{rms}} = \sqrt{\frac{3\pi}{8}} \times 400$$

$$= \sqrt{\frac{3 \times 3.14}{8}} \times 400$$

$$\Rightarrow U_{\text{rms}} = 434.17 \text{ m/s.}$$

11. $U_{\text{rms}} = \sqrt{\frac{3RT}{M}} \dots\dots(1)$

The average kinetic energy (E) of the gas is given by the following expression.

$$E = \frac{3}{2} RT$$

$$RT = \frac{2}{3} E \dots\dots(2)$$

Substitute (2) into (1)

$$U_{\text{rms}} = \sqrt{\frac{3 \times \frac{2}{3} E}{M}}$$

$$U_{\text{rms}} = \sqrt{\frac{2E}{M}}$$

12. (B)

Sol. $\frac{r_{\text{He}}}{r_{\text{CH}_4}} = \sqrt{\frac{16}{4}} = 2$

13. $(U_{\text{rms}})_x \text{ at } 400 \text{ K} = (U_{\text{rms}})_y \text{ at } 60 \text{ K}$

$$\Rightarrow \sqrt{\frac{3R \times 400}{40}} = \sqrt{\frac{2R \times 60}{m_y}}$$

$$\Rightarrow \frac{3 \times 400}{40} = \frac{2 \times 60}{m_y}$$

$$\Rightarrow m_y = \frac{2 \times 60 \times 40}{3 \times 400}$$

$$\Rightarrow m_y = 4$$

14. Partial pressure of He = $1 - 0.68 = 0.32$

$$V = \frac{n_{\text{He}} \cdot R_T}{P_{\text{He}}}$$

$$= \frac{0.1 \times 0.082 \times 273}{0.32}$$

$$\Rightarrow V = 7 \text{ lit.}$$

\Rightarrow Volume of container = volume of He.

15. (C)

Sol. Let distance covered by X is d, then distance covered by Y is (24 - d)

If r_x & r_y are the rate of diffusion of gases X & Y

$$\frac{r_x}{r_y} = \frac{d}{24-d} = \sqrt{\frac{40}{10}} = 2$$

$$\Rightarrow d = 16 \text{ cm}$$

16. The experimental value of d is found to be smaller than the estimated value obtained using Graham's law. This is due to increased collision frequency of Y with the inert gas as compared to that of X with the inert gas. (\because As, the collision frequency increases, the molecular speed decreases much more than expected.)

17. (DC) Diffusion coefficient $\propto \lambda$ (mean free path) $\propto U_{\text{mean}}$

Thus (DC) $\propto \lambda U_{\text{mean}}$

$$\text{But } \lambda = \frac{RT}{\sqrt{2} N_0 \sigma p} \Rightarrow \lambda \propto \frac{T}{p}$$

$$\text{and } U_{\text{mean}} = \sqrt{\frac{8RT}{\pi M}}$$

$$U_{\text{mean}} \propto \sqrt{T}$$

$$\therefore \text{DC} \propto \frac{(T)^{3/2}}{p}$$

$$\begin{aligned} \frac{(\text{DC})_2}{(\text{DC})_1} (x) &= \left(\frac{p_1}{p_2} \right) \left(\frac{T_2}{T_1} \right)^{3/2} = \left(\frac{p_1}{2p_1} \right) \left(\frac{4T_1}{T_1} \right)^{3/2} \\ &= \left(\frac{1}{2} \right) (8) = 4 \end{aligned}$$

18. Finally, $P_A = P_B$ & $T_A = T_B$

$$\text{So, } \frac{n_A}{n_B} = \frac{V_A}{V_B}$$

$$\frac{5}{\frac{400R}{3}} = \frac{V_A}{300R}$$

$$\Rightarrow \frac{V_A}{V_B} = \frac{5}{4} \Rightarrow V_A = \frac{5}{9} \times 4 = \frac{20}{9} = 2.22$$

19. The root mean square speed (U_{rms}) and average translational kinetic energy (ϵ_{av}) has following relation with temperature and molecular mass

$$\epsilon_{\text{av}} = \frac{3}{2} RT, U_{\text{rms}} = \sqrt{\frac{3RT}{M}} \text{ and } U_{\text{rms}} \propto \frac{1}{\sqrt{M}}$$

$\therefore \epsilon_{\text{av}}$ doesn't depend on its molecular mass.

According to the relation given above ϵ_{av} gets doubled when the temperature is increased 2 times. Thus option B is incorrect.