# **CUED - Engineering Tripos Part IIB 2021-2022**

# **Module Coursework**

| Modul                                     | e   | 4A7              | Title of report                            | Aviation an    | nd the Environment Coursework |                                    |      |                                |              |         |                   |  |  |
|---|---|------------------|--|----------------|-------------------------------|------------------------------------|------|--------------------------------|--------------|---------|-------------------|--|--|
| Data a                                    | ه ندمه دا د   | to do 07/12/202  | <b>)</b> 1                                 |                |                               |                                    | I    | Assessment for this module is  | 100% cour    | rsework |                   |  |  |
| Date submitted: 07/12/2021                |   |                  |  |                |                               | of which this assignment forms 50% |      |                                |              |         |                   |  |  |
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| Candidate number: 5726A                   |   |                  |  |                |                               | Name:                              |      |                                | College:     |         |                   |  |  |
|   |   | to the stude     |  |                |                               |                                    |      |                                | Very<br>good | Good    | Needs<br>improvmt |  |  |
|   |   |                  | ntity of content:<br>ed all aspects of the | lab? Has the a | ana                           | lysis beer                         | n ca | rried out thoroughly?          |              |         |                   |  |  |
| C   | Correctness, quality of content Is the data correct? Is the analysis of the data correct? Are the conclusions correct?                            |                  |  |                |                               |                                    |      |                                |              |         |                   |  |  |
| C<br>O<br>N<br>T<br>E<br>N<br>T           | Depth of understanding, quality of discussion  Does the report show a good technical understanding? Have all the relevant conclusions been drawn? |                  |  |                |                               |                                    |      |                                |              |         |                   |  |  |
|   | Com   | ments:           |  |                |                               |                                    |      |                                |              |         |                   |  |  |
| P   | Atter   | ntion to detail, | typesetting and ty                         | pographical e  | rro                           | ors                                |      |                                |              |         |                   |  |  |
| R   |   |                  |  |                |                               |                                    | fere | nces presented professionally? |              |         |                   |  |  |
| E<br>S<br>E<br>N<br>T<br>A<br>T<br>I<br>O | Com   | ments:           |  |                |                               |                                    |      |                                |              |         |                   |  |  |

Marker: Date:

# Aviation and the Environment Coursework

CCN: 5726A 08/12/2021

## 1 Summary

Aircraft engines and their cruise operating conditions have been optimised to maximise commercial profits which have led to some focus on fuel efficiency but not on their environmental impacts. This coursework asks the question: How could the environmental impact be improved by operating aircraft differently? A code is developed to investigate effects of varying cruise altitude and overall pressure ratio (OPR) to help answer this question. Other limits on operating conditions are considered and the need to compromise between cost (fuel burn) and environmental impacts is discussed.

## 2 Model

This coursework was carried out using Python 3.7. The full script can be found in the Appendix. The atmosphere is modelled with the International Standard Atmosphere (ISA) conditions:

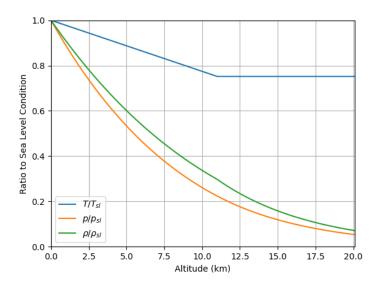


Figure 1: ISA conditions at different altitudes, plotted with matplotlib

A look-up table was created to allow the code to get atmospheric conditions at any altitude. Next, basic reference data of the aircraft and engine were set:

Table 1: Model Reference Data

| Aircraft                  |             | Engine  |        |  |  |
|---------------------------|-------------|---|--------|--|--|
| Number of Passengers:     | 240         | Temperature Ratio $\theta$ :                      | 6      |  |  |
| Range:                    | 12000 km    | Turbine, Compressor Efficiencies $\eta_t, \eta_c$ | 0.9    |  |  |
| Payload Mass $w_p$ :      | 40 tonnes   | Fan Pressure Ratio FPR:                           | 1.45   |  |  |
| Empty Mass $w_e$ :        | 106 tonnes  | Fan Efficiency $\eta_f$ :                         | 0.92   |  |  |
| Initial Fuel Mass $w_f$ : | 74 tonnes   | Transfer Efficiency $\eta_{tr}$ :                 | 0.9    |  |  |
| Take Off Mass $w_{TO}$ :  | 220 tonnes  | Parabolic drag law constants $K1$ :               | 0.0125 |  |  |
| Wing Area $S$ :           | $315 \ m^2$ | Parabolic drag law constants $K2$ :               | 0.0446 |  |  |

### 2.1 Multiple Staged Flight

The flight is split into 10 stages, with all calculated quantities being constant within each stage. Sequence of calculated values are summarised (detailed calculations in Appendix):

Optimum Equivalent Air Speed (EAS)  $\rightarrow$  Actual EAS  $\rightarrow$  True Air Speed (TAS)  $\rightarrow$  Aircraft Mach  $\rightarrow$  Jet Mach  $\rightarrow$  Jet Temperature  $\rightarrow$  Propulsive Efficiency  $\rightarrow$  L/D  $\rightarrow$  Range Parameter H  $\rightarrow$  New Weight & Fuel Burnt  $\rightarrow$  Emission Indices ( $EI_{CO_2}$  &  $EI_{NO_X}$ )  $\rightarrow$  Total Emissions per stage

After each stage has been iterated, the total fuel burnt and emissions for both Carbon Dioxide  $(CO_2)$  and Nitrogen Oxides  $(NO_X)$  are summed up to calculate the overall fuel burnt per passenger-km and emissions per passenger-km. These are the most important quantities that are compared when varying parameters.

At a flight of altitude = 9.5km and OPR = 45, the variation of Mach numbers and emissions during the whole flight can be visualised:

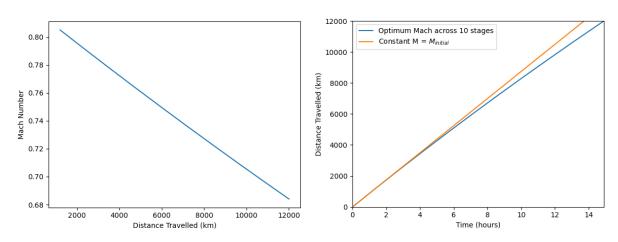


Figure (2a) Mach number during flight

Figure (2b) x-t diagram of the whole flight

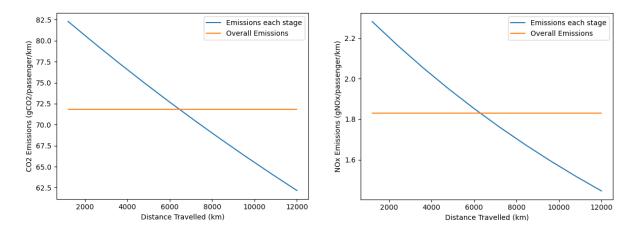


Figure 3: Emissions / pass-km for  $CO_2$  and  $NO_X$ 

Because the altitude and optimum L/D are fixed, the velocity and Mach number decrease as fuel is burnt. In Figure 2a, the Mach number almost decreases linearly. This decrease lengthens the flight duration compared to if the Mach number was kept constant at the initial speed. This can be seen in Figure 2b, where the flight duration increases from 13.6 to 14.8 hours.

This optimising of flight speed leads to a decrease in both  $CO_2$  and  $NO_X$  emissions per passenger-km. In Figure 3, both emissions decrease almost linearly relative to the overall emission per passenger-km. This is evidence for how shorter journeys have a lower emission per passenger-km, because less fuel needs to be carried, leading to lower optimum Mach numbers and hence emissions.

#### 2.2 Model Limitations

As weight decreases due to fuel burn, to keep the lift coefficient  $(C_L)$  constant the velocity or density must decrease. The latter can be done by flying at higher altitudes. In this model, each flight has a fixed cruise altitude and an decreasing flight speed. Whereas in practice flight speed is fixed with an increasing cruise altitude, known as 'cruise climb'.

Secondly, the calculations for emissions do not take into account 'k' which adjusts the fuel burn equation for the initial take off and climb. However, this is negligible as k is typically 1.5% for long journeys.

Lastly, this model ignores the effects of transonic drag rise, such as buffeting and shock-induced separations, in the optimum velocity. A check has been implemented to print out a warning if Mach exceeds 0.85, which it can be seen later this occurs for some higher cruise altitudes. This must be considered when analysing the results.

## 3 Effects of Cruise Altitude

Although in the model cruise altitude is fixed for each flight, it can be varied for different flights. Altitudes from 8km to 12.5km are investigated, with OPR fixed at 45.

#### 3.1 Fuel Burnt

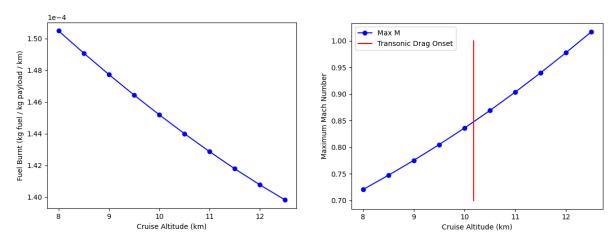


Figure (4a) Overall fuel burnt

Figure (4b) Maximum Mach number

Figure 4a suggests that the higher the cruise altitude the better the fuel economy. However, the Mach number also increases due to a lower density and a fixed  $C_L$ . Figure 4b shows that the maximum Mach reaches 0.85 at an altitude of 10.2km, where the transonic drag becomes significant. This implies the optimum altitude for fuel economy is just beyond 10.2km, where the drawbacks of transonic drag outweigh the decrease in fuel burnt. This agrees with practice, which places this optimum height at 35000ft, or 10.8km.

One might make the assumption that lower fuel burnt means lower  $CO_2$  and  $NO_X$  emissions. However, not only does altitude affect the atmospheric temperature, hence  $T_{03}$  and the  $NO_X$  emission index  $(EI_{NO_X})$ , but more significantly the Global Warming Potential (GWP) also scales with height.

## 3.2 Global Warming Potential

GWP describes the relative global warming impacts of 1 tonne of a greenhouse gas relative to 1 tonne of  $CO_2$ . Svennson et al. (2004) quantified the GWP of  $NO_X$  for varying altitudes. Figure 5 shows that the impacts of  $NO_X$  are significant around h = 8km to 12km, 50-60 times larger than  $CO_2$ . However, this is the impacts of the same mass of gas, in our analysis it can be seen that the amount of  $NO_X$  produced is also a magnitude smaller than  $CO_2$ .

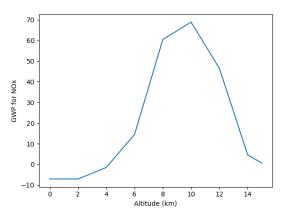


Figure 5: Svennson et al.'s GWP of  $NO_X$  relative to  $CO_2$ 

#### 3.3 Emissions and GWP

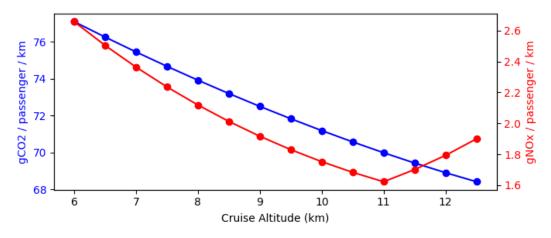


Figure 6: Emissions per passenger-km against altitude

Figure 6 shows that increasing altitudes decreases both gases' emissions but up to 11km for  $NO_X$ .  $CO_2$  follows the same trend as fuel burnt because  $EI_{CO_2}$  is constant at  $3088gCO_2/kgfuel$ . Above 11km the atmospheric temperature is constant, which with an increasing velocity means  $T_{02}$ ,  $T_{03}$  and  $EI_{NO_X}$  all increase. Below 11km the lower temperature outweighs the higher velocity, leading to an overall lower emission. This explains the discontinuity at 11km. To understand the full impact of these emissions, the GWP from Figure 5 is multiplied to the  $NO_X$  emissions:

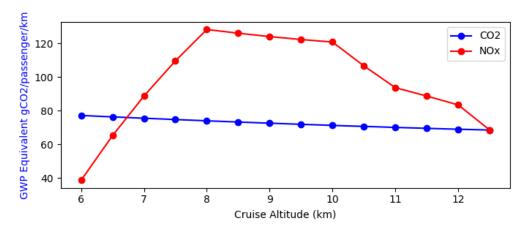


Figure 7: GWP Equivalent  $gCO_2/passenger - km$ 

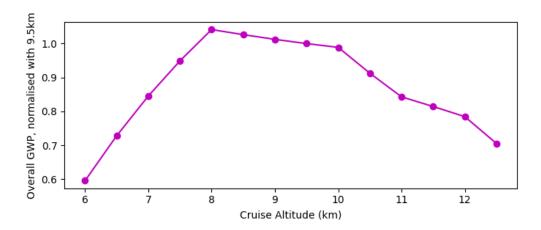


Figure 8: Overall GWP normalised with h = 9.5km

The GWP of both emissions are summed up in Figure 8, where it is normalised with the value at 9.5km. It can be seen that the global warming effects are the highest around 8-10km, dropping rapidly on either side. This is due to the GWP of  $NO_X$  (Figure 5) being the more dominating factor. The high levels of emissions at low altitude (and later increasing  $NO_X$  past 11km) are outweighed by the negligible relative global warming effects at these altitudes. Ideally the cruise altitude should be very low or very high, but limitations of transonic drag and minimum altitude apply, which will be discussed in 5.1.

# 4 Effects of Engine Overall Pressure Ratio

OPR from 20 to 55 are investigated, with cruise altitude fixed at 9.5km.

#### 4.1 Fuel Burnt

The cycle efficiency increases as OPR increases, leading to a decreasing overall fuel burnt. This decrease levels off at OPR = 55 as seen in Figure 10. The optimum OPR for fuel economy is at the highest OPR possible, limited by current technology (discussed later).

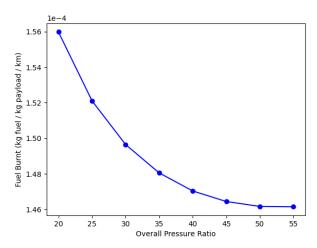


Figure 9: Overall fuel burnt

### 4.2 Emissions and GWP

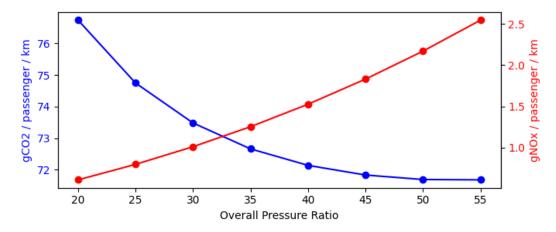


Figure 10: Emissions per passenger-km against OPR

The  $CO_2$  emissions follow the same trend as fuel burnt because  $EI_{CO_2}$  is constant at  $3088gCO_2/kgfuel$ . The  $NO_X$  emissions have an opposite trend which increases as OPR increases. This is a result of a higher compressor exit temperature, hence  $T_{03}$  and  $EI_{NO_X}$ . The higher  $EI_{NO_X}$  exceeds the lower fuel burnt. To understand the full impact of these emissions, a GWP = 66.8 at 9.5km from Figure 5 is multiplied to  $NO_X$  emissions:

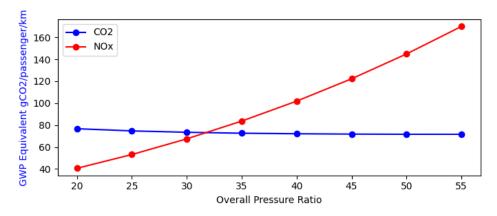


Figure 11: GWP equivalent  $gCO_2$ /passenger-km

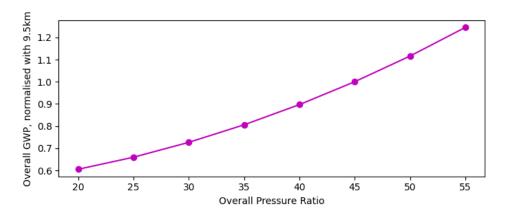


Figure 12: Overall GWP normalised with OPR=45

Combining the global warming effects of both gases shows that the overall effects are dominated by the  $NO_X$  at high OPR. In Figure 12 the lower the OPR, the lower the overall global warming impacts the emissions have. This concludes that the optimum OPR for the environment is at the lowest OPR possible. However, this contradicts the optimum OPR for fuel economy, and this will be discussed in the next section. Moreover, the altitude was set at 9.5km, where the GWP of  $NO_X$  is significant. Therefore, it is worthwhile to run the same model for all altitudes and OPR.

# 5 Optimum Operating Points

By running the program for altitudes from 6 - 13.5km and OPR from 10 - 55, contours for the overall global warming potential and fuel burnt are visualised. This allows the best operating points to be identified. This will show what is best for the environment versus what is best in terms fuel burnt and hence cost.

#### 5.1 The Environment

Figure 13 shows that the best operational points for the environment lie in regions of low OPR, at very high or very low altitudes. However, the maximum altitude is limited by the onset of transonic wave drag, which occurs at around 10.8km as discussed in section 3.1. Above this altitude the extra emissions due to transonic drag starts to dominate the lower GWP due to altitude. Secondly, the minimum altitude is limited by mountain ranges, for example the Himalayan mountain ranges can reach up to 9km. This lower limit means the GWP at 9km is greater than the GWP at the upper limit of 10.8km. The minimum OPR is limited by the net work output, or thrust, the engine produces. For temperature ratio of  $\theta = 6$ , the non-dimensionalised specific power drops abruptly below OPR = 15. To conclude, the optimum operating condition to minimise overall global warming effects: OPR = 15 and OPR = 1

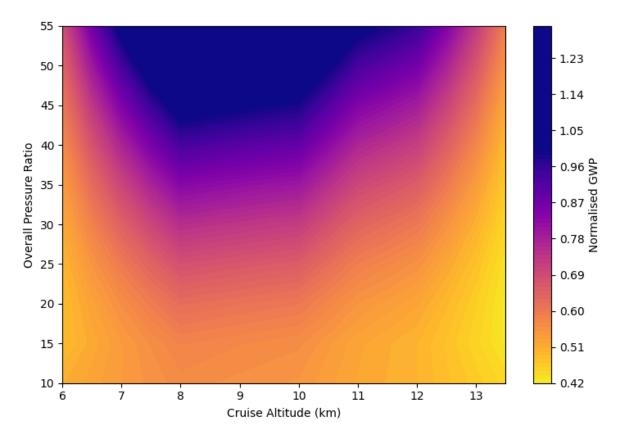


Figure 13: Contour of overall GWP, normalised with h = 9.5km, OPR = 45

However, for flight paths that do not cross high mountain ranges, it is also worth operating at low altitudes for a similar reduced GWP. This is especially applicable to short flights where the relative fuel burn due to climbing to high altitudes becomes significant.

#### 5.2 The Costs

The operating condition found in the previous section assumes airliners have the environment's best interests in mind. However, fuel burnt is directly related to operating costs. A contour is plotted for the overall fuel burnt in Figure 14. This shows the optimum operating condition for fuel economy is at the highest altitude and OPR possible. The maximum altitude is once again limited by transonic drag, but now the maximum OPR is limited by the material's thermal properties and number of compressor stages required. This places the limit at 55-60.

With this in mind, airliners must compromise between mitigating environmental impacts by flying at low OPR, and minimising costs by flying at high OPR. At the moment the focus is on the latter, hence the development of high OPR engines, but with the right governmental and societal shift airliners could easily fly at lower OPR in favour of the environment. The optimum altitude for environmental and costs is both at the highest altitude allowed by the onset of transonic wave drag.

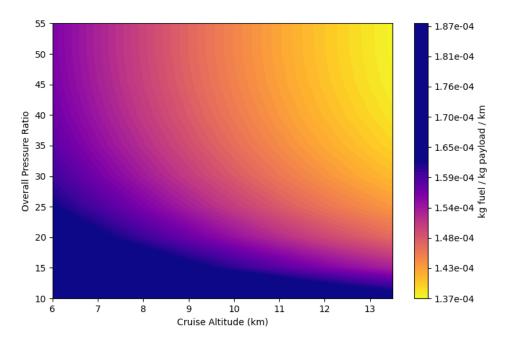


Figure 14: Contour of overall fuel burnt, normalised with h=9.5km, OPR=45

### 5.3 Other Operating Conditions and Technology

Other conditions such as temperature ratio  $\theta$  and using 'short hops' for long flights could also be utilised to mitigate global warming effects. The latter was seen briefly in Figure 2a and Figure 3, where shorter journeys reduce fuel burnt and emissions significantly. Technological advancements to improve various efficiencies in the engine and propeller, as well as aerodynamic designs to increase L/D, could also contribute to reducing emissions. Lastly, alternative fuels such as hydrogen and electricity are also means to reduce GWP.

## 6 Conclusion

A code was developed in Python to analyse the  $CO_2$  and  $NO_X$  emissions as well as their relative global warming impacts for various cruise altitudes and OPR. Each flight had a fixed altitude, leading to an increasing Mach and decreasing emissions throughout the flight. Flying at higher altitudes decreased the amount of fuel burnt and emissions. Due to significant GWP of  $NO_X$  at mid-range cruise altitudes, the overall GWP for  $CO_2$  and  $NO_X$  were lowest outside 8-10km. Flying at higher OPR decreased the amount of fuel burnt but levelled off at 50.  $CO_2$  and  $NO_X$  had opposite emission trends with OPR, but  $NO_X$  dominated in terms of overall GWP. A contour of overall GWP was plotted for all altitudes and OPR, the optimum operating condition was at OPR = 15 and altitude = 11km. Maximum and minimum altitudes are limited by transonic wave drag and mountain ranges respectively, and minimum OPR limited by thrust required. A compromise between the environment (low OPR) and cost (high OPR) must be made.

# 7 Appendix

### 7.1 Detailed Calculations in Python Iteration

i. Optimum Equivalent Air Speed (EAS) = 
$$V_e^* = \left[\frac{mg}{0.5\rho_0 S}\right]^{0.5} \left[\frac{K_2}{K_1}\right]^{0.25}$$

ii. Actual EAS = 
$$V_e = V_e^* \times \nu$$
 , where  $\nu = 1$  is the selected speed ratio

iii. True Air Speed (TAS) = 
$$V = V_e \sqrt{\rho_0/\rho_a}$$

iv. Mach Number M = V/a, where a is the local speed of sound

v. Jet Mach 
$$M_j^2 = \frac{2}{\gamma - 1} \left[ (FPR \times p_{02}/p_a)^{(\gamma - 1)/\gamma} - 1 \right]$$

vi. Jet Temperature 
$$\frac{T_j}{T_a} = \frac{1+0.5(\gamma-1)M^2}{1+0.5(\gamma-1)M_j^2}FPR^{(\gamma-1)/(\gamma\,\eta_f)}$$

vii. Propulsive Efficiency 
$$\eta_{prop}=2\left(1+M_{j}/M\sqrt{T_{j}/T_{a}}\right)^{-1}$$

viii. 
$$L/D = \left(\sqrt{K_1 K_2} \left(\nu^2 + 1/\nu^2\right)\right)^{-1}$$

ix. Range Parameter 
$$H = \eta_{prop} \, \eta_{cycle} \, \eta_{tr} \, L/D \times LCV/g$$

x. New Weight 
$$w_{end} = w_{start} e^{s_{stage}/H}$$

xi. 
$$EI_{CO_2} = 3088, EI_{NO_X} = 0.011445 e^{0.006766 \times T_{03}}, \text{ where } T_{03} = T_{02} \times \left(1 + \left(OPR^{(\gamma-1)/\gamma}/\eta_c\right)\right)$$

xii. Total Emissions for this stage =  $EI \times Fuel\ Burnt$ 

## 7.2 Full Python Script

NOTE: Change h and OPR in lines 82-85, then comment/uncomment corresponding plots starting at lines 192 (vary h) 264 (vary OPR) 296 (contour)

```
1 import numpy as np
 2 import math
 3 import matplotlib
 4 import matplotlib.pyplot as plt
 6 # Aircraft parameters
7 \text{ Np} = 240
                           # max number of passengers
 8 range max = 12000
                        # range at max payload (km)
 9 \text{ wp} = 40*1000
                           # max payload weight (kg)
10 we = 106*1000
                           # empty weight
11 wf = 74*1000
                   # fuel capacity at max payload
12 wto = 220*1000
                         # max take off weight
13 V = 256
                           # cruise TAS
14 M = 0.85
                           # cruise mach number
15 h_initial = 9.5
                           # initial cruise altitude (km)
16 LD_optimum = 21
                            # cruise L/D
17 betastar = 1/LD optimum
                            # 1/(L/D)
18 S = 315
                           # wing area (m^2)
19 v = 1.0
                           # speed ratio = Ve/Ve*
20
21 # Engine parameters
22 OPR_initial = 45
                           # overall pressure ratio = p03/p02
23 theta = 6
                   # turbine entry temp. ratio = T04/T02
24 nc = nt = 0.9 # turbine and compressor efficiencies
                   # fan pressure ratio
25 FPR = 1.45
26 \text{ nf} = 0.92
                   # fan efficiency
27 \text{ ntr} = 0.9
                   # transfer efficiency
28 \text{ cp} = 1005
29 \text{ gamma} = 1.4
30 fga = (gamma-1)/gamma
31 LCV = 42.7*10**6
                      # keroscene
32
33 # Modelling constants
34 k = 0.015
                           # Breguet range equation fuel burn offset
35 c1,c2 = 0.3, 1.0
                           # aircraft weight correlation
36 K1, K2 = 0.0125, 0.0446
                           # parabolic drag low constants
37
38 #**************
39 # ISA conditions
40 \text{ Tsl} = 288.15
41 psl = 101325
42 \text{ rhosl} = 1.225
43 \text{ asl} = 340.3
44 dh = 0.1 # step size in height
45
46 hlow = np.arange(0,11+dh,dh)
47 Tlow = Tsl - 6.5*hlow
48 plow = psl * (Tlow/Tsl)**5.256
49 rholow = rhosl * (Tlow/Tsl)**4.256
```

```
\overline{50} alow = asl * (Tlow/Tsl)**0.5
51 hhigh = np.arange(11+dh, 20+dh, dh)
52 Thigh = np.array([216.65]*(len(hhigh)))
53 phigh = plow[-1]*np.exp(-0.1577*(hhigh-11))
54 rhohigh = rholow[-1]*np.exp(-0.1577*(hhigh-11))
55 ahigh = asl * (Thigh/Tsl)**0.5
56
57 hlist = np.concatenate((hlow,hhigh))
58 Tlist = np.concatenate((Tlow,Thigh))
59 plist = np.concatenate((plow,phigh))
60 rholist = np.concatenate((rholow, rhohigh))
61 alist = np.concatenate((alow,ahigh))
62
63 # print(T[np.where(h==11)])
64
65 def find_nearest(array, value):
       idx = (np.abs(array - value)).argmin()
66
67
       if idx==0 or idx==len(hlist)-1:
68
           print("Value lookup out of range!")
       return idx
69
70
71 # plt.plot(hlist,Tlist/Tsl)
72 # plt.plot(hlist,plist/psl)
73 # plt.plot(hlist,rholist/rhosl)
74 # plt.legend(["Temperature", "Pressure", "Density"])
75 # plt.xlabel("Altitude (km)")
76 # plt.ylabel("Ratio to Sea Level")
77 # plt.grid()
78 # plt.show()
79 #********************************
80
81 Nstage = 10
82 + h = [9.5]
83 h = np.arange(6,14,0.5)
84 # OPR = [45]
85 OPR = np.arange(10,60,5)
86 s = range_max*1000/Nstage
                               # distance of 1 stage, m
87 CO2_ovr = np.zeros((len(h),len(OPR)))
88 NOx_{ovr} = np.zeros((len(h), len(OPR)))
89 fuel_ppkm = np.zeros((len(h),len(OPR))) # fuel burnt per kg payload per km
90 M_max = np.zeros(len(h))
91
92 for i in range(len(h)): # CHANGE ALTITUDES
93
       index = find_nearest(hlist, h[i]) # altitude
94
       Ta = Tlist[index]
95
       pa = plist[index]
96
       rhoa = rholist[index]
       aa = alist[index]
97
98
```

```
for j in range(len(OPR)): # CHANGE OVERALL PRESSURE RATIO
 99
100
            ncycle = (theta*(1-1/OPR[j]**fga)*nt-(OPR[j]**fga-1)/nc)/(theta-1-(OPR →
              [j]**fga-1)/nc)
101
            w = we + wp + wf
                                # total mass
102
            Eppkm_CO2, Eppkm_NOx, M = [],[],[]
103
            for stage in range(Nstage):
                104
                print("h = ", h[i], "km", "OPR = ", OPR[j], "Stage ", stage+1, " out >
105
                   of ", Nstage)
                Ve_star = (w*9.81/(0.5*rhosl*S))**0.5 * (K2/K1)**0.25 # optimum EAS
106
                Ve = Ve_star * v
107
108
                V = Ve * (rhos1/rhoa)**0.5 # TAS
                print("TAS = ", "%.2f" % V, " m/s")
109
                rho = rhosl * (Ve/V)**2
110
111
112
                M.append(V/aa)
                                # Mach number
113
                if M[-1]>M_max[i]:
114
                    M_{max}[i]=M[-1]
                print("M = ", "%.2f" % M[-1])
115
116
                if M[-1]>0.85:
117
                    print("Mach number exceed transonic drag rise, M = ", M[-1])
118
119
                p02 = pa * (1+(gamma-1)/2*M[-1]**2)**(1/fga)
120
                Mj = ((2/(gamma-1))*((FPR*p02/pa)**fga-1))**0.5
121
                print("Mj = ", Mj)
                Tj = Ta * (1+0.5*(gamma-1)*M[-1]**2)/(1+0.5*(gamma-1)*Mj**2)*FPR** 
122
                  (fga/nf)
123
                nprop = 2*(1+Mj/M[-1]*(Tj/Ta)**0.5)**-1
124
                beta = 0.5*betastar*(v**2+1/v**2)
125
                H = nprop*ncycle*ntr * 1/beta * LCV / 9.81
                print("H = ", "%.2f" % (H/1000), " km")
126
127
                wnew = w / math.exp(s/H)
128
                wf_burnt = w - wnew
                                       # this stage, in kg
                print("mf = ", "%.2f" % wf_burnt, " kg")
129
130
                w = wnew
                \# T02 = Ta + V**2/(2*cp)
131
                T02 = Ta * (1+(gamma-1)/2*M[-1]**2)
132
133
                T03 = T02 * (1+(OPR[j]**fga-1)/nc)
                EI_NOx = 0.011445*math.exp(0.00676593*T03) # gNOx / kg air
134
135
                EI CO2 = 3088
                              # gCO2/kg fuel, depends only on fuel
136
                Eppkm CO2.append(wf burnt / (s/1000*Np) * EI CO2) # gCO2 per
137
                  passenger km
                {\tt Eppkm\_NOx.append(EI\_NOx~*~wf\_burnt~/~(s/1000*Np)~*~15.1~*~2)}
138
                  15.1 is Stoichiometric, assume 2x stoichiometric
                print("CO2 Emissions = ", "%.2f" % Eppkm_CO2[-1], " gCO2/pas/km")
139
                print("NOx Emissions = ", "%.2f" % Eppkm_NOx[-1], " gNO2/pas/km")
140
```

```
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                                                                                 4
            CO2\_ovr[i][j] = sum(Eppkm\_CO2)/len(Eppkm\_CO2)
142
            NOx_ovr[i][j] = sum(Eppkm_NOx)/len(Eppkm_NOx)
143
144
            fuel_ppkm[i][j] = (wto-w)/range_max/wp + 0.015*wto/range_max/wp
                                                                                 P
              fuel burnt per payload per km (kg/kgkm)
145
146
   for i in range(len(h)):
147
        for j in range(len(OPR)):
148
            149
            print("h = ", h[i], "km", "OPR = ", OPR[j])
150
            print("Overall CO2 Emissions = ", "%.2f" % CO2_ovr[i][j], " gCO2/pas/
151
            print("Overall NOx Emissions = ", "%.2f" % NOx_ovr[i][j], " gNOx/pas/
152
              km")
153
            print("Total fuel burnt = ", fuel_ppkm[i][j]*range_max*wp, " kg")
            print("Fuel per payload km = ", "%.2e" % fuel_ppkm[i][j], " kg fuel/kg >
154
              payload/km")
            155
156
157 # SET UP GWP FOR GREEN AND SVENSSON
158 hlist_s = np.arange(0,15.5,0.5)
159 GWP_NOx_old =
      [-7.1, -7.1, -7.1, -4.3, -1.5, 6.5, 14.5, 37.5, 60.5, 64.7, 68.9, 57.7, 46.5, 25.6, 4.6, 0.6 
           # Svensson
160 GWP_NOx_s = np.zeros(len(hlist_s))
161 for i in range(len(GWP_NOx_old)):
162
        if i==0:
163
            GWP_NOx_s[0] = GWP_NOx_old[0]
164
        else:
165
            GWP_NOx_s[i*2-1] = (GWP_NOx_old[i]+GWP_NOx_old[i-1])/2
166
            GWP_NOx_s[i*2] = GWP_NOx_old[i]
167
168 hlist_g = np.arange(5,12.5,0.5)
    GWP_NOx_old = np.concatenate((np.linspace(10, 47,5),np.array([63,105,126])))
       # Green
170 GWP CO2 old = np.concatenate((np.linspace(147, 126,5),np.array([110,100,100])))
171 GWP_NOx_g = np.zeros(len(hlist_g))
172 GWP_CO2_g = np.zeros(len(hlist_g))
173 for i in range(len(GWP_NOx_old)):
174
        if i==0:
175
            GWP CO2 g[0] = GWP CO2 old[0]
            GWP NOx g[0] = GWP NOx old[0]
176
177
        else:
            GWP_CO2_g[i*2-1] = (GWP_CO2_old[i]+GWP_CO2_old[i-1])/2
178
179
            GWP\_CO2\_g[i*2] = GWP\_CO2\_old[i]
            GWP\_NOx\_g[i*2-1] = (GWP\_NOx\_old[i]+GWP\_NOx old[i-1])/2
180
181
            GWP_NOx_g[i*2] = GWP_NOx_old[i]
182 for i in range(len(hlist_g)):
        GWP_NOx_g[i] = GWP_NOx_g[i]/GWP_CO2_g[i]
183
```

```
184 # plt.plot(hlist_s,GWP_NOx_s)
185 # plt.xlabel('Altitude (km)')
186 # plt.ylabel('GWP for NOx')
187 # # plt.plot(hlist_g,GWP_NOx_g/10*147)
188 # plt.show()
189
190
191
192 # # PLOT OVERALL EMISSIONS FOR EACH OPR
193 # CO2_ovr = np.transpose(CO2_ovr)
194 # NOx ovr = np.transpose(NOx ovr)
195 # fuel ppkm = np.transpose(fuel ppkm)
196 # fig, ax1 = plt.subplots(3)
197 # ax1[0].set ylabel('CO2',color='b')
198 # ax1[0].set_title('Emissions (g/passenger/km)')
199 # # ax1[0].set_xlabel('Cruise Altitude (km)')
200 # ax1[0].plot(h, CO2 ovr[0], '-ob')
201 # ax1[0].tick_params(axis='y',labelcolor='b')
202 # ax2 = ax1[0].twinx() # instantiate a second axes that shares the same x-axis
203 # ax2.set ylabel('NOx',color='r') # we already handled the x-label with ax1
204 # ax2.plot(h, NOx_ovr[0], '-or')
205 # ax2.tick_params(axis='y',labelcolor='r')
206 # fig.tight_layout() # otherwise the right y-label is slightly clipped
207 # # plt.show()
208
209 # # plt.plot(h,M_max,'-ob')
210 # # plt.xlabel('Cruise Altitude (km)')
211 # # plt.ylabel('Maximum Mach Number')
212 # # plt.plot([10.18]*2,[0.7,1.0],'-r')
213 # # plt.legend(['Max M','Transonic Drag Onset'])
214 # # plt.show()
215
216
217
218
219 # PLOT OVERALL GWP
220 ovr_s = np.zeros((len(h),len(OPR)))
221 ovr_g = np.zeros(len(h))
222 # NOx_ovr_new = np.zeros(len(h))
223 for i in range(len(h)):
224
        for j in range(len(OPR)):
225
             si = find nearest(hlist s, h[i])
             NOx_ovr_new = NOx_ovr[i][j]*GWP_NOx_s[si]
226
227
             ovr_s[i][j] = CO2_ovr[i][j] + NOx_ovr_new
228
        # gi = find nearest(hlist g, h[i])
229
230
        # NOx_ovr_new = NOx_ovr[0][i]*GWP_NOx_g[gi]
        \# \text{ ovr}_g[i] = \text{CO2}_o\text{vr}[0][i] + \text{NOx}_o\text{vr}_n\text{ew}
231
232
```

```
233 # # ax1[1].set_xlabel('Cruise Altitude (km)')
234 # # ax1[1].set_ylabel('CO2 Emissions (gCO2/passenger/km)', color='b')
235 # ax1[1].set_title('Relative Greenhouse Effects, normalised with CO2')
236 # ax1[1].plot(h, CO2_ovr[0], '-ob')
237 # ax1[1].plot(h, NOx ovr new, '-or')
238 # ax1[1].legend(['CO2','NOx'])
239
240 # ax1[2].set xlabel('Cruise Altitude (km)')
241 # # ax1[2].ylabel('Overall GWP, normalised with h=9.5km')
242 # ax1[2].set_title('Overall GWP, normalised with h=9.5km')
243 # ax1[2].plot(h, ovr_s/ovr_s[find_nearest(h, 9.5)], '-om')
244 # # plt.plot(h, ovr g/ovr g[find nearest(h, 9.5)], '-or')
245 # plt.show()
246
247 # ## PLOT FUEL BURNT
248 # # plt.plot(h, fuel_ppkm[0],'-ob')
249 # # plt.xlabel('Cruise Altitude (km)')
250 # # plt.ylabel('Fuel Burnt (kg fuel/kg payload/km')
251 # # plt.ticklabel_format(style='sci', axis='y', scilimits=(0,0))
252 # # plt.show()
253
254
255
256
257
258 # # PLOT OVERALL EMISSIONS FOR EACH OPR
259 # fig, ax1 = plt.subplots(3)
260 # # ax1[0].set_xlabel('Overall Pressure Ratio')
261 # # ax1[0].set_ylabel('CO2 Emissions (gCO2/passenger/km)', color='b')
262 # ax1[0].set ylabel('CO2',color='b')
263 # ax1[0].set_title('Emissions (g/passenger/km)')
264 # ax1[0].plot(OPR, CO2_ovr[0], '-ob')
265 # ax1[0].tick_params(axis='y',labelcolor='b')
266 # # ax1[0].legend(['CO2','NOx'])
267 # ax2 = ax1[0].twinx() # instantiate a second axes that shares the same x-axis
268 # # ax2.set ylabel('NOx Emissions (gNOx/passenger/km)',color='r') # we already >
       handled the x-label with ax1
269 # ax2.set_ylabel('NOx',color='r')
270 # ax2.plot(OPR, NOx_ovr[0], '-or')
271 # # ax2.legend(['NOx'])
272 # ax2.tick_params(axis='y',labelcolor='r')
273 # fig.tight layout() # otherwise the right y-label is slightly clipped
274 # # plt.show()
275
276 # ax1[1].plot(OPR, CO2_ovr[0], '-ob')
277 # ax1[1].plot(OPR, NOx_ovr[0]*66.8, '-or')
278 # ax1[1].legend(['CO2','NOx'])
279 # ax1[1].set_title('Relative Greenhouse Effects, normalised with CO2')
280 # # plt.show()
```

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7
```

```
281
282 # # PLOT OVERALL GWP
283 # # plt.xlabel('Overall Pressure Ratio')
284 # ax1[2].set_title('Overall GWP, normalised with OPR=45')
285 # ovr = CO2 ovr[0]+NOx ovr[0]*66.8
286 # ax1[2].plot(OPR, ovr/ovr[5], '-om')
287 # ax1[2].set_xlabel('Overall Pressure Ratio')
288 # plt.show()
289
290 # # plt.plot(OPR, fuel_ppkm[0],'-ob')
291 # # plt.xlabel('Cruise Altitude (km)')
292 # # plt.ylabel('Fuel Burnt (kg fuel/kg payload/km')
293 # # plt.ticklabel_format(style='sci', axis='y', scilimits=(0,0))
294 # # plt.show()
295
296
297 # PLOT CONTOUR
298 colour = plt.get_cmap('plasma_r')
299 # colour = matplotlib.colors.LinearSegmentedColormap.from_list("",
      ["green", "yellow", "red"])
300 X, Y = np.meshgrid(h, OPR)
301 cp = plt.contourf(X,Y, np.transpose
      (ovr s)/194.074,100,cmap=colour,norm=matplotlib.colors.CenteredNorm
      (vcenter=0.7, halfrange=0.3))
302 plt.colorbar(cp,label='Normalised GWP')
303 plt.xlabel('Cruise Altitude (km)')
304 plt.ylabel('Overall Pressure Ratio')
305 plt.show()
306
307 cp = plt.contourf(h,OPR, np.transpose
      (fuel_ppkm), 100, cmap=colour, norm=matplotlib.colors.CenteredNorm
                                                                                      P
      (vcenter=1.5e-4, halfrange=0.125e-4))
308 plt.colorbar(cp, label='kg fuel / kg payload / km',format='%.2e')
309 plt.xlabel('Cruise Altitude (km)')
310 plt.ylabel('Overall Pressure Ratio')
311 plt.show()
312
313
314
315
316
317
318
319
320
321
322
323
324 s_total = [s/1000]
```

```
325 for i in range(Nstage-1):
326
        s_total.append(s_total[-1]+s/1000)
327
328 ## PLOT VARIATION OF MACH AND X-T DIAGRAM
329 # plt.plot(s total,M)
330 # plt.xlabel('Distance Travelled (km)')
331 # plt.ylabel('Mach Number')
332 # plt.show()
333 # speed=[]
334 # time=[]
335 # time2 = 12000000/M[0]/aa/3600
336 # for i in range(Nstage):
337 #
          speed.append(M[i]*aa)
338 #
          time.append(s/speed[i]/3600)
339 # for i in range(Nstage-1):
340 #
          time[i+1]=time[i]+time[i+1]
341 # plt.plot([0]+time,[0]+s total)
342 # plt.plot([0,time2],[0,12000])
343 # plt.xlabel('Time (hours)')
344 # plt.ylabel('Distance Travelled (km)')
345 # plt.xlim([0, time[-1]])
346 # plt.ylim([0, s_total[-1]])
347 # plt.legend(['Optimum Mach across 10 stages','Constant M = $M_{initial}$'])
348 # plt.show()
349
350 ## PLOT VARIATION OF EMISSIONS ACROSS STAGES
351 # plt.plot(s_total,Eppkm_CO2)
352 # plt.plot([s_total[0],s_total[-1]],[CO2_ovr[0]]*2)
353 # plt.xlabel('Distance Travelled (km)')
354 # plt.ylabel('CO2 Emissions (gCO2/passenger/km)')
355 # plt.legend(['Emissions each stage','Overall Emissions'])
356 # plt.show()
357 # plt.plot(s_total,Eppkm_NOx)
358 # plt.plot([s_total[0],s_total[-1]],[NOx_ovr[0]]*2)
359 # plt.xlabel('Distance Travelled (km)')
360 # plt.ylabel('NOx Emissions (gNOx/passenger/km)')
361 # plt.legend(['Emissions each stage','Overall Emissions'])
362 # plt.show()
```