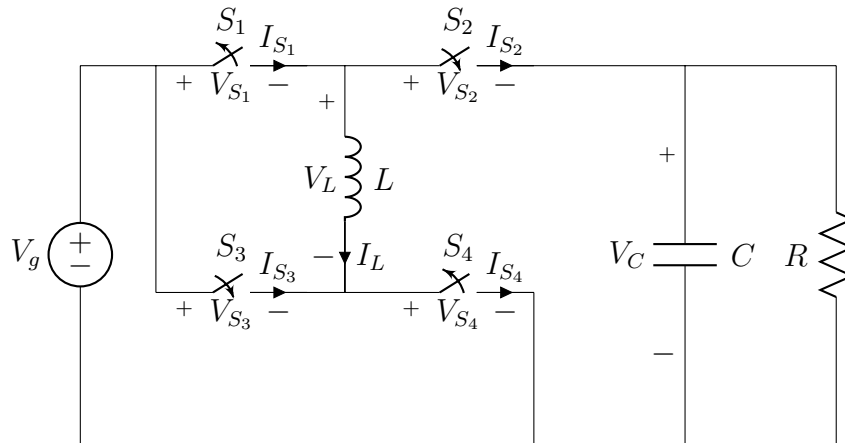


3.1: The input voltage V_g is dc and positive with the polarity shown. Specify how to implement the switches using a minimal number of diodes and transistors, such that the converter operates over the entire range of duty cycles $0 \leq D \leq 1$. The switch states should vary as shown. You may assume that the inductor current ripples and capacitor voltage ripples are small.

- (a) Realize the switches using SPST ideal switches, and explicitly define the voltage and current of each switch.

The new circuit would look like:



- (b) Express the on-state current and off-state voltage of each SPST switch in terms of the converter inductor currents, capacitor voltages, and/or input source voltage.

In position 1, S_2 and S_3 are both closed and S_1 and S_4 are both open. This is the inverse in position 2. We can find the voltages and currents, in position 1:

$$V_{S2} = 0, V_{S3} = 0, I_{S1} = 0, I_{S4} = 0$$

$$V_{S4} = V_g, V_{S1} = V_L = V_g - V_C, I_{S3} = I_{S2} = -I_L$$

In position two:

$$V_{S1} = 0, V_{S4} = 0, I_{S2} = 0, I_{S3} = 0$$

$$V_{S2} = V_g - V_C, V_{S3} = V_g, I_{S1} = I_{S4} = I_L$$

- (c) Solve the converter to determine the inductor currents and capacitor voltages, as in chapter 2.

To do this we must use KVL and KCL, in position 1:

$$V_L = V_C - V_G, I_C = -\frac{V}{R} - I_L$$

In position 2:

$$V_L = V_G, I_C = -\frac{V}{R}$$

We then use our knowledge of the inductor current balance:

$$\left(-\frac{V}{R}\right)DT_S + \left(-\frac{V}{R} - I_L\right)(1-D)T_S = 0$$

$$I_L = \frac{V}{R(D-1)}$$

And capacitor charge balance:

$$(V_g)D + (V_G - V_C)(1-D) = 0$$

$$2V_G D - V_g + V_C - V_C D = 0$$

$$V_C = \frac{(1-2D)V_g}{1-D}$$

Combining these we find that:

$$I_L = \frac{(1-2D)V_g}{R(1-D)(D-1)} \text{ and } V_C = \frac{(1-2D)V_g}{1-D}$$

- (d) Determine the polarities of the switch on-state currents and off-state voltages. Do the polarities vary with duty cycle?

Using the same knowledge from part (b), we only need V_C and I_L . In position 1 we can see that:

$$V_{S_1} = V_g - V_C = V_g - \frac{(1-2D)V_g}{1-D}$$

Which is always positive, additionally:

$$I_{S_3} = I_{S_2} = -I_L = -\frac{(1-2D)V_g}{R(1-D)(D-1)}$$

Which is positive for $D < 0.5$ and negative for $D > 0.5$. we know from before:

$$V_{S_2} = 0, V_{S_3} = 0, I_{S_1} = 0, I_{S_4} = 0$$

In position two:

$$V_{S_2} = V_g - V_C = V_g - \frac{(1 - 2D)V_g}{1 - D}$$

which is positive, and:

$$I_{S_1} = I_L = \frac{(1 - 2D)V_g}{R(1 - D)(D - 1)}$$

Which is positive for $D > 0.5$ and negative for $D < 0.5$. In all this tells us that in position 1:

$$V_{S_2} = 0, V_{S_3} = 0, I_{S_1} = 0, I_{S_4} = 0$$

$$V_{S_4} = \text{positive}, V_{S_1} = \text{positive}, I_{S_3} = I_{S_2} = \text{positive for } D < 0.5, \text{ negative for } D > 0.5$$

And in position two:

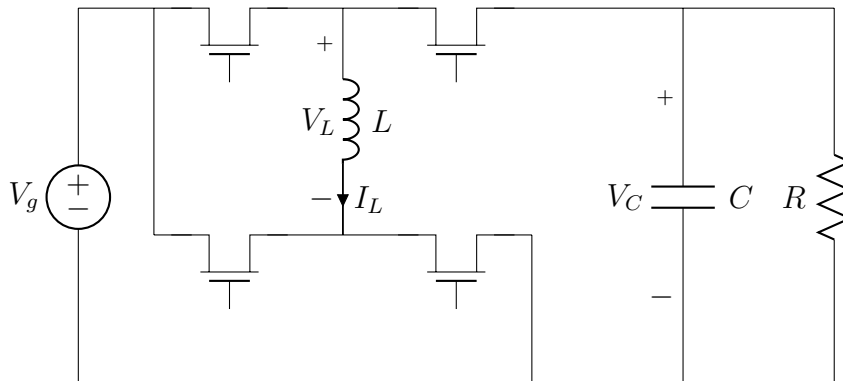
$$V_{S_1} = 0, V_{S_4} = 0, I_{S_2} = 0, I_{S_3} = 0$$

$$V_{S_2} = \text{positive}, V_{S_3} = \text{positive}, I_{S_1} = I_{S_4} = \text{positive for } D > 0.5, \text{ negative for } D < 0.5$$

- (e) State how each switch can be realized using transistors and/or diodes, and whether the realization requires single-quadrant, current-bidirectional two-quadrant, voltage-bidirectional two-quadrant, or four-quadrant switches.

We need voltage to only go in one direction (positive) but current must be able to go in both directions in all switches. That means current-bidirectional two-quadrant switches. The component that best realizes this is a MOSFET. We would need four of them.

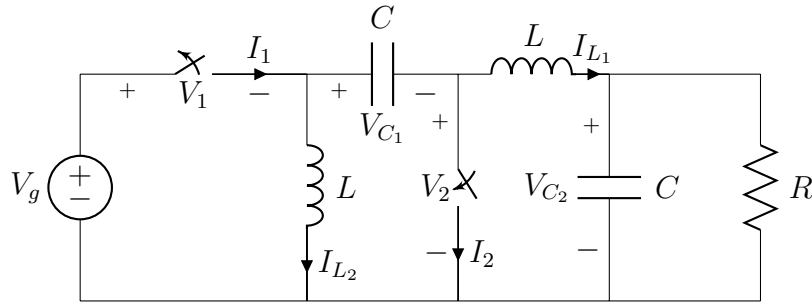
- (f) draw the converter circuit, including your realization of the switch elements using MOSFETs and diodes.



3.2: The input voltage V_g is dc and positive with the polarity shown. Specify how to implement the switches using a minimal number of diodes and transistors, such that the converter operates over the entire range of duty cycles $0 \leq D \leq 1$. The switch states should vary as shown. You may assume that the inductor current ripples and capacitor voltage ripples are small.

- (a) Realize the switches using SPST ideal switches, and explicitly define the voltage and current of each switch.

The new circuit would look like:



- (b) Express the on-state current and off-state voltage of each SPST switch in terms of the converter inductor currents, capacitor voltages, and/or input source voltage.

In position 1, we can see that:

$$V_1 = V_g - V_{C_1} \text{ and } V_2 = 0$$

$$I_1 = 0 \text{ and } I_2 = I_{L_1}$$

In position 2:

$$V_1 = 0 \text{ and } V_2 = V_g - V_{C_1}$$

$$I_1 = I_{L_2} \text{ and } I_2 = 0$$

- (c) Solve the converter to determine the inductor currents and capacitor voltages, as in chapter 2.

First we can use KVL when we are in state 1:

$$V_{L_1} = V_{C_2} \text{ and } V_{L_2} = -V_{C_1}$$

$$I_{C_1} = -I_{L_2} \text{ and } I_{C_2} = I_{L_1} - \frac{V_{C_2}}{R}$$

in state 2:

$$V_{L_1} = V_g - V_{C_1} - V_{C_2} \text{ and } V_{L_2} = V_g$$

$$I_{C_1} = I_{L_1} \text{ and } I_{C_2} = I_{L_1} - \frac{V_{C_2}}{R}$$

We can solve these:

$$D(V_{C_2}) + (1 - D)(V_g - V_{C_1} - V_{C_2}) = 0$$

$$(2D - 1)V_{C_2} + (D - 1)V_{C_1} + (D - 1)V_g = 0$$

$$D(-V_{C_1}) + (1 - D)(V_g) = 0$$

$$V_{C_1} = \frac{1 - D}{D}V_g$$

$$D(-I_{L_2}) + (1 - D)(I_{L_1}) = 0$$

$$I_{L_2} = \frac{1 - D}{D}I_{L_1}$$

$$I_{L_1} = \frac{V_{C_2}}{R}$$

Thats a lot of unknowns and a lot of equations, but I think we can do this. Plugging in our equation for V_{C_1} into the first equation we find that:

$$V_{C_2} = \frac{D - 1}{D}V_g$$

That means that:

$$I_{L_1} = \frac{D - 1}{DR}V_g$$

and

$$I_{L_2} = \frac{(D - 1)(1 - D)}{D^2R}V_g$$

and as we know:

$$V_{C_1} = \frac{1 - D}{D}V_g$$

- (d) Determine the polarities of the switch on-state currents and off-state voltages. Do the polarities vary with duty cycle?

Going back to part (b) we find that in position 1:

$$V_1 = V_g - \frac{1 - D}{D}V_g \text{ and } V_2 = 0$$

$$I_1 = 0 \text{ and } I_2 = \frac{D - 1}{DR}V_g$$

In position 2:

$$V_1 = 0 \text{ and } V_2 = V_g - \frac{1-D}{D}V_g$$

$$I_1 = \frac{(D-1)(1-D)}{D^2 R}V_g \text{ and } I_2 = 0$$

Which, it can be easily shown, that in position 1:

$$V_1 = \text{positive for } D > 0.5, \text{ negative for } D < 0.5 \text{ and } V_2 = 0$$

$$I_1 = 0 \text{ and } I_2 = \text{negative}$$

In position 2:

$$V_1 = 0 \text{ and } V_2 = \text{positive for } D > 0.5, \text{ negative for } D < 0.5$$

$$I_1 = \text{positive and } I_2 = 0$$

- (e) State how each switch can be realized using transistors and/or diodes, and whether the realization requires single-quadrant, current-bidirectional two-quadrant, voltage-bidirectional two-quadrant, or four-quadrant switches.

Both switches must have bidirectional voltage two quadrant switches, but only require one direction of current. This can be realized with each switch consisting of a MOSFET and a diode, as shown in the next part.

- (f) draw the converter circuit, including your realization of the switch elements using MOSFETs and diodes.

