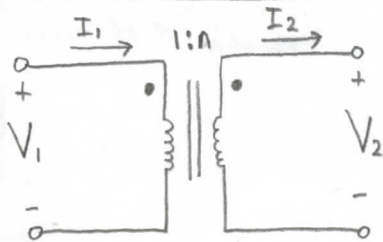
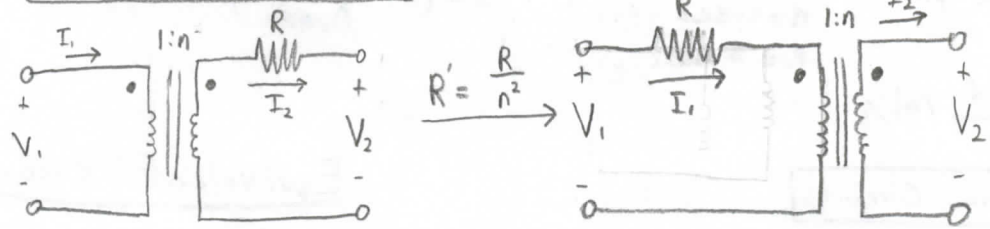


Ideal Transformer

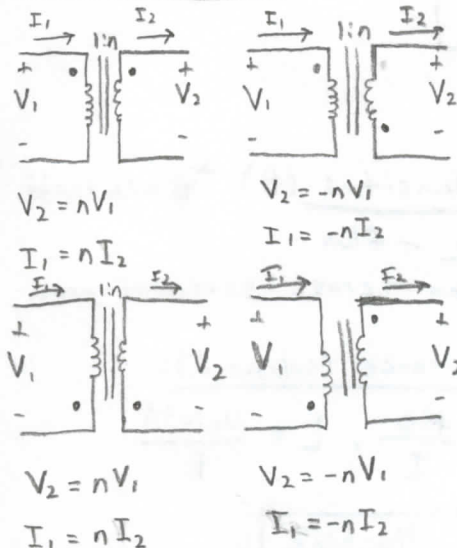


① $V_2 = nV_1$ ② $I_1 = nI_2$

Transforming Impedances



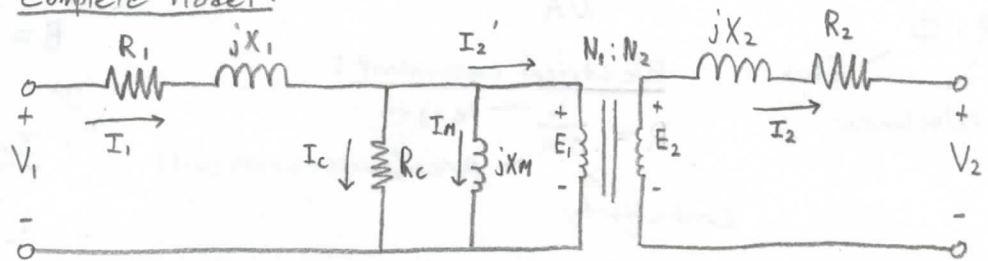
Dot Convention



"Whatever spot the current on the primary enters (Dot or non-Dot) that will be the higher voltage on the secondary (Dot or non-Dot)"

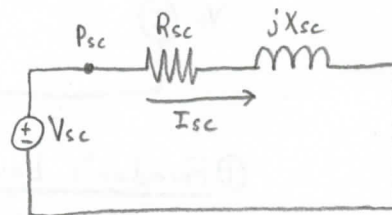
Ideal Transformer

Complete Model:



Short Circuit Test

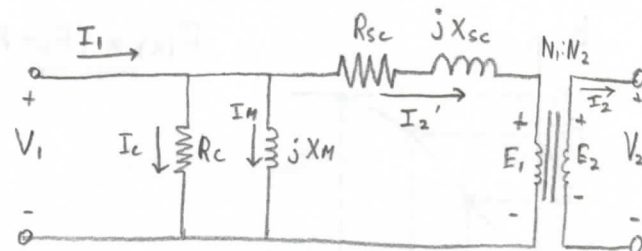
- Determines R_{sc}, X_{sc}
- Apply rated current to HVS



① $R_{sc} = \frac{P_{sc}}{I_{sc}^2}$

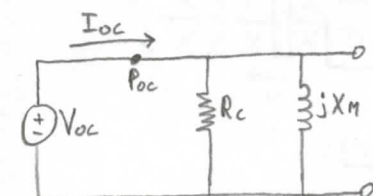
② $X_{sc} = \sqrt{\left(\frac{V_{sc}}{I_{sc}}\right)^2 - R_{sc}^2}$

Simplified Model:



Open Circuit Test

- Determines R_c, X_M
- Apply rated voltage to LVS



① $R_c = \frac{V_{oc}^2}{P_{oc}}$ • $I_c = \frac{V_{oc}}{R_c}$

② $X_M = \frac{V_{oc}}{I_M}$ • $I_M = \sqrt{I_{oc}^2 - I_c^2}$

Induction Motors

Slip:

$$\eta_{rotor} = (1-s) \eta_{RMF}$$

Rotor Speed / Torque:

"Rotor follows the speed of the RMF"

4.44 Law

$$\eta_{rotor} = \frac{120f}{p} \text{ rpm}$$

Where:
 n = speed
 p = # Poles / 2

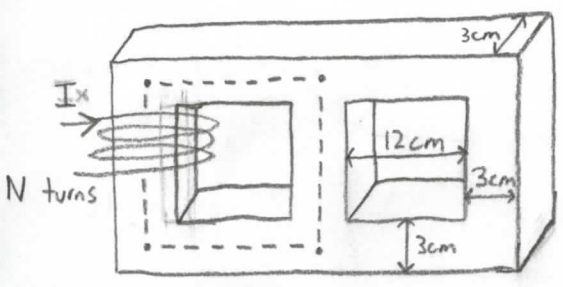
$$s = \left(\frac{\eta_{RMF} - \eta_{rotor}}{\eta_{RMF}} \right) \cdot 100\%$$

$$E_{rms} = 4.44 f N \Phi_{peak}$$

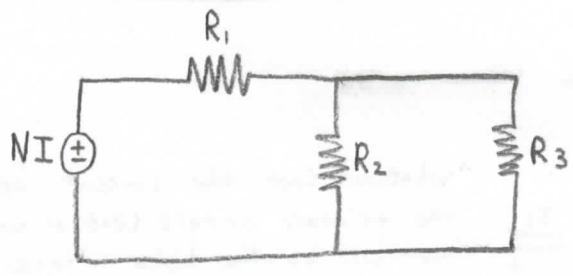
induced voltage / frequency / # of turns / flux

$$\omega = \frac{2\pi f}{p} \text{ rad/s}$$

Magnetic Circuits



Equivalent circuit:



Ohm's Law:

$$U = R \cdot \Phi$$

mmf / reluctance / flux

$$R = \frac{L}{NA} \text{ (assuming constant } N, A)$$

$$\text{Flux Density: } (B) \cdot B = \mu_0 \mu_r H$$

$$B = \frac{\Phi}{\text{Area}} \text{ - flux / cross-sectional area}$$

Electrical equivalent:

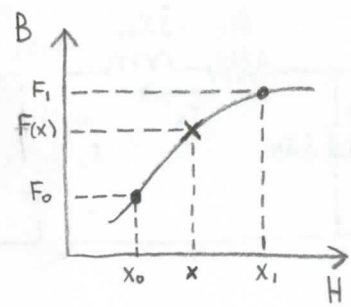
$$R = \frac{L}{\sigma A}$$

length / conductivity / Area (cross-sectional)

Inductance (solenoid):

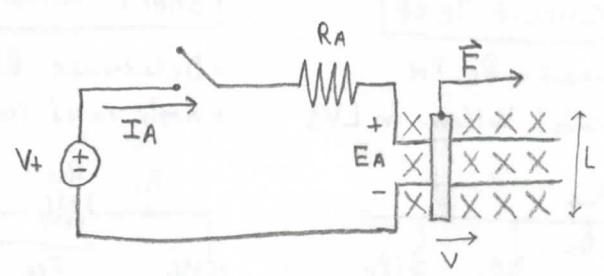
$$L = \frac{N\Phi}{I}, L = \frac{\mu_0 N^2 A}{l}$$

Logarithmic Interpolation



$$F(x) = (F_1 - F_0) \left[\frac{\log(\frac{x}{x_0})}{\log(\frac{x_1}{x_0})} \right] + F_0$$

Linear DC Machine



Linear DC Machine states

① Faraday's Law (Motor):

$$E_A = L \cdot (\vec{v} \times \vec{B}) = BLv$$

② Lorentz Force Law (Generator):

$$\vec{F} = I(\vec{L} \times \vec{B}) = BIL$$

③ Kirchhoff's Voltage Law:

$$V_t - I_A R_A - E_A = 0$$

① Start up: ($E_A = 0$)

$$I_A = \frac{V_t}{R_A}, F = BIL$$

② No load steady state: ($I_A = 0$)

$$E_A = V_t, E_A = BLV_{ss}$$

③ load ($I_A \neq 0$)

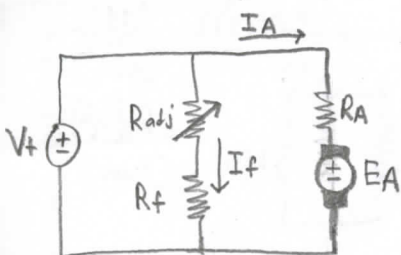
$$I_A = \frac{F_{load}}{BL}, E_A = V_t - I_A R_A, E_A = BLV_{ss}$$

torque:

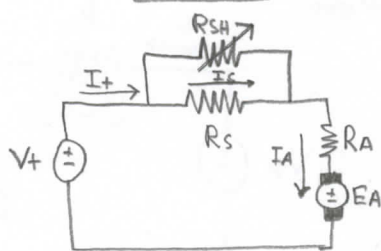
$$T = \frac{m R_A}{(B l)^2}$$

Motor Excitations

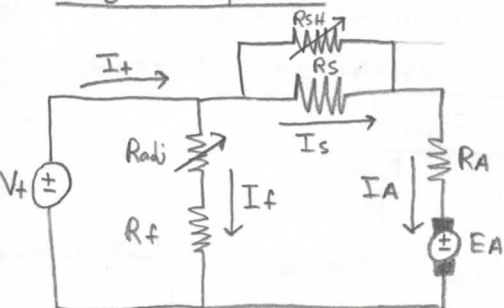
① Shunt:



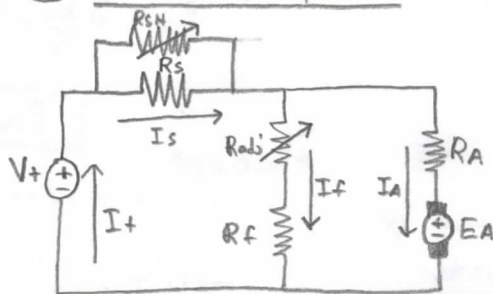
② Series:



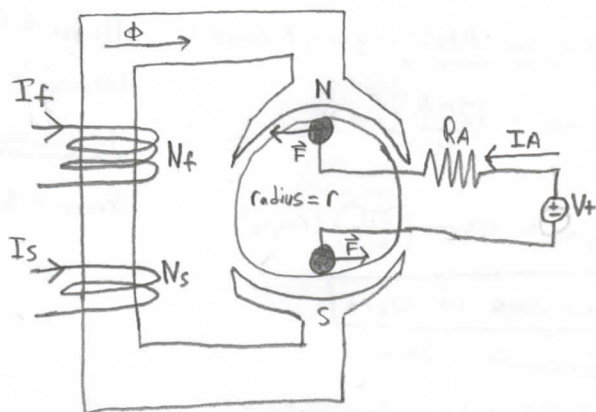
③ Long - Compound:



④ Short - Compound:



$$MMF = N_f I_f + N_s I_s$$



$$T = 2rFN = 2rBILN = 2Nr \frac{\Phi}{A} LI$$

where

$$k = \frac{2Nrl}{A}$$

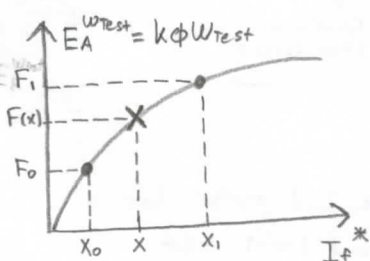
Power Flow

$$P_{out} = P_{conv} - P_{losses}$$

$$P_{conv} = EAIA$$

$$P_{out} = T_{out} \omega_{mech}$$

DC motor Magnetization Curve



Coffee Formulas:

$$EA = k\Phi W$$

$$T_{ind} = k\Phi IA$$

$$I_f^* = \frac{N_f I_f + N_s I_s}{N_f}$$

Two Egn's, Two Unknowns

$$① P_{out} = EAIA - P_{losses}$$

$$② V_t - I_A R_A - EA = 0$$

Armature Reaction

* Compensation windings means no armature reaction

$$I_f^* = I_f + I_s \left(\frac{N_s}{N_f} \right) - k_{AR}^* I_A$$

armature reaction

$$k_{AR}^* = \frac{k_{AR}}{I_A} \text{ } ^* \text{ test, given}$$

$$\frac{EA_1}{W_1} = \frac{EA_2}{W_2}, \therefore W_2 = \left(\frac{EA_2}{EA_1} \right) W_1$$

Linear Interpolation:

$$F(x) = (F_1 - F_0) \left(\frac{x - x_0}{x_1 - x_0} \right) + F_0$$

**** IND motor** (to find R_2)

$$V_{th} = V_1 (\text{opening } Z_2)$$

Z_{th} = "looking back from Z_2 "

$$R_{th} = Re(Z_{th})$$

$$X_{th} = Im(Z_{th})$$

$$\frac{P_{conv}}{W_{rotor}} = \frac{3}{W_{sync}} \cdot \frac{V_{th}^2 \cdot (R_2/s)}{[(R_{th} + R_2/s)^2 + (X_{th} + X_2)^2]} = T_{ind}$$

Induction Motor

Creating RMF: (Squirrel cage)

$$n_{sync} = \frac{120f}{P} \text{ (rpm)}$$

$$\omega_{sync} = n_{sync} \left(\frac{2\pi}{60} \right) \text{ (rad/s)}$$

How does it Work

- 1 Generate RMF
- 2 RMF cuts rotor wires
- 3 Induced voltage in wire (Current flows)
- 4 Force on wires = torque
- 5 Rotor starts rotating

Induced Torque

$$T_{ind} = \frac{P_{AG}}{\omega_{sync}} \rightarrow P_{AG} = \text{Power drained by } \frac{R_2}{s} \text{ resistor}$$

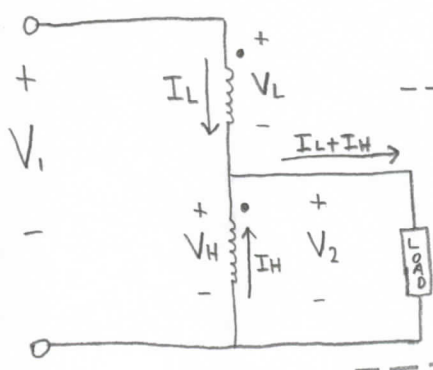
$$T_{ind} = \frac{P_{conv}}{\omega_{rotor}}$$

States:

- 1 Max torque: $\frac{R_2}{s} = |Z_{th}|$ "looking back"
- 2 Startup: Set $s=1$, resolve for V_1, I_2 and calculate P_{GAP} which is now just drained by R_2 (ie: $s=1$)

Auto transformer

"A 27.5kVA 2200/680V"



$$S_T = 27.5 \text{ kVA}$$

$$V_H = 2200 \text{ V}$$

$$V_L = 680 \text{ V}$$

$$I_L = \frac{S_T}{V_L}, I_H = \frac{S_T}{V_H}$$

$$S_{load} = \left(\frac{V_H + V_L}{V_L} \right) S_T$$

"ie: much larger"

$$R_c = \frac{V_o^2}{P_o}, X_M = \frac{V_o}{I_o^2 - \left(\frac{V_o}{R_c} \right)^2}$$

$$R_{sc} = \frac{P_{sc}}{I_{sc}^2}, X_{sc} = \sqrt{\left(\frac{V_{sc}}{I_{sc}} \right)^2 - R_{sc}^2}$$

Rotor Slip (% difference in speed) (1/3 Phase)

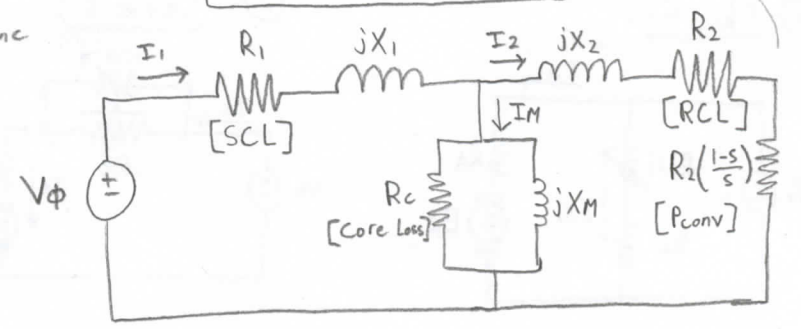
$$n_{rotor} = (1-s)n_{sync}$$

$$\omega_{rotor} = (1-s)\omega_{sync}$$

frequency:

$$f_{rotor} = s f_{sync}$$

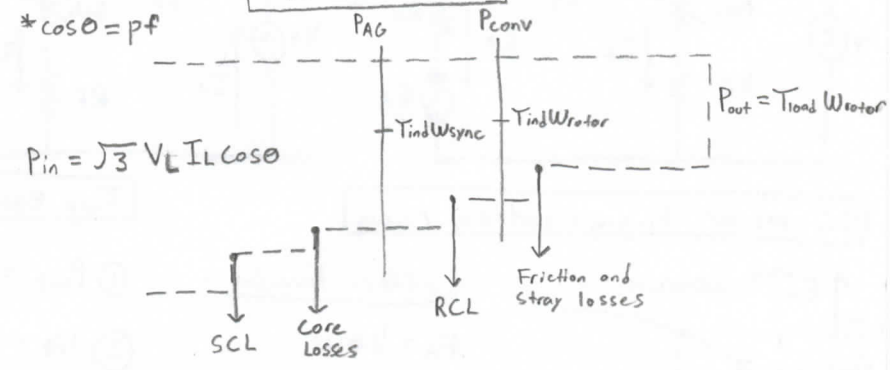
Equivalent Circuit



Gap Power:

$$P_{gap} = 3 \frac{R_2}{s} \cdot I_2^2 \text{ (Current drained by } \frac{R_2}{s} \text{ resistor in 1/3 phase)}$$

Power Flow



Example:

"A 250V, 85hz, 70hp, three phase Ind motor has a power factor of 0.8 lagging and draws 45A"

$$V_L = 480 \text{ V}$$

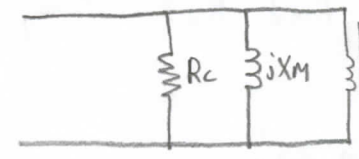
$$I_L = 45 \text{ A}$$

$$pf = \cos\theta = 0.8$$

(Get everything per phase)

Transformer Parameters (P.U.)

Ex: "A 130kVA, 24,000/277V Δ-Y"



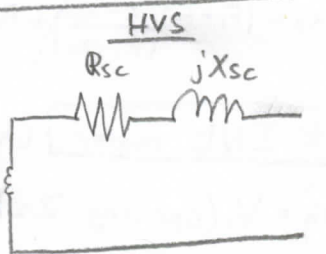
V_o, I_o, P_o

$$S_{base} = 130 \text{ k}$$

$$V_{Lbase} = 277 \text{ V}$$

$$I_{Lbase} = \frac{S_{base}}{V_{Lbase}}$$

$$Z_{Lbase} = \frac{V_{Lbase}}{I_{Lbase}}$$



V_{sc}, I_{sc}, P_{sc}

$$S_{base} = 130 \text{ k}$$

$$V_{Hbase} = 24 \text{ kV}$$

$$I_{Hbase} = \frac{S_{base}}{V_{Hbase}}$$

$$Z_{Hbase} = \frac{V_{Hbase}}{I_{Hbase}}$$

Single Phase and Special Purpose Motors

Why: "Common household devices don't use three phase and don't generate an RMF" [Pulse]

Starting Single Phase induction motors:

- ① Split-Phase windings
- ② Capacitor-type windings
- ③ Shaded stator windings

Capacitor Start

- ① Expensive, give high starting torque
- "Capacitor placed in series with the auxillary winding"

Different types of motors

"Can accelerate up to n_{sync} by themselves"

① Reluctance Motor:

"Relies on induced reluctance torque from iron for operation, orients itself to line up with external magnetic field"

③ Stepper Motor:

"Rotates a specific number of degrees discretely based on pulses from the source"

- ① Permanent magnet type
- ② Reluctance type

"Useful in control and positioning systems"

Universal Motor

"Take a series DC motor and apply an AC source voltage instead of DC"

Characteristics:

- ① poles and frame have to be laminated [otherwise enormous core losses]
- ② Good for light weight and high torque applications
- ③ Examples: Vacuum cleaner, drill, blender etc

② Hysteresis Motor:

"RMF magnetizes the metal of the rotor and induces poles within it"

④ Brushless Motor:

"Brush wear and sparking is a real problem for maintenance on small DC machines"

- Similar to stepper but include a position sensor

- ① High Price
- ② Low maintenance
- ③ Long lifespan

Conditions for Parallel Operation

(3 ϕ Transformers)

- ① Same ratio
- ② Same clock number
- ③ same short circuit impedance

Synchronous Vs. Induction Motor

IND has exact same stator, but different rotor (Cage or Wound)

Why have a squirrel cage on a SYNCH

"To start the motor, RMF rotating too fast"

Downside of DC motors

- Maintenance

Gap Power

"Power crossing the gap from stator to rotor"

$$P_{AG} = T_{ind} \omega_{sync}$$

of slip rings

Slip rings $\begin{cases} 2 \text{ [SYNCH]} \\ 3 \text{ [Induction]} \end{cases}$

Round vs Salient poles

Round \rightarrow High speed

Salient \rightarrow More poles