MOSFETs balance supercapacitors with zero power burn

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The use of supercapacitor series stacks are growing for many systems used in backup power storage or battery life extension. One of the most critical circuit design goals for such systems is minimizing the steady state DC power dissipation. For that reason, MOSFETs deployed in circuits that balance voltage and leakage current in supercapacitor series-connected stacks of two or more, can be configured to burn zero power.

To grasp the concept of zero power burn in balancing the individual supercapacitor cells, I will describe a circuit with current burn of 0.003 micro amperes (uA), or ~0.1% of 2.80 uA. While this is not absolute zero, the amount of energy used is so minimal that it is virtually zero. Using MOSFETs to balance voltage in supercapacitor cells stacked in a series contrasts to balancing voltage using op amp, which burns quiescent current.

Supercapacitors are becoming increasingly useful in high-voltage applications as energy storage devices. When an application requires more voltage than a single 2.7-volt cell can provide, supercapacitors are stacked in series of two or more. An essential part of ensuring long operational life for these stacks is to balance each cell to prevent leakage current from causing damage to other cells through over-voltage. For those seeking more information on how this works, I invite you to read our previous submitted article, "MOSFET-based current balancing cuts power use in supercapacitor stacks"

There are actually three possible scenarios of zero power burn of balancing circuitry. First, the power dissipated can be near zero, meaning that it is substantially less than a reference power dissipation level.

In this case, l use the highest leakage current within a group of a given make and model of supercapacitor as a benchmark reference power dissipation. The highest leakage current of one of the supercapacitors used is the actual minimum leakage current possible for the entire supercapacitor stack, not including any power used by any balancing component or circuitry.

Ten percent of this reference current level can be selected as the threshold limit for zero power burn. An easy way to establish this reference current is to take the maximum leakage current specification from the supercapacitor manufacturer and use that as the reference current. A user can also establish his or her own reference current based upon the operating conditions that the system experiences, including, for example, temperature or aging effects. All supercapacitors deployed in a system should first be independently tested for this reference leakage current.

The second scenario is that the possible power dissipation is actually zero at a steady state DC level.

The third scenario is that the power dissipation of the balancing circuit dissipates negative current burn of the supercapacitor stack, meaning that after the balancing circuits are installed, the total power burn is less than when there is no balancing circuitry. This is possible because MOSFETs operate by changing the balancing voltage bias of each of the supercapacitor in a series stack so that the highest leakage of the same benchmark supercapacitor is actually reduced by reducing its voltage bias after balancing is achieved. For any given supercapacitor, a reduced voltage bias reduces its leakage current level as well.

To understand how these three scenarios play out and achieve zero power burn, it is best to go through an example and analyze in three small steps what actually happens when a SAB MOSFET goes through its balancing act.

Supercapacitors connected in series with MOSFET auto-balancing

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Basic Equations:

- M1 connects across C1,

$V_{IN1} = V_{C1}$

- M2 connects across C2,

$V_{IN2} = V_{C2}$

- $V+ = V_{IN1} + V_{IN2} = V_{C1} + V_{C2}$
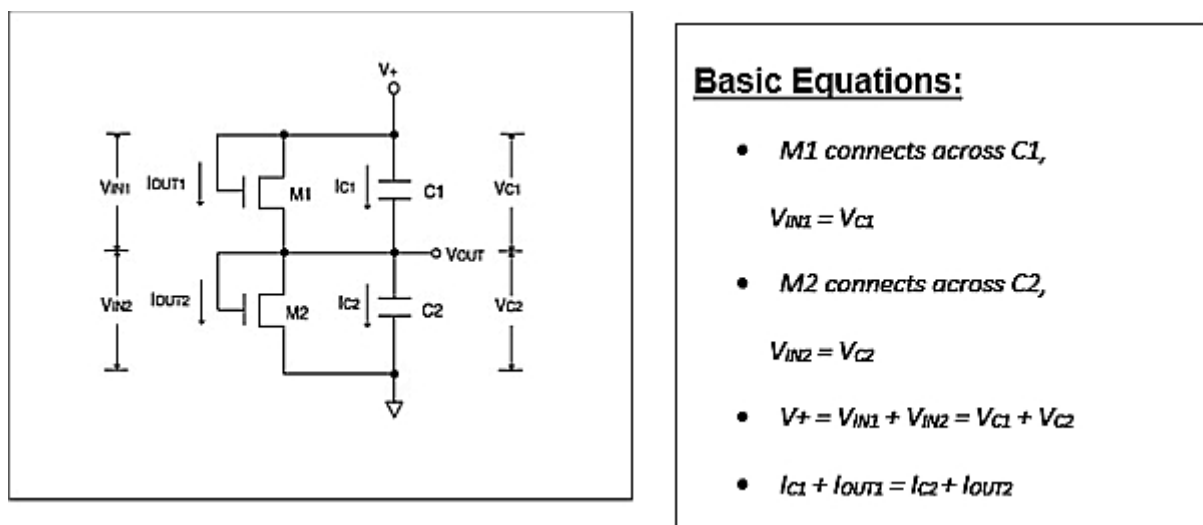
- $I_{C1} + I_{OUT1} = I_{C2} + I_{OUT2}$

Figure 1 Two supercapacitors stacked in series with MOSFETs.

The above **Figure 1** shows a pair of SAB MOSFETs placed across two supercapacitors. SAB MOSFET 1, or M1, is connected across C1, so input V_{IN1} of the SAB MOSFET is equal to supercapacitor voltage V_{C1}. M2 is across C2 so V_{IN2} is equal to V_{C2}.

There is leakage (bias controlled) current going through each one of the MOSFETs, referred to as I_{OUT1} for M1 and I_{OUT2} for M2.

Notice the equation, which states: $V+ = V_{IN1} + V_{IN2} = V_{C1} + V_{C2}$. In other words, the two voltages across M1 and M2 are equal to the two voltages across both supercapacitors C1 and C2.

The total leakage current now becomes equal to $I_{C1} + I_{OUT1} = I_{C2} + I_{OUT2}$.

A step-by-step example will illustrates how Supercap Auto Balancing (SAB) MOSFETs balance supercapacitor stacks with zero power burn. Assume that supercapacitors C1 and C2 have same capacitance values but different leakage currents profiles as shown in the graph featured in **Figure 2** below.

An [ALD910024](ALD910024) SAB MOSFET device is used for this example to highlight the tremendous swings in current levels. Cells C1 and C2 leakage current characteristics as a function of cell voltages were shown in the graph. With no balancing, leakage currents of C1 would follow its curve whereas that of C2 would have followed the dotted line to reach a balanced leakage current level of 1.1 uA for both cells, reaching $V_{C2} = 2.9V$, exceeding its rated voltage. Adding SAB MOSFETs would bend C2 leakage current curve to follow $I_{C2} + I_{OUT2}$ curve instead. The leakage currents of C1 and C2 would now balance at 2.203 uA, at $V_{C1} = 2.15V$ and $V_{C2} = 2.45V$ respectively, protecting both cells from over-voltage.

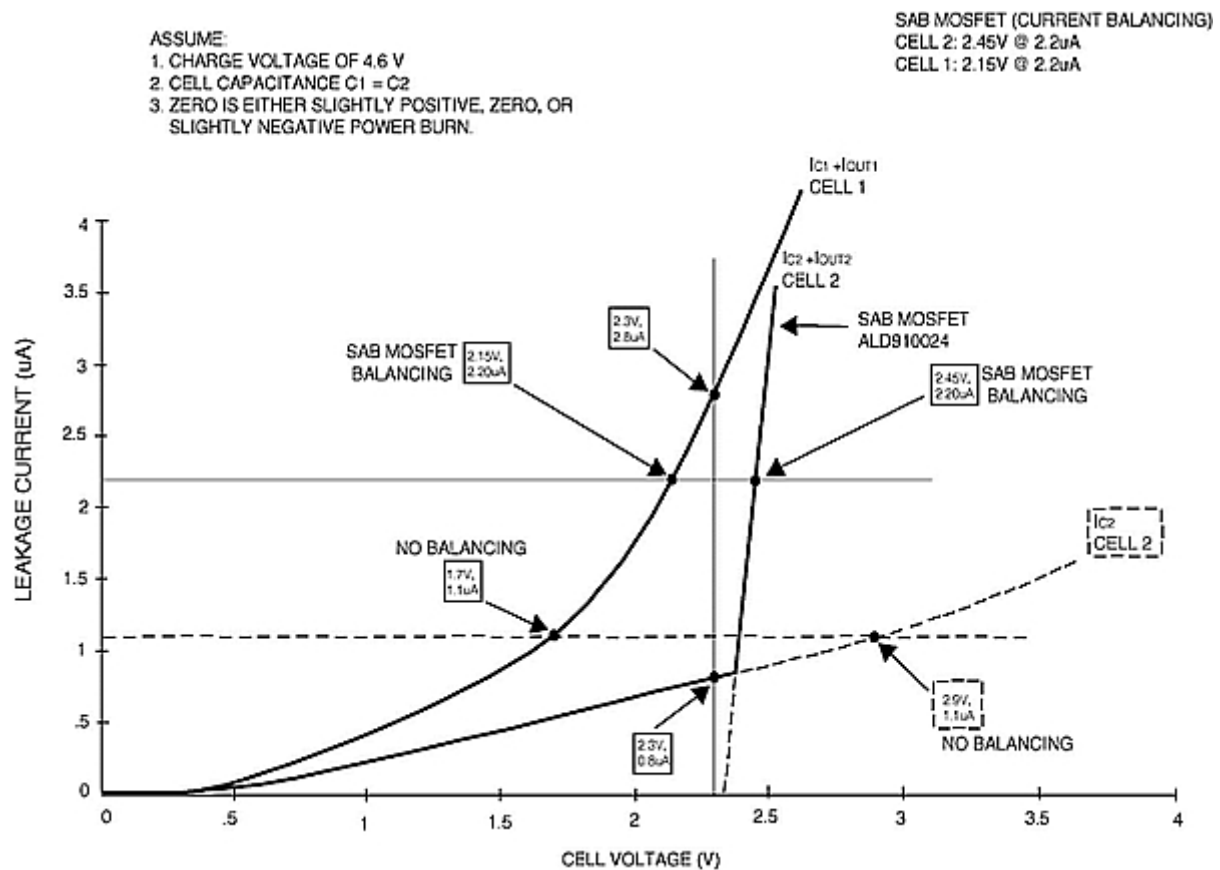**MOSFET active balancing while achieving zero power burn**

Figure 2 Adding ALD ALD910024 SAB MOSFETs would bend C2 leakage current curve to follow I_{C2} + I_{OUT2} curve.

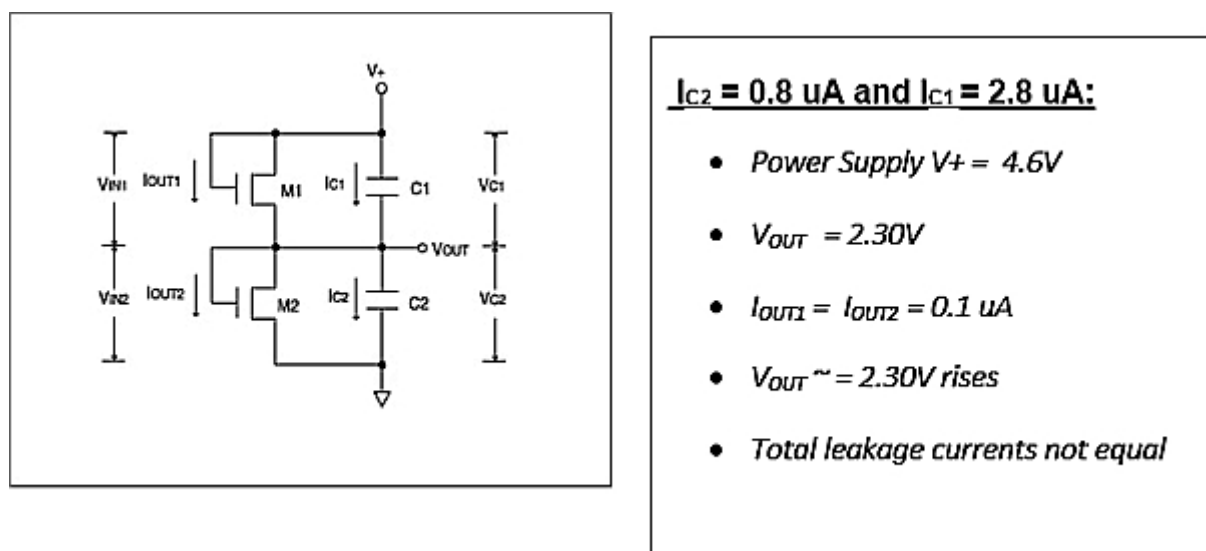**MOSFETs interact with supercapacitors for zero power burn**

Figure 3 Two supercapacitors stacked in series with ALD910024SAL MOSFETs.

The circuit action in **Figures 2** and **3** above can best be illustrated in three separate smaller steps.

Step 1

At Step 1, initially when V_{OUT} voltage is at 2.30V, the leakage currents of $I_{OUT1} + I_{C1}$ add up to 2.9 uA while $I_{OUT2} + I_{C2}$ add up to 0.9 uA. In other words, the leakage currents are not in balance while $V_{C1} = V_{C2} = 2.30V$. Therefore $V_{OUT} = 2.30V$ voltage is going to rise a little bit as I_{C1} current charges C2 up until SAB MOSFET M2 is turned on a little bit harder while M1 is turned off a little bit softer.

As SAB MOSFET output current changes exponentially with its bias voltage, I_{OUT1} and I_{OUT2} changes exponentially in opposite directions with small V_{OUT} voltage changes.

At Step 2, which is an arbitrary intermediate voltage point, V_{OUT} voltage now rises to 2.40V, which translates to $V_{C1} = 2.20V$ and $V_{C2} = 2.40V$. The total leakage current equation is still $I_{C1} + I_{OUT1} = I_{C2} + I_{OUT2}$.

Now let's take a look at the different currents under this new voltage condition. I_{C1} is now approximately 2.40 uA (see graph in **Figure 2**). I_{OUT1} is now at approximately 0.01 uA (see datasheet of ALD910024). Similarly, I_{C2} is at approximately 0.85 uA and I_{OUT2} is at approximately 1.0 uA. The leakage currents of $I_{OUT1} + I_{C1}$ now add up to 2.41 uA while $I_{C2} + I_{OUT2}$ add up to 1.85 uA. The leakage currents are still not in balance, which forces V_{OUT} voltage to continue to rise.

Without the SAB MOSFETs, V_{OUT} voltage continues to rise towards 4.60V. If it does, it will slowly destroy C2 as the $V_{C2} = V_{OUT}$ voltage exceeds 2.7V maximum rated voltage towards 2.9V, causing for example, an open circuit to C2 and rendering the entire supercapacitor series stack to become inoperative in a catastrophic failure event.

At Step 3, the V_{OUT} voltage reaches 2.45V. At this V_{OUT} voltage, all the currents are again changed. $V_{C1} = 2.15V$ and $V_{C2} = 2.45V$. I_{C1} is now approximately 2.20 uA (see graph in **Figure 2**). I_{OUT1} is now at approximately 0.003 uA. I_{C2} is at approximately 0.90 uA and I_{OUT2} is at approximately 1.303 uA. The leakage currents of $I_{OUT1} + I_{C1}$ now add up to 2.203 uA while $I_{OUT2} + I_{C2}$ also add up to 2.203 uA. The leakage currents are now in balance, which stabilizes V_{OUT} voltage at about 2.45V. V_{C1} and V_{C2} voltages are both within the 2.70V maximum rated voltage limits, and without any further changes, will not damage either of the two supercapacitors C1 and C2.

Any attempt to increase V_{OUT} voltage will meet with significant increases of I_{OUT2} thereby limiting further V_{OUT} voltage increase. At this point V_{OUT} resists any further changes due to minor changes in supercapacitor leakage currents of both C1 and C2. When this equilibrium point is reached, the total leakage current of $I_{OUT1} + I_{C1}$ is now ~2.203 uA instead of the I_{C1} of 2.80 uA without leakage current balancing. This example illustrates that "negative", or below zero power burn is possible when the balancing circuitry utilizing SAB MOSFET is deployed.

Example

In this example, the extra power is dissipated by I_{OUT1} which is about 0.003 uA. I_{C1} of C1, now at ~2.20 uA is the dominant leakage component internal to the supercapacitor, and it is less than the reference leakage current specified as 2.80 uA at 2.3V cell voltage. Net additional current burn is 0.003 uA, ~0.1% of 2.80 uA, which is approximated to zero power burn. Note that this 0.1% is that of the leakage current specification of the supercapacitor. So if that leakage current is greater or lesser, for different make or models, the extra power burn can be scaled accordingly.

For circuits described above, MOSFETs sense that the voltage wants to go up, so one of them starts leaking current very quickly, without allowing the voltage to go up much. Because it is exponential in nature and the current goes up, it will automatically float to a point where the MOSFET current I_{OUT1}, plus the I_{C1} current would be equal to the leakage current of MOSFET, I_{OUT2} plus I_{C2}.

There is a push-pull dynamic relationship. In other words, there are two supercapacitors and two MOSFETS, but only one MOSFET is turned on harder at any given time while the other MOSFET would be turned on a little softer. Since there is no way to know which supercapacitor has higher leakage, placing the MOSFET across both supercapacitors will balance the network automatically. Since the specific leakage of each cell is unknown, the one that has the higher leakage would be automatically balanced by the corresponding MOSFET. When a MOSFET is placed across each supercapacitor, it automatically balances the system, by equalizing whichever supercapacitor has the highest leakage current.

To summarize, MOSFETs can:

• lower additional leakage current to zero levels
• completely and automatically balance supercapacitors
• offers low component count and low implementation costs
• provide simple and yet elegant solution
• offer scalability to any number of supercapacitors
• adjusts for changing environmental conditions and leakage currents.

The examples illustrated above explain the zero power dissipation operation of the balancing circuit action. However, there are numerous other possible combinations, where the SAB MOSFET balancing solution, while adding little or no leakage, does allow a lower voltage bias on the leakier supercapacitor. The actual total leakage current, and hence the power dissipation caused by the series-connected supercapacitors can be potentially less than not balancing the circuit at all.

Selecting the right SAB MOSFET requires knowledge of the supercapacitor operating voltage and maximum rated leakage current. This balancing method limits leakage current better than any other method. SAB MOSFETs also actively adjust to different temperature or supercapacitor chemistry changes. A designer can just pick the maximum operating voltage margin and the maximum leakage current for the particular supercapacitor(s) and look up the correct SAB MOSFET part number. For more information, go to the ALD website and search: sab mosfet.