# SiO Molecular Jets around young stars - A numerical perspective

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#### ABSTRACT

**Key words:** MHD – methods:numerical – ISM: jets and outflows

### INTRODUCTION

### NUMERICAL SETUP

#### Numerical code and Equations

For our study, we carry out axisymmetric numerical ideal MHD simulations using the PLUTO code (Mignone et al. 2007) which is based on a conservative scheme of Godunov type. We have modified the original code to incorporate molecular cooling from self-consistent evolution of hydrogen chemistry (see Sect. 3).

In general, the MHD code considers the following set of equations. The conservation of the mass and the momentum,

$$\frac{\partial \rho}{\partial t} + (\vec{v} \cdot \nabla)\rho + \rho \nabla \cdot \vec{v} = 0 \tag{1}$$

$$\rho(\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \nabla)\vec{v}) = -\nabla P + \frac{1}{4\pi}(\nabla \times \vec{B}) \times \vec{B} \qquad (2)$$

where  $\rho$  is gas density,  $\vec{v}$  the velocity vector, P the gas pressure, and  $\vec{B}$  the magnetic field vector with the poloidal and toroidal components -  $\vec{B}_{\rm p}, B_{\phi}$ . Note that the forces due to gravity are neglected for this problem as the domain of interest is far away from the central object (i.e., star).

The cooling function  $\Lambda$  which dependents on temperature T, mass density  $\rho$  and chemical abundances X, appears in the energy equation as a source term,

$$\frac{\partial}{\partial t}(\rho E) + \nabla \cdot \left[ \rho E \vec{v} + (P + \frac{B^2}{8\pi}) \vec{v} \right] - \vec{B}(\vec{v} \cdot \vec{B}) = \Lambda(\rho, T, \mathbf{X}), \tag{3}$$

where the total energy density of the flow E comprises contributions from the internal energy  $\epsilon$ , the mechanical energy and the magnetic energy,

$$E = \epsilon + \frac{v^2}{2} + \frac{B^2}{8\pi\rho}.\tag{4}$$

The gas pressure in the flow is related to the density assuming an equation of state with the adiabatic index  $\gamma$ ,

$$P = (\gamma - 1)\rho\epsilon. \tag{5}$$

The evolution of chemical abundances for each spiecies is solved via,

$$\frac{\partial \rho \mathbf{X}_i}{\partial t} + \nabla \cdot (\rho \mathbf{X}_i \vec{v}) = \rho \mathbf{S}_i, \tag{6}$$

where  $S_i$  represents the net creation or destruction of a given spiecies through chemical reactions (see Sect. 3).

The evolution of the magnetic field is governed by induction equation,

$$\frac{\partial \vec{B}}{\partial t} = \nabla \times \left( \vec{v} \times \vec{B} \right). \tag{7}$$

In addition to the above set of equations the code obeys the condition of divergence-free magnetic fields,  $\nabla \cdot \vec{B} = 0$ , which is numerically achieved by construction since using the Powell's eight wave formulation.

#### 2.2Initial Condition

Describe initial condition - Geometry, domian size, boundary conditions

Physical motivation of initial condition.

### CHEMISTRY AND COOLING

Atomic Cooling

Molecular cooling fixed abundance – Tabulated Cooling Molecular cooling with chemistry.

Mention briefly Adiabatic and Powerlaw cooling.

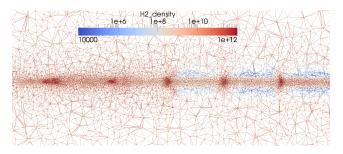
### RADIATIVE TRANSFER

Radiative transfer modelling used for post processing.

Table 1. Summary of the chemistry reaction set. T is the temperature in Kelvin,  $T_{\rm eV}$  is the temperature in electron-volts,  $T_5 = T/1 \times 10^5$  and  $T_2 = T/100$ 

No.	Reaction	Rate Coeff (cm <sup>3</sup> s <sup>-1</sup> )	Reference a
1.	$H + e^{-} \rightarrow H^{+} + 2e^{-}$	$k_1 = 5.85 \times 10^{-11} \ T^{0.5} \ \exp(-157,809.1/T)/(1.0 + T_5^{0.5})$	1
2.	$\mathrm{H^+ + e^-} \rightarrow \mathrm{H + h}\nu$	$k_2 = 3.5 \times 10^{-12} (T/300.0)^{-0.8}$	2
3.	$H_2 + e^- \to 2H + e^-$	$k_3 = 4.4 \times 10^{-10} T^{0.35} \exp(-102,000.0/T)$	3
4.	$H_2 + H \rightarrow 3H$	$k_4 = 1.067 \times 10^{-10} T_{\rm eV}^{2.012} (\exp(4.463/T_{\rm eV})^{-1} ((1.+0.2472T_{\rm eV})^{3.512})^{-1}$	4
5.	$\mathrm{H_2}+\mathrm{H_2}\rightarrow\mathrm{H_2}+\mathrm{2H}$	$k_5 = 1.0 \times 10^{-8} \exp(-84, 100/T)$	2
6.	$H + H \stackrel{dust}{\longrightarrow} H_2$	$k_6 = 3.0 \times 10^{-17} \sqrt{T_2} (1.0 + 0.4 \sqrt{T_2 + 0.15} + 0.2T_2 + 0.8T_2^2)$	5

<sup>a</sup> REFERENCES – (1) Cen (1992) [Eq. 26a]; (2) Woodall et al. (2007) [UMIST Database] (3) Galli & Palla (1998) [Eq. H17]; (4) Abel et al. (1997) [Tab. 3 Eq. 13]; (5) Hollenbach & McKee (1979) [Eq. 3.8]



**Figure 1.** A plot of the points selected by the gridding process and the paths down which photons can propagate for points in the r,z plane. The points are colour coded by the density distribution (in  ${\rm m}^{-3}$ , as used in LIME) and are more concentrated in the high density knots.

### 4.1 The radiative transfer code

The radiative transfer program used is LIME (LIne Modelling Engine; Brinch & Hogerheijde 2010), which calculates line intensities based on a weighted sample of randomly chosen points in a continuous 3D model. The method of selecting these points is given in section 4.2. At each of these points, the density of the main collision partner (equivalent amount of  $H_2$ , given by  $n(H_2) + 0.5 n(H)$ , gas and dust temperatures, velocity, molecular abundances and unresolved turbulent velocity are specified. These points are then smoothed by Lloyd's algorithm (Lloyd 1982) in order to minimise the variation in distance between points whilst keeping the same underlying distribution. These points are then connected by Delaunay triangulation and it is between the points connected by this method that photon are allowed to propagate (fig. 1). The level populations of the selected molecules are calculated at each of these points from collisional and radiative (de)excitation and the local radiation field is calculated. This is repeated 20 times with the populations of each level converging towards a single value. This number of iterations is sufficient for the signal to noise ratio of the level populations (as defined in Brinch & Hogerheijde 2010) to exceed 1000 for 99% of the points, ensuring that the simulation has converged on a stable level population. After 20 iterations the model is ray-traced in order to produce synthetic brightness maps. The average of ten separate runs was taken to minimise the artefacts in the output images, resulting from the grid construction (Fig. 2).

#### 4.2 Grid construction

In order to construct the grid, candidate points are randomly selected from the volume to be simulated. These candidates then have their equivalent H<sub>2</sub> number density, and the number density of SiO, compared against those of a reference point in order to decide if the candidate point is to be used in the grid or not. Candidate grid points are selected at random in a cylindrical coordinates that is linearly spaced in z and  $\theta$  and logarithmically spaced in r. For each point to be selected, a random number  $\alpha$  is drawn from the semi-open set [0,1) as a threshold. After selection of random coordinates, the H<sub>2</sub> density and SiO density at the candidate point (n and m, respectively) are compared against the densities of a reference point in the unpeturbed ambient medium multipled by  $\frac{4\eta}{5}$  (n<sub>0</sub> and m<sub>0</sub>). If  $\alpha < \left(\frac{n}{n_0}\right)^{0.3}$  or  $\alpha < \left(\frac{m}{m_0}\right)^{0.3}$  then the point is selected for use. Otherwise another r,  $\theta$ , z co-ordinate is selected and it becomes the candidate point. In addition to this method of selection, 5% of the points are linearly distributed in x, y and z with no bias with regards to density or abundance. This provides a minimum level of sampling for the large low density regions in the outer parts of the simulated volume. See fig. 2 for an example of the points distribution in r, z. The function comparing the candidate point to the reference point and the candidate point distribution were selected empirically to sample all scales while ensuring that the majority of points are located in the inner disc where the density is higher.

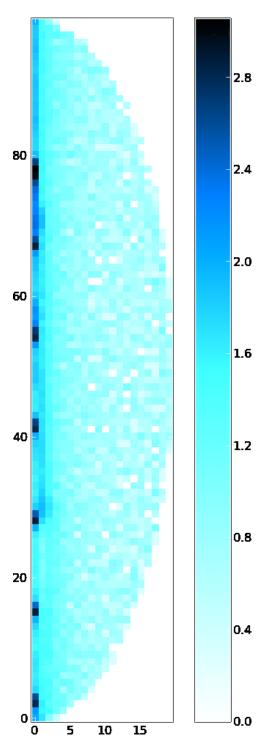
### 4.3 SiO abundance

Need refs for this!!The amount of SiO is determined by the

local velocity and temperature. The fractional abundance is given by the equation:

$$log(X) = -2.48 \times 10^{-8} v^5 + 5.50 \times 10^{-6} v^4 - 4.28 \times 10^{-4} v^3 + 1.24 \times 10^{-2} v^2 + 2.52 \times 10^{-2} v - 1.20 \times 10^1$$

where v is in kilometres per second. In addition to this if the temperature at the point is greater than 92,000K (the temperature of the Si-O bond disassociation energy) the abundance is reduced to  $10^{-30}$ .



**Figure 2.** A 2D histogram of the point distribution throughout the model. The disc and envelope can be seen as two separate entities which have to be sampled using different point distributions.

### 5 RESULTS

Table 1 – Parameter runs with changing  $\beta$  (magnetic fields) and  $\eta$  (density contrast) for cooling

Results should have Peak Intensity after convolution., FWHM at tip of bow shock.

Our reference run –  $\beta = 10.0$ ,  $\eta = 2.0$ , with cooling and

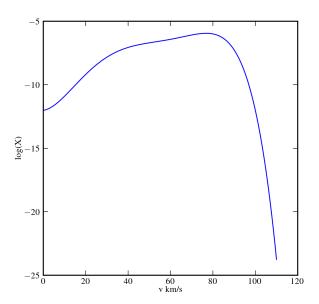


Figure 3. The polynomial used to calculate an abundace of SiO as a function of local velocity.

velocity dependent SiO Abundance.

Figure 3 – Output from MHD simulations (Reference run). Figure 4 – Output from Rad Transfer (Reference run). Integrated Intensity Maps for different transitions for three different cooling prescribtions. (TODO: TOM)

Figure 5 – Spectra for the reference runs all transitions. (TODO : TOM)  $\,$ 

Figure 6 – PV diagrams (TODO : TOM) for one transition in two directions. Figure 7 – Angle of Inclination dependence

### 6 DISCUSSION

Effects of varying  $\beta$ ,  $\eta$ Importance of cooling prescriptions RADEX plots ratio of Line intensities??? Comparison with Observed results Limitations

### 7 ALMA VIEW

ALMA view of the reference run and stress of applying our synthetic techniques to study the molecular outflows in more details.

Figure 6. for ALMA –

### 8 CONCLUSION

We are the best in modelling SiO outflows.

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