

# ARPA-E Review: TEA Update

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# Relevant Milestone

**M2.1 TEA trade-off analysis on expended operational design space:** Detailed TEA that allows precise quantitative target metrics for the following most critical drivers of overall system cost: electrodialyzer current density, electrodialyzer voltage, membrane contactor operating pH, membrane contactor CO<sub>2</sub> removal rate, and three different power generation sources (solar, solar-battery, grid assisted renewables). This ensures that target values for milestones are precise and will be used to inform future system designs.

# TEA Outline

Overview & comparison to previous work

TEA Trade-Off Analysis:

1. Electrodialyzer current density & voltage
2. Power generation source
3. Membrane contactor vacuum level and CO<sub>2</sub> removal rate
4. Membrane contactor pH

Integration with thermodynamic system tradeoff analysis (M2.2)

# TEA Outline

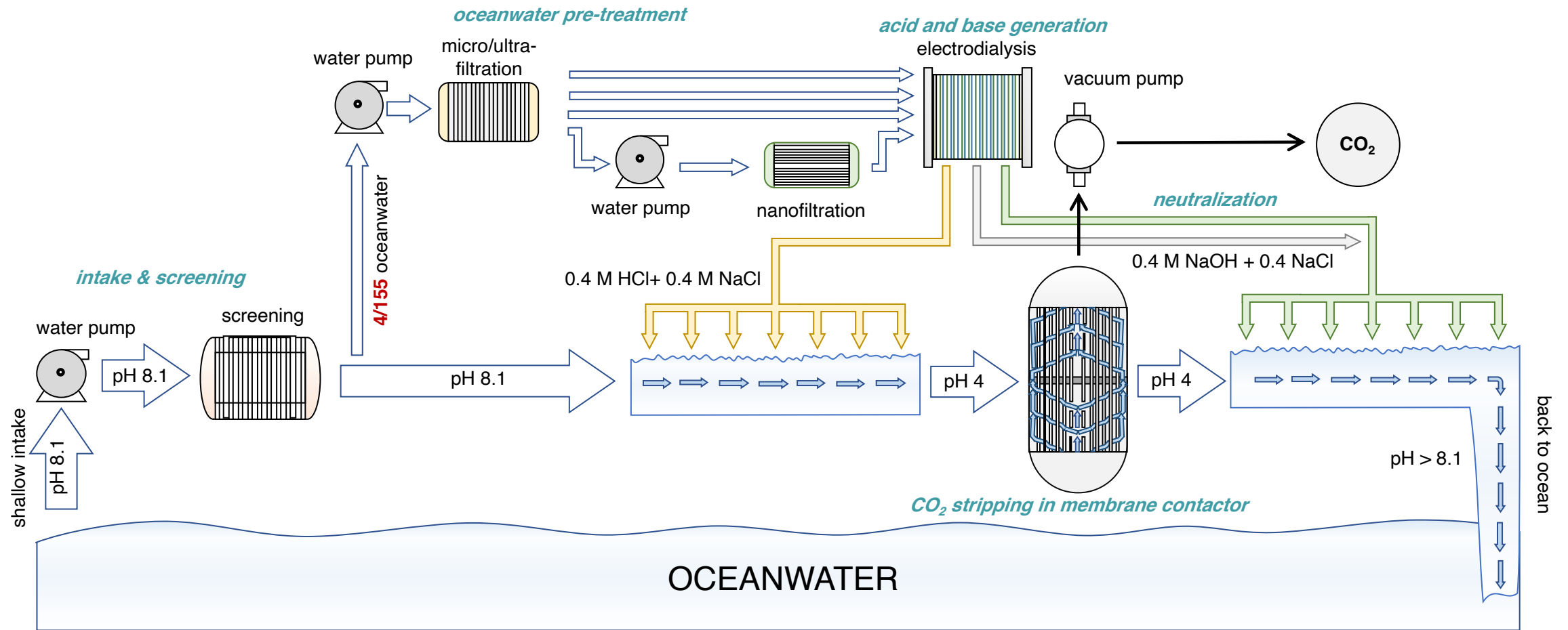
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# Current TEA is based on this system

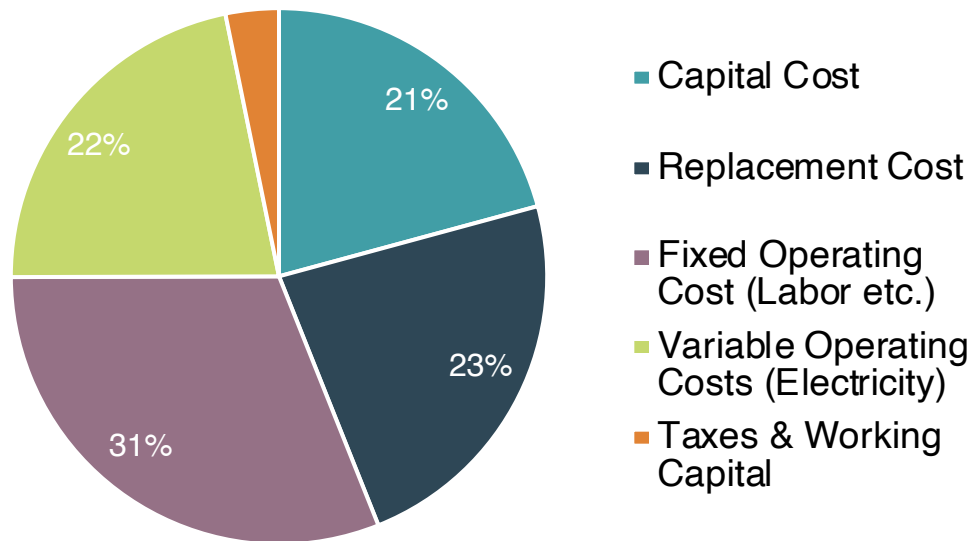


# Key costs and parameter values

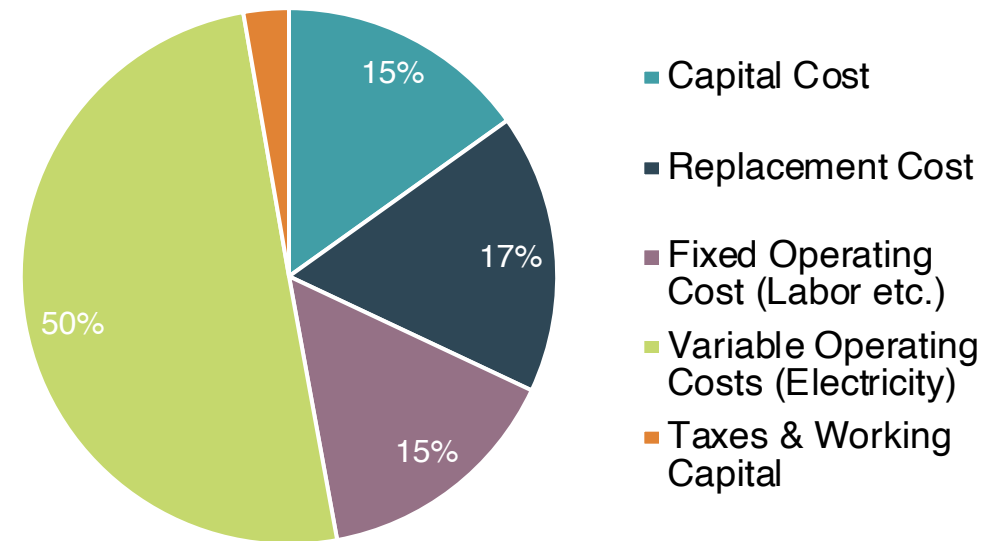
Item	Cost	Parameter	Value
Centrifugal pump (27,000 m <sup>3</sup> /day)	\$42,000	Oceanwater target pH**	4
Electrodialysis membrane cost	\$0.05/cm <sup>2</sup>	Membrane contactor efficiency	90%
Membrane contactor cost (1,920 m <sup>3</sup> oceanwater/day)	\$6600	Electrodialyzer current density**	500 mA/cm <sup>2</sup>
Vacuum pump cost (240,000 m <sup>3</sup> /day)	\$252,000	Electrodialyzer voltage**	2.5 V per cell
Intake piping* (400,000 m <sup>3</sup> /day)	\$420,000	Liquid ring vacuum pump base pressure**	35 Torr
Microscreening* (400,000 m <sup>3</sup> /day)	\$3,247,000	Scale	10 kiloton/yr ( <b>current</b> ) 1 megaton/yr ( <b>future</b> )
Microfiltration* (10,000 m <sup>3</sup> /day)	\$1,555,000	Electricity price	\$0.04/kWh ( <b>current</b> ) \$0.02/kWh ( <b>future</b> )
Nanofiltration (3,000 m <sup>3</sup> /day)	\$135,000	Labor cost (12.5 full-time employees at 10-kiloton/yr scale)	\$40,000/year average salary

Current cost is **\$537/ton**, future cost is **\$117/ton CO<sub>2</sub>**

**10 Kiloton Scale: Cost Breakdown**



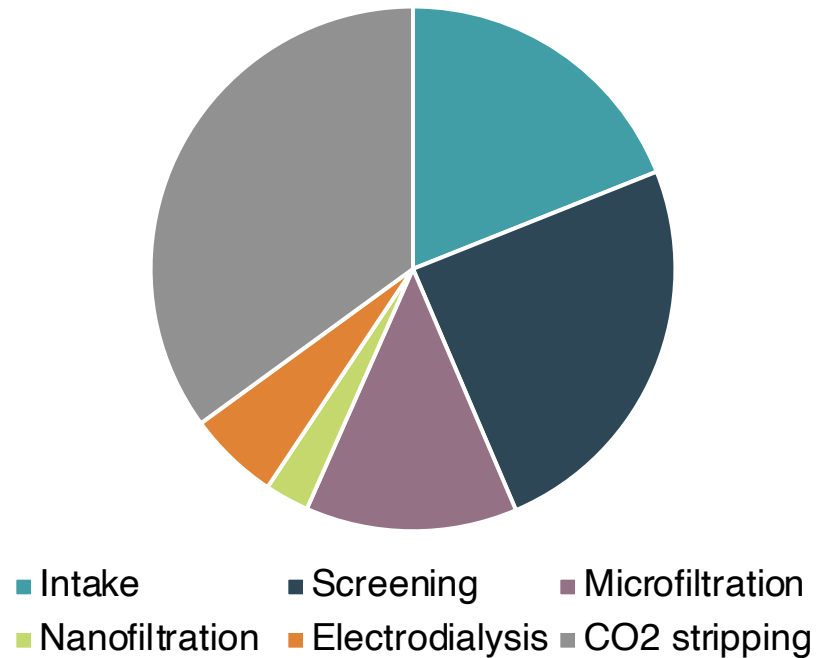
**1 Megaton Scale: Cost Breakdown**



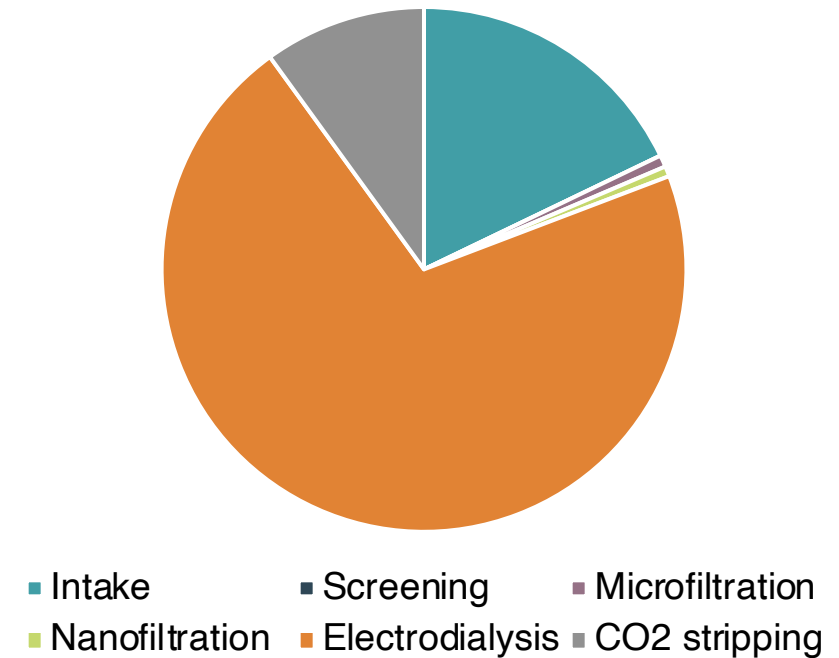
→ CapEx scales according to 6/10 rule, so becomes less significant at larger scales

# CO<sub>2</sub> stripping dominates CapEx, electrodialysis electricity dominates OpEx

**Direct Capital Cost by Process Step**



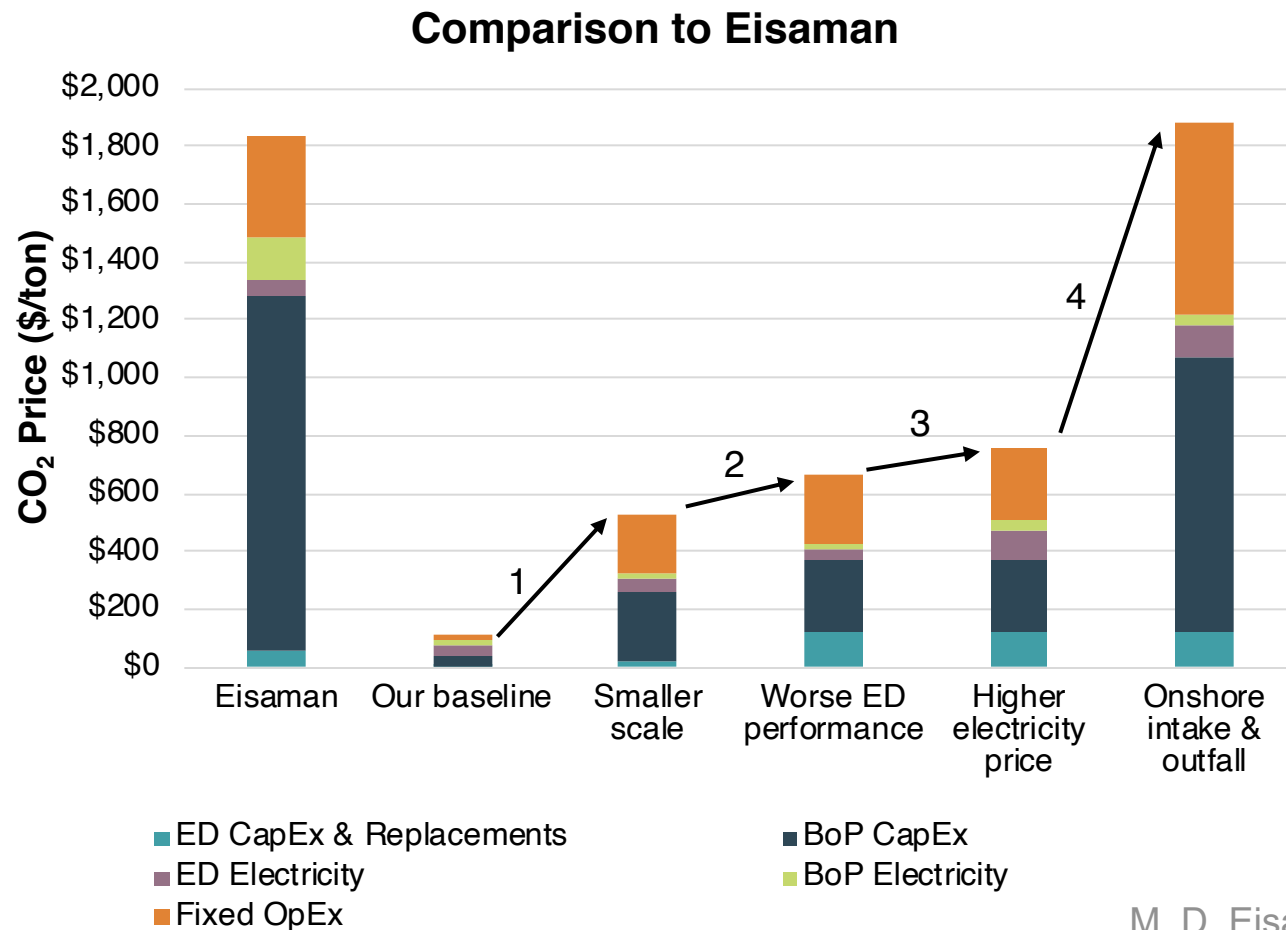
**Electricity Cost by Process Step**



→ Within each category (CapEx vs. electricity), breakdown by process step is the same at different scales



We achieve much lower CO<sub>2</sub> prices than previous papers (Eisaman *et al*) mostly due to larger scale, offshore intake



1. **Scale**  
1 megaton/year (us) → 7700 tons/year (them)
2. **Electrodialyzer current density**  
500 mA/cm<sup>2</sup> (us) → 100 mA/cm<sup>2</sup> (them)
3. **Electricity cost**  
\$0.02/kWh (us) → \$0.04/kWh (them)
4. **Intake/outfall**  
20x higher intake/outfall costs due to onshore intake & outfall

M. D. Eisaman *et al.*, *Int. J. Greenh. Gas Control.* **70**, 254–261 (2018)

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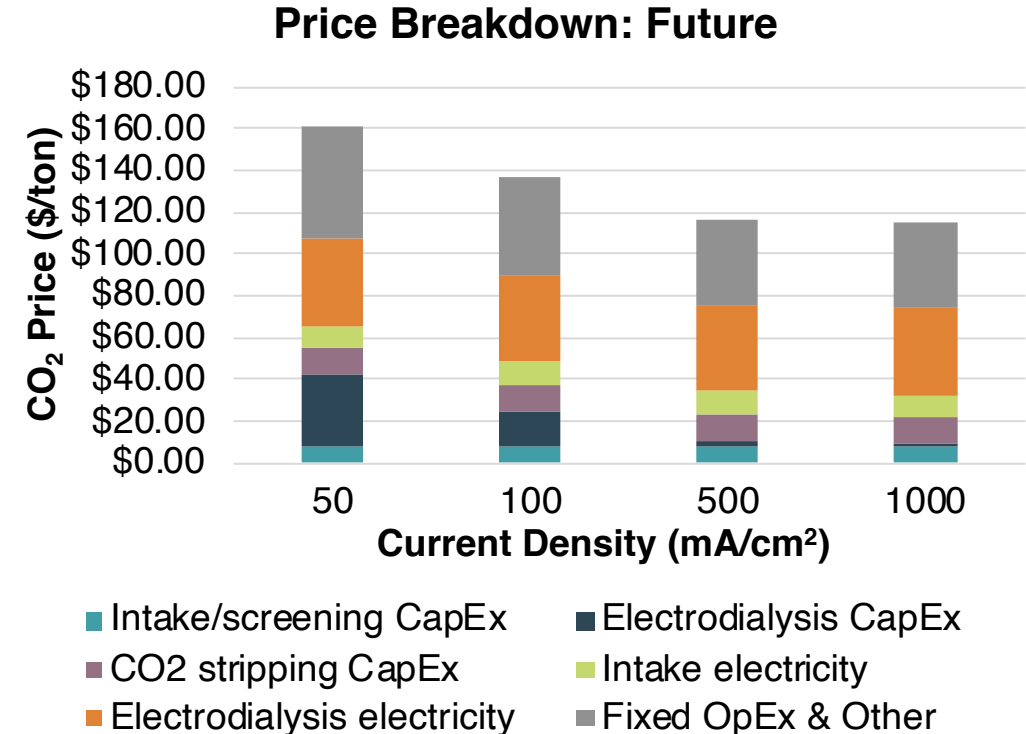
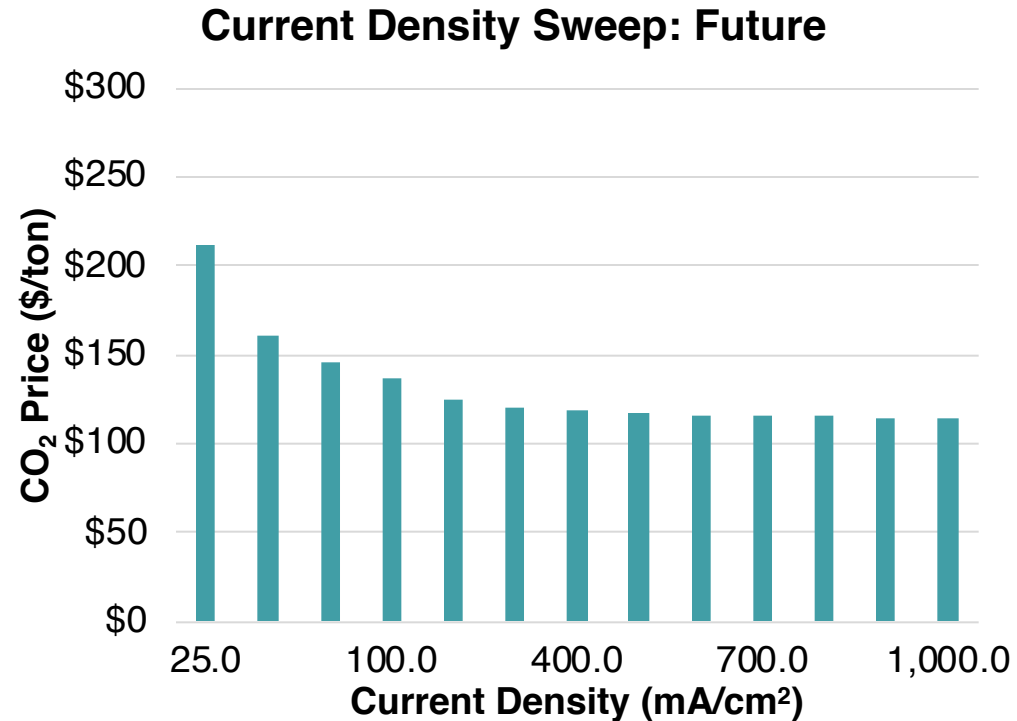
1. **Electrodialyzer current density & voltage**
2. Power generation source
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4. Membrane contactor pH

Integration with thermodynamic system tradeoff analysis (M2.2)

# Diminishing returns to increasing current density above 500 mA/cm<sup>2</sup> at megaton scale

Current density only affects electrolyzer CapEx, not OpEx

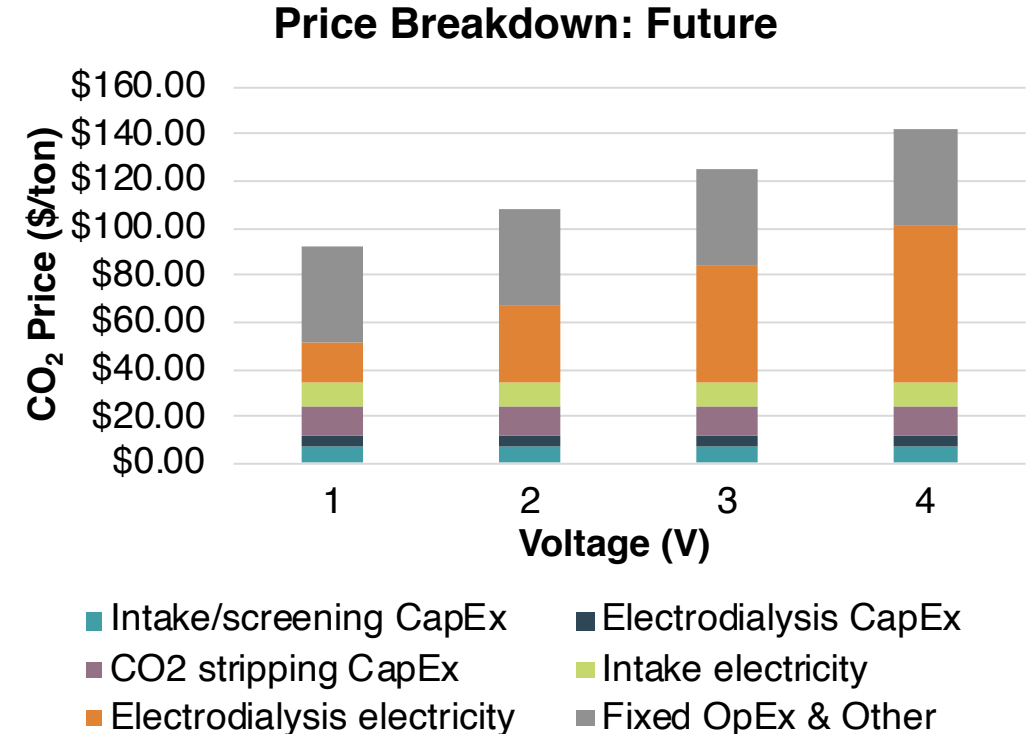
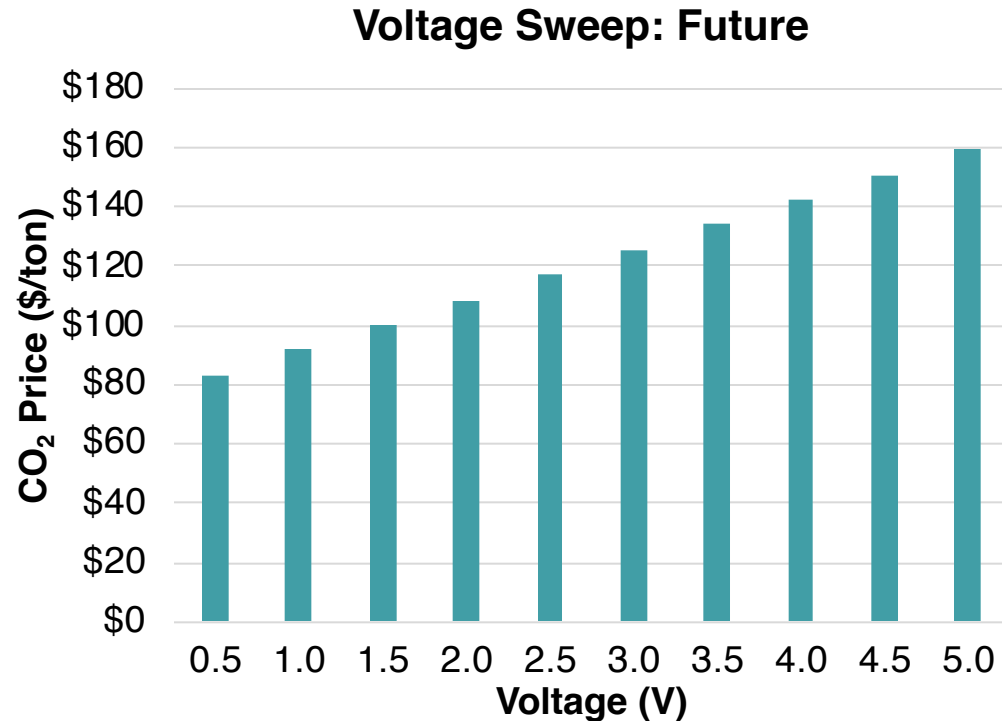
Above 500 mA/cm<sup>2</sup>, electrolyzer CapEx (dark blue bars) becomes negligible (same finding holds at 10-kiloton scale)



# At megaton scale, reducing voltage reduces CO<sub>2</sub> price monotonically

Voltage only affects electrolyzer OpEx, not CapEx

Electrolyzer electricity price alone varies with voltage & remains significant down to 1 V (same finding holds at 10-kiloton scale)



# TEA Outline

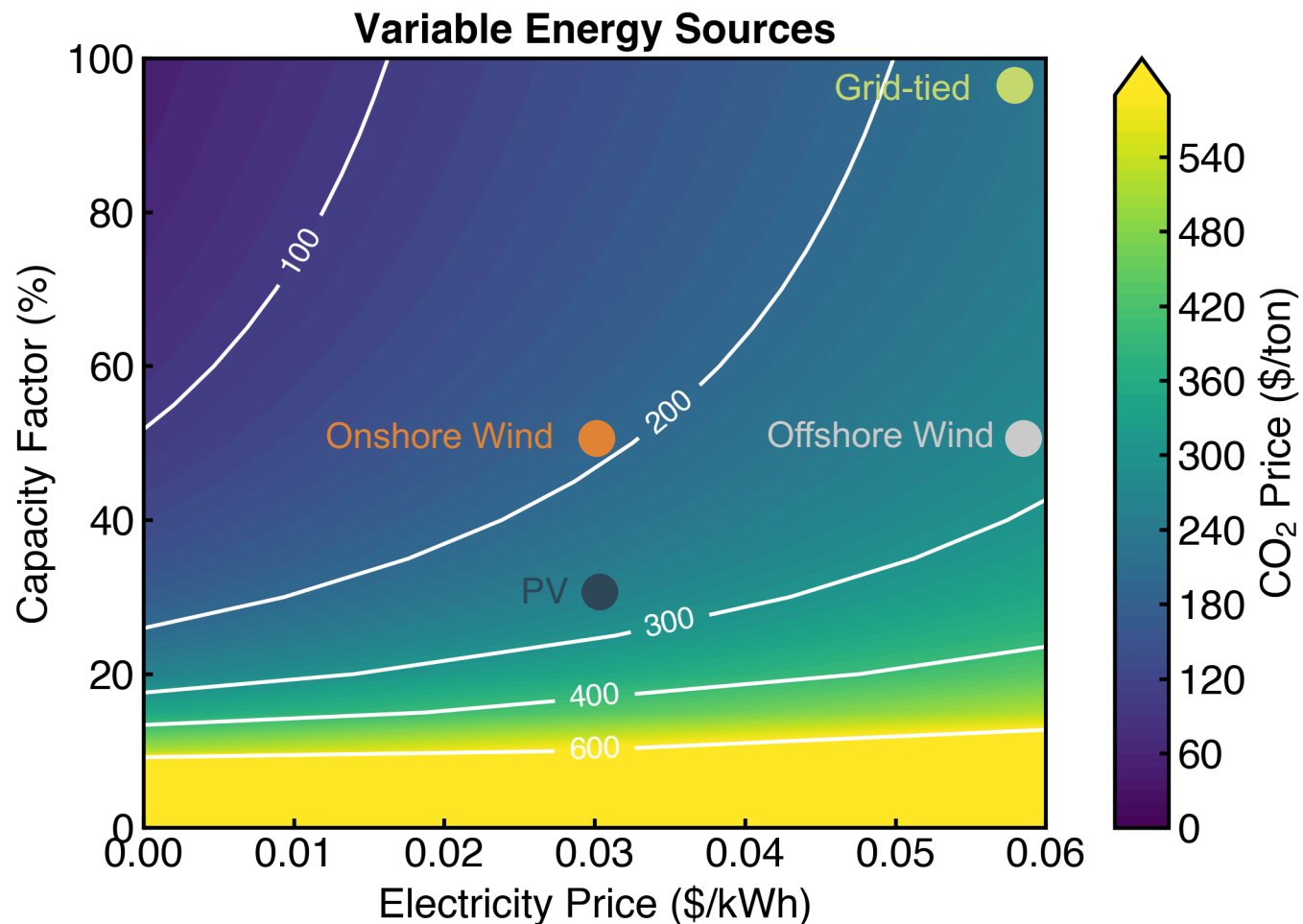
Overview & comparison to previous work

TEA Trade-Off Analysis:

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Integration with thermodynamic system tradeoff analysis (M2.2)

# What if we have an electricity source that's almost free, but with a lower capacity factor?



- Renewables on grid may eventually lead to need for curtailment: using extra electricity when wind/solar are overproducing
- If electricity is free, we can have capacity factors as low as 50% and achieve less than \$100/ton
- If we are paid to use electricity for optimizing grid load, we can have even lower capacity factors

*Capacity factors & electricity prices from EIA Energy Outlook, NREL ATB, Lazard*

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Overview & comparison to previous work

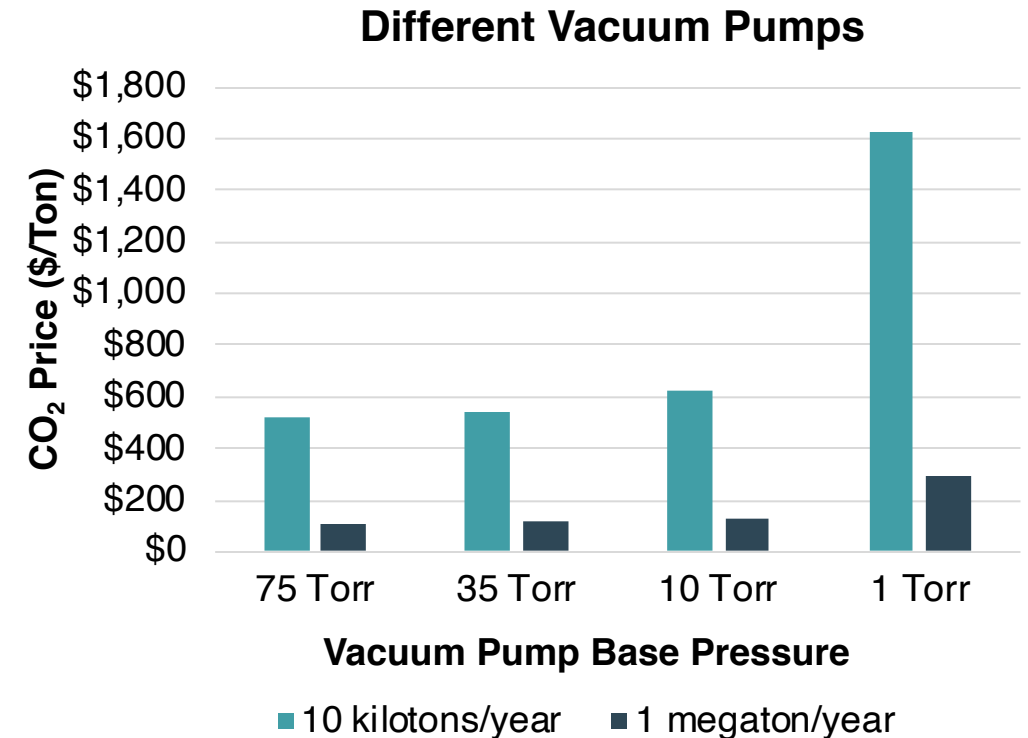
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Integration with thermodynamic system tradeoff analysis (M2.2)

# CO<sub>2</sub> cost is very sensitive to level of vacuum, because vacuum pumps have a maximum volumetric flow rate

- Most pumps have a maximum volumetric flow rate, since they are positive displacement pumps (remove a volume of gas over and over)
- At lower base pressures and the same **volumetric** flow rate, our **molar** flow rate becomes much smaller
- We need 10x as many pumps with the same max flow rate to get the same CO<sub>2</sub> throughput if we go from 10 Torr to 1 Torr
- Effect of increasing number of pumps becomes significant around 1 Torr





# TEA Outline

Overview & comparison to previous work

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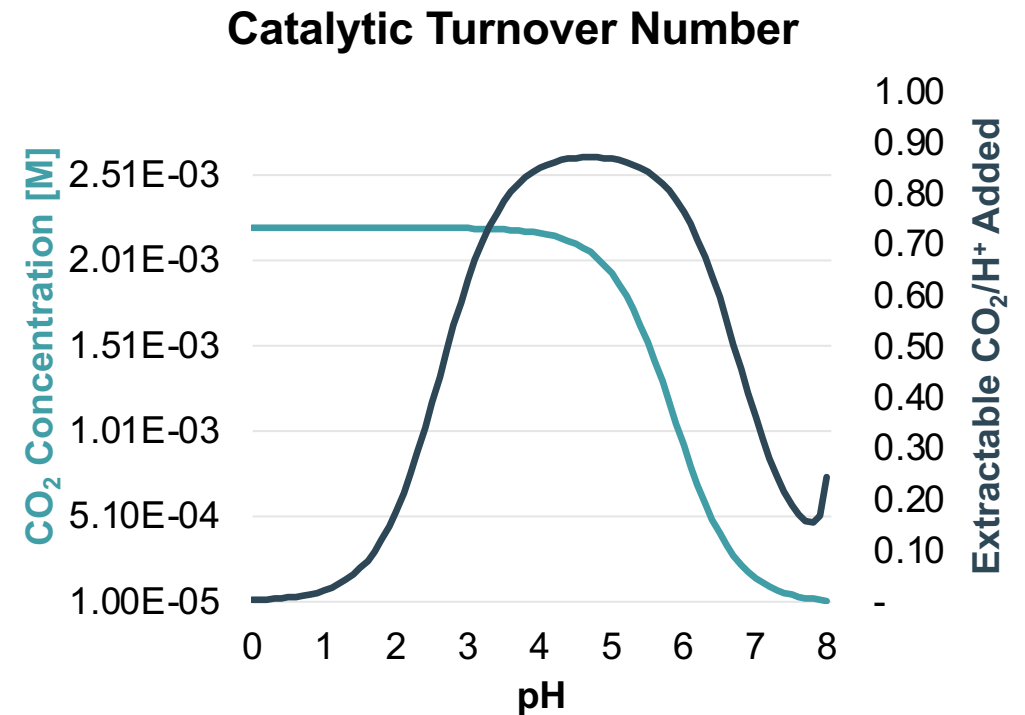
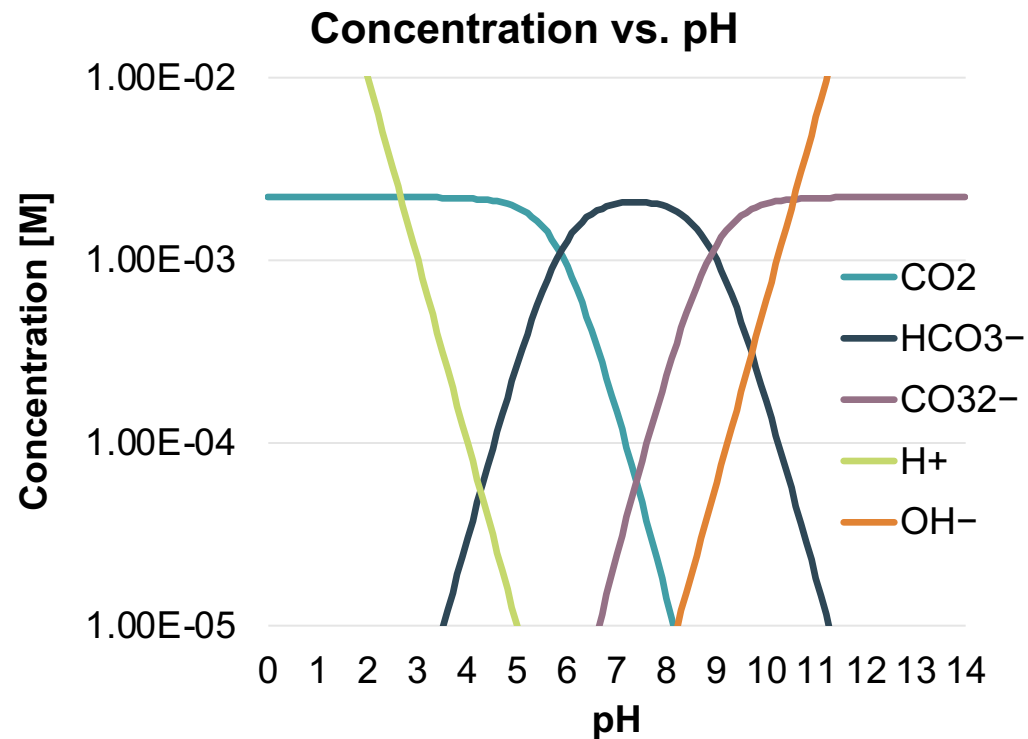
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Integration with thermodynamic system tradeoff analysis (M2.2)

Key metric: catalytic turnover number, which is extractable  $\text{CO}_2$  per  $\text{H}^+$  added

Can also define a catalytic turnover factor  $F_{\text{CT}}$  that denotes the catalytic reaction rate enhancement

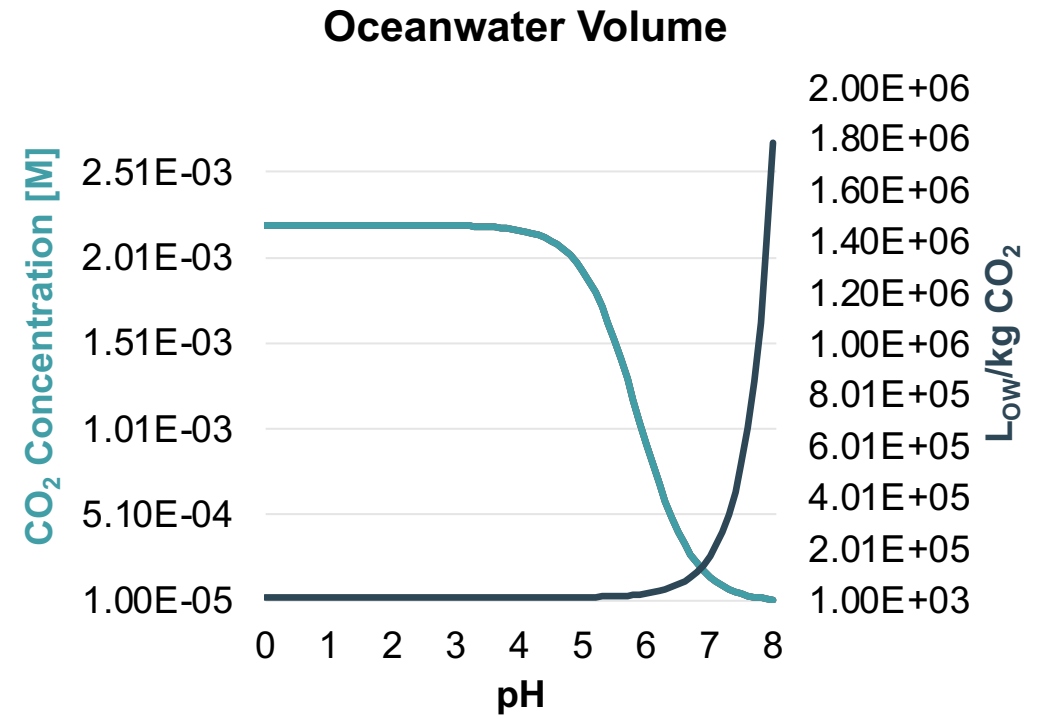
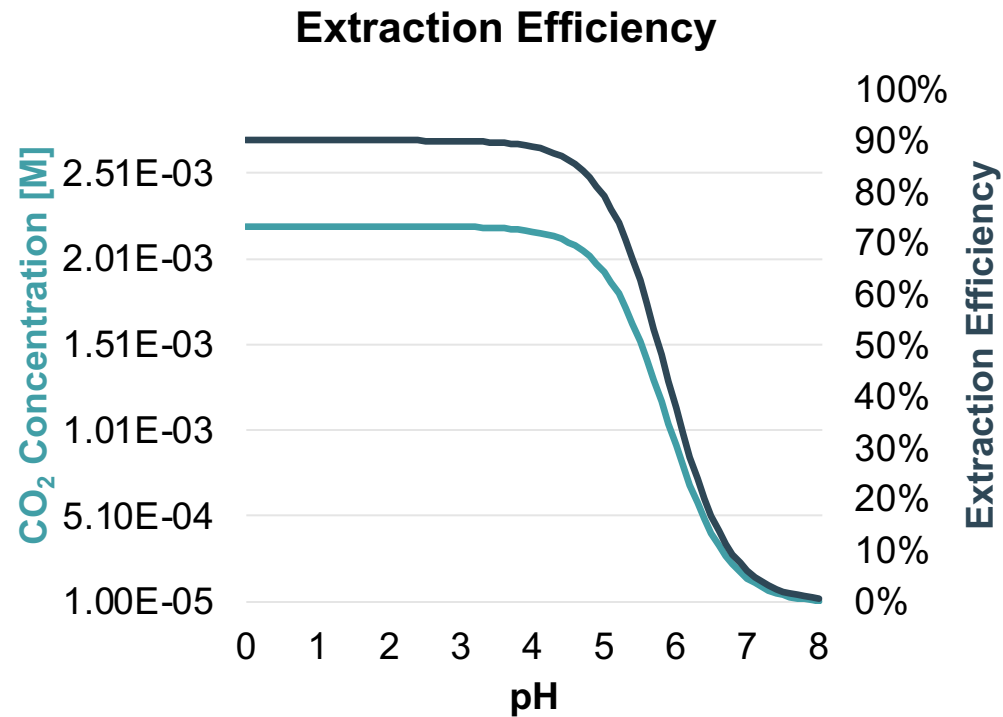
When extracting equilibrium concentration of  $\text{CO}_2(\text{aq})$ ,  $F_{\text{CT}} = 1$ . Otherwise,  $F_{\text{CT}}$  could be  $>1$  or  $<1$



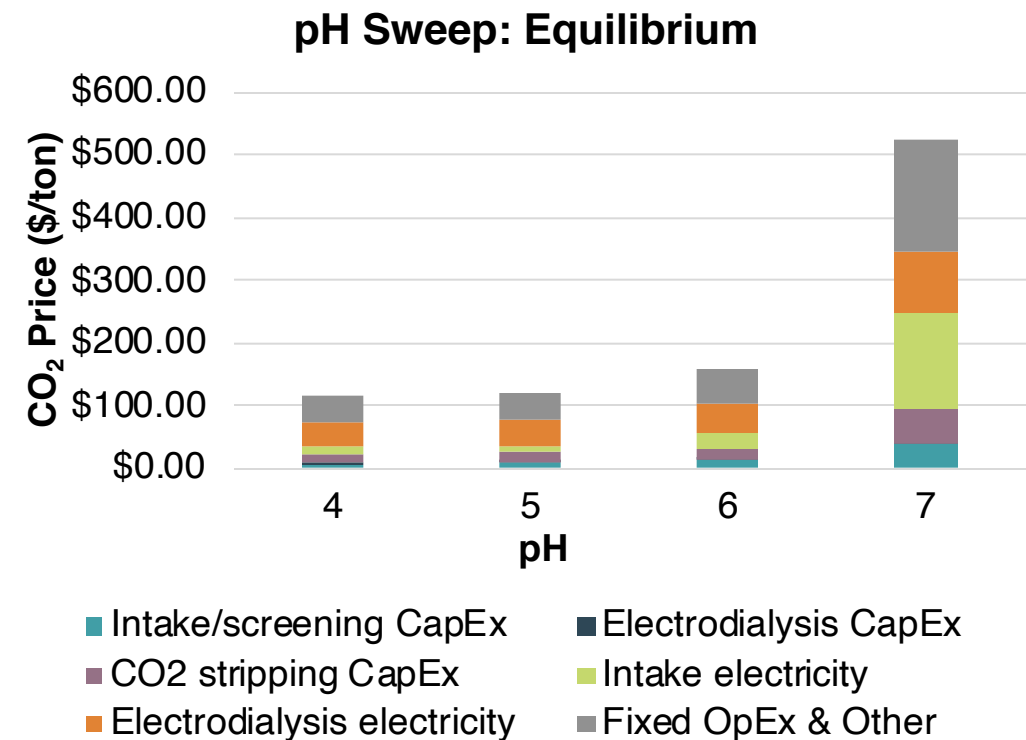
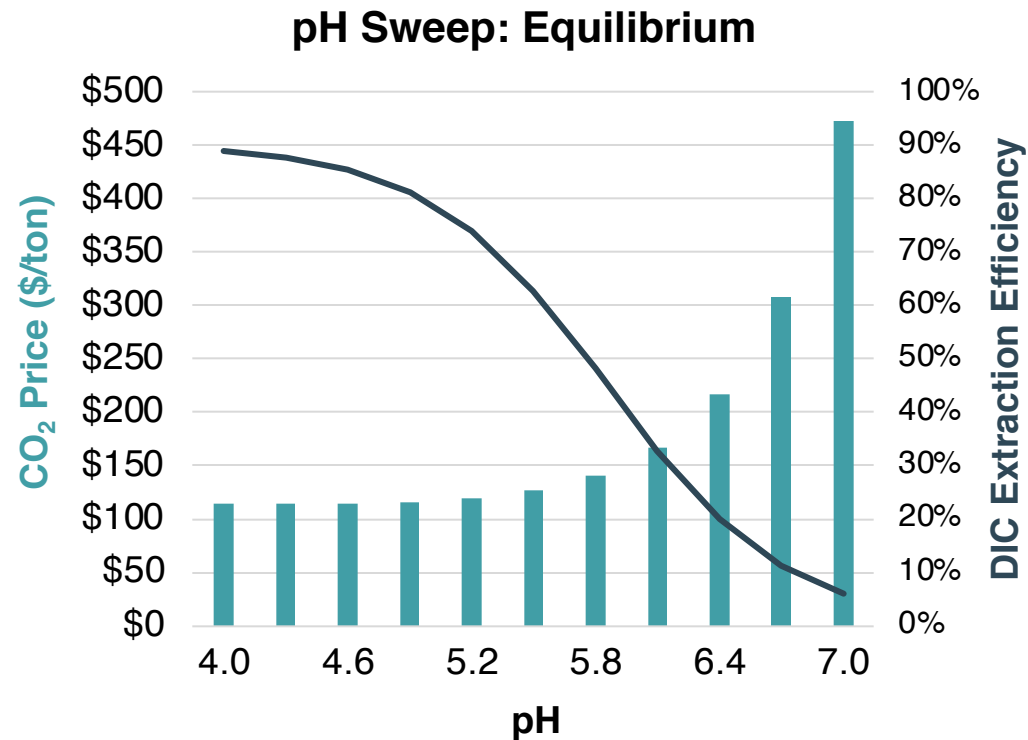
# Extraction efficiency is CO<sub>2</sub> extracted per DIC in oceanwater

Equilibrium curves are shown here – pumping huge oceanwater volumes at higher pH

In steady-state or with catalysis, extraction efficiency could be enhanced by a factor equal to the “catalytic turnover factor”



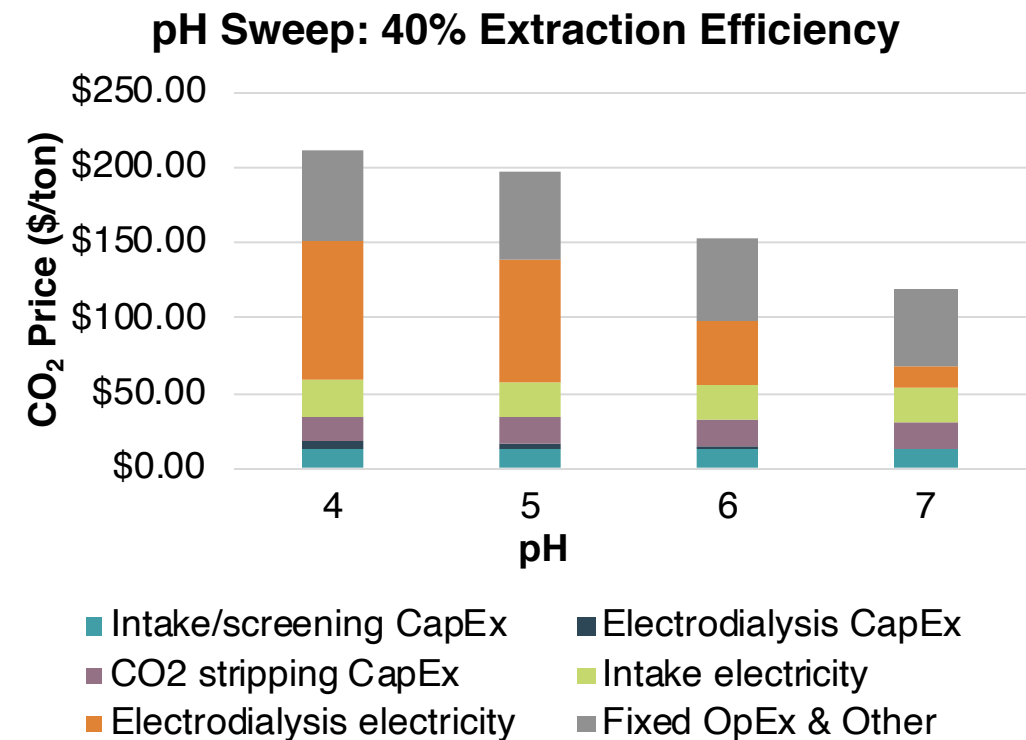
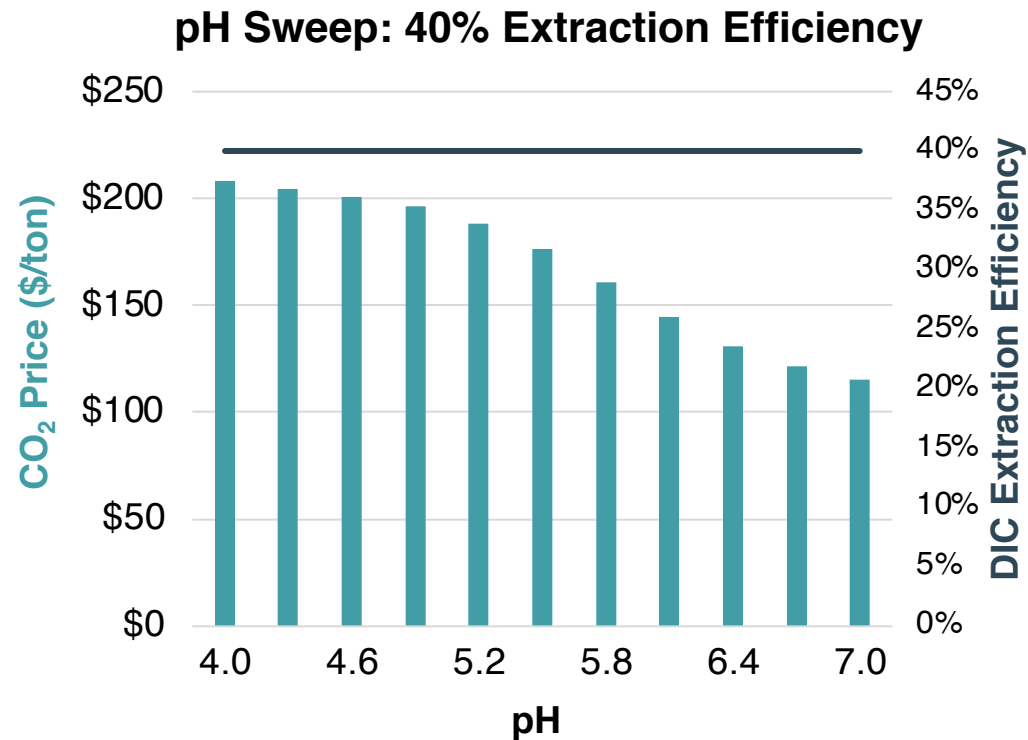
Extracting the equilibrium concentration of CO<sub>2</sub> at a given pH, CO<sub>2</sub> price increases as pH increases



Due to decreased extraction efficiency

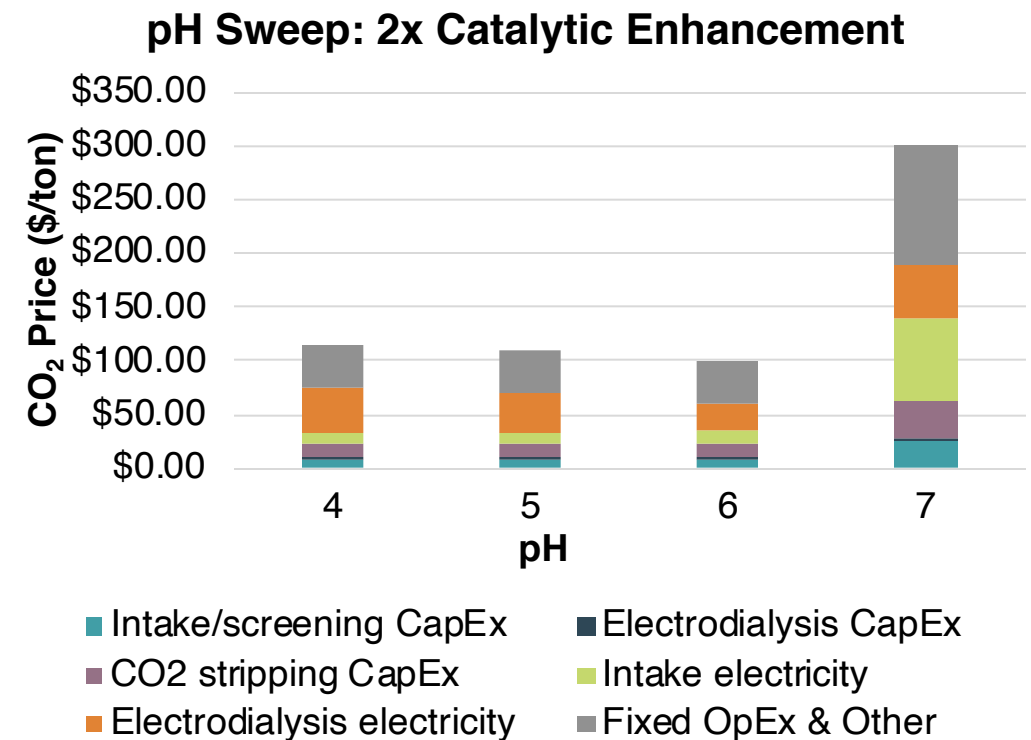
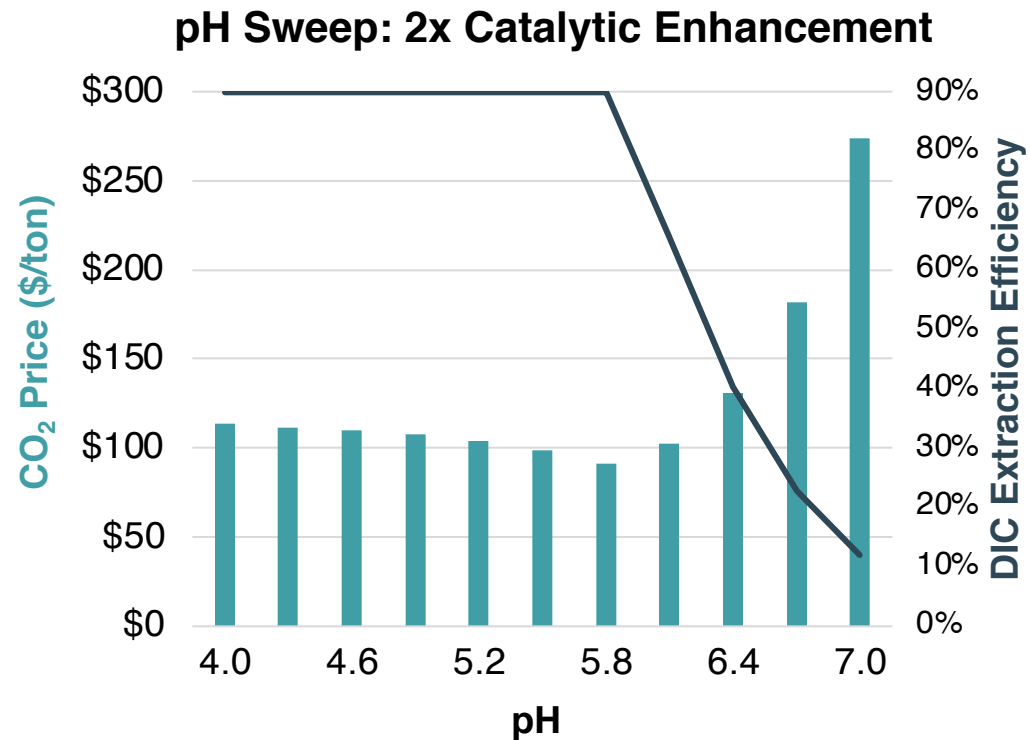
This mostly increases intake electricity costs (green bars) – at lower extraction efficiencies, we process more water

If we can achieve higher extraction efficiency at higher pH via catalysis, cost drops substantially



Price decreases as pH increases since we have to acidify a smaller fraction of the oceanwater through electrodesialysis – leads to savings in electrodesialysis electricity (orange bars)

Intermediate pH values between 4.0 and 8.1 are worth pursuing if we can achieve some small catalytic enhancement of CO<sub>2</sub> production



In this scenario, we have catalyzed CO<sub>2</sub> production by a factor of 2 (e.g. with a carbonic anhydrase mimic) and we can remove double the amount of CO<sub>2</sub> we could remove at equilibrium

This leads to lower CO<sub>2</sub> prices at intermediate pH (e.g. pH 6)

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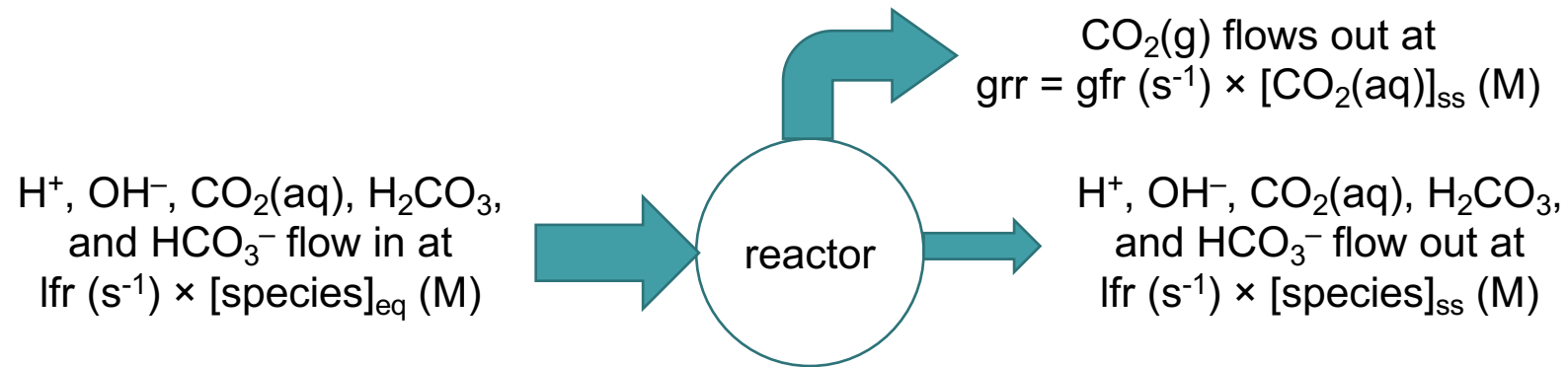
**Integration with thermodynamic system tradeoff analysis (M2.2)**

## Relevant Milestone

**M2.2 Thermodynamic system trade-off analysis:** Perform thermodynamic analysis of dissolved CO<sub>2</sub> dependence on pH. Use the data to analyze tradeoff between the required pH shift (energy requirement for electrodialysis) vs. the required CO<sub>2</sub> partial pressure at the headspace over the saturated solution (energy requirement for vacuum pumping for CO<sub>2</sub> stripping).



0D reactor model in COMSOL allows us to model steady-state operation of our system (developed by Leanna @ UCI)



Steady-state operation is important! Cannot assume we extract equilibrium concentration of CO<sub>2</sub>

- Flowing oceanwater infinitely slowly → extract more DIC as CO<sub>2</sub>, even at high pH
- Flowing oceanwater very quickly → cannot extract all dissolved CO<sub>2</sub>(aq)

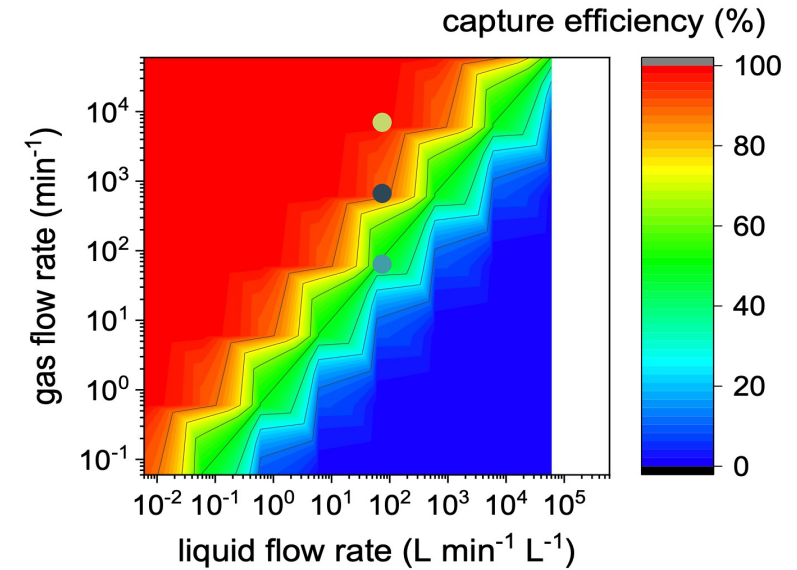
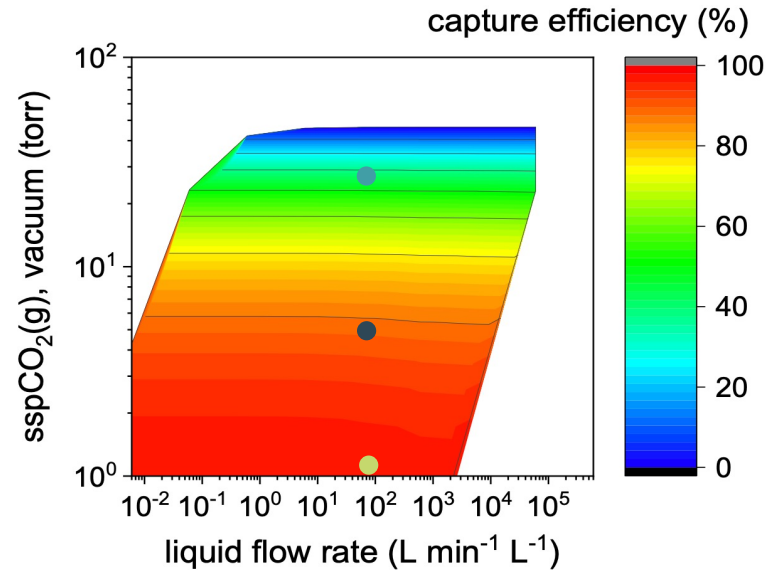
Lfr = liquid flow rate; Gfr = gas flow rate; Grr = gas reaction rate

# Output of the 0D reactor model can be used as input for our TEA

- **Extraction efficiency** (not liquid flow rate!) determines the necessary oceanwater flow rate for a given CO<sub>2</sub> scale
  - Want this to be high
- **CO<sub>2</sub> partial pressure** determines the vacuum base pressure in our membrane contactor
  - Want this to be high
- **Liquid flow rate** determines how many membrane contactors (MCs) we need
  - Want this to be within membrane contactor specs (10–100 L/min/L)

# At pH 4, best operating point is close to 4 Torr, 91% extraction efficiency

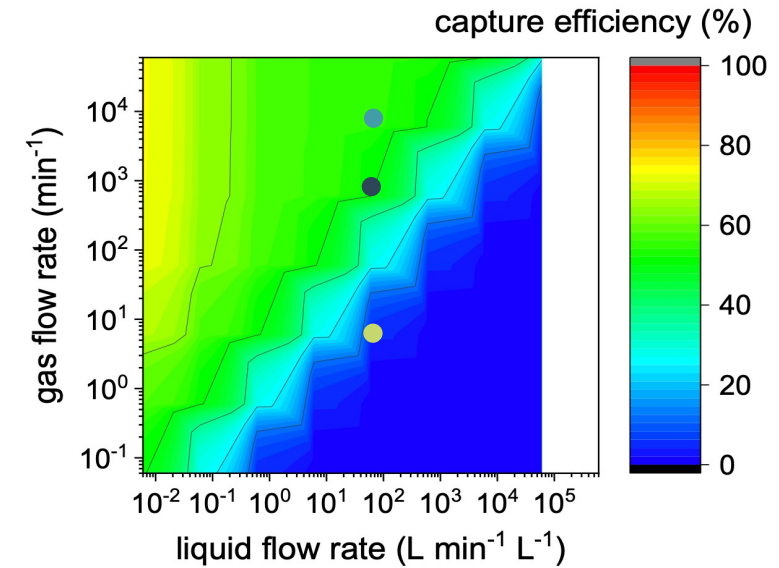
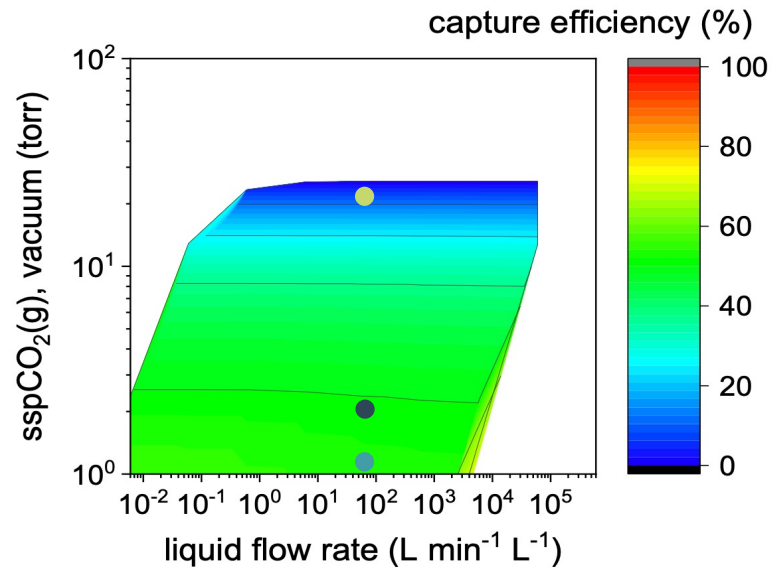
Assuming equilibrium extraction, CO<sub>2</sub> price was lower (\$115/ton)



	pCO <sub>2</sub> (torr)	Extraction efficiency (%)	lfr (min <sup>-1</sup> )	gfr (min <sup>-1</sup> )	CO <sub>2</sub> Price
●	23	50	60	60	\$178
●	4	91	60	600	\$158
●	0.5	99	60	6000	\$479

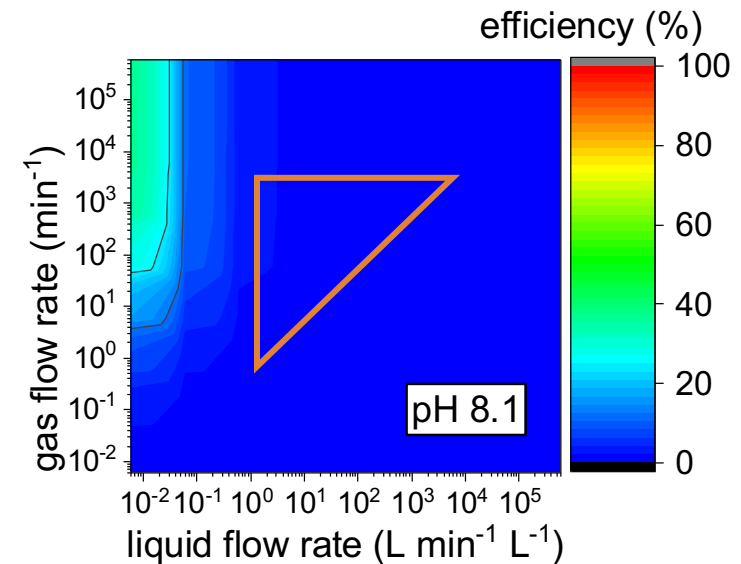
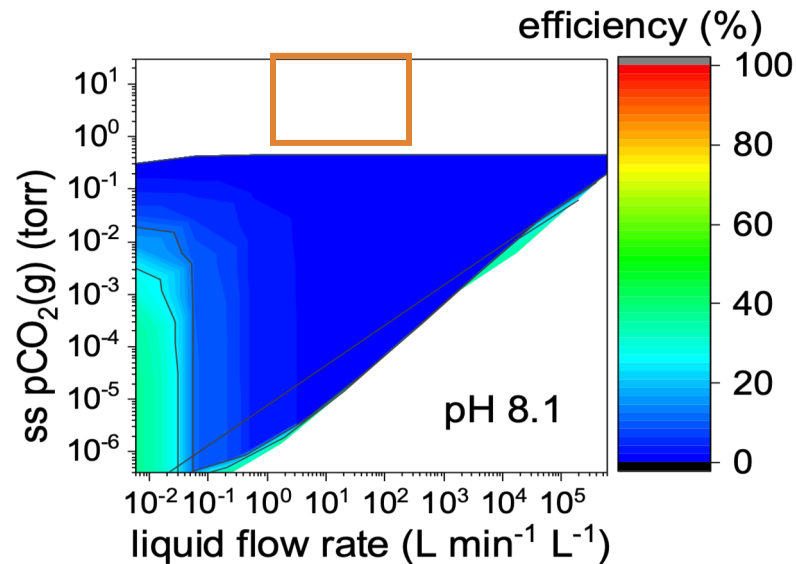
# At pH 6, best operating point is close to 2 Torr, 50% extraction efficiency

Assuming equilibrium extraction, CO<sub>2</sub> price was lower (\$156/ton)



	pCO <sub>2</sub> (torr)	Extraction efficiency (%)	lfr (min <sup>-1</sup> )	gfr (min <sup>-1</sup> )	CO <sub>2</sub> Price
●	23	5	60	6	\$805
●	2	50	60	600	\$201
●	0.3	55	60	6000	\$612

# Operation at pH 8.1 is not realistic without catalysis



- Orange boxes mark target areas for low-cost operation
  - High pressure (equivalently, low gfr)
  - Gfr > lfr for high extraction efficiency
  - Lfr in membrane contactor operating range (1-100 min<sup>-1</sup>)
- Extraction efficiency low in those target areas – CO<sub>2</sub> price ends up being >\$1000/ton

# Main conclusions

- At 10 kiloton scale, CapEx and OpEx (mostly electricity) are both significant. At megaton scale, electricity cost dominates CO<sub>2</sub> cost.
- We achieve much lower costs than previous reports mostly due to 1) larger scale and 2) offshore floating platform reducing intake/outfall costs.
- CapEx is proportional to electrodialyzer current density, and OpEx is proportional to electrodialyzer voltage. Therefore, at megaton scale, we can tolerate lower current densities – diminishing returns to achieving greater than 500 mA/cm<sup>2</sup>.
- If electricity is basically free, we can tolerate a lower capacity factor, as low as 50%.
- Vacuum level for pulling CO<sub>2</sub> off with membrane contactor must be greater than 1 Torr, otherwise we incur prohibitively large vacuum pump costs.
- Steady-state operation can yield different ideal operating points & a minimum cost operating point exists.