Quantifying nitrogen oxides and ammonia via frequency modulation in gas sensors

- DRAFT

Kvantifiering av kväveoxider och ammoniak via frekvensmodulering i gassensorer

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Abstract

The abstract resides in file Abstract.tex. Here you should write a short summary of your work.

Acknowledgments

Thank you for reading my draft! :)

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List of acronyms and abbreviations

AC Alternating Current. 2 CV Cross Validation. 14 GBCO Gate Bias Cycled Operation. 2 Hz Hertz. 5 mA miliamperes. 4 MSE Mean Squared Error. 14 NIPALS Nonlinear Iterative Partial Least Squares. 10, 12 OLS Ordinary Least Squares. 2, 7, 10, 12, 13 PC Principal Component. 8, 9, 10, 11, 14 PCA Principal Components Analysis. 8, 9, 10, 11 PCR Principal Components Regression. 2, 8, 11 PLS Partial Least Squares. 12, 14 PLSR Partial Least Squares Regression. 2, 8, 11, 12 ppm parts per million. 4 RMSE Root Mean Squared Error. 14 RSS Residual Sum of Squares. 8, 13, 14 SAS Sensor and Actuator Systems. 4 SCR Selective Catalytic Reduction. 1, 2

SiC-FET Silicon Carbide Field Effect Transistor. 2, 4

TCO Temperature Cycled Operation. 2



Introduction

1.1 Motivation

Nitric Oxide (NO) and Nitrogen Dioxide (NO_2), commonly referred together as NO_x , are hazardous gases to the environment and to humans. Its main sources are combustion processes in transportation, and industrial processes such as (but not limited to) auto mobiles, trucks, boats, industrial boilers, turbines, etc. (USEPA 2019).

 NO_x exposure to humans can cause respiratory illnesses such bronchitis, emphysema and can worsen heart disease (Boningari and Smirniotis 2016). Environmentally, NO_x are deemed precursors of adverse phenomena such as smog, acid rain, and the depletion of ozone (O_3) (Alberto Bernabeo, Webster, and Onofri n.d.). It is of high interest, therefore, to reduce NO_x emissions.

One well studied and successful method of reducing emissions is Selective Catalytic Reduction (SCR), which consists in the reduction of NO_x by ammonia (NH_3) into nitrogen gas (N_2) and water (H_2O) (Forzatti 2001), both harmless components. The process is based in the following reactions (Forzatti 2001):

•
$$4 \text{ NH}_3 + 4 \text{ NO} + \text{O}_2 \longrightarrow 4 \text{ N}_2 + 6 \text{ H}_2 \text{O}$$

•
$$2 NH_3 + NO + NO_2 \rightarrow 2 N_2 + 3 H_2O$$

•
$$8 \text{ NH}_3 + 6 \text{ NO}_2 \longrightarrow 7 \text{ N}_2 + 12 \text{ H}_2 \text{O}$$

One key element in these reactions, however, is the amount of ammonia dosed into the SCR systems. Ammonia itself is hazardous to humans, causing skin and respiratory irritation, among other illnesses (ASTDR 2004). More importantly, ammonia is one of the main sources of nitrogen pollution and it has direct negative impact on biodiversity via nitrogen deposition in soil and water (Guthrie, Giles, Dunkerley, Tabaqchali, Harshfield, Joppolo, and Manville 2018).

Hence it is also desired to keep ammonia emissions to a minimum. Too much ammonia in the SCR catalyst will guarantee NO_x reduction at the expense of undesired ammonia emissions. Concurrently, too little ammonia will impede SCR to occur properly, beating the purpose of the catalyst and as a consequence, undesired NO_x emissions.

To monitor gasses concentrations, chemical sensors are deployed, one of which is the Silicon Carbide Field Effect Transistor (SiC-FET). The identification and quantification of gasses is normally achieved through multiple sensor in so called sensor arrays. Ideally each sensor in the array needs to have different responses to different compounds (Bastuck 2019). The deployment of multiple sensors, on the other hand, proves itself cumbersome due to the increased chances of failure, and decalibration of the system should one or multiple sensors be replaced (Bastuck 2019).

One solution to this problem is the cycled operation of one single sensor, referred as virtual multi-sensor (Bastuck 2019). By cycling the working point parameters of the sensor, different substances react differently in the sensor surface, which in turn produces different responses. Temperature Cycled Operation (TCO), Gate Bias Cycled Operation (GBCO), and the combination of the two have been proven to increase selectivity of SiC-FET sensors (Bastuck 2019).

TCO, in contrast with a constant temperature evaluation, produces unique transient sensor responses, i.e. each gas mixture yields a slightly different sensor output. This unique gas signature increases selectivity (Bur, Bastuck, Lloyd Spetz, Andersson, and Schütze 2014). Additionally, the high temperatures reached in these cycles help in the cleansing of the sensor surface, preparing it for the new mixtures to come.

Frequency modulation tries to achieve the same goal: avoid steady state responses in exchange of unique signatures that could help identify/quantify the gasses at hand. It consists on operating the sensor in Alternating Current (AC). One then can regulate the frequency of this operation and create cycles of different frequencies, similar to what is done in TCO. This is equivalent to GBCO, but with more frequency changes and achieving overall higher frequencies.

The main question is: given these set of unique sensor responses, how one can quantify the gasses that produced them? The answer lies in multivariate regression techniques. Partial Least Squares Regression (PLSR) has been used in chemometrics extensively and it has been proven to be good at this task (Bastuck 2019) (Wold, Sjöström, and Eriksson 2001). Other multivariate regression methods, naturally, can also be used. This is the aim of this thesis work, which is shown in the following section.

1.2 Aim

The aim of this thesis is to investigate different regression methods, namely: Ordinary Least Squares (OLS) regression, Principal Components Regression (PCR), PLSR and Ridge Regression, and their fit to correctly quantify gas mixtures such NO_x and Ammonia subjected to sensor frequency modulation.

1.3 Research questions

- 1. Is it possible to achieve acceptable prediction levels for NO_x and Ammonia using frequency modulation?
- 2. Which method yields best predictions of gas concentrations?



2.1 Data acquisition

The data was acquired at the Sensor and Actuator Systems (SAS) laboratory at Linköping University. The experiment — as shown on Figure 2.1 — consisted of exposing different gas combinations to the SiC-FET sensor under a certain frequency cycle and recording its response, measured in miliamperes (mA). The is then used to extract secondary features, namely average and slope values from certain regions of the frequency cycle.

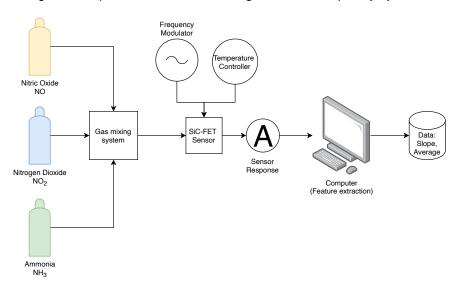


Figure 2.1: Schema of the data acquisition process.

In more detail, NO, NO₂ and NH₃ had five possible concentration values each: 10, 20, 40, 80 and 160 parts per million (ppm). The experiment was designed to encompass all possible combinations of these gasses, which totals to 125 different gas mixtures. Each feature was

submitted to the same frequency cycle five times. The cycle consists of 16 unique frequencies: 0.05, 0.1, 0.25, 0.5, 1, 2, 5, 10, 25, 50, 100, 200, 500, 1000, 2500 and 5000 Hertz (Hz). A typical raw sensor response for frequency modulation experiments is shown on Figure 2.2.

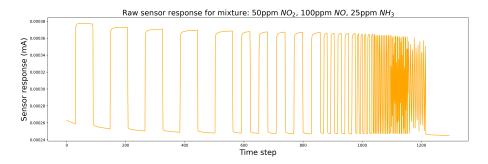


Figure 2.2: An example of row sensor response

For each frequency in each cycle, two slope and two average features were extracted. These measurements were taken during a 0.4 second window, alternating between slope and average as shown on Figure 2.3. Note that the y-axis of Figure 2.3 is in log-scale due to the different orders of magnitude that frequency achieves. Moreover, Figure 2.4 gives more insight into feature measurement.

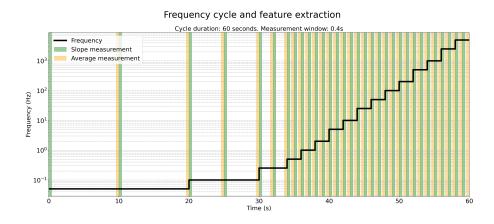


Figure 2.3: Feature measurements times per cycle.

Finally, all 125 gas mixtures were subjected to the experiment three times, each time at a different temperature as shown on Figure 2.5. Table 2.1 summarizes the data acquisition details.

For specific timestamps and measurement durations, the reader is referred to Appendix A.

2.2 Raw data

2.3 Secondary data

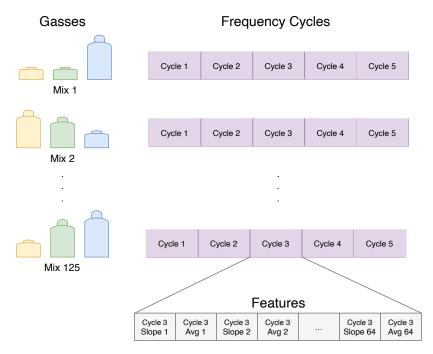


Figure 2.4: A visualization of the feature measurement process for each gas mixture in each frequency cycle

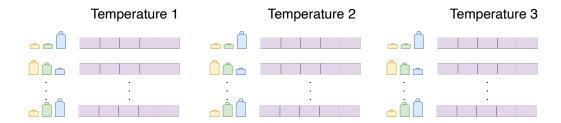
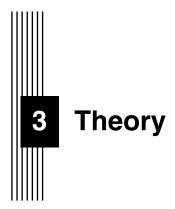


Figure 2.5: The same experiment was run with the sensor set to three different constant temperatures.

Table 2.1: Data acquisition details

Parameter	Value
Factors (gases)	3
Levels (concentrations)	5
Frequencies	16
Features per frequency	4 (2 slopes and 2 averages)
Features per cycle	64
Number of cycles	5
Data points per mixture	320
Number of mixtures	125
Datapoints per experiment	40.000
Number of experiments	3
Total data points	120.000



Question to supervisor/examiner: Do you think this chapter goes 'deep' enough?

TODO: Add bias-variance trade-off section. Complete ridge section. Add bootstrapping section

The quantification of gases based on the sensor response can be viewed as a multivariate multiple regression problem where the predictors, i.e. features derived from the sensor signal, are used to predict multiple responses, i.e. the concentrations of pertinent gases. This chapter briefly exposes the theory behind some of these models.

The models here listed were chosen as a natural progression from a statisticians point of view: starting with simple models and progressively increasing complexity as insights from the data and the problem are gathered.

3.1 Ordinary Least Squares Regression

A simple, first approach would be to tackle the problem with a Ordinary Least Squares (OLS) regression model. As Friedman, Hastie, Tibshirani, et al. 2001 explains, each output $\mathbf{Y} = [\mathbf{y_1}, \mathbf{y_2}, ..., \mathbf{y_K}]^{\mathsf{T}}$ has its own linear model. Now, given a set of n observations $\mathbf{X} = [\mathbf{x_1}, \mathbf{x_2}, ..., \mathbf{x_n}]^{\mathsf{T}}$ and each observation having p+1 features, e.g. $\mathbf{x}_i = [1, x_{i1}, x_{i2}, ... x_{ip}]$, i = 1, 2, ...n, the concatenation of all linear models can be written in matrix form as in Equation 3.1.

$$Y = XB + E ag{3.1}$$

Where:

- B: $[p+1\times K]$ matrix of regression coefficients (with the +1 referring to the intercept term);
- \mathbf{E} : $[N \times K]$ matrix of residuals.

The objective is then to find the coefficients $\hat{\mathbf{B}}$ which minimizes the Residual Sum of Squares (RSS), which is summarized by Equation 3.3 (Friedman, Hastie, Tibshirani, et al. 2001):

$$\mathbf{\hat{B}}^{OLS} = \arg\min_{\mathbf{B}} \mathsf{RSS}(\mathbf{B}) \tag{3.2}$$

In turn, the RSS, as the name suggests, is defined as the difference between real and predicted values, squared, which in matrix form is written as (Friedman, Hastie, Tibshirani, et al. 2001):

$$RSS(B) = Tr[(Y - XB)^{T}(Y - XB)]$$
(3.3)

Finally, solving for $\hat{\mathbf{B}}$ yields (Friedman, Hastie, Tibshirani, et al. 2001):

$$\hat{\mathbf{B}}^{\mathsf{OLS}} = (\mathbf{X}^{\mathsf{T}}\mathbf{X})^{-1}\mathbf{X}^{\mathsf{T}}\mathbf{Y} \tag{3.4}$$

For the problem at hand, in addition to the high number of features, it is often the case that sensor data points are acquired in quick succession, which in turn leads to highly correlated features (Bastuck 2019), which can result in high variance in a least squares model (Friedman, Hastie, Tibshirani, et al. 2001). It is natural, therefore, to progress towards methods that incorporate dimensionality reduction such as Principal Components Regression (PCR) and Partial Least Squares Regression (PLSR) or shrinkage such as Ridge Regression.

3.2 Principal Component Analysis

One way to define Principal Components Analysis (PCA) is to view it as a orthogonal projection of the data into a principal space of lower dimension such that the variance of this projection is maximized (Bishop 2006).

Just as before, consider the collection of n observations is $\mathbf{X} = [\mathbf{x_1}, \mathbf{x_2}, ..., \mathbf{x_n}]^{\mathsf{T}}$ with covariance matrix $\mathbf{\Sigma}$. Additionally, consider a matrix $\mathbf{P} = [\mathbf{p_1}, \mathbf{p_2}, ..., \mathbf{p_n}]^{\mathsf{T}}$ where $\mathbf{p_i}$ is a row vector of coefficients referring to the i-th linear combination (Johnson and Wichern 2013):

$$t_i = \mathbf{x_i} \mathbf{p_i}^{\mathsf{T}} \qquad i = 1, 2, ..., n \tag{3.5}$$

The variance and covariance of these new variables t_i can be written as follows:

$$Var(t_i) = \mathbf{p}_i^{\mathsf{T}} \mathbf{\Sigma} \mathbf{p}_i \qquad i = 1, 2, ..., n$$
(3.6)

$$Cov(t_i, t_k) = \mathbf{p}_i^{\mathsf{T}} \mathbf{\Sigma} \mathbf{p_k} \qquad i, k = 1, 2, ..., n$$
(3.7)

The first Principal Component (PC) is then the linear combination with maximum variance, i.e. the linear combinations that maximizes $Var(t_1)$, with the constraint that the coefficient

vector $\mathbf{p_1}$ has unit length. In summary, the first PC is computed as (Johnson and Wichern 2013):

$$t_1 = \mathbf{x_1} \mathbf{p_1}^{\mathsf{T}}$$

that maximizes $\mathsf{Var}(\mathbf{x_1} \mathbf{p_1}^{\mathsf{T}})$ (3.8)
subject to $\mathbf{p_1}^{\mathsf{T}} \mathbf{p_1} = 1$

The second PC, similarly to the first, is the linear combination with maximum variance, but with an added extra constraint: this new linear combination must be orthogonal to the previous one, i.e. they must be linearly independent:

$$t_2 = \mathbf{x_2} \mathbf{p_2^{\top}}$$

that maximizes $Var(\mathbf{x_2} \mathbf{p_2^{\top}})$
subject to $\mathbf{p_2^{\top}} \mathbf{p_2} = 1$
and $Cov(t_1, t_2) = 0$ (3.9)

The k-th PC is then:

$$t_k = \mathbf{x_k} \mathbf{p_k^{\top}}$$

that maximizes $Var(\mathbf{x_k} \mathbf{p_k^{\top}})$
subject to $\mathbf{p_k^{\top}} \mathbf{p_k} = 1$
and $Cov(t_j, t_k) = 0$ for $k > j$

In summary, the objective of PCA is find a matrix P such that the linear transformation

$$\mathbf{T} = \mathbf{X} \mathbf{P}^{\mathsf{T}} \tag{3.11}$$

yields new variables that are uncorrelated and arranged in decreasing order of variance.

It can be shown that these desired linear combinations can be written in terms of the eigenvalues (λ) and eigenvectors (e) of Σ , the covariance matrix of X (Johnson and Wichern 2013). The elements of eigenvectors are called loadings, while the new features T are scores. In short, for the k-th PC:

$$t_k = \mathbf{X_k} \mathbf{e_k^{\mathsf{T}}}$$

$$\mathsf{Var}(t_k) = \mathbf{e_k^{\mathsf{T}}} \mathbf{\Sigma} \mathbf{e_k} = \lambda_k$$

$$\mathsf{Cov}(t_j, t_k) = \mathbf{e_k^{\mathsf{T}}} \mathbf{\Sigma} \mathbf{e_j} = 0 \quad \text{for } k \neq j$$
(3.12)

There are several ways of computing PCs. Many of which involving finding aforementioned eigenvalues and eigenvectors. These calculations can be computationally expensive,

depending on the desired number of extracted PCs (Bishop 2006). One option is the Nonlinear Iterative Partial Least Squares (NIPALS) algorithm, also called Power Method. It has two clear advantages: "it can handle missing data and computes the components sequentially" (Dunn 2021).

The NIPALS algorithm to compute the first k-th PCs, PC_i , i = 1, 2, ..., k us displayed below as Algorith 1 (Dunn 2021) (Ng 2013) (Wright 2017). Since it computes the loadings and scores sequentially, it is possible to stop it as early as desired. The "truncated" loadings and scores that project X into the principal subspace of k PCs is defined in Equation 3.13:

$$\mathbf{T}_{|\mathbf{k}} = \mathbf{X} \mathbf{P}_{|\mathbf{k}}^{\mathsf{T}} \tag{3.13}$$

Algorithm 1: Nonlinear Iterative Partial Least Squares (NIPALS) for PCA

```
Result: Matrices of loadings P_{\mid k} and scores T_{\mid k} of the k-th first Principal Components
 _{1}\, Initialize T_{|k} and P_{|k}
 2 i = 1
 3 X_1 := X
 4 while i < k do
           repeat
 5
                 Choose \mathbf{t_i} as any column of \mathbf{X_i}
 6
                 Compute loadings \mathbf{p_i} = \left(\mathbf{t_i^{\intercal}t_i}\right)^{-1}\mathbf{t_i^{\intercal}X_i}
 7
                 Scale \mathbf{p_i} = \frac{\mathbf{p_i}}{\sqrt{\mathbf{p_i^T}\mathbf{p_i}}}
 8
                 Compute scores \mathbf{t_i} = (\mathbf{p_i}^{\mathsf{T}} \mathbf{p_i})^{-1} \mathbf{p_i}^{\mathsf{T}} \mathbf{X_i}
 9
           until ti converges
10
           Append t_i to T_{|k}
11
           Append \mathbf{p_i} to \mathbf{P_{|k}}
12
           Deflate: X_{i+1} = X_i - t_i p_i^T
13
           i += 1
14
15 end
16 return T_{|k}, P_{|k}
```

In other words:

- Line 1: Initilize the algorithm taking into account all data X;
- Line 6: Arbitrarily choose a column of X as the scores vector ti;
- Line 7: Compute the i-th loadings vector $\mathbf{p_i}$ by regressing every column of \mathbf{X} via OLS onto the scores ti;
- Line 8: Scale the loadings vector p_i to have unit length;
- Line 9: Compute the i-th scores vector t_i by regressing every column of X via OLS onto the loadings p_i ;
- Line 10: Repeat until change in t_i between iterations is small enough;

- Lines 11 and 12: Once convergence is achieved, scores t_i and loadings p_i are stored as the i-th column of matrices T and P of Equation 3.11, respectively;
- Line 13: Remove the variability explained by $\mathbf{t_i}$ and $\mathbf{p_i}$ from \mathbf{X} . A procedure called deflation.

3.3 Principal Component Regression

With the inner workings of PCA explained in the previous section, PCR can be simply reduced to a Least Squares regression on the first k-th PCs, i.e. performing linear regression on \mathbf{T}_{lk} instead of \mathbf{X} :

$$Y = T_{|k}B + E \tag{3.14}$$

And the regression coefficients are found analogously to Equation 3.4:

$$\hat{\mathbf{B}}^{PCR} = (\mathbf{T}_{|\mathbf{k}}^{\mathsf{T}} \mathbf{T}_{|\mathbf{k}})^{-1} \mathbf{T}_{|\mathbf{k}}^{\mathsf{T}} \mathbf{Y}$$
(3.15)

Although useful, PCR has a potential flaw: while the new found projection of X is guaranteed to best explain the variance of predictors, this cannot be said about the responses Y (James, Witten, Hastie, and Tibshirani 2013). PLSR, on the other hand, solves this issue by supervising the identification of PCs (James, Witten, Hastie, and Tibshirani 2013).

3.4 Partial Least Squares Regression

PLSR, much like PCR, also aims to reduce dimensionality via linear combinations of the inputs. This technique, however, also takes into account the response variables Y. One key advantage of PLSR is that it seeks axes with most variance (like PCR) and high correlation with response variables (Friedman, Hastie, Tibshirani, et al. 2001).

The main idea can be described as finding linear combinations for the data matrix design matrix X and response matrix Y as follows (Ng 2013), similarly to what was done in Section 3.2.

$$\mathbf{W} = \mathbf{X} \mathbf{L}^{\mathsf{T}} \tag{3.16}$$

$$\mathbf{U} = \mathbf{Y}\mathbf{Q}^{\mathsf{T}} \tag{3.17}$$

Instead of simply running NIPALS on X and Y separately. PLSR uses information from Y to decompose X and *vice-versa* (Ng 2013). Algorithm 2 is an adaptation of Algorithm 1 to incorporate this intended behavior.

Algorithm 2: NIPALS for Partial Least Squares Regression (PLSR)

```
Result: Matrices of loadings L_{|\mathbf{k}}, Q_{|\mathbf{k}} and scores W_{|\mathbf{k}}, U_{|\mathbf{k}} of the k-th first Partial
                     Least Squares directions
 1 Initialize \mathbf{L_{|k}}, \mathbf{Q_{|k}} and \mathbf{W_{|k}}, \mathbf{U_{|k}}
 2 i = 1
 \mathbf{3} \ \mathbf{X_1} \coloneqq \mathbf{X}
 4 \mathbf{Y_1} \coloneqq \mathbf{Y}
 5 while i < k do
            repeat
                  Choose \mathbf{u_i} as any column of \mathbf{Y_i}
 7
                  Compute loadings of X_i based on score of Y_i: \ell_i = (\mathbf{u}_i^{\mathsf{T}} \mathbf{u}_i)^{-1} \mathbf{u}_i^{\mathsf{T}} X_i
 8
                  Scale \ell_i = \frac{\ell_i}{\sqrt{\ell_i^{\scriptscriptstyle \mathsf{T}} \ell_i}}
 9
                  Compute score of X_i: w_i = (\ell_i^T \ell_i)^{-1} \ell_i^T X_i
10
                  Compute loadings of Y_i based on score of X_i: q_i = (w_i^T w_i)^{-1} w_i^T Y_i
11
                  Scale \mathbf{q}_i = \frac{\mathbf{q}_i}{\sqrt{\mathbf{q}_i^{\scriptscriptstyle T}\mathbf{q}_i}}
12
                  Compute score of Y_i: u_i = (q_i^T q_i)^{-1} q_i^T Y_i
13
            until ui converges
14
            Append w_i to W_{|k|}
15
            Append \ell_{\mathbf{i}} to \mathbf{L}_{|\mathbf{k}}
16
            Append \mathbf{u_i} to \mathbf{U_{|k}}
17
18
            Append \mathbf{q_i} to \mathbf{Q_{|k}}
           Deflate X_i: X_{i+1} = X_i - w_i \ell_i^T
19
            Deflate Y_i: Y_{i+1} = Y_i - u_i q_i^T
20
           i += 1
21
22 end
23 return \mathbf{W_{|k}}, \mathbf{L_{|k}}, \mathbf{U_{|k}}, \mathbf{Q_{|k}}
```

In summary, highlighting the most important parts:

- Line 7: Arbitrarily choose a column of Y_i as the initial response score vector \mathbf{u}_i ;
- Line 8: Compute the i-th loadings vector $\mathbf{w_i}$ of \mathbf{X} by regressing every column of \mathbf{X} via OLS onto scores vector of \mathbf{Y} , $\mathbf{u_i}$;
- Line 9: Scale the data loadings vector w_i to have unit length;
- Line 10: Compute the i-th data scores vector $\mathbf{w_i}$ by regressing every column of $\mathbf{X_i}$ via OLS onto the column ℓ_i ;
- Line 11: Compute the i-th loadings vector $\mathbf{q_i}$ of $\mathbf{Y_i}$ by regressing every column of \mathbf{Y} via OLS onto scores vector of \mathbf{X} , $\mathbf{w_i}$;

- Line 12: Scale the response loadings vector q_i to have unit length;
- Line 13: Compute the i-th response scores vector $\mathbf{u_i}$ by regressing every column of $\mathbf{Y_i}$ via OLS onto the column $\mathbf{q_i}$;
- Line 14: Repeat until change in $\mathbf{u_i}$ between iterations is small enough;
- Lines 15 and 16: Once convergence is achieved, w_i and ℓ_i are stored as the i-th column of matrices W and L of Equation 3.16;
- Lines 17 and 18: Once convergence is achieved, u_i and q_i are stored as the i-th column of matrices U and Q of Equation 3.17;
- Lines 19 and 20: Remove the variability explained by $\mathbf{w_i}, \ell_i$ and $\mathbf{u_i}, \mathbf{q_i}$ from $\mathbf{X_i}$ and $\mathbf{Y_i}$, respectively;

After finding the k partial least squares directions from Algorithm 2 above, the problem, as in Section 3.3, reduces to performing Least Squares Regression using the newfound transformations.

$$Y = W_{|k}B + E \tag{3.18}$$

Which in turn, analogously to Equations 3.4 and 3.15 yields the coefficients:

$$\hat{\mathbf{B}}^{\mathsf{PLSR}} = (\mathbf{W}_{|\mathbf{k}}^{\mathsf{T}} \mathbf{W}_{|\mathbf{k}})^{-1} \mathbf{W}_{|\mathbf{k}}^{\mathsf{T}} \mathbf{Y} \tag{3.19}$$

3.5 Ridge Regression

Ridge regression is also a viable alternative to reduce the problem of highly correlated features (Friedman, Hastie, Tibshirani, et al. 2001). Instead of fitting a least squares model on a subset of predictors or a transformation of them, Ridge allows the use of all features with a continuous shrinkage of its coefficients, which results in less variance (Friedman, Hastie, Tibshirani, et al. 2001).

For the multi-output case, there are two options: use the same penalization parameter λ for all variables $\mathbf{Y} = [\mathbf{y_1}, \mathbf{y_2}, ..., \mathbf{y_K}]^{\mathsf{T}}$ or apply different parameters $\lambda = [\lambda_1, \lambda_2, ..., \lambda_K]^{\mathsf{T}}$. In this work, the latter is preferred over the former, as it allows a more fine tuned control of the regression models for each studied gas.

Analogous to Section 3.1, the goal is to minimize the RSS, but now with the penalization term taken into account. Equation 3.20 below shows this objective function in matrix form.

$$RSS^{Ridge}(\mathbf{B}, \lambda) = Tr[(\mathbf{Y} - \mathbf{X}\mathbf{B})^{\mathsf{T}}(\mathbf{Y} - \mathbf{X}\mathbf{B})] + Tr[\mathbf{B}^{\mathsf{T}}\mathbf{B} + \lambda \mathbf{I}]$$
(3.20)

$$\hat{\mathbf{B}}^{\text{Ridge}} = \underset{\mathbf{B}}{\operatorname{arg\,min}} \, \text{RSS}^{\text{Ridge}}(\mathbf{B}) \tag{3.21}$$

The coefficients that minimize the RSS is shown in Equation 3.22 below.

$$\hat{\mathbf{B}}^{\mathsf{Ridge}} = (\mathbf{X}^{\mathsf{T}}\mathbf{X} + \lambda \mathbf{I})^{-1}\mathbf{X}^{\mathsf{T}}\mathbf{Y} \tag{3.22}$$

The choice of hyper-parameters $\lambda \geq 0$ controls how much shrinkage is applied to the coefficients: larger λ implies more penalization to complex models. Although the coefficients are shrunk towards zero, they never reach zero, which makes Ridge regularization unsuitable for feature selection (Friedman, Hastie, Tibshirani, et al. 2001).

3.6 Cross Validation

There are several choices to make for the aforementioned models: what polynomial degree fits the data best? How many PCs/PLS components to use? How much penalization to impose in Ridge regression?

A first answer to this would be to split the data into training and validation sets. After fitting models to the former, the latter is used to measure the prediction error via some scoring function. In that sense, it is important to distinguish test error rate from training error rate. The first, also called generalization error, is the score of the fit on an independent, previously unseen test sample. The second, on the other hand, is the average score over the training sample (Friedman, Hastie, Tibshirani, et al. 2001).

Scoring functions measure how much the data deviates from the fit and can be used as a qualitative tool for model selection and comparison. Once this is done, the choice of the model that yields minimum error is trivial. Two examples of wildly used score functions are Mean Squared Error (MSE) and Root Mean Squared Error (RMSE). For the multi-output case of m responses and n observations, they are defined respectively as:

$$MSE = \frac{1}{n} \sum_{i=1}^{n} \left(\sum_{j=1}^{m} (y_{ij} - \hat{y}_{ij}) \right)^{2}$$
 (3.23)

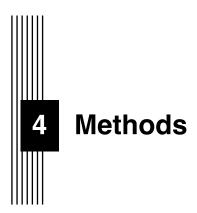
$$RMSE = \sqrt{MSE}$$
 (3.24)

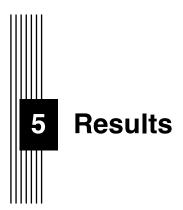
This approach, however, is sensitive to the choice of these sets. Additionally, reserving part of the data just for validation might be detrimental for the model fitting process, specially if the number of observations is low (James, Witten, Hastie, and Tibshirani 2013).

One tool that can help alleviating these problems is Cross Validation (CV). Dividing

3.7 Bootstrapping

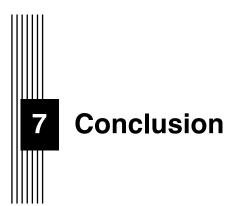
With the theoretical background laid out, this work proceeds to apply them to the problem at hand.

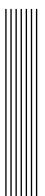




6 Discussion

- 6.1 Results
- 6.2 Method
- 6.3 The work in a wider context





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Data acquisition time stamps

Table A.1: Data acquisition timestamps.

Frequency (Hz)	Duration (s)	Feature	Start time (s)	End time (s)
		Slope	0,0	0,4
0.05	20	Average	9,6	10,0
0.05	20	Slope	10,0	10,4
		Average	19,6	20,0
	10	Slope	20,0	20,4
0.1		Average	24,6	25,0
0.1	10	Slope	25,0	25,4
		Average	29,6	30,0
		Slope	30,0	30,4
0.05	4	Average	31,6	32,0
0.25	4	Slope	32,0	32,4
		Average	33,6	34,0
		Slope	34,0	34,4
0.5	2	Average	34,6	35,0
0.5		Slope	35,0	35,4
		Average	35,6	36,0
	2	Slope	36,0	36,4
1.0		Average	36,6	37,0
1.0		Slope	37,0	37,4
		Average	37,6	38,0
	2	Slope	38,0	38,4
2.0		Average	38,6	39,0
2.0		Slope	39,0	39,4
		Average	39,6	40,0
		Slope	40,0	40,4
5.0	2	Average	40,6	41,0
5.0		Slope	41,0	41,4
		Average	41,6	42,0
	2	Slope	42,0	42,4
10.0		Average	42,6	43,0
10.0		Slope	43,0	43,4
		Average	43,6	44,0

Frequency (Hz)	Duration (s)	Feature	Start time (s)	End time (s)
		Slope	44,0	44,4
25.0	2	Average	44,6	45,0
25.0	2	Slope	45,0	45,4
		Average	45,6	46,0
	2	Slope	46,0	46,4
50.0		Average	46,6	47,0
30.0		Slope	47,0	47,4
		Average	47,6	48,0
	2	Slope	48,0	48,4
100.0		Average	48,6	49,0
100.0	2	Slope	49,0	49,4
		Average	49,6	50,0
		Slope	50,0	50,4
200.0	2	Average	50,6	51,0
200.0	2	Slope	51,0	51,4
		Average	51,6	52,0
	2	Slope	52,0	52,4
500.0		Average	52,6	53,0
300.0		Slope	53,0	53,4
		Average	53,6	54,0
	2	Slope	54,0	54,4
1000.0		Average	54,6	55,0
1000.0		Slope	55,0	55,4
		Average	55,6	56,0
	2	Slope	56,0	56,4
2500.0		Average	56,6	57,0
2300.0		Slope	57,0	57,4
		Average	57,6	58,0
	2	Slope	58,0	58,4
5000.0		Average	58,6	59,0
3000.0		Slope	59,0	59,4
		Average	59,6	60,0