
CE412 A

Water Supply & Wastewater Disposal Systems

**Instructor :
Dr Vinod Tare**

Part I

CE 412 A
Water Supply & Wastewater Disposal Systems

Dr Vinod Tare

Components of Water Supply System

➤ 1. Water Intake

☐ Types - Refer to Drawings

- Surface Water
- Lake / Reservoir
- River
- Dams
 - Concrete
 - Earthen
- Canals
- Groundwater

- ☐ Specifications to be provided Location, Type and Capacity based on Demand or Yield whichever is lower.

Part I

CE 412 A
Water Supply & Wastewater Disposal Systems

Dr Vinod Tare

Components of Water Supply System

➤ 2. Water Transmission/ Conveyance System

- ☐ Raw water from source to water treatment plant
 - Both open and close conduits can be used
- ☐ Treated water to water distribution system from water treatment plant
- ☐ Specifications to be provided
 - Alignment, type of conduit, shape and size of the conduit.
 - Most economical diameter of the pressure pipe.

Darcy–Weisbach Equation

$$s = \frac{H}{L} = \frac{f v^2}{2g D}$$

$$g \rightarrow m/s^2$$

$$v \rightarrow mps$$

$$L \rightarrow m$$

$$d \rightarrow m$$

Manning's Formulae

$$v = \frac{1}{n} r^{2/3} s^{1/2}$$

$$= \frac{0.3968 d^{2/3} s^{1/2}}{n}$$

$$Q = 0.31168 \frac{1}{n} d^{8/3} s^{1/2}$$

v is velocity in m/s; Q is flow or discharge in m³/s; r is hydraulic radius in m; and d is diameter in m

$n = 0.010 - 0.030$ (Most commonly use value = 0.013)

Part I

CE 412 A
Water Supply & Wastewater Disposal Systems

Dr Vinod Tare

Hazen-Williams Formula

$$v = 0.849 C r^{0.63} s^{0.54}$$

$$v = 0.35449 C d^{0.63} s^{0.54}$$

$$Q = 0.27842 C d^{2.63} s^{0.54}$$

For $c = 100$

$$v = 35.449 (d)^{0.63} (s)^{0.54}$$

v is velocity in $\frac{m}{s}$; Q is flow in $\frac{m^3}{s}$; r is hydraulic radius in m; d is diameter in m;

s is slope i.e. headloss per unit length; and c is Hazen – Williams (Roughness) coefficient (100 – 150)

$$Q = 27.842 d^{2.63} (h_f/L)^{0.54}$$

$$h_f = \left[\frac{Q}{27.842 d^{2.63}} \right]^{1/0.54} L = k Q^{1.85} L; \quad k = \left[\frac{1}{27.842 d^{2.63}} \right] \text{ for given diameter and } c = 100$$

Part I

CE 412 A
Water Supply & Wastewater Disposal Systems

Dr Vinod Tare

Equation for Correction in Flow at the end of any iteration in Hardy-Cross Method

The **Hardy Cross method** is an application of continuity of flow and continuity of potential to iteratively solve for flows in a pipe network. In the case of pipe flow, conservation of flow means that the flow in is equal to the flow out at each junction in the pipe.

$$h_f = kQ^{1.85}L$$

$$= k(Q_i + \Delta Q)^{1.85} = k(Q_i^{1.85} + 1.85 Q_i^{1.85-1} \Delta Q + \dots)L$$

$$\sum h_f = \sum kQ^{1.85} + 1.85 \Delta Q \sum Q^{1.85-1} = 0$$

Or

$$\Delta Q = - \frac{\sum kQ^{1.85}}{1.85 \sum kQ^{1.85-1}} = - \frac{\sum h_i}{1.85 \sum h_i / Q_i}$$

Part I

CE 412 A
Water Supply & Wastewater Disposal Systems

Dr Vinod Tare

Pipes in Series:

n number of pipes with diameter (*d_i*), Hazen William Coefficient (*C_i*) and Length (*L_i*) in series:
d₁, c₁, L₁; d₂, c₂, L₂; d_n, c_n, L_n

Equivalent Pipe: d_{eq}, c_{eq}, L_{eq}

$$h_{feq} = h_{f1} + h_{f2} + h_{f3} \dots \dots \dots + h_{fn}$$

$$Q_{eq} = Q_1 = Q_2 = Q_3 \dots \dots \dots = Q_n$$

$$\left[\frac{Q_{eq}}{0.27842 c_{eq} d_{eq}^{2.63}} \right]^{1.85} L_{eq} = \left[\frac{Q_1}{0.27842 c_1 d_1^{2.63}} \right]^{1.85} L_1 + \left[\frac{Q_2}{0.27842 c_2 d_2^{2.63}} \right]^{1.85} L_2$$

$$+ \dots \dots \dots + \left[\frac{Q_n}{0.27842 c_n d_n^{2.63}} \right]^{1.85} L_n$$

$$\left[\frac{1}{c_{eq} d_{eq}^{2.63}} \right]^{1.85} L_{eq} = \left[\frac{1}{c_1 d_1^{2.63}} \right]^{1.85} L_1 + \left[\frac{1}{c_2 d_2^{2.63}} \right]^{1.85} L_2 + \dots \dots \dots + \left[\frac{1}{c_n d_n^{2.63}} \right]^{1.85} L_n$$

Part I

CE 412 A
Water Supply & Wastewater Disposal Systems

Dr Vinod Tare

Pipes in Parallel:

n number of pipes with diameter (d_i), Hazen William C

$d_1, c_1, L_1; d_2, c_2, L_2; \dots \dots \dots d_n, c_n, L_n$

Equivalent Pipe: d_{eq}, c_{eq}, L_{eq}

$$Q_{eq} = Q_1 + Q_2 + \dots \dots \dots + Q_n$$

$$h_{feq} = h_{f1} = h_{f2} = \dots \dots \dots = h_{fn}$$

$$0.27842 d_{eq}^{2.63} \left(\frac{h_{feq}}{L_{eq}}\right)^{0.54} = 0.27842 d_1^{2.63} \left(\frac{h_{f1}}{L_1}\right)^{0.54} + 0.27842 d_2^{2.63} \left(\frac{h_{f2}}{L_2}\right)^{0.54} + \dots \dots \dots + 0.27842 d_n^{2.63} \left(\frac{h_{fn}}{L_n}\right)^{0.54}$$

$$h_{feq} = h_{f1} = h_{f2} = h_{f3} = \dots \dots \dots = h_{fn}$$

$$d_{eq}^{2.63} \left(\frac{1}{L_{eq}}\right)^{0.54} = d_1^{2.63} \left(\frac{1}{L_1}\right)^{0.54} + d_2^{2.63} \left(\frac{1}{L_2}\right)^{0.54} + \dots \dots \dots + d_n^{2.63} \left(\frac{1}{L_n}\right)^{0.54}$$

Part I

CE 412 A
Water Supply & Wastewater Disposal Systems

Dr Vinod Tare

Population Calculation

- Arithmetic method : $dp/dt = \text{constant}$ Formula: $P_n = P_o + n \cdot x$
- Geometric method : $dp/dt \propto P$ Formula: $P_n = P_o(1+r/100)^n$
- Decreasing growth rate method: $dp/dt \propto (P_s - P)$

P_n = prospective or forecasted population after n decades from the present (i.e. the last known census)

P_o = Population at present (i.e. the last known census)

X = arithmetic mean of population increase in known decades

r = assumed growth rate (%) (take geometric mean)

P_s = Saturation population value

Part I

CE 412 A
Water Supply & Wastewater Disposal Systems

Dr Vinod Tare

Logistic Growth Method

$$P = \frac{P_s}{1 + m \cdot \exp(n \cdot t)}$$

$$P_s = \frac{2P_o P_1 P_2 - P_1^2 (P_o + P_2)}{P_o P_2 - P_1^2} \quad m = \frac{P_s - P_o}{P_o}$$

$$n = \frac{2.3}{t_1} \log_{10} \frac{P_o (P_s - P_1)}{P_1 (P_s - P_o)}$$

P_o P_1 P_2 are population values chosen at times t_o t_1 t_2 and the interval between t_o t_1 t_2 remains constant

Fire Demand Formulae

- Kuichling's Formula : $Q = 3182\sqrt{P}$
- Freeman Formula : $Q = 1136 \left[\frac{P}{10} + 10 \right]$
- American Insurance Association : $Q = 4637\sqrt{P} [1 - 0.01\sqrt{P}]$

P = Population in thousands

Q = Amount of water required in litres/minute