

Impact of rigid bodies

Impact means collision of two bodies in which large forces act for a very short duration leading to finite appreciable impulses.

e.g. impact of hammer on a pile

impact of meteorite on earth

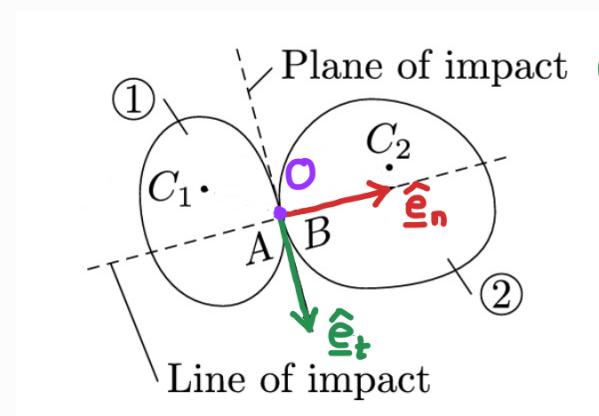
In general, impact phenomena is complex and the modeller usually makes simplifications for modelling purposes:

Simplifications:

- 1) Rigid body assumption just before & after impact
- 2) Almost zero contact time (impulses due to finite forces over the duration of contact is zero)
- 3) Impulsive forces (arising due contact) and the energy dissipation is modelled in terms of an empirical parameter ' e ' \leftarrow coefficient of restitution

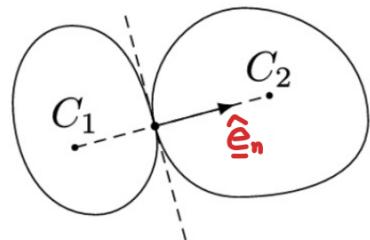
4) The impulsive forces cause instantaneous change in velocities of the bodies, without changing their positions

Consider impact of two unconstrained RBs, so that point A of body ① of mass m_1 collides with point B of body ② of mass m_2

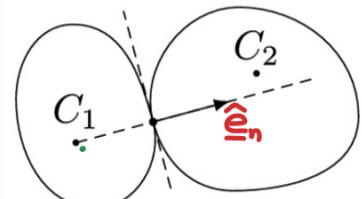
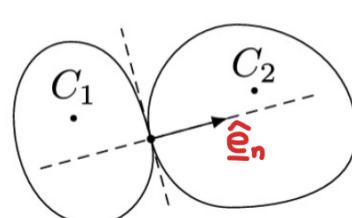


Plane of impact (tangent plane at the contact pt O which is coincident with A and B)

Central Impact

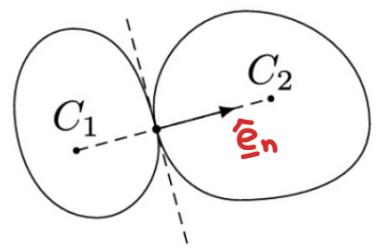


Non-central Impact

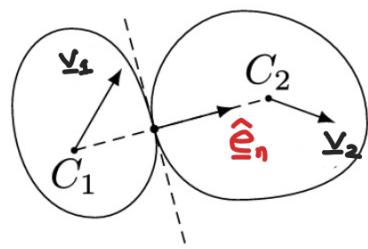


The COMs of the two bodies lie on the line of impact

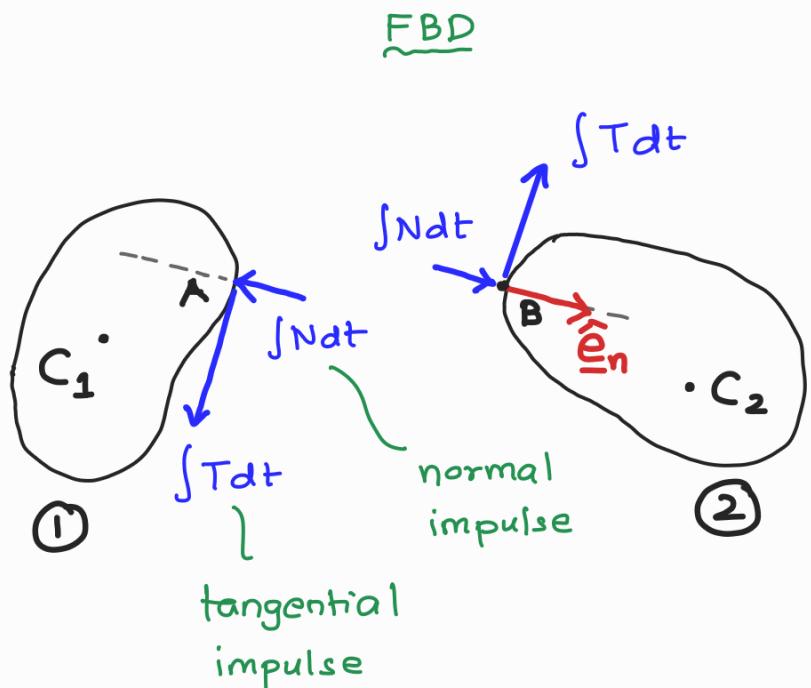
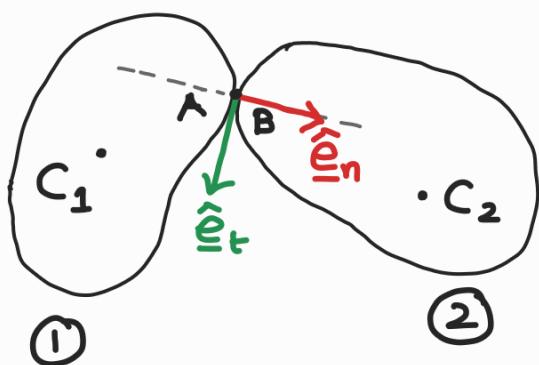
Direct central impact



Oblique central impact



Smooth collision vs Non-smooth collision



Normal component of impulse : $\int N dt$

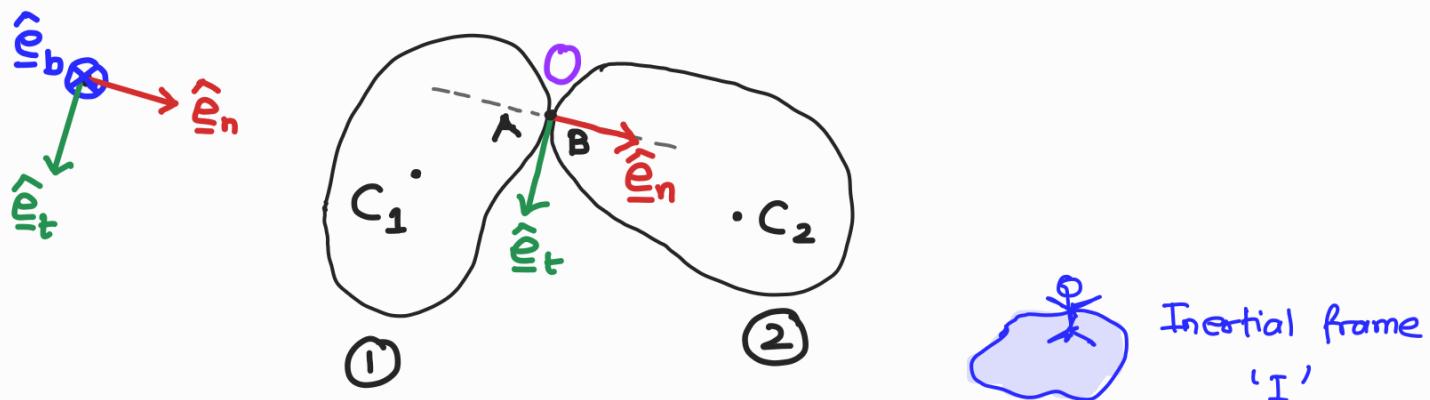
Tangential component of impulse : $\int T dt$ ← may arise due to friction

If bodies are "smooth", then $\int T dt = 0$

Otherwise $\int T dt \neq 0$

In this course, bodies are assumed to be smooth and we will look at smooth impact/collision problems

Impact / Collision Problem Setup:



- 1) Coincident pt 'O' is a geometric point that is not attached to any of the RBs but is fixed in the inertial frame \Rightarrow acc of pt 'O' is zero, i.e., $\ddot{\alpha}_{O|I} = \underline{0}$
- 2) Points A (\in RB 1) and B (\in RB 2) do not move during the very short duration of collision
 - \rightarrow although $\dot{\gamma}_A$ and $\dot{\gamma}_B$ are not zero but finite!
 - \rightarrow acceleration of pts A and B are also not zero, however, acceleration of the geometric point 'O' is zero w.r.t the inertial frame

Before impact

RB ① :

$$\underline{v}_{c_1}, \underline{\omega}_1$$

RB ② :

$$\underline{v}_{c_2}, \underline{\omega}_2$$

known

$$\underline{v}_{c_1} = \underline{v}_{t_1} \hat{e}_t + \underline{v}_{n_1} \hat{e}_n + \underline{v}_{b_1} \hat{e}_b$$

$$\underline{v}_{c_2} = \underline{v}_{t_2} \hat{e}_t + \underline{v}_{n_2} \hat{e}_n + \underline{v}_{b_2} \hat{e}_b$$

After impact

RB ① :

$$\underline{v}'_{c_1}, \underline{\omega}'_1$$

RB ② :

$$\underline{v}'_{c_2}, \underline{\omega}'_2$$

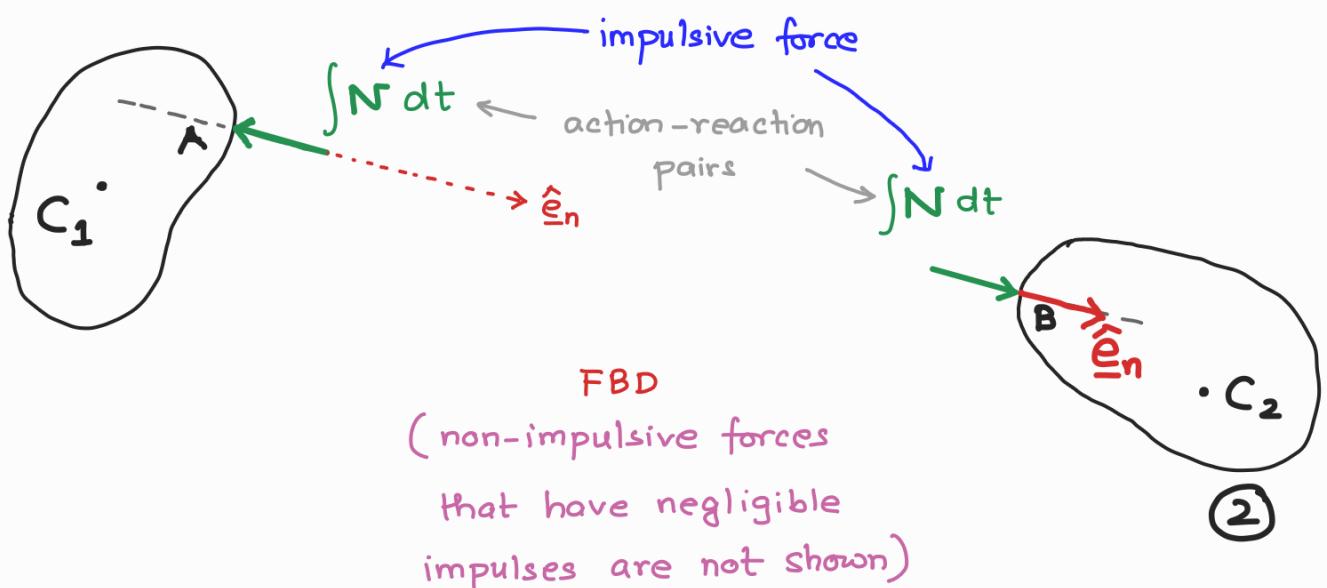
to be
found

3 components each \Rightarrow 12 unknowns

$$\underline{v}'_{c_1} = \underline{v}'_{t_1} \hat{e}_t + \underline{v}'_{n_1} \hat{e}_n + \underline{v}'_{b_1} \hat{e}_b$$

$$\underline{v}'_{c_2} = \underline{v}'_{t_2} \hat{e}_t + \underline{v}'_{n_2} \hat{e}_n + \underline{v}'_{b_2} \hat{e}_b$$

At the instant of collision, if we draw the FBD of RB ① & ②, we will have a normal reaction force N along the \hat{e}_n direction and the impulse will be $\int N dt$



A finite impulse will cause change in velocity in the direction of impulse

Using Impulse-momentum relation for RB ① and ②

$$m_1 \underline{v}_{c_1}' - m_1 \underline{v}_{c_1} = - \int N dt \hat{\underline{e}}_n$$

\leftarrow impulse only along $\hat{\underline{e}}_n$

$$m_2 \underline{v}_{c_2}' - m_2 \underline{v}_{c_2} = \int N dt \hat{\underline{e}}_n$$

There is no impulse along $\hat{\underline{e}}_t$ and $\hat{\underline{e}}_b$ directions

⇒ conserve LINEAR MOMENTUM for each body separately in $\hat{\underline{e}}_t$ and $\hat{\underline{e}}_n$ directions:

RB ①

$$\underline{v}_{t_1} = \underline{v}_{t_1}' - ①$$

$$\underline{v}_{b_1} = \underline{v}_{b_1}' - ②$$

RB ②

$$\underline{v}_{t_2} = \underline{v}_{t_2}' - ③$$

$$\underline{v}_{b_2} = \underline{v}_{b_2}' - ④$$

[4 equations]

Note: These are velocity components of respective COMs

Now, if we consider the system = 'RB ① + RB ②'

⇒ Impulse $\int N dt \hat{\underline{e}}_n$ will be an internal impulse for the entire system ('RB ① + RB ②')

Therefore, for the system subjected to **only non-impulsive external forces**, the linear momentum is conserved for the system during the internal impulsive interval. Therefore,

$$m_1 v_{n_1} + m_2 v_{n_2} = m_1 v'_{n_1} + m_2 v'_{n_2} \quad \text{--- (5)}$$

before collision after collision

Next, consider the angular impulse of the two RBs about pt 'O' fixed in the inertial frame.

→ $I_{ang O} = \int \underline{M}_O^{imp} dt = \underline{\Omega}$ (for both RBs)

Since impulsive force $\underline{N}\hat{\underline{e}}_n$ passes through pt 'O', the net resultant impulsive moment $\underline{M}_O^{imp} = \underline{\Omega}$

⇒ Angular momentum is conserved for the two RB separately

'O' is fixed in frame 'I' \Rightarrow 'O' is a valid pt for $M_O = H_{O|I}$

RB ① : $H_O = H'_O$ (pt 'O' coincides with pt 'A')

$$\Rightarrow H_{c_1} + \underline{r}_{c_1 O} \times m \underline{v}_{c_1} = H'_{c_1} + \underline{r}_{c_1 O} \times m \underline{v}'_{c_1}$$

['I' frame reference dropped for ease of writing]

$$\Rightarrow \underbrace{\underline{H}_{c_1}}_{\underline{I}^{c_1} \underline{\omega}_1} = \underbrace{\underline{H}'_{c_1}}_{\underline{I}^{c_1} \underline{\omega}'_1} + \underline{r}_{c_1 O} \times m_1 (\underline{v}'_{c_1} - \underline{v}_{c_1})$$

↓
 only v_{n_1}
 changes after
 impact
 $(v'_{n_1} - v_{n_1}) \hat{e}_n$

$$\Rightarrow \boxed{\underline{I}^{c_1} \underline{\omega}_1 = \underline{I}^{c_1} \underline{\omega}'_1 + \underline{r}_{c_1 O} \times m [(v'_{n_1} - v_{n_1}) \hat{e}_n]}$$

Equate \hat{e}_n , \hat{e}_t , and \hat{e}_b components on both sides

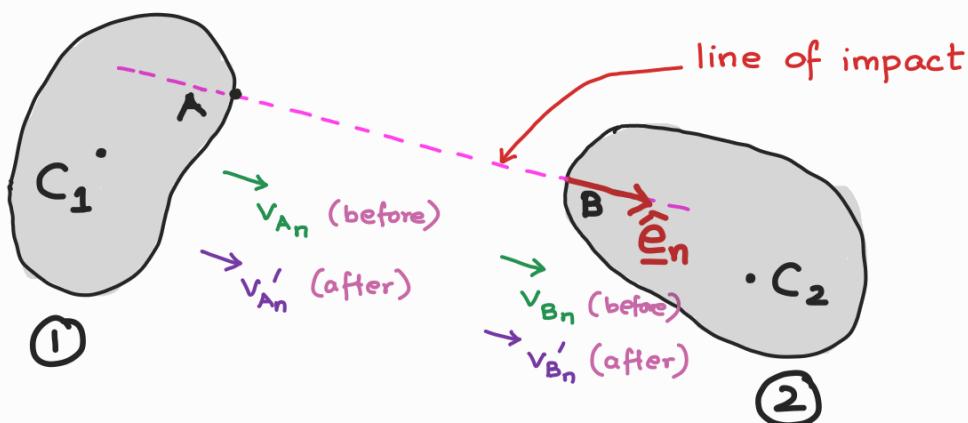
and we get three equations $\rightarrow ⑥, ⑦, ⑧$

RB ② : Just like RB 1, we can proceed similarly and we get three more equations for RB ② $\rightarrow ⑨, ⑩, ⑪$

$$\Rightarrow \boxed{\underline{I}^{c_2} \underline{\omega}_2 = \underline{I}^c \underline{\omega}'_2 + \underline{r}_{c_2 O} \times m [(v'_{n_2} - v_{n_2}) \hat{e}_n]}$$

The 12th equation comes from through the use of the Coefficient of Restitution (e) !

$e \rightarrow$ an empirical parameter which models the dissipation of energy during impact



defined as
 $e \equiv \frac{\text{velocity of separation of contact pts}}{\text{velocity of approach of contact pts}}$

experimentally determined
(Range $0 \leq e \leq 1$)

$$\Rightarrow e = - \frac{(v'_{Bn} - v'_{An})}{(v_{Bn} - v_{An})} \quad - (12)$$

along
normal
direction
(\hat{e}_n)

Note: The above formula involves contact point velocities and not COM velocities and they can be expressed in terms of the velocities of the COMs as:

$$v_{An} = \underline{v}_A \cdot \hat{e}_n = (\underline{v}_{C_1} + \underline{\omega}_1 \times \underline{r}_{AC_1}) \cdot \hat{e}_n$$

$$v'_{An} = \underline{v}'_A \cdot \hat{e}_n = (\underline{v}'_{C_1} + \underline{\omega}'_1 \times \underline{r}_{AC_1}) \cdot \hat{e}_n$$

[\because 'A' and 'C₁' are both points on RB ①]

and

$$v_{B_n} = \underline{v}_B \cdot \hat{\underline{e}}_n = (\underline{v}_{c_2} + \underline{\omega}_2 \times \underline{x}_{BC_2}) \cdot \hat{\underline{e}}_n$$

$$v'_{B_n} = \underline{v}'_B \cdot \hat{\underline{e}}_n = (\underline{v}'_{c_2} + \underline{\omega}'_2 \times \underline{x}_{BC_2}) \cdot \hat{\underline{e}}_n$$

[\because 'B' and ' C_2 ' are both points on RB ②]

What happens when RB ② is massive? ($m_2 \rightarrow \infty$)

$m_2 \rightarrow \infty \Rightarrow \int N dt$ does not affect RB ②

$$\Rightarrow \underline{\omega}'_2 \approx \underline{\omega}_2 \text{ and } \underline{v}'_{c_2} \approx \underline{v}_{c_2}$$

\Rightarrow ONLY 6 unknowns in this case

$$\underline{\omega}'_1 \text{ and } \underline{v}'_{c_1}$$

of RB ① after

impact are unknown

1) Smooth impact

$$\Rightarrow v_{t_1} = v'_{t_1} \text{ and } v_{b_1} = v'_{b_1} \quad (2 \text{ eqns})$$

2) Linear momentum conservation for entire system

$$m_1 v_{n_1} + m_2 v_{n_2} = m_1 v'_{n_1} + m_2 v'_{n_2}$$

$$\Rightarrow m_1 (v_{n_1} - v'_{n_1}) = \cancel{m_2} \underbrace{(v'_{n_2} - v_{n_2})}_{\approx 0} \quad \times \quad \begin{matrix} \text{Not} \\ \text{useful} \end{matrix}$$

finite but unknown

3) Angular momentum conservation abt coincident point

'O' fixed in 'I' frame separately for two RBs

$$\text{RB } \textcircled{1} : \underline{H}_{C_1} + \underline{\gamma}_{C_1 O} \times m_1 \underline{v}_{C_1} = \underline{H}_{C_1}' + \underline{\gamma}_{C_1 O} \times m_1 \underline{v}_{C_1}'$$

(3 eqns)

$$\text{RB } \textcircled{2} : \underline{H}_{C_2} + \underline{\gamma}_{C_2 O} \times m_2 \underline{v}_{C_2} = \underline{H}_{C_2}' + \underline{\gamma}_{C_2 O} \times m_2 \underline{v}_{C_2}'$$

$$\underline{I}^{c_2} \underline{\omega}_2$$

\downarrow since
 $\underline{\omega}_2' \approx \underline{\omega}_2$

\Rightarrow no equations obtained from RB $\textcircled{2}$

A) Relating contact point velocities via coefficient of restitution

$$e = - \frac{\underline{v}_{B_n}' - \underline{v}_{A_n}'}{\underline{v}_{B_n} - \underline{v}_{A_n}}$$

We have $\underline{v}_{B_n}' \approx \underline{v}_{B_n}$ (\because B is the pt of impact of massive RB $\textcircled{2}$)

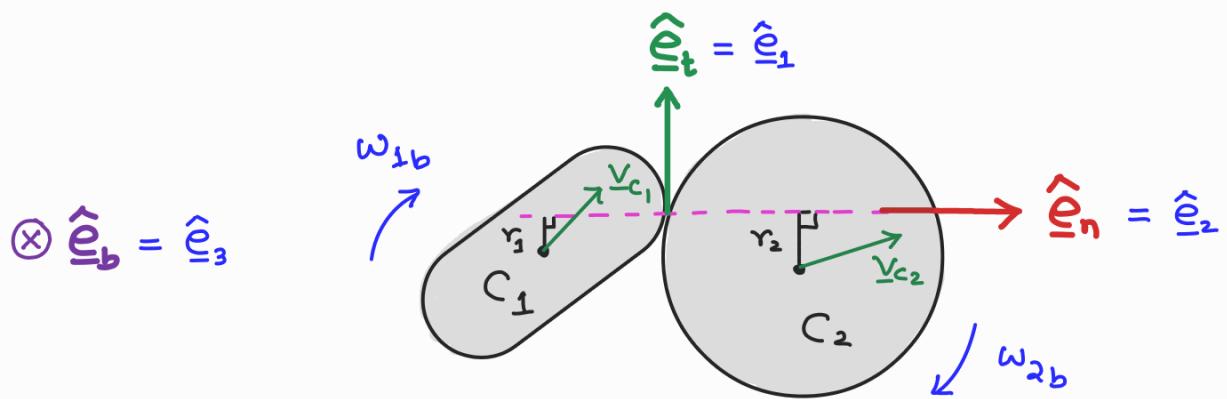
$$\Rightarrow e = - \frac{(\underline{v}_{B_n} - \underline{v}_{A_n}')}{(\underline{v}_{B_n} - \underline{v}_{A_n})} \quad (1 \text{ eqn})$$

So we get total 6 equations for 6 unknowns

Smooth Planar Impact

In this case, the two RBs ① and ② maintain planar motion ($\hat{e}_n - \hat{e}_t$ plane) before and after impact

→ this is possible if and only if C_1 and C_2 lie in the $\hat{e}_n - \hat{e}_t$ plane AND \hat{e}_b is a principal axis at C_1 for RB ① AND at C_2 for RB ②



Note: $\underline{\omega}'_1$ and $\underline{\omega}'_2$ have components ONLY in \hat{e}_b direction

Unknowns: v'_n, v'_t, ω'_{1b} (for RB 1 after impact)

v'_n, v'_t, ω'_{2b} (for RB 2 after impact)

⇒ 6 unknowns (instead of 12 unknowns)

We need to get 6 equations to solve for 6 unknowns:

1) Smooth impact \Rightarrow no impulse along \hat{e}_t direction

$$v_{t_1} = v_{t_1}' \quad \text{and} \quad v_{t_2} = v_{t_2}' \rightarrow \textcircled{1} \quad \textcircled{2} \quad \textcircled{2}$$

2) Conservation of linear momentum for entire system (RB)

(1) + RB (2) along \hat{e}_n

$$m_1 v_{n_1} + m_2 v_{n_2} = m_1 v_{n_1}' + m_2 v_{n_2}' \rightarrow \textcircled{3}$$

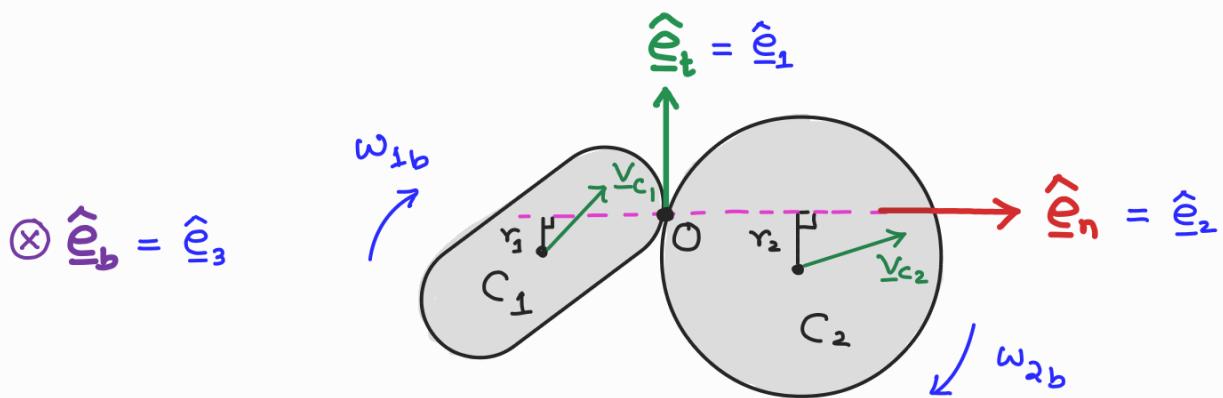
3) Conservation of angular momentum about coincident point

'O' fixed in inertial frame 'I' for each body

$$\begin{aligned} \text{RB (1)} : \underline{H}_{C_1} + \underline{r}_{C_1 O} \times m_1 \underline{v}_{C_1} &= \underline{H}_{C_1}' + \underbrace{\underline{r}_{C_1 O} \times m_1 \underline{v}_{C_1}'}_{\text{III}} \\ \underline{I}_c \underline{\omega}_1 &= \underline{r} \hat{e}_1 \times m [v_{t_1}' \hat{e}_1 + v_{n_1}' \hat{e}_2] \end{aligned}$$

(i) $[\underline{\omega}_1] \begin{bmatrix} \hat{e}_1 \\ \hat{e}_2 \\ \hat{e}_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \omega_{b_1} \end{bmatrix}; \quad [\underline{\omega}_1'] \begin{bmatrix} \hat{e}_1 \\ \hat{e}_2 \\ \hat{e}_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \omega_{b_1}' \end{bmatrix} \quad \left. \begin{array}{l} \text{simplifies computation} \\ \text{of } \underline{I}_c \underline{\omega}_1 \text{ and} \\ \underline{I}_c \underline{\omega}_1' \end{array} \right\}$

(ii) $\hat{e}_3 = \hat{e}_b$ is a principal axis at C_1
 $\Rightarrow I_{23}^{C_1} = I_{13}^{C_1} = 0$



$$\text{RB ① : } H_{C_1} + r_{C_1 O} \times m_1 v_{c_1} = H'_{C_1} + \underbrace{r_{C_1 O} \times m_1 v'_{c_1}}_{\text{III}} + I_C \omega'_1 - r \hat{e}_1 \times m [v'_{t_1} \hat{e}_1 + v'_{n_1} \hat{e}_2]$$

$$\Rightarrow I_{33}^{C_1} \omega_{b_1} + m_1 v_{n_1} r_1 = I_{33}^{C_1} \omega'_{b_1} + m_1 v'_{n_1} r_1 \quad ④$$

⊕ or ⊖ sign will depend on the outcome of the cross-product

RB ② : Doing similarly for RB 2, we get another equation:

$$I_{33}^{C_2} \omega_{b_2} + m_2 v_{n_2} r_2 = I_{33}^{C_2} \omega'_{b_2} + m_2 v'_{n_2} r_2 \quad ⑤$$

4) Relating contact point velocities through coefficient of restitution:

$$v'_{B_n} - v'_{A_n} = -e(v_{B_n} - v_{A_n}) \quad — ⑥$$

We now have 6 eqns and 6 unknowns!