

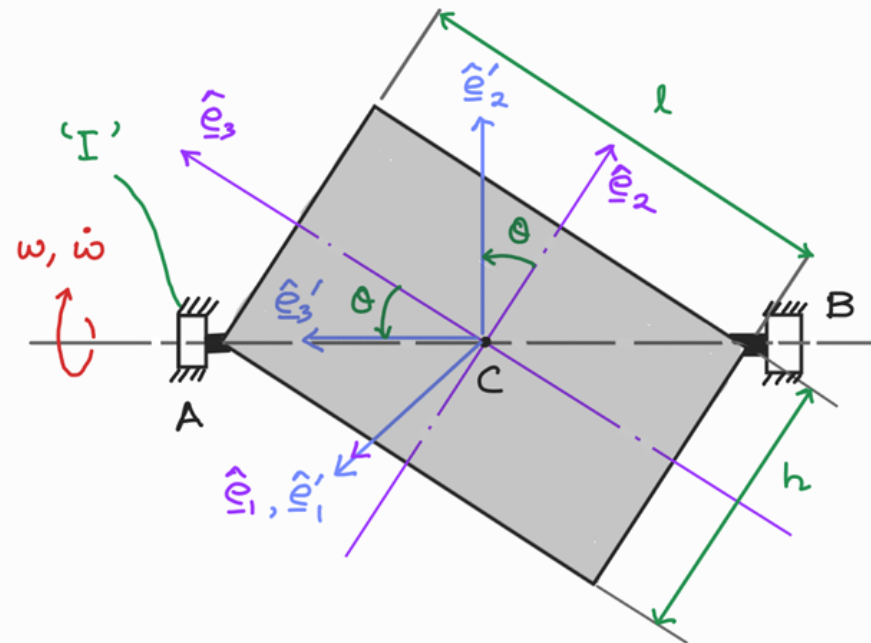
Tutorial 6 (Part A)

A thin homogeneous rectangular plate, as shown, rotates about a diagonal axis with angular velocity $\underline{\omega}$ and angular acceleration $\underline{\dot{\omega}}$.

- (i) Determine the total moment \underline{M}_C exerted on the plate about the COM C , using the coordinate system $\hat{e}'_1, \hat{e}'_2, \hat{e}'_3$ in terms of the rotational motion $\underline{\omega}$ and $\underline{\dot{\omega}}$.
- (ii) Find the relation between a drive torque $\underline{T} = T\hat{e}'_3$ (applied about \hat{e}'_3 -axis) to the rotational motion. Also, determine the bearing support reaction forces (assuming bearing support reaction couples are zero).

Given: $\underline{\omega}_{m|I} = \omega \hat{e}'_3$
 $\underline{\dot{\omega}}_{m|I} = \dot{\omega} \hat{e}'_3$

plate lies in the plane of
 $x_2(\hat{e}_2) - x_3(\hat{e}_3) / x'_2(\hat{e}'_2) - x'_3(\hat{e}'_3)$
 Both CSs are body-fixed.



Solution: RB 'm' \leftarrow rectangular plate rotates about an axis

We can make use of the simplified Euler's 2nd equation for an RB rotating about a fixed axis.

Recall the simplified Euler's 2nd equation at point A of the RB rotating about a fixed body axis $\hat{\underline{e}}_3$

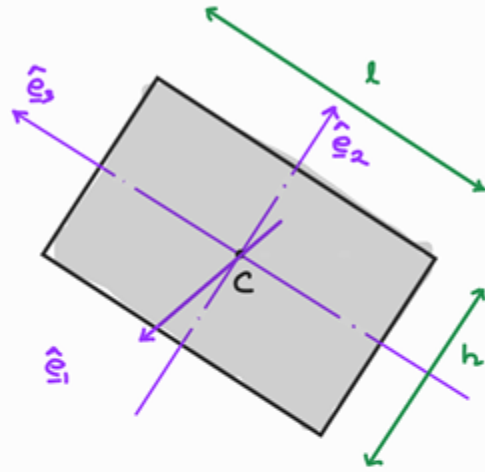
$$\underline{M}_A = \underbrace{\left(I_{13}^A \dot{\omega} - I_{23}^A \omega^2 \right)}_{M_{A,1}} \hat{\underline{e}}_1 + \underbrace{\left(I_{23}^A \dot{\omega} + I_{13}^A \omega^2 \right)}_{M_{A,2}} \hat{\underline{e}}_2 + \underbrace{I_{33}^A \dot{\omega}}_{M_{A,3}} \hat{\underline{e}}_3$$

With the body-fixed csys being $\hat{\underline{e}}_1' - \hat{\underline{e}}_2' - \hat{\underline{e}}_3'$, we rewrite the equation as: $A \equiv C$, $\hat{\underline{e}}_i \rightarrow \hat{\underline{e}}_i'$

$$\underline{M}_C = \underbrace{\left(I_{13}^C \dot{\omega} - I_{23}^C \omega^2 \right)}_{M_{C,1}'} \hat{\underline{e}}_1' + \underbrace{\left(I_{23}^C \dot{\omega} + I_{13}^C \omega^2 \right)}_{M_{C,2}'} \hat{\underline{e}}_2' + \underbrace{I_{33}^C \dot{\omega}}_{M_{C,3}'} \hat{\underline{e}}_3'$$

To determine \underline{M}_C , we need to calculate the inertia matrix components in $\hat{\underline{e}}_1' - \hat{\underline{e}}_2' - \hat{\underline{e}}_3'$ csys.

Note: $\hat{\underline{e}}_1 - \hat{\underline{e}}_2 - \hat{\underline{e}}_3$ csys coincide with the principal axes of inertia of the rectangular plate (due to planes of symmetry)



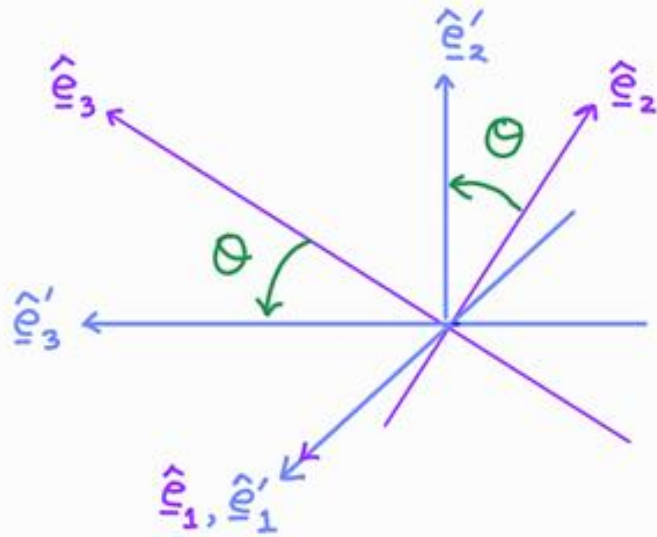
$$\Rightarrow [\underline{\underline{I}}^C] \begin{pmatrix} \hat{\underline{e}}_1 \\ \hat{\underline{e}}_2 \\ \hat{\underline{e}}_3 \end{pmatrix} = \begin{bmatrix} I_{11}^C & 0 & 0 \\ 0 & I_{22}^C & 0 \\ 0 & 0 & I_{33}^C \end{bmatrix} = \begin{bmatrix} \frac{m(l^2 + h^2)}{12} & 0 & 0 \\ 0 & \frac{ml^2}{12} & 0 \\ 0 & 0 & \frac{mh^2}{12} \end{bmatrix}$$

Next we will use inertia matrix transformation law

to find the components of $\underline{\underline{I}}^C$ in $\hat{\underline{e}}'_1 - \hat{\underline{e}}'_2 - \hat{\underline{e}}'_3$ csys

$$[\underline{\underline{I}}^c] \begin{pmatrix} \hat{\underline{\underline{e}}}_1' \\ \hat{\underline{\underline{e}}}_2' \\ \hat{\underline{\underline{e}}}_3' \end{pmatrix} = [\underline{\underline{A}}] [\underline{\underline{I}}_c] \begin{pmatrix} \hat{\underline{\underline{e}}}_1 \\ \hat{\underline{\underline{e}}}_2 \\ \hat{\underline{\underline{e}}}_3 \end{pmatrix} [\underline{\underline{A}}]^T$$

Find transformation matrix $[\underline{\underline{A}}]$: Use $A_{ij} = \hat{\underline{\underline{e}}}_i' \cdot \hat{\underline{\underline{e}}}_j$



$$A_{22} = \hat{\underline{\underline{e}}}_2' \cdot \hat{\underline{\underline{e}}}_2 = \cos \Theta = c$$

$$A_{23} = \hat{\underline{\underline{e}}}_2' \cdot \hat{\underline{\underline{e}}}_3 = \sin \Theta = s$$

$$A_{32} = \hat{\underline{\underline{e}}}_3' \cdot \hat{\underline{\underline{e}}}_2 = -\sin \Theta = -s$$

$$A_{33} = \hat{\underline{\underline{e}}}_3' \cdot \hat{\underline{\underline{e}}}_3 = \cos \Theta = c$$

$$A_{11} = 1, \quad A_{21} = A_{31} = 0$$

$$\begin{aligned}
 [\underline{I}^c] \begin{pmatrix} \hat{e}_1' \\ \hat{e}_2' \\ \hat{e}_3' \end{pmatrix} &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & c & s \\ 0 & -s & c \end{bmatrix} \begin{bmatrix} I_{11}^c & 0 & 0 \\ 0 & I_{22}^c & 0 \\ 0 & 0 & I_{33}^c \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & c & s \\ 0 & -s & c \end{bmatrix} \\
 &= \begin{bmatrix} I_{11}^c & 0 & 0 \\ 0 & c^2 I_{22}^c + s^2 I_{33}^c & cs(-I_{22}^c + I_{33}^c) \\ 0 & \text{sym} & s^2 I_{22}^c + c^2 I_{33}^c \end{bmatrix}
 \end{aligned}$$

From geometry of plate: $\sin \theta = \frac{h}{\sqrt{l^2 + h^2}}$, $\cos \theta = \frac{l}{\sqrt{l^2 + h^2}}$

Given: $[\underline{\omega}] \begin{pmatrix} \hat{e}_1' \\ \hat{e}_2' \\ \hat{e}_3' \end{pmatrix} = \begin{bmatrix} 0 \\ 0 \\ \omega \end{bmatrix}$ & $[\underline{\dot{\omega}}] \begin{pmatrix} \hat{e}_1' \\ \hat{e}_2' \\ \hat{e}_3' \end{pmatrix} = \begin{bmatrix} 0 \\ 0 \\ \dot{\omega} \end{bmatrix}$

Let's now use simplified Euler's 2nd equation:

$$\underline{M}_C = \underbrace{\left(I_{13}^C \dot{\omega} - I_{23}^C \omega^2 \right)}_{M'_{C,1}} \hat{e}'_1 + \underbrace{\left(I_{23}^C \dot{\omega} + I_{13}^C \omega^2 \right)}_{M'_{C,2}} \hat{e}'_2 + \underbrace{I_{33}^C \dot{\omega}}_{M'_{C,3}} \hat{e}'_3$$

$$M'_{C,1} = - \frac{1}{12} m (-l^2 + h^2) \sin \Theta \cos \Theta \omega^2$$

$$= - \frac{m l h}{12} \frac{(-l^2 + h^2)}{(l^2 + h^2)} \omega^2$$

$$M'_{C,2} = \frac{m l h}{12} \frac{(-l^2 + h^2)}{(l^2 + h^2)} \dot{\omega}$$

$$M'_{C,3} = \left(\sin^2 \Theta \frac{m l^2}{12} + \cos^2 \Theta \frac{m h^2}{12} \right) \dot{\omega}$$

$$= \frac{m}{12} \left(\frac{h^2 l^2}{l^2 + h^2} + \frac{l^2 h^2}{l^2 + h^2} \right) \dot{\omega}$$

$$= \frac{m h^2 l^2}{6 (l^2 + h^2)} \dot{\omega}$$

(*)

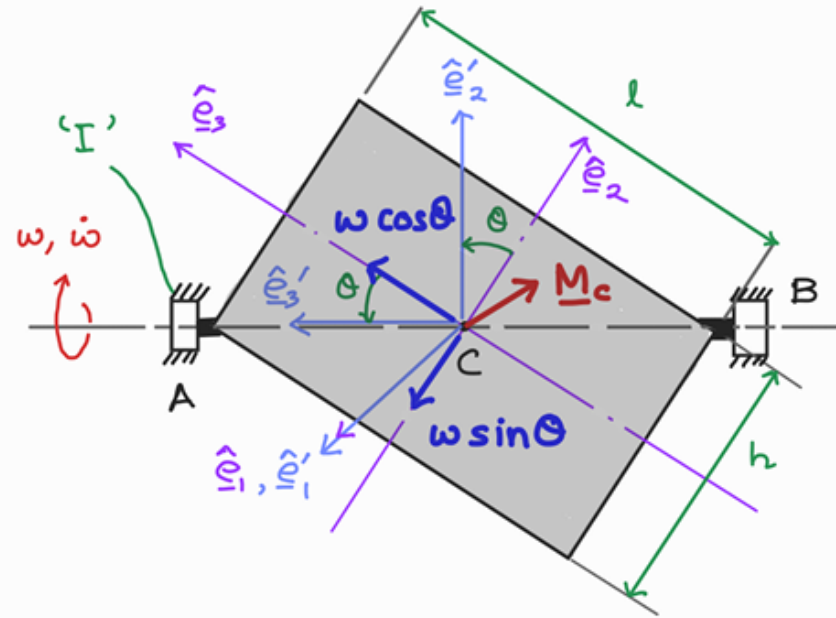
Alternative way : Using simplified Euler's 2nd equation

in csys $\hat{e}_1 - \hat{e}_2 - \hat{e}_3$ (coinciding with p-axes of plate)

Let's solve the problem
using p-axes csys!

$$\begin{bmatrix} \underline{\omega} \end{bmatrix} \begin{pmatrix} \hat{e}_1 \\ \hat{e}_2 \\ \hat{e}_3 \end{pmatrix} = \begin{bmatrix} 0 \\ -\omega \sin \Theta \\ \omega \cos \Theta \end{bmatrix}$$

$$\begin{bmatrix} \dot{\underline{\omega}} \end{bmatrix} \begin{pmatrix} \hat{e}_1 \\ \hat{e}_2 \\ \hat{e}_3 \end{pmatrix} = \begin{bmatrix} 0 \\ -\dot{\omega} \sin \Theta \\ \dot{\omega} \cos \Theta \end{bmatrix}$$



$$\text{where } \sin \Theta = \frac{h}{\sqrt{l^2 + h^2}} \equiv S$$

$$\cos \Theta = \frac{l}{\sqrt{l^2 + h^2}} \equiv C$$

Since $\hat{\underline{e}}_1 - \hat{\underline{e}}_2 - \hat{\underline{e}}_3$ coincides with p-axes of inertia of the rectangular plate

$$[\underline{\underline{I}}^C] \begin{pmatrix} \hat{\underline{e}}_1 \\ \hat{\underline{e}}_2 \\ \hat{\underline{e}}_3 \end{pmatrix} = \begin{bmatrix} \frac{m(l^2 + h^2)}{12} & 0 & 0 \\ 0 & \frac{ml^2}{12} & 0 \\ 0 & 0 & \frac{mh^2}{12} \end{bmatrix}$$

Now let's use simplified Euler's equation at pt C in the $\hat{\underline{e}}_1 - \hat{\underline{e}}_2 - \hat{\underline{e}}_3$ csys (coinciding with p-axes of RB at C)

$$\underline{M}_c = M_{c,1} \hat{e}_1 + M_{c,2} \hat{e}_2 + M_{c,3} \hat{e}_3$$

$$\begin{aligned} \underline{M}_c = & \left[I_{11}^c \cancel{\dot{\omega}_1}^0 - (I_{22}^c - I_{33}^c) \omega_2 \omega_3 \right] \hat{e}_1 \\ & + \left[I_{22}^c \cancel{\dot{\omega}_2}^{-\dot{\omega}_3} - (I_{33}^c - I_{11}^c) \omega_3 \cancel{\omega_1}^0 \right] \hat{e}_2 \\ & + \left[I_{33}^c \cancel{\dot{\omega}_3}^{\dot{\omega}_c} - (I_{11}^c - I_{22}^c) \cancel{\omega_1}^0 \omega_2 \right] \hat{e}_3 \end{aligned}$$

$$= - \underbrace{\frac{m}{12} c s (l^2 - h^2)}_{M_{c,1}} \omega^2 \hat{e}_1 + \underbrace{\frac{m}{12} (-s l^2)}_{M_{c,2}} \hat{e}_2 + \underbrace{\frac{m}{12} c h^2}_{M_{c,3}} \hat{e}_3 \dot{\omega}$$

Note that $M_{c,1}$, $M_{c,2}$, and $M_{c,3}$ are components of \underline{M}_c in the $\hat{e}_1 - \hat{e}_2 - \hat{e}_3$ csys.

To get the components of \underline{M}_c in $\hat{\underline{e}}_1' - \hat{\underline{e}}_2' - \hat{\underline{e}}_3$ csys, one needs to use a transformation of coordinate sys :

$$[\underline{M}_c] \begin{pmatrix} \hat{\underline{e}}_1' \\ \hat{\underline{e}}_2' \\ \hat{\underline{e}}_3' \end{pmatrix} = [\underline{A}] [\underline{M}_c] \begin{pmatrix} \hat{\underline{e}}_1 \\ \hat{\underline{e}}_2 \\ \hat{\underline{e}}_3 \end{pmatrix}$$

$$\Rightarrow \begin{bmatrix} M_{c,1}' \\ M_{c,2}' \\ M_{c,3}' \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & c & s \\ 0 & -s & c \end{bmatrix} \begin{bmatrix} M_{c,1} \\ M_{c,2} \\ M_{c,3} \end{bmatrix}$$

$$\therefore M_{c,1}' = M_{c,1} = -\frac{m \ell h}{12} \frac{(-\ell^2 + h^2)}{(\ell^2 + h^2)} \omega^2$$

$$\begin{aligned}
 M_{c,2}' &= c M_{c,2} + s M_{c,3} \\
 &= \frac{m}{12} c s (-l^2 + h^2) \dot{\omega} \\
 &= \frac{m}{12} l h \frac{(-l^2 + h^2)}{(l^2 + h^2)} \dot{\omega}
 \end{aligned}$$

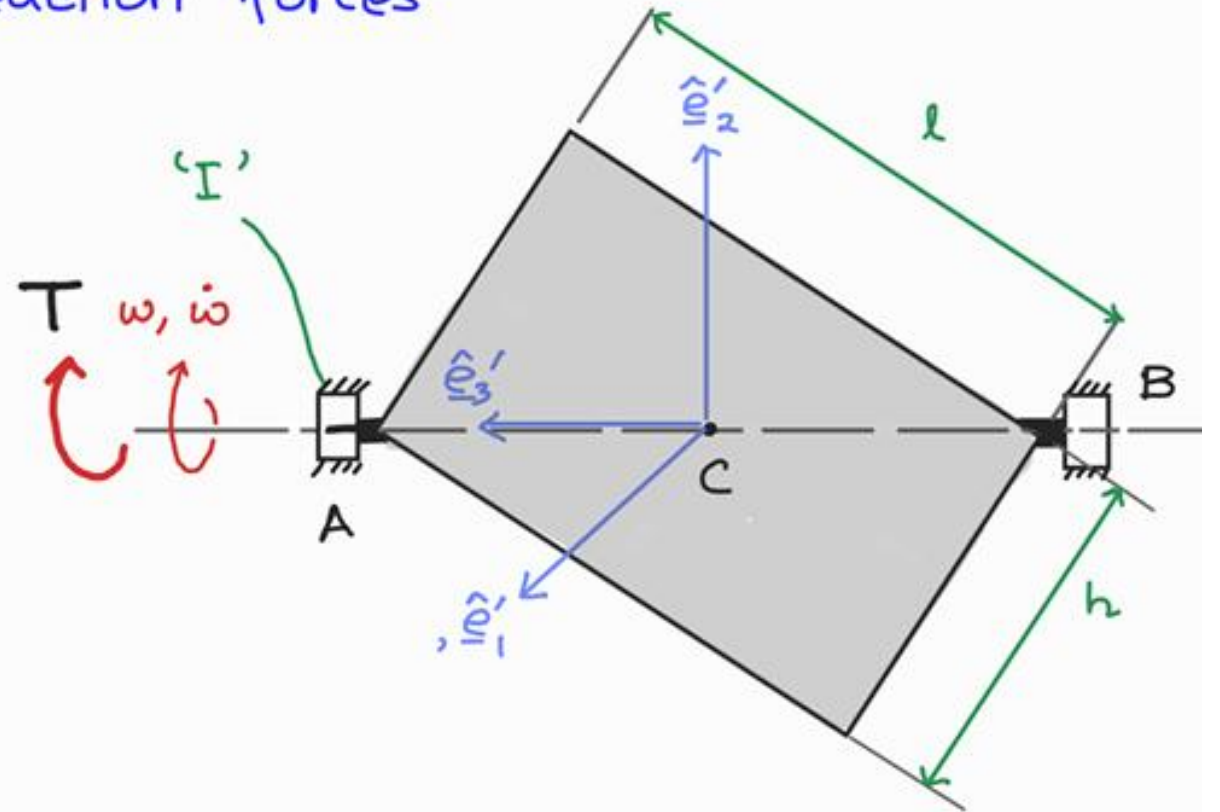
$$\begin{aligned}
 M_{c,3}' &= -s M_{c,2} + c M_{c,3} \\
 &= \frac{m}{12} (s^2 l^2 + c^2 h^2) \dot{\omega} = \frac{m h^2 l^2}{6 (l^2 + h^2)} \dot{\omega}
 \end{aligned}$$

These are the same components we obtained using the 1st method.

Note that even if $\dot{\omega} = 0$, still $\underline{M}_c \neq 0$ for a rotational motion with constant angular velocity ω .

ii) Equation relating drive torque \underline{I} to the rotation and dynamic bearing reaction forces

$$\underline{I} = T \hat{e}_3'$$



Draw the FBD

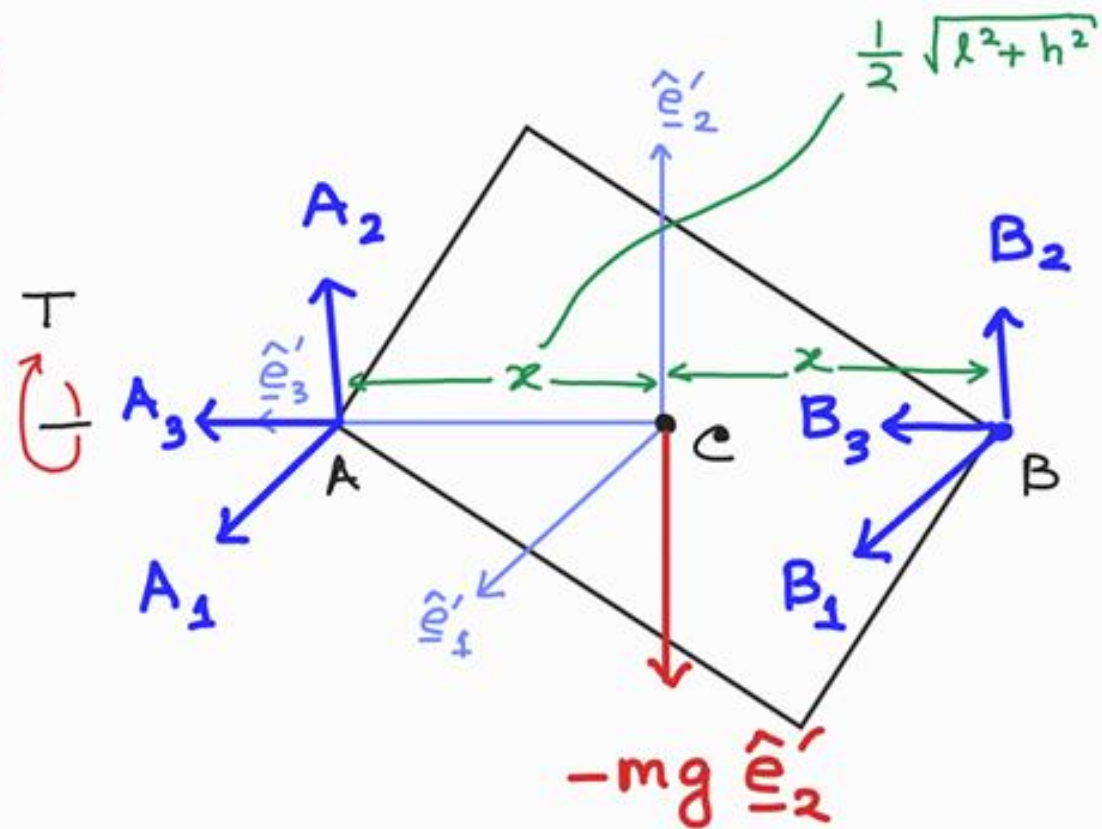
FBD

Assume zero reaction couples
at supports (Given)

Reaction forces at
supports A and B

$$\underline{A} = A_1 \underline{\hat{e}}'_1 + A_2 \underline{\hat{e}}'_2 + A_3 \underline{\hat{e}}'_3$$

$$\underline{B} = B_1 \underline{\hat{e}}'_1 + B_2 \underline{\hat{e}}'_2 + B_3 \underline{\hat{e}}'_3$$



From Euler's 1st eqn:

$$\underline{A} + \underline{B} - mg \hat{e}_2' = m \overset{0}{\underline{a}_C} = 0$$

because C is
on the \hat{e}_3' -axis
itself at all times!

$$\Rightarrow \underline{A} + \underline{B} = mg \hat{e}_2'$$

Component-wise: $B_1 = -A_1$

$$A_2 + B_2 = mg$$

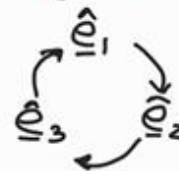
$$B_3 = -A_3$$

Express \underline{M}_C in terms of the external force system

$$\underline{M}_C = \underline{I} + \underline{r}_{AC} \times \underline{A} + \underline{r}_{BC} \times \underline{B} \quad (-mg \hat{e}_2' \text{ passes through C})$$

$$= I \hat{e}_3' + (\underline{r} \hat{e}_3') \times (A_1 \hat{e}_1' + A_2 \hat{e}_2' + A_3 \hat{e}_3')$$

$$+ (-\underline{r} \hat{e}_3') \times (\overset{-A_1}{B_1} \hat{e}_1' + B_2 \hat{e}_2' + \overset{-A_3}{B_3} \hat{e}_3')$$



$$\begin{aligned}
&= T \hat{\underline{e}}_3' + A_1 \times \hat{\underline{e}}_2 - A_2 \times \hat{\underline{e}}_1' + A_1 \times \hat{\underline{e}}_2 + B_2 \times \hat{\underline{e}}_1' \\
&= \underbrace{(-A_2 + B_2) \times \hat{\underline{e}}_1'}_{= M_{C,1}} + \underbrace{A_1 (2 \times) \hat{\underline{e}}_2'}_{= M_{C,2}} + \underbrace{T \hat{\underline{e}}_3'}_{= M_{C,3}}
\end{aligned}$$

Comparing these relations with the values obtained in (*)

$$\Rightarrow T = \frac{m h^2 l^2}{6(l^2 + h^2)} \dot{\omega}, \quad A_1 = -B_1 = -\frac{m l h}{12} \frac{(-l^2 + h^2)}{(l^2 + h^2)^{3/2}} \omega^2$$

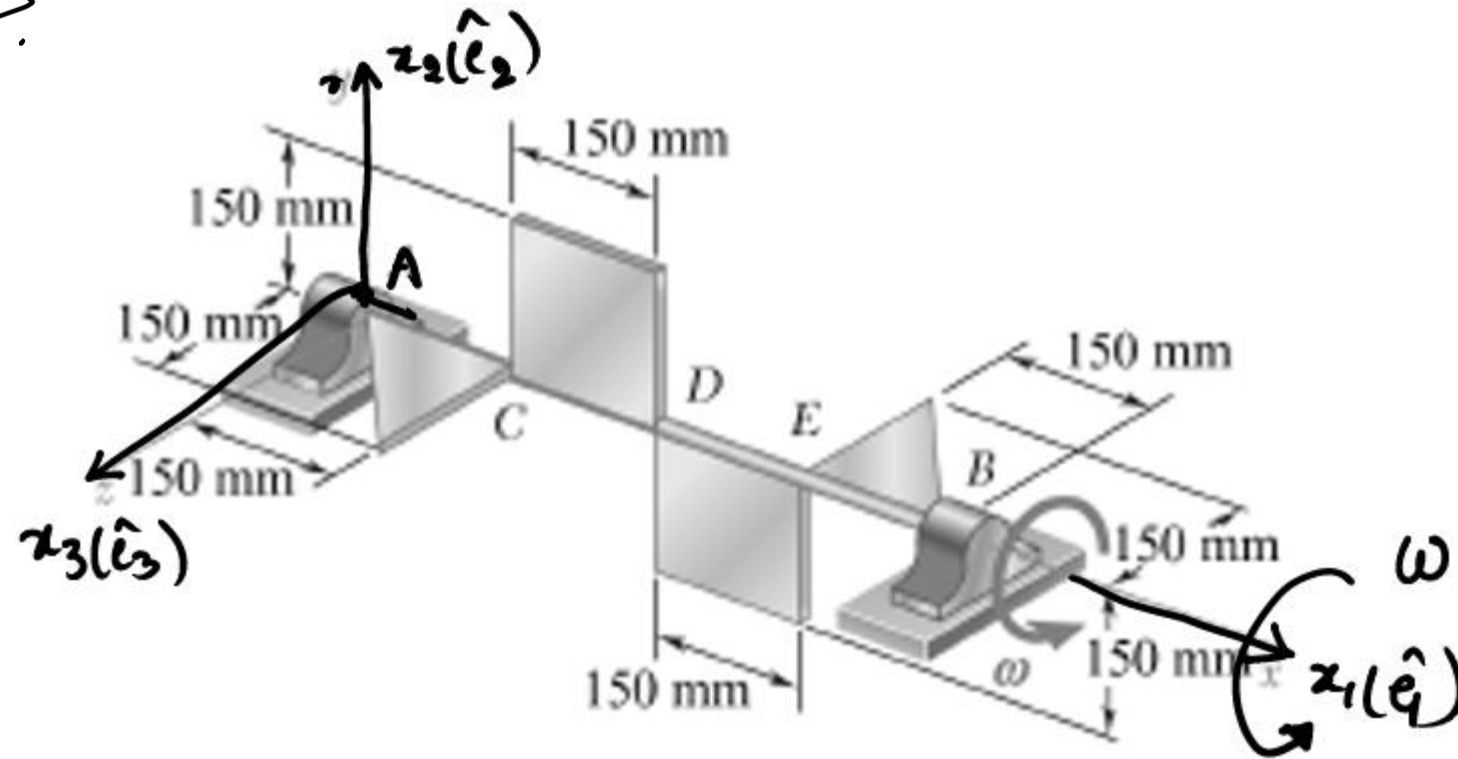
and, finally

$$\left. \begin{aligned}
A_2 + B_2 &= mg \\
A_2 - B_2 &= \frac{m l h}{24} \frac{(-l^2 + h^2)}{(l^2 + h^2)^{3/2}} \dot{\omega}
\end{aligned} \right\} \begin{array}{l} \text{Solve} \\ \text{to get} \\ \text{values of} \\ A_2 \text{ \& } B_2 \end{array}$$

The axial reaction force components along $\hat{\underline{e}}_3'$, A_3 & B_3 cannot be determined from this analysis.

Q1. Relate the reaction forces and moments of couples at A and B to the motion of the shaft. Angular velocity of the shaft is constant.

Set 6 B



Answer: $A_1 + B_1 = 0$, $A_2 + B_2 = mg$, $A_3 + B_3 = 0$

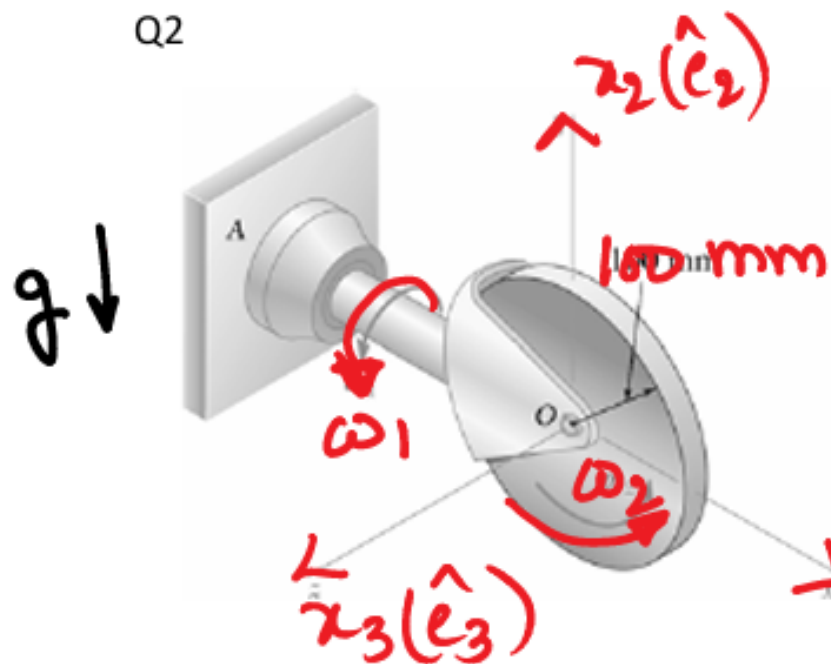
$$0.3A_3 - 0.3B_3 + C_{A2} + C_{B2} = -I_{31}^D \omega^2$$

$$-0.3A_2 + 0.3B_2 + C_{A3} + C_{B3} = I_{21}^D \omega^2$$

Set 6 B: Q 2

(Type II: problem)

Q2



PROBLEM 18.83 (Beer Johnston)

The uniform thin 2.5-kg disk spins at a constant rate $\omega_2 = 6 \text{ rad/s}$ about an axis held by a housing attached to a horizontal rod that rotates at the constant rate $\omega_1 = 3 \text{ rad/s}$. ~~Determine the couple which represents the dynamic reaction at the support A.~~

Find the force and moment of couple acting on the rod at A. (at this instant).
 (Ao is massless)

$AO = 1\text{m}$

$$\underline{F} = 24.5 \text{ N vertically up}$$

$$\underline{C} = -0.225 \text{ Nm } \hat{e}_2 + 24.5 \text{ Nm } \hat{e}_3$$

$\hat{x}_1(\hat{e}_1) \hat{x}_2(\hat{e}_2) \hat{x}_3(\hat{e}_3)$ is fixed to the disk.