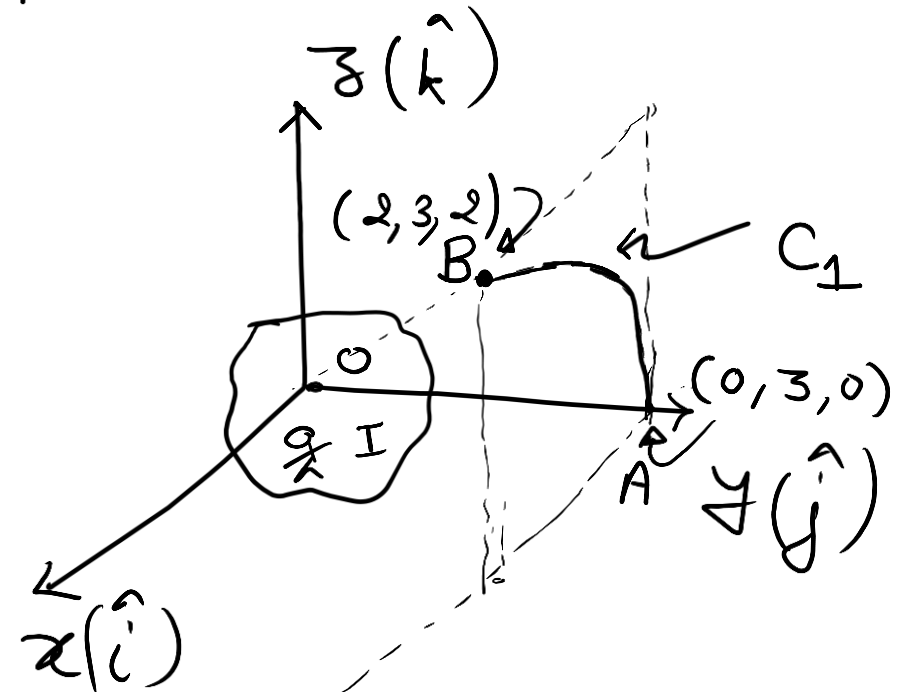


Q 1) Is the force  $\underline{F} = (-2xy + yz)\hat{i} + (-x^2 + xz - 3)\hat{j} + (xy - y)\hat{k}$  conservative?

(b) If it is conservative, find its potential function.

(c) Find the work done by this force while a particle (say P) moves along an open quarter circular path  $C_1$ . (Start at A, end at B)



$$\nabla \times \underline{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ -2xy + yz & -x^2 + xz - z & xy - y \end{vmatrix}$$

$$= \hat{i} (x - 1 - x + 1) - \hat{j} (y - y) + \hat{k} (-2x + z + 2x - z)$$

$$= \hat{i} (0) - \hat{j} (0) + \hat{k} (0)$$

$$= 0 \quad \forall x, y, z$$

$\Rightarrow \underline{F}$  is conservative

$\Rightarrow$  Work done by this force when a particle moves from point A to point B is path independent. We need to find  $V$ .

$$W_{\underline{A \rightarrow B}} = -[V(2,3,2) - V(0,3,0)] \quad \text{where } V \text{ is the potential function of } \underline{F}.$$

What is  $V(x,y,z)$

$$F_x = -\frac{\partial V}{\partial x}$$

$$F_y = -\frac{\partial V}{\partial y}$$

$$F_z = -\frac{\partial V}{\partial z}$$

$$-2xy + yz = -\frac{\partial V}{\partial x} \Rightarrow \int (-2xy + yz) dx = -V(x,y,z) + f(y,z) \quad (i)$$

$$-x^2 + xz - z = -\frac{\partial V}{\partial y} \Rightarrow \int (-x^2 + xz - z) dy = -V(x,y,z) + g(z,x) \quad (ii)$$

$$xy - y = -\frac{\partial V}{\partial z} \Rightarrow \int (xy - y) dz = -V(x,y,z) + h(x,y) \quad (iii)$$

Complete the integration of the left hand sides of (i) (ii) (iii)

$$-x^2y + yz = -V(x, y, z) + f(y, z) \quad (iv)$$

$$-x^2y + xzy - zy = -V(x, y, z) + g(z, x) \quad (v)$$

$$xyz - yz = -V(x, y, z) + h(x, y) \quad (vi)$$

$$\text{or, } V(x, y, z) = x^2y - xyz + f(y, z). \quad (vii)$$

$$\rightarrow V(x, y, z) = x^2y - xyz + yz + g(z, x) \quad (viii)$$

$$\rightarrow V(x, y, z) = -xyz + yz + h(x, y) \quad (ix)$$

vii, viii, ix are simultaneously satisfied if we choose

$$f(y, z) = yz, \quad g(z, x) = 0, \quad h(x, y) = x^2y.$$

$$\Rightarrow V(x, y, z) = x^2y - xyz + yz$$

$$\therefore W_{A \rightarrow B} = - \left[ V(2, 3, 2) - V(0, 3, 0) \right]$$

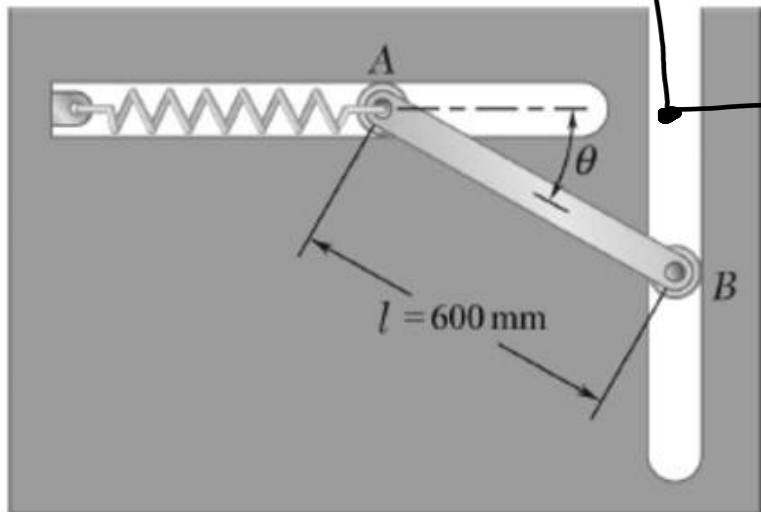
$$= -6 \text{ Nm.}$$

$$= - \left[ (2^2 \cdot 3 - 2 \cdot 3 \cdot 2 + 3 \cdot 2) - (0 - 0 + 0) \right]$$

$$= - \left[ 12 - 12 + 6 \right]$$

$$= - \left[ +6 \right] = -6 \text{ Nm.}$$

Q2

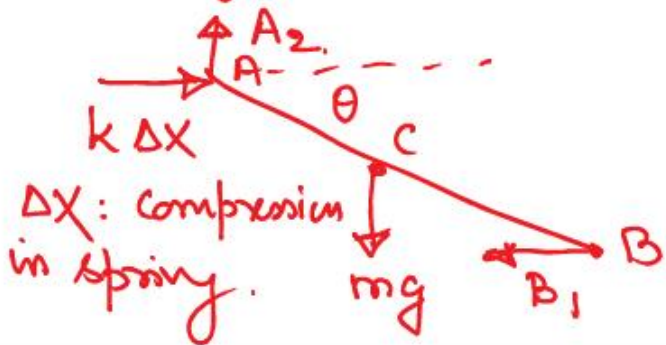


### PROBLEM 17.40

No friction force anywhere.

The ends of a 4.5 kg rod  $AB$  are constrained to move along slots cut in a vertical plane as shown. A spring of constant  $k = 600 \text{ N/m}$  is attached to end  $A$  in such a way that its tension is zero when  $\theta = 0$ . If the rod is released from rest when  $\theta = 0$ , determine the angular velocity of the rod and the velocity of end  $B$  when  $\theta = 30^\circ$ .

System = rod. FBD.



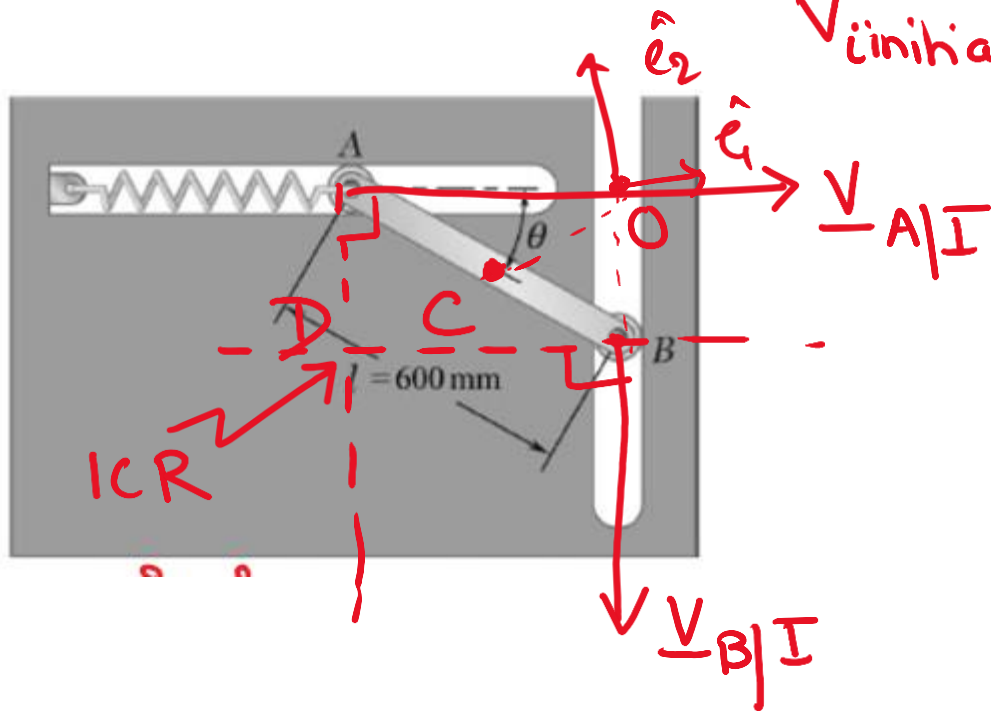
mass of rod:  $m$ ,  $k$ : spring constant (friction not present).  
 $B_1, A_2$  are workless forces and the remaining two forces are conservative.  
 $\therefore (T+V)_f - (T+V)_i = 0$  where  $i$ : initial state  $\theta = 0^\circ$   
 $f$ : final state  $\theta = 30^\circ$   
 $V = V_{\text{spring force}} + V_{\text{gravitational force}}$   
 $= -mg \frac{L}{2} \sin \theta + \frac{1}{2} k L^2 (1 - \cos \theta)^2$

$$V_{\text{gravitational force}} = mg x_2 \quad (x_2 \uparrow +ve)$$

$$V_{\text{spring force}} = \frac{1}{2} k (x_1 - x_0)^2 \quad x_0 = 0 \text{ here}$$

In the initial state:  $T_i = 0$  (motion starts from rest)

$$V_{\text{initial}} = V_{\text{initial}}^{\text{gravitation}} + V_{\text{initial}}^{\text{spring force}} = 0 + 0$$



Point D is the ICR of Rod AB

$$\Rightarrow \underline{v}_{C/I} = \underline{\omega}_{AB/I} \times \underline{r}_{CD}$$

$$= |\underline{v}_{C/I}| = \omega |\underline{r}_{CD}|$$

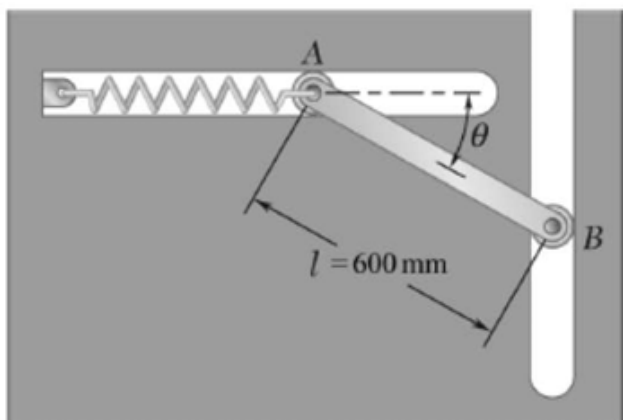
$$= \omega \frac{\sqrt{(L \cos \theta)^2 + (L \sin \theta)^2}}{2}$$

$$|\underline{v}_{C/I}| = \omega L/2$$

$$\Rightarrow \underline{v}_{C/I} \cdot \underline{v}_{C/I} = \omega^2 L^2/4$$

$$\therefore T = \frac{1}{2} m L^2 \frac{\omega^2}{4} + \frac{1}{2} \frac{m L^2 \omega^2}{12} = m L^2 \omega^2/6$$

Since  $(T+V)_f = 0$ ,  $\Rightarrow$  find  $\omega$



$$\frac{mL^2\omega^2}{6} = mgL\frac{\sin\theta}{2} - \frac{kL^2}{2}(1-\cos\theta)^2$$

$$\omega = \sqrt{\frac{mgL\frac{\sin\theta}{2} - \frac{kL^2}{2}(1-\cos\theta)^2}{mL^2/6}}$$

Answer.

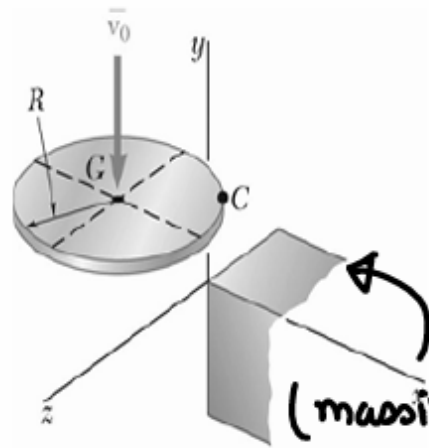


Q3

# PROBLEM 18.29

State the principle of conservation of angular momentum.

A circular plate of mass  $m$  is falling with a velocity  $\bar{v}_0$  and no angular velocity when its edge  $C$  strikes an obstruction. Assuming the impact to be perfectly plastic ( $e = 0$ ), determine the angular velocity of the plate immediately after the impact.

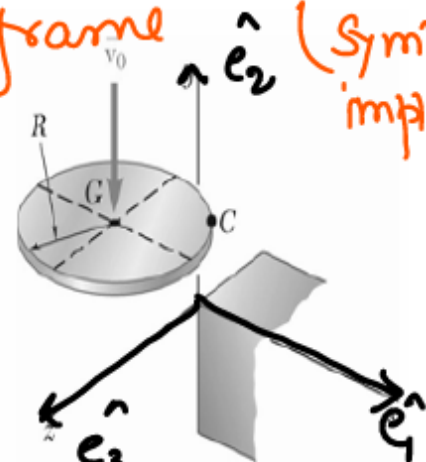
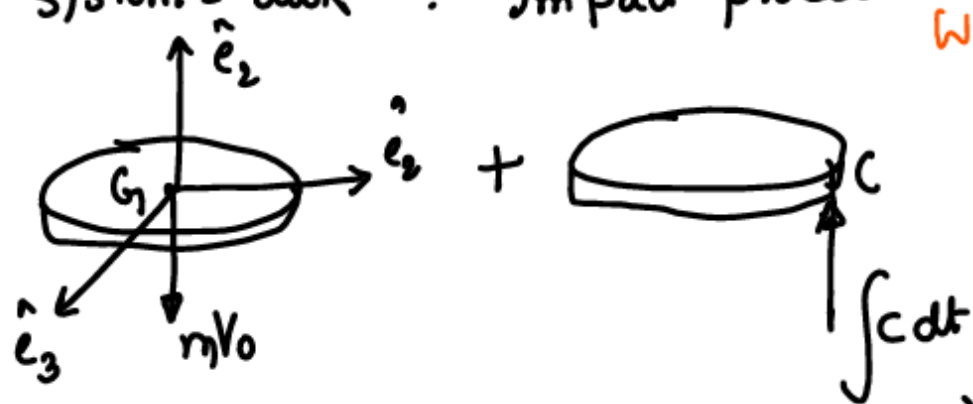


(massive, will undergo no change in its momentum)

Angular momentum

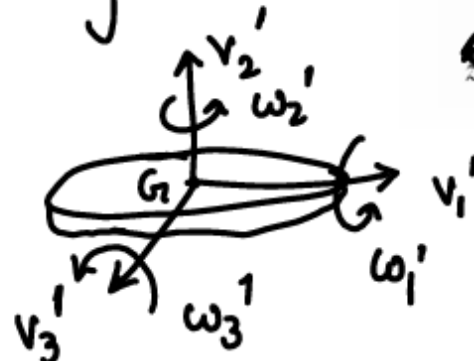
all velocity & angular momentum vectors are w.r.t. I frame (symbol implied)

System = disk : Impact process



Before impact

=



Find  $\omega_1', \omega_2', \omega_3'$

Find  $\omega_1', \omega_2', \omega_3'$

Unknowns : 7 unknowns. . 6 eqns from momentum  
- impulse (MI)  
eqns

7th eqn: coeff. of resilt. eqn.

Linear-momentum impulse eqn

$$\int \underline{F}^{\text{impulse}} dt = m [\underline{v}_{G/I}' - \underline{v}_{G/I}] \quad \underline{v}_{G/I} = -v_0 \hat{e}_2$$

$$\left( \int c dt \right) \hat{e}_2 = m [v_1' \hat{e}_1 + v_2' \hat{e}_2 + v_3' \hat{e}_3 - (-v_0 \hat{e}_2)]$$

$$\left( \int c dt \right) \hat{e}_2 = m v_1' \hat{e}_1 + (m v_2' + m v_0) \hat{e}_2 + v_3' \hat{e}_3$$

$$\Rightarrow \underbrace{v_1' = 0}, \underbrace{v_3' = 0}, \underbrace{\int c dt = mv_2' + mv_0}_{\text{Angular momentum - impulse eqn}} \quad (i)$$

Now using &

$$\int \underline{M}_A^{\text{impulse}} dt = \left[ m \underline{r}_{GA} \times \underline{v}_A(t_2) + \underline{H}_A(t_2) \right] - \left[ m \underline{r}_{GA} \times \underline{v}_A(t_1) + \underline{H}_A(t_1) \right]$$

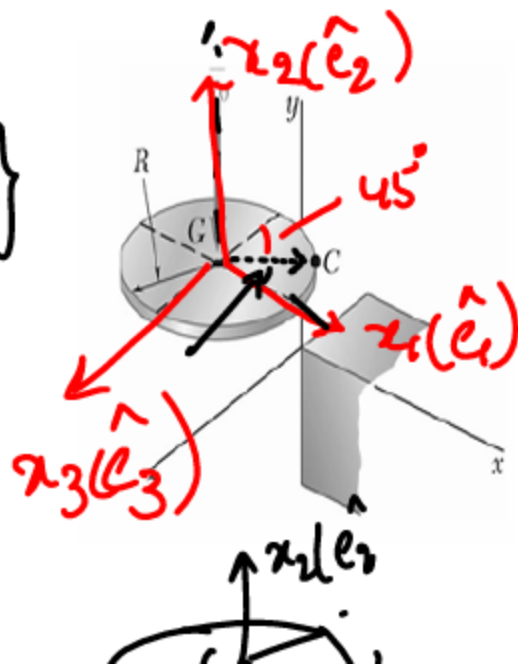
Choose

then  $A = G$  ✓  $\underline{r}_{GA} = 0$ .

$$\text{LHS} = \int \underline{M}_G^{\text{impulse}} dt = \left( \underline{r}_{CG} \times \int c dt \hat{e}_2 \right) \cdot \underline{r}_{CG} = \frac{R}{\sqrt{2}} \{ \hat{e}_1 - \hat{e}_3 \}$$

$$= \frac{R}{\sqrt{2}} (\hat{e}_1 - \hat{e}_3) \times \hat{e}_2 \int c dt$$

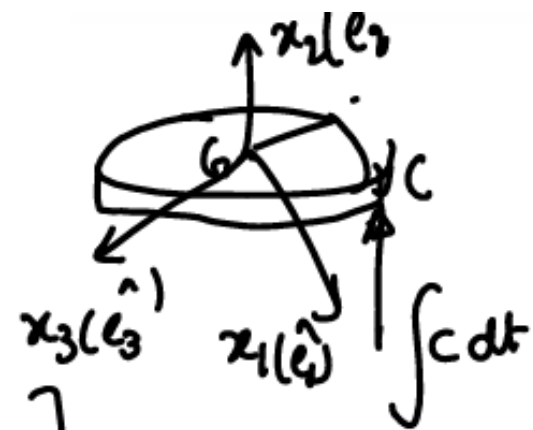
$$= \frac{R}{\sqrt{2}} \int c dt [\hat{e}_3 + \hat{e}_1] \quad (iv)$$



$$\frac{1}{\sqrt{2}} \begin{bmatrix} e_3 + e_1 \end{bmatrix} \quad (iv)$$

$$RHS = \underline{H}_G(t_2) - \underline{H}_G(t_1)$$

$$\underline{H}_G(t_2) = \begin{bmatrix} \frac{mR^2}{4} & 0 & 0 \\ 0 & \frac{mR^2}{2} & 0 \\ 0 & 0 & \frac{mR^2}{4} \end{bmatrix} \begin{bmatrix} \omega_1' \\ \omega_2' \\ \omega_3' \end{bmatrix}$$



$$\underline{\omega}_{m|I} = \omega_1' \hat{e}_1 + \omega_2' \hat{e}_2 + \omega_3' \hat{e}_3$$

$$\underline{H}_G(t_2) = \frac{mR^2}{4} \omega_1' \hat{e}_1 + \frac{mR^2}{2} \omega_2' \hat{e}_2 + \frac{mR^2}{4} \omega_3' \hat{e}_3 \quad (v)$$

$\underline{H}_G(t_1) = 0$ , matching (iv) and (v)

$$\Rightarrow \frac{R \int c dt}{\sqrt{2}} \hat{e}_1 + \frac{R \int c dt}{\sqrt{2}} \hat{e}_3 = \frac{mR^2}{4} \omega_1' \hat{e}_1 + \frac{mR^2}{2} \omega_2' \hat{e}_2 + \frac{mR^2}{4} \omega_3' \hat{e}_3$$

$$\Rightarrow \underbrace{\omega_2' = 0}, \quad \underbrace{\frac{R \int c dt}{\sqrt{2}}}_{(vii)} = \underbrace{\frac{m R^2}{4} \omega_1'}_{(viii)}, \quad \underbrace{\frac{R \int c dt}{\sqrt{2}} e_3}_{(viii)} = \underbrace{\frac{m R^2}{4} \omega_3' e_3}_{(viii)}$$

Co-eff of restitution  $e = 0$

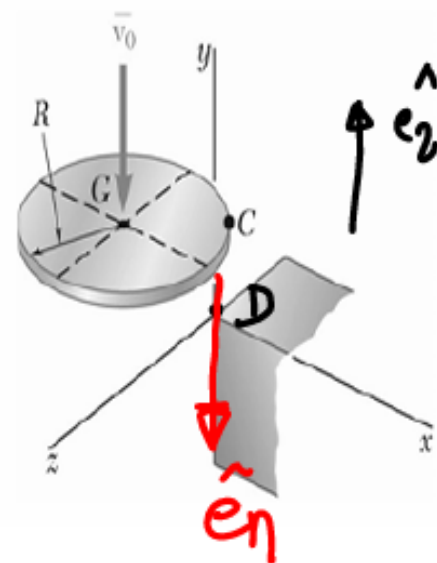
$$(\underline{V}'_D)_n - (\underline{V}'_C)_n = 0$$

$$(\underline{V}'_D)_n = (\underline{V}'_C)_n$$

(massive body)  $\Rightarrow (\underline{V}'_C)_n = 0$

$$(\underline{V}'_C) \cdot \hat{e}_2 = 0$$

$D \in$  massive body  
participating in impact



1. D.

(-v) <sup>^</sup> using m as I.F. and G as I.P.

V'<sub>C</sub>

$$\underline{V}'_C = \underline{V}'_G + \underline{\omega}'_m \underline{I} \times \underline{r}_{CG} + 0$$

$$= v'_2 \hat{e}_2 + (\omega'_1 \hat{e}_1 + \omega'_3 \hat{e}_3) \times (\hat{e}_1 - \hat{e}_3) \frac{R}{\sqrt{2}}$$

$$\underline{V}'_C = v'_2 \hat{e}_2 + \omega'_1 \frac{R}{\sqrt{2}} \hat{e}_2 + \omega'_3 \frac{R}{\sqrt{2}} \hat{e}_2$$

$$m (\underline{V}'_C) \cdot \hat{e}_2 = 0 \Rightarrow$$

$$\Rightarrow v'_2 + (\omega'_1 + \omega'_3) \frac{R}{\sqrt{2}} = 0 \quad (ix)$$

Solve (i), vii, viii and (ix)

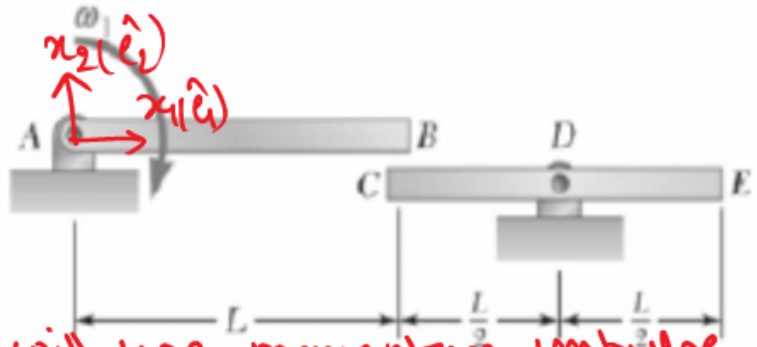
$$\omega'_1 = \frac{2\sqrt{2}}{5} \frac{V_0}{R}, \quad \omega'_2 = 0, \quad \omega'_3 = \frac{2\sqrt{2}}{5} \frac{V_0}{R}$$

$$\underline{\omega}' = \frac{2\sqrt{2}}{5} \frac{V_0}{R} [\hat{e}_1 + \hat{e}_3]$$

Solve &  
Verify.

Example of "2D" problem

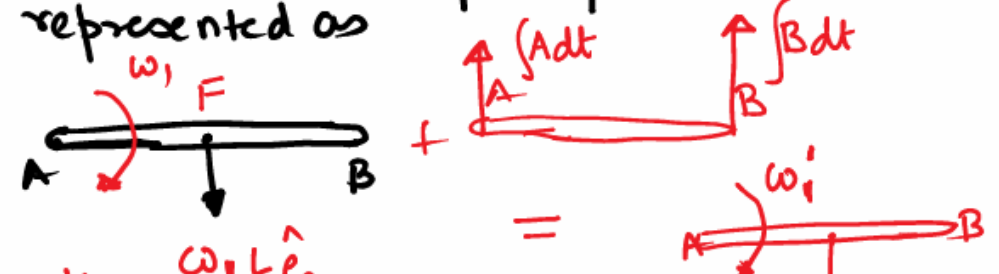
all velocity & angular momentum vectors are w.r.t. frame I (Symbol implied)  
**PROBLEM 17.146**



A slender rod  $CDE$  of length  $L$  and mass  $m$  is attached to a pin support at its midpoint  $D$ . A second and identical rod  $AB$  is rotating about a pin support at  $A$  with an angular velocity  $\omega_1$  when its end  $B$  strikes end  $C$  of rod  $CDE$ . Denoting by  $e$  the coefficient of restitution between the rods, determine the angular velocity of each rod immediately after the impact.

We will use momentum-impulse eqn set for  $AB$  and  $CDE$ .

Rod  $AB$ : the impact process is represented as



Rod  $AB$ :  $\underline{V}_F = -\frac{\omega_1 L}{2} \hat{e}_2$

$$\int \underline{F} \text{ impulsive } dt = m \{ \underline{V}'_F - \underline{V}_F \}$$

w.r.t. ground frame

along  $\hat{e}_1$ :  $0 = m \{ (\underline{V}'_F)_1 - (\underline{V}_F)_1 \}$

w.r.t. ground frame

Symbol implied

Component along  $\hat{e}_1$

0,  $= m(0 - 0)$

along  $\hat{e}_2$ :

$$\int A dt + \int B dt = m \{ (\underline{V}'_F)_2 - (\underline{V}_F)_2 \}$$

$$\int A dt + \int B dt = m \left\{ -\frac{\omega'_1 L}{2} - \left( -\frac{\omega_1 L}{2} \right) \right\}$$

$$\int A dt + \int B dt = \frac{mL}{2} (\omega_1 - \omega'_1) \rightarrow (i)$$

Moment of momentum-impulse about point  $F$

$$\int (\underline{M}_F)_{\text{impulsive}} dt = \left( \underline{H}_F \right)'_3 - \left( \underline{H}_F \right)_3 \quad \text{where}$$

$\underline{H}_F$  represents ang. momentum of  $AB$  about  $F$



$$\text{or } -\int A dt \frac{L}{2} + \frac{L}{2} \int B dt = I_{33}^F \{ -\omega_1' - (-\omega_1) \}$$

(counterclockwise is +ve)

$$\frac{L}{2} \left\{ \int B dt - \int A dt \right\} = \frac{mL^2}{12} (\omega_1 - \omega_1')$$

$$\text{or } \int B dt - \int A dt = \frac{mL}{6} (\omega_1 - \omega_1') \quad \text{(ii)}$$

Add (ii) and (i)

$$2 \int B dt = \frac{mL}{6} (\omega_1 - \omega_1') + \frac{mL}{2} (\omega_1 - \omega_1')$$

$$\int B dt = mL(\omega_1 - \omega_1') \left[ \frac{1}{12} + \frac{1}{4} \right] \rightarrow \text{(iii)}$$

$$\int B dt = \frac{mL}{3} (\omega_1 - \omega_1')$$

We need more eqns to find all the unknowns.

Go to RB(CDE)

Rod CDE.



Angular momentum impulse eqn about point D (center of mass of rod CDE).

$$\int B dt \frac{L}{2} = (H_D')_3 - (H_D)_3$$

Where  $H_D$  is ang. momentum of rod CDE about D (w.r.t. ground)

$$\frac{L}{2} \int B dt = I_{33}^D \omega_2' - I_{33}^D (0)$$

$$\frac{L}{2} \int B dt = \frac{mL^2}{12} \omega_2' \rightarrow \text{(iv)}$$

Sub  $\int B dt$  from (iii)

$$\int B dt = \frac{mL}{3} (\omega_1 - \omega_1') = \frac{mL}{6} \omega_2'$$

$$\text{or } 2\omega_1 - 2\omega_1' = \omega_2' \rightarrow \text{(v)}$$

next, use coeff. of restitution between points B and C.



$$(\underline{V}_C')_n - (\underline{V}_B')_n = e \{ (\underline{V}_B)_n - (\underline{V}_C)_n \}$$

where 'n' means component along  $-\hat{e}_2$

$$\omega_2' \frac{L}{2} - (\omega_1' L) = e \{ \omega_1 L - 0 \}$$

$$\omega_2' - 2\omega_1' = 2e\omega_1$$

$$\omega_2' = 2e\omega_1 + 2\omega_1' \rightarrow (vi)$$

Sub (vi) in (v)

$$2\omega_1 - 2\omega_1' = 2e\omega_1 + 2\omega_1'$$

$$(1-e)\omega_1 = 2\omega_1'$$

$$\text{or } \boxed{\omega_1' = \frac{\omega_1}{2}(1-e)}$$

$$\text{and } \omega_2' = 2e\omega_1 + 2 \cdot \frac{\omega_1}{2}(1-e)$$

$$= 2e\omega_1 + \omega_1 - \omega_1 e.$$

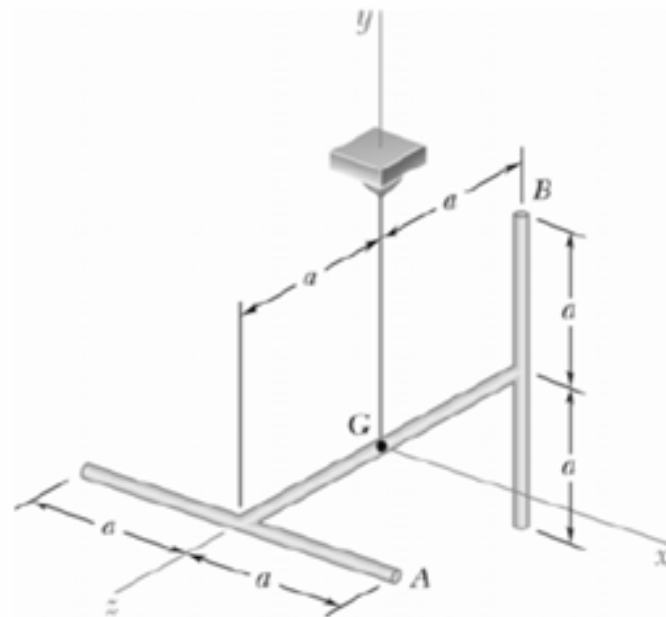
$$\boxed{\omega_2' = \omega_1(1+e)}$$

In vector form:

$$\left. \begin{aligned} \underline{\omega}_{AB|I} &= -\frac{\omega_1}{2}(1-e) \hat{e}_3 \\ \underline{\omega}_{CD|I} &= \omega_1(1+e) \hat{e}_3 \end{aligned} \right\}$$

Answer

## Set 9 B: Problem 18.25

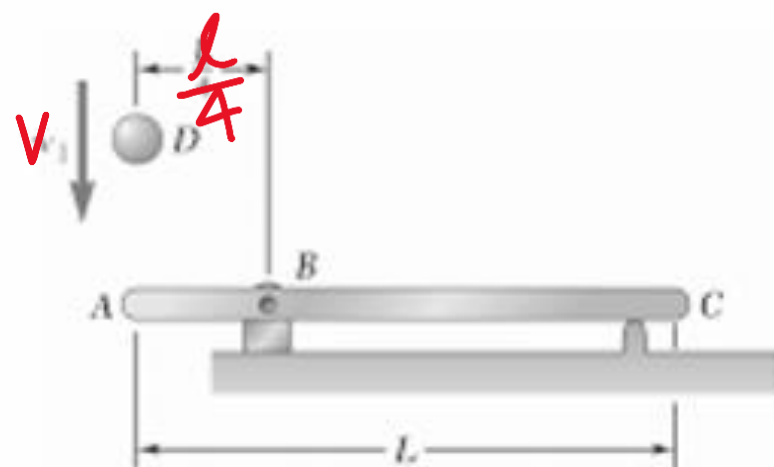


### PROBLEM 18.25

Three slender rods, each of mass  $m$  and length  $2a$ , are welded together to form the assembly shown. The assembly is hit at  $A$  in a vertical downward direction. Denoting the corresponding impulse by  $\mathbf{F} \Delta t$ , determine immediately after the impact ( $a$ ) the velocity of the mass center  $G$ , ( $b$ ) the angular velocity of the rod.

$$\boldsymbol{\omega} = (3F \Delta t / 8ma)(\mathbf{i} - 4\mathbf{k}) \quad \blacktriangleleft$$

$$\bar{\mathbf{v}} = 0 \quad \blacktriangleleft$$

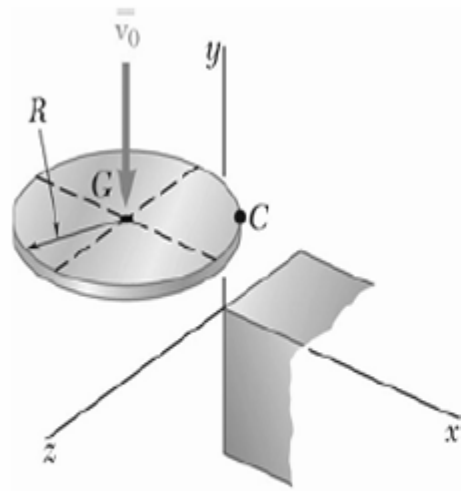


### PROBLEM 17.127

Member  $ABC$  has a mass of 2.4 kg and is attached to a pin support at  $B$ . An 800-g sphere  $D$  strikes the end of member  $ABC$  with a vertical velocity  $v_1$  of 3 m/s. Knowing that  $L = 750$  mm and that the coefficient of restitution between the sphere and member  $ABC$  is 0.5, determine immediately after the impact (a) the angular velocity of member  $ABC$ , (b) the velocity of the sphere.

$$\omega' = 3.00 \text{ rad/s} \curvearrowright \blacktriangleleft$$

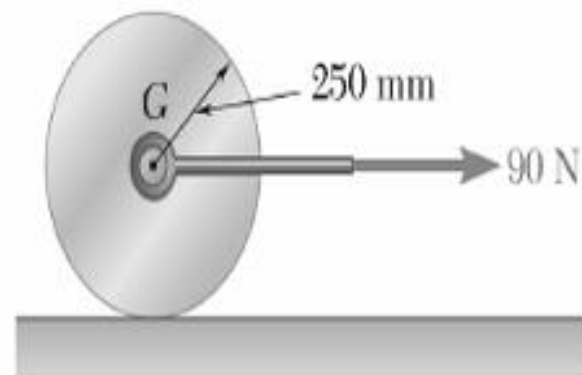
$$v'_D = 0.938 \text{ m/s} \uparrow \blacktriangleleft$$



### PROBLEM 18.51

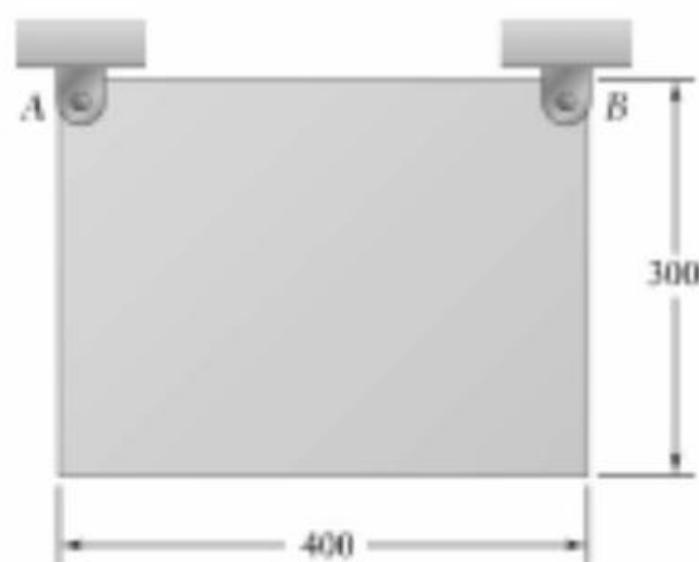
Determine the kinetic energy lost when edge  $C$  of the plate of Problem 18.29 hits the obstruction.

$$T_0 - T = \frac{1}{10} m \bar{v}_0^2 \quad \blacktriangleleft$$



### PROBLEM 17.27

A 20-kg uniform cylindrical roller, initially at rest, is acted upon by a 90-N force as shown. Knowing that the body rolls without slipping, determine (a) the velocity of its center  $G$  after it has moved 1.5 m, (b) the friction force required to prevent slipping.



### PROBLEM 17.137

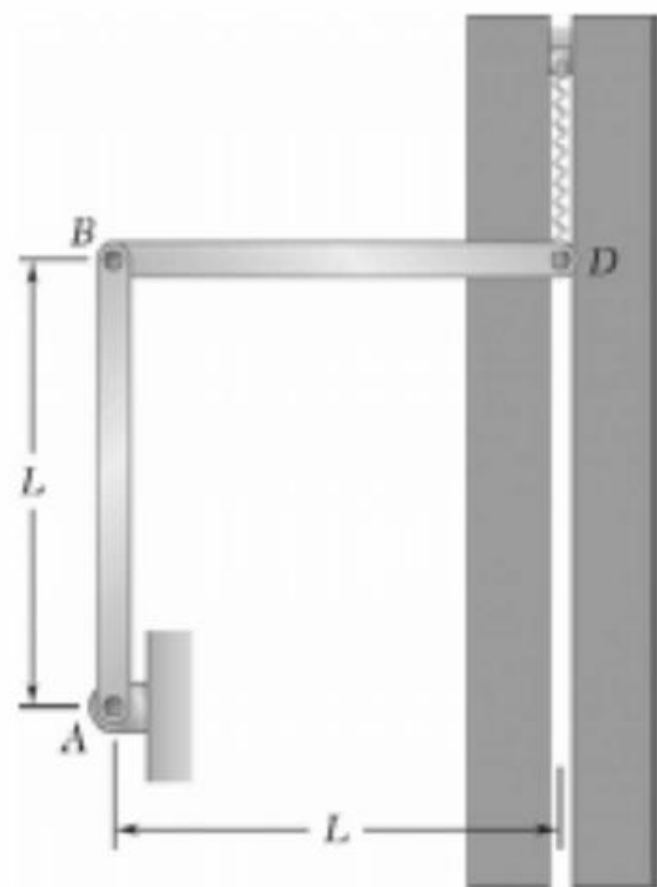
A  $300 \times 400$  mm-rectangular plate is suspended by pins at  $A$  and  $B$ . The pin at  $B$  is removed and the plate swings freely about pin  $A$ . Determine  
(a) the angular velocity of the plate after it has rotated through  $90^\circ$ ,  
(b) the maximum angular velocity attained by the plate as it swings freely.

$$\omega_2 = 3.43 \text{ rad/s} \quad \curvearrowleft$$

$$\omega_3 = 4.85 \text{ rad/s} \quad \curvearrowleft$$

### PROBLEM 17.42

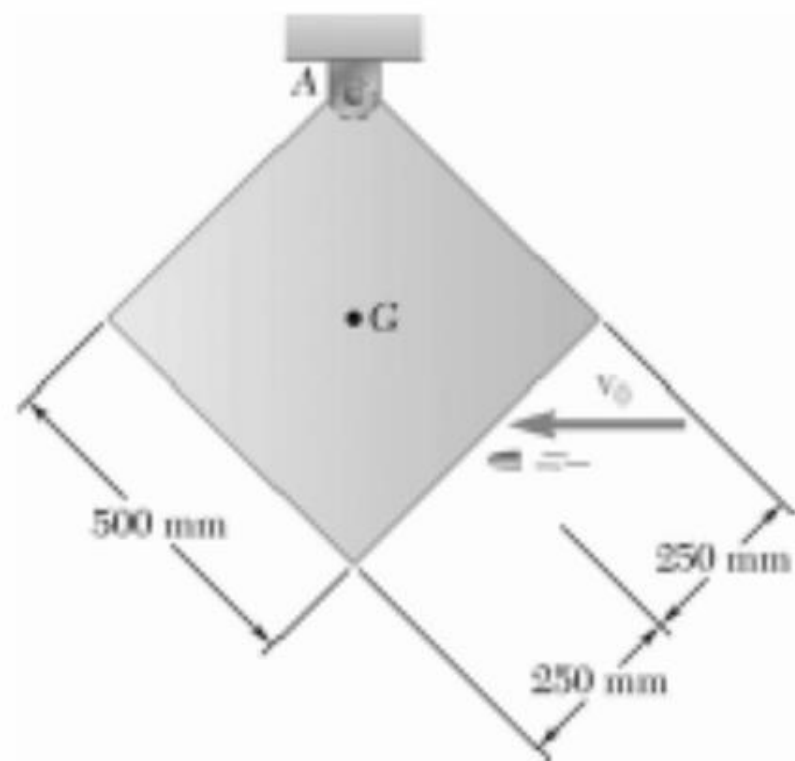
Each of the two rods shown is of length  $L = 1$  m and has a mass of 5 kg. Point  $D$  is connected to a spring of constant  $k = 20$  N/m and is constrained to move along a vertical slot. Knowing that the system is released from rest when rod  $BD$  is horizontal and the spring connected to Point  $D$  is initially unstretched, determine the velocity of Point  $D$  when it is directly to the right of Point  $A$ .



$$v_D = 2.69 \text{ m/s} \downarrow \blacktriangleleft$$

### PROBLEM 17.141

A 35-g bullet  $B$  is fired horizontally with a velocity of 400 m/s into the side of a 3-kg square panel suspended from a pin at  $A$ . Knowing that the panel is initially at rest, determine the components of the reaction at  $A$  after the panel has rotated  $45^\circ$ .



$$A_x = 189.7 \text{ N} \rightarrow \blacktriangleleft$$

$$A_y = 7.36 \text{ N} \uparrow \blacktriangleleft$$