

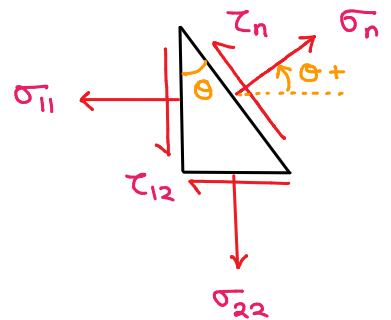
# Plane Stress Transformation

$\theta \rightarrow +ve$  (counter-clockwise)



The normal stress on the  $\underline{n}$ -plane is

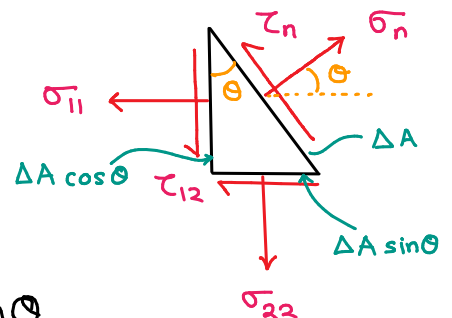
$$\begin{aligned}\sigma_n &= \sigma_{11} n_1^2 + \sigma_{22} n_2^2 + 2\tau_{12} n_1 n_2 \\ &= \sigma_{11} \cos^2 \theta + \sigma_{22} \sin^2 \theta + 2\tau_{12} \cos \theta \sin \theta \\ &= \sigma_{11} \frac{(1 + \cos 2\theta)}{2} + \sigma_{22} \frac{(1 - \cos 2\theta)}{2} + \tau_{12} \sin 2\theta \\ &= \frac{\sigma_{11} + \sigma_{22}}{2} + \frac{\sigma_{11} - \sigma_{22}}{2} \cos 2\theta + \tau_{12} \sin 2\theta\end{aligned}$$



The above form can also be arrived at by doing force equilibrium of the wedge in the  $\underline{n}$ -direction

$$\uparrow + \sum F_n = 0$$

$$\begin{aligned}\Rightarrow & \sigma_n \Delta A - (\tau_{12} \Delta A \sin \theta) \cos \theta \\ & - (\sigma_{22} \Delta A \sin \theta) \sin \theta - (\tau_{12} \Delta A \cos \theta) \sin \theta \\ & - (\sigma_{11} \Delta A \cos \theta) \cos \theta = 0\end{aligned}$$



$$\begin{aligned}\Rightarrow & \sigma_n = \sigma_{11} \cos^2 \theta + \sigma_{22} \sin^2 \theta + 2\tau_{12} \sin \theta \cos \theta \\ & = \frac{\sigma_{11} + \sigma_{22}}{2} + \frac{\sigma_{11} - \sigma_{22}}{2} \cos 2\theta + \tau_{12} \sin 2\theta\end{aligned}$$

The shear stress on the  $\eta$ -plane can be obtained from the geometry conveniently by doing force equilibrium of the wedge in the direction perpendicular to  $\eta$

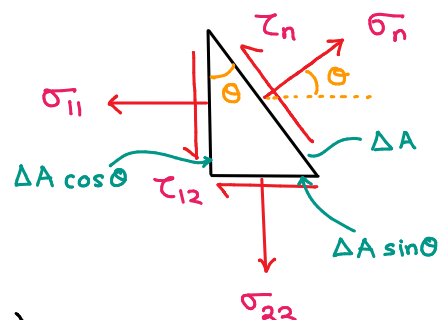
$$\uparrow \sum F_{n\perp} = 0$$

$$\Rightarrow \tau_n \Delta A + (\tau_{12} \Delta A \sin \theta) \sin \theta - (\sigma_{22} \Delta A \sin \theta) \cos \theta$$

$$+ (\sigma_{11} \Delta A \cos \theta) \sin \theta - (\tau_{12} \Delta A \cos \theta) \cos \theta = 0$$

$$\Rightarrow \tau_n = (\sigma_{22} - \sigma_{11}) \sin \theta \cos \theta + \tau_{12} (\cos^2 \theta - \sin^2 \theta)$$

$$\Rightarrow \tau_n = - \frac{(\sigma_{11} - \sigma_{22})}{2} \sin 2\theta + \tau_{12} \cos 2\theta$$



So we get two relations for  $\sigma_n$  and  $\tau_n$  in plane stress

$$\sigma_n = \frac{\sigma_{11} + \sigma_{22}}{2} + \frac{\sigma_{11} - \sigma_{22}}{2} \cos 2\theta + \tau_{12} \sin 2\theta$$

$$\tau_n = - \frac{\sigma_{11} - \sigma_{22}}{2} \sin 2\theta + \tau_{12} \cos 2\theta$$

### Maximum/Minimum normal stress planes

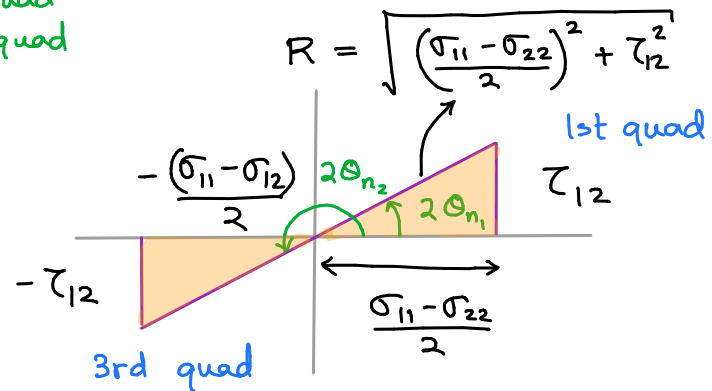
To determine the orientation that causes the normal stress to be maximum/minimum, we can take a derivative of  $\sigma_n$  w.r.t to plane inclination  $\theta$

$$\frac{d\sigma_n}{d\theta} = - \frac{\sigma_{11} - \sigma_{22}}{2} (2 \sin 2\theta) + 2\tau_{12} \cos 2\theta = 0$$

Solving the above equation, we obtain the orientation  $\Theta = \Theta_n$  of the planes of maximum and minimum normal stress

Assume  $\sigma_{11} > \sigma_{22}$ ,  $\tan \phi \rightarrow +ve$   $\begin{cases} \text{1st quad} \\ \text{3rd quad} \end{cases}$

$$\tan 2\Theta_n = \frac{\tau_{12}}{\left(\frac{\sigma_{11} - \sigma_{22}}{2}\right)}$$



The solution has two roots  $\Theta_{n_1}$  and  $\Theta_{n_2}$ . Specifically, the values of  $2\Theta_{n_1}$  and  $2\Theta_{n_2}$  are  $180^\circ$  apart, so in reality  $\Theta_{n_1}$  and  $\Theta_{n_2}$  planes will be  $90^\circ$  apart.

To obtain maximum and minimum normal stress, we must substitute the angles  $\Theta_{n_1}$  and  $\Theta_{n_2}$ .

$$\begin{aligned} \sigma_{n_1, n_2} &= \frac{\sigma_{11} + \sigma_{22}}{2} \pm \frac{\sigma_{11} - \sigma_{22}}{2} \cos 2\Theta_{n_1} \pm \tau_{12} \sin 2\Theta_{n_1} \\ &= \frac{\sigma_{11} + \sigma_{22}}{2} \pm \frac{\sigma_{11} - \sigma_{22}}{2} \left( \frac{\sigma_{11} - \sigma_{22}}{2R} \right) \pm \tau_{12} \left( \frac{\tau_{12}}{R} \right) \\ &= \frac{\sigma_{11} + \sigma_{22}}{2} \pm \frac{(\sigma_{11} - \sigma_{22})^2}{4R} \pm \frac{\tau_{12}^2}{R} \\ &= \frac{\sigma_{11} + \sigma_{22}}{2} \pm \frac{1}{R} \left[ \underbrace{\left( \frac{\sigma_{11} - \sigma_{22}}{2} \right)^2 + \tau_{12}^2}_{R^2} \right] \\ &= \frac{\sigma_{11} + \sigma_{22}}{2} \pm \sqrt{\left( \frac{\sigma_{11} - \sigma_{22}}{2} \right)^2 + \tau_{12}^2} \end{aligned}$$

This result gives the maximum and minimum normal stress acting at a point and the angles  $\Theta_{n_1}$ ,  $\Theta_{n_2}$  are the directions

$$\sigma_{\max} \big|_{\text{plane normal } \underline{n}_1} = \frac{\sigma_{11} + \sigma_{22}}{2} + \sqrt{\left(\frac{\sigma_{11} - \sigma_{22}}{2}\right)^2 + \tau_{12}^2}$$

$$\sigma_{\min} \big|_{\text{plane normal } \underline{n}_2} = \frac{\sigma_{11} + \sigma_{22}}{2} - \sqrt{\left(\frac{\sigma_{11} - \sigma_{22}}{2}\right)^2 + \tau_{12}^2}$$

Lets us also check what are the shear stresses on planes where normal stress components are maximum or minimum

For this, we can put value of  $\sin 2\theta_p$  and  $\cos 2\theta_p$  in the relation for shear stress component  $\tau_n$ :

$$\begin{aligned} \tau_n &= - \frac{\sigma_{11} - \sigma_{22}}{2} \sin 2\theta_p + \tau_{12} \cos 2\theta_p \\ &= - \frac{\sigma_{11} - \sigma_{22}}{2} \left( \frac{\tau_{12}}{R} \right) + \tau_{12} \left( \frac{\sigma_{11} - \sigma_{22}}{2R} \right) \\ &= 0 \end{aligned}$$

We find that the shear stress components are zero on planes where normal stress components are maximized or minimized. Coincidentally, principal planes are also planes where there are only normal stress components and no shear stresses. Thus, principal planes are also planes where the normal stresses are max/min and shear stresses are zero

## Maximum Shear Stress and corresponding plane

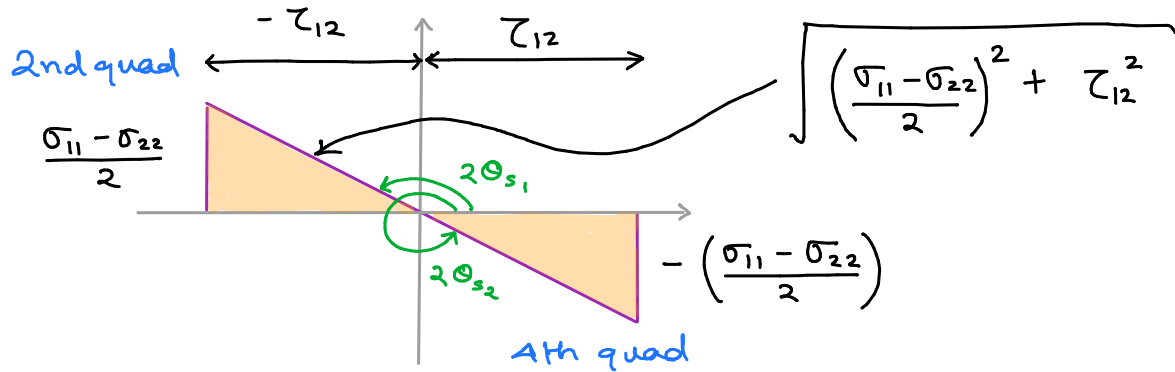
$$\tau_n = - \frac{\sigma_{11} - \sigma_{22}}{2} \sin 2\theta + \tau_{12} \cos 2\theta$$

To find the maximum or minimum value of  $\tau_n$  w.r.t  $\theta$ , set

$$\frac{\partial \tau_n}{\partial \theta} = 0 \Rightarrow \tan 2\theta_s = - \frac{(\sigma_{11} - \sigma_{22})}{2 \tau_{12}}$$

Without loss of generality, assume  $\sigma_{11} > \sigma_{22}$

$\tan \phi$  is -ve in 2nd and 4th quadrant, therefore  $2\theta_s$  must belong to either the 2nd or 4th quadrant.



There are two planes  $\theta_{s1}$  and  $\theta_{s2}$ , where  $\tan 2\theta_s$  is -ve. By comparison,  $\tan 2\theta_s$  is the negative reciprocal of  $\tan 2\theta_n$ , so each plane  $2\theta_s$  must be  $90^\circ$  from  $2\theta_n$ , and in reality

the principal planes and the planes of maximum shear occur at angles of  $45^\circ$  to each other

The maximum value of shear stress is obtained by putting the values of  $\theta_s$  in the relation of  $\tau_n$

$$\tau_{n,\max} = \sqrt{\left(\frac{\sigma_{11} - \sigma_{22}}{2}\right)^2 + \tau_{12}^2}$$