

1) Think of  $(\underline{e}_1 - \underline{e}_2 - \underline{e}_3)$  and  $(\hat{\underline{e}}_1 - \hat{\underline{e}}_2 - \hat{\underline{e}}_3)$  are two coordinate sys.

$$\underline{e}_j = \sum_i (\underline{e}_j \cdot \hat{\underline{e}}_i) \hat{\underline{e}}_i$$

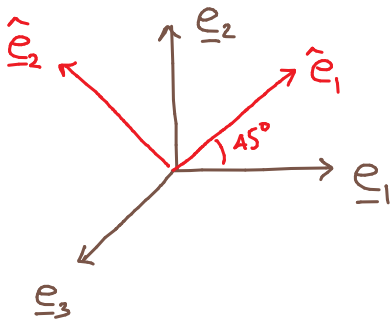
$$\begin{aligned} \underline{T}^n &= \underline{T}^{\hat{1}} \hat{n}_1 + \underline{T}^{\hat{2}} \hat{n}_2 + \underline{T}^{\hat{3}} \hat{n}_3 \\ &= \underline{T}^{\hat{1}} (\underline{n} \cdot \hat{\underline{e}}_1) + \underline{T}^{\hat{2}} (\underline{n} \cdot \hat{\underline{e}}_2) + \underline{T}^{\hat{3}} (\underline{n} \cdot \hat{\underline{e}}_3) \\ &= \sum_{i=1}^3 \underline{T}^{\hat{i}} (\underline{n} \cdot \hat{\underline{e}}_i) \end{aligned}$$

Lets express  $\underline{T}^{\hat{i}}$  in terms of traction on planes  $(\underline{e}_1 - \underline{e}_2 - \underline{e}_3)$

$$\underline{T}^{\hat{i}} = \sum_{j=1}^3 T^j (\hat{\underline{e}}_i \cdot \underline{e}_j)$$

$$\begin{aligned} \underline{T}^n &= \sum_{i=1}^3 \left( \sum_{j=1}^3 T^j (\hat{\underline{e}}_i \cdot \underline{e}_j) \right) (\underline{n} \cdot \hat{\underline{e}}_i) \\ &= \sum_{j=1}^3 T^j \underline{n} \cdot \left( \sum_{i=1}^3 (\underline{e}_j \cdot \hat{\underline{e}}_i) \hat{\underline{e}}_i \right) \\ &= \sum_{j=1}^3 T^j (\underline{n} \cdot \underline{e}_j) \end{aligned}$$

$$2) \quad [\underline{T}^1]_{e_i} = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}, \quad [\underline{T}^2]_{e_i} = \begin{bmatrix} 1 \\ 5 \\ 7 \end{bmatrix}, \quad [\underline{T}^3]_{e_i} = \begin{bmatrix} 0 \\ 7 \\ 9 \end{bmatrix}$$



$$[\hat{e}_1]_{e_i} = \begin{bmatrix} 1/\sqrt{2} \\ 1/\sqrt{2} \\ 0 \end{bmatrix}$$

$$\underline{T}^{\hat{1}} = \sum_{i=1}^3 \underline{T}^i (\hat{e}_1 \cdot \underline{e}_i)$$

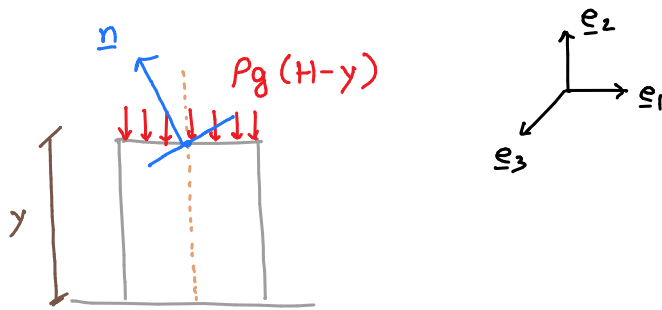
$$\begin{aligned} [\underline{T}^{\hat{1}}]_{e_i} &= \sum_{i=1}^3 [\underline{T}^i]_{e_i} ([\hat{e}_1]_{e_i} \cdot [\underline{e}_i]_{e_i}) \\ &= \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} \frac{1}{\sqrt{2}} + \begin{bmatrix} 1 \\ 5 \\ 7 \end{bmatrix} \frac{1}{\sqrt{2}} + \begin{bmatrix} 0 \\ 7 \\ 9 \end{bmatrix} 0 \\ &= \frac{1}{\sqrt{2}} \begin{bmatrix} 1 \\ 6 \\ 7 \end{bmatrix} \end{aligned}$$

$$\text{Normal component of traction} = \underline{T}^{\hat{1}} \cdot \hat{e}_1$$

$$\text{Shear component of traction} = \underline{T}^{\hat{1}} - (\underline{T}^{\hat{1}} \cdot \hat{e}_1) \cdot \hat{e}_1$$

$$\begin{aligned} 3) \quad \underline{T}^n \cdot \underline{m} &= [\underline{m}]^T [\underline{T}^n] \\ &= [\underline{m}]^T [\underline{\sigma}] [\underline{n}] \\ &= [\underline{n}]^T [\underline{\sigma}] [\underline{m}] \\ &= [\underline{n}]^T [\underline{T}^m] \\ &= \underline{T}^m \cdot \underline{n} \end{aligned}$$

4)



$$\underline{I}^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \underline{I}^2 = \begin{bmatrix} 0 \\ -\rho g(H-y) \\ 0 \end{bmatrix}, \quad \underline{I}^3 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$[\underline{I}^n] = \sum_{i=1}^3 [\underline{I}^i] ([\underline{n}] \cdot [\underline{e}_i])$$

$$= \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} (-\sin \Theta) + \begin{bmatrix} 0 \\ -\rho g(H-y) \\ 0 \end{bmatrix} (\cos \Theta) + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} (1)$$

$$= \begin{bmatrix} 0 \\ -\rho g(H-y) \cos \Theta \\ 0 \end{bmatrix}$$

Normal component of traction

$$\sigma_n = \underline{I}^n \cdot \underline{n} = -\rho g(H-y) \cos \Theta \underline{e}_2 \cdot \underline{n}$$

Shear component of traction

$$\begin{aligned} \tau_n &= \underline{I}^n \cdot \underline{n}^\perp = -\rho g(H-y) \cos \Theta \underline{e}_2 \cdot \underline{n}^\perp \\ &= -\rho g(H-y) \cos \Theta \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}^T \begin{bmatrix} \cos \Theta \\ \sin \Theta \\ 1 \end{bmatrix} \\ &= -\rho g(H-y) \cos \Theta \sin \Theta \end{aligned}$$

unit vector  
perpendicular to  
 $\underline{n}$   
lying  
in plane  
section

5) We want  $\underline{T}^n = \underline{\sigma} \underline{n} = \underline{0}$  for some  $\underline{n}$

$$[\underline{\sigma}] [\underline{n}] = \underline{0}$$

It implies  $[\underline{\sigma}]$  is rank-deficient  $\Leftrightarrow \det([\underline{\sigma}]) = 0$

$$\Rightarrow \det([\underline{\sigma}]) = \begin{vmatrix} \sigma_{11} & -4 \\ 2 & -2 \end{vmatrix} - \begin{vmatrix} 2 & -2 \\ 1 & 4 \end{vmatrix} + \begin{vmatrix} 1 & 4 \\ 1 & 4 \end{vmatrix} = 0$$

$$\Rightarrow -4\sigma_{11} + 4 + 4 = 0 \Rightarrow \sigma_{11} = 2$$

Now, use the relation:

$$\underline{T}^n = \underline{\sigma} \underline{n}$$

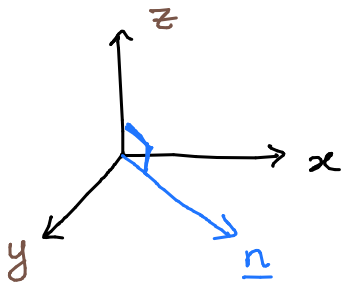
$$\Rightarrow \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} \overset{2}{\cancel{\sigma_{11}}} & 2 & 1 \\ 2 & 0 & 2 \\ 1 & 2 & 0 \end{bmatrix} \begin{bmatrix} n_1 \\ n_2 \\ n_3 \end{bmatrix}$$

$$\Rightarrow \left. \begin{array}{l} 2n_1 + 2n_2 + n_3 = 0 \\ 2n_1 + \quad \quad \quad 2n_3 = 0 \\ n_1 + 2n_2 \quad \quad = 0 \end{array} \right\} \begin{array}{l} \text{Solve these} \\ \text{to get } \underline{n} \end{array}$$

In addition, use  $n_1^2 + n_2^2 + n_3^2 = 1$  to get

$$\underline{n} = \begin{bmatrix} \pm 2/3 \\ \pm 1/3 \\ \pm 2/3 \end{bmatrix}$$

6) We have to find  $[\underline{n}] = \begin{bmatrix} n_x \\ n_y \\ 0 \end{bmatrix}$   $n_z = 0$  since  $\underline{n} \perp \underline{z}$



$$\underline{I}^n \cdot \underline{n} = 0 \quad (\text{normal component is zero})$$

$$\Rightarrow (\underline{\sigma} \underline{n}) \cdot \underline{n} = 0$$

$$\Rightarrow [\underline{n}]^T [\underline{\sigma}] [\underline{n}] = 0$$

$$\Rightarrow [n_x \ n_y \ 0] \begin{bmatrix} a & 0 & d \\ 0 & b & e \\ d & e & c \end{bmatrix} \begin{bmatrix} n_x \\ n_y \\ 0 \end{bmatrix} = 0$$

$$\Rightarrow a n_x^2 + b n_y^2 = 0 \quad \text{--- (1)}$$

Also,  $\underline{n}$  being an unit normal,

$$n_x^2 + n_y^2 + n_z^2 = 1$$

$$\Rightarrow n_x^2 + n_y^2 = 1$$

$$\Rightarrow n_y^2 = 1 - n_x^2 \quad \text{--- (2)}$$

$$a n_x^2 + b (1 - n_x^2) = 0$$

$$\Rightarrow n_x = \pm \left( \frac{b}{b-a} \right)^{1/2}, \quad n_y = \pm \left( \frac{a}{a-b} \right)^{1/2}$$

$$n_z = 0$$

7)

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} + \gamma_x = 0 \quad \text{--- (1)}$$

$$\frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \tau_{zy}}{\partial z} + \gamma_y = 0 \quad \text{--- (2)}$$

$$\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} + \gamma_z = 0 \quad \text{--- (3)}$$

$$\underbrace{\gamma_x = 0, \gamma_z = 0}_{\text{no self-weight in } x \text{ or } z \text{ directions}}, \quad \gamma_y = \rho \quad \leftarrow \begin{array}{l} \text{specific weight} \\ \text{(not density)} \end{array}$$

Stress equilibrium equations are automatically satisfied for (1) & (3). For eqn (2)

$$\left( \frac{\gamma}{\tan^2 \beta} - \rho \right) - \frac{\gamma}{\tan^2 \beta} + \rho = 0 \quad (\text{satisfied})$$

Let's verify the traction boundary condition on face OB

Traction on face OB

$$\underline{T}^{-1} \big|_{(x=0, y, z)} = \underline{\sigma} \cdot (-\underline{e}_1)$$

$$= - \begin{bmatrix} \sigma_{xx} & \tau_{xy} & \tau_{xz} \\ \tau_{xy} & \sigma_{yy} & \tau_{yz} \\ \tau_{xz} & \tau_{yz} & \sigma_{zz} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$$

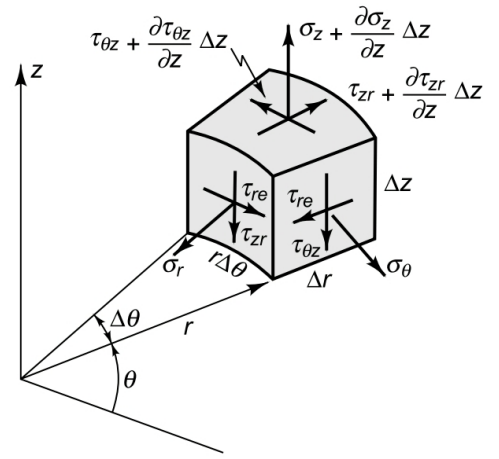
$$= - \begin{bmatrix} \sigma_{xx} \\ \tau_{xy} \\ \tau_{xz} \end{bmatrix}_{x=0, y, z} = - \begin{bmatrix} -\gamma_y \\ -\frac{\gamma}{\tan^2 \beta} x \\ 0 \end{bmatrix} = \begin{bmatrix} \gamma_y \\ 0 \\ 0 \end{bmatrix}$$

External load on OB

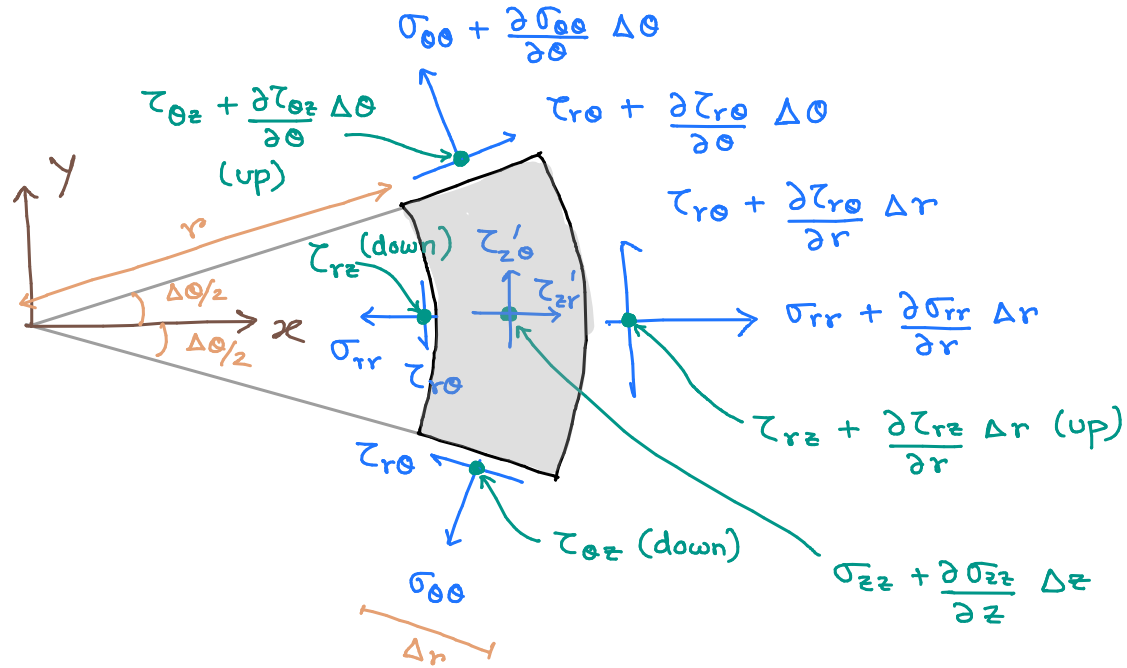
$$\underline{f}^{\text{ext}} \big|_{\text{face OB}} = \gamma_y \underline{e}_1 = \begin{bmatrix} \gamma_y \\ 0 \\ 0 \end{bmatrix}$$

$\swarrow$   
matching

8) The elementary volume has three pairs of faces in the  $r$ ,  $\theta$  and  $z$  directions



Thickness =  $\Delta z$



$$\rightarrow \sum F_x = 0$$

$$\Rightarrow \left[ \left( \sigma_{rr} + \frac{\partial \sigma_{rr}}{\partial r} \Delta r \right) \underbrace{(r + \Delta r) \Delta \theta \Delta z}_{\text{area}} - (\sigma_{rr}) (r \Delta \theta \Delta z) \right]$$

$$+ \left( \tau_{r\theta} + \frac{\partial \tau_{r\theta}}{\partial r} \Delta r \right) \Delta r \Delta z \cos \left( \frac{\Delta \theta}{2} \right) - \tau_{r\theta} \Delta r \Delta z \cos \left( \frac{\Delta \theta}{2} \right)$$

$$- 2 \left( \sigma_{\theta\theta} + \frac{\partial \sigma_{\theta\theta}}{\partial \theta} \Delta \theta \right) \Delta r \Delta z \sin \left( \frac{\Delta \theta}{2} \right) - 2 \sigma_{\theta\theta} \Delta r \Delta z \sin \left( \frac{\Delta \theta}{2} \right)$$

$$+ \left( \tau_{zr} + \frac{\partial \tau_{zr}}{\partial z} \Delta z \right) r \Delta \theta \Delta r - \tau_{zr} r \Delta \theta \Delta r ]$$

$$= 0$$

Area of the shaded region =  $\frac{1}{2} (r \Delta \theta + (r + \Delta r) \Delta \theta) \Delta r = \frac{1}{2} (2r + \Delta r) \Delta \theta \Delta r$   
 $\approx r \Delta \theta \Delta r$  (ignoring  $(\Delta r)^2$ )

$$\rightarrow \Sigma F_x = 0$$

$$\cos\left(\frac{\Delta\theta}{2}\right) \approx 1$$

$$\sin\left(\frac{\Delta\theta}{2}\right) \approx \frac{\Delta\theta}{2}$$

$$\begin{aligned} \Rightarrow & \left[ \left( \sigma_{rr} + \frac{\partial \sigma_{rr}}{\partial r} \Delta r \right) \underbrace{(\cancel{r} + \Delta r) \Delta\theta \Delta z}_{\text{area}} - (\sigma_{rr}) (\cancel{r} \Delta\theta \Delta z) \right. \\ & + \left( \cancel{\tau_{r\theta}} + \frac{\partial \tau_{r\theta}}{\partial r} \Delta r \right) \Delta r \Delta z \cos\left(\frac{\Delta\theta}{2}\right) - \cancel{\tau_{r\theta} \Delta r \Delta z \cos\left(\frac{\Delta\theta}{2}\right)} \\ & - 2 \left( \sigma_{\theta\theta} + \frac{\partial \sigma_{\theta\theta}}{\partial \theta} \Delta\theta \right) \Delta r \Delta z \sin\left(\frac{\Delta\theta}{2}\right) - 2 \sigma_{\theta\theta} \Delta r \Delta z \sin\left(\frac{\Delta\theta}{2}\right) \\ & \left. + \left( \cancel{\tau_{zr}} + \frac{\partial \tau_{zr}}{\partial z} \Delta z \right) \cancel{r \Delta\theta \Delta r} - \cancel{\tau_{zr} r \Delta\theta \Delta r} \right] = 0 \end{aligned}$$

$$\begin{aligned} \Rightarrow & \sigma_{rr} \Delta r \Delta\theta \Delta z + r \frac{\partial \sigma_{rr}}{\partial r} \Delta r \Delta\theta \Delta z + \frac{\partial \sigma_{rr}}{\partial r} (\Delta r)^2 \Delta\theta \Delta z \\ & + \frac{\partial \tau_{r\theta}}{\partial r} \Delta r \Delta\theta \Delta z - \sigma_{\theta\theta} \Delta r \Delta\theta \Delta z - \frac{\partial \sigma_{\theta\theta}}{\partial \theta} \Delta r (\Delta\theta)^2 \Delta z \\ & + r \frac{\partial \tau_{zr}}{\partial z} \Delta r \Delta\theta \Delta z = 0 \end{aligned}$$

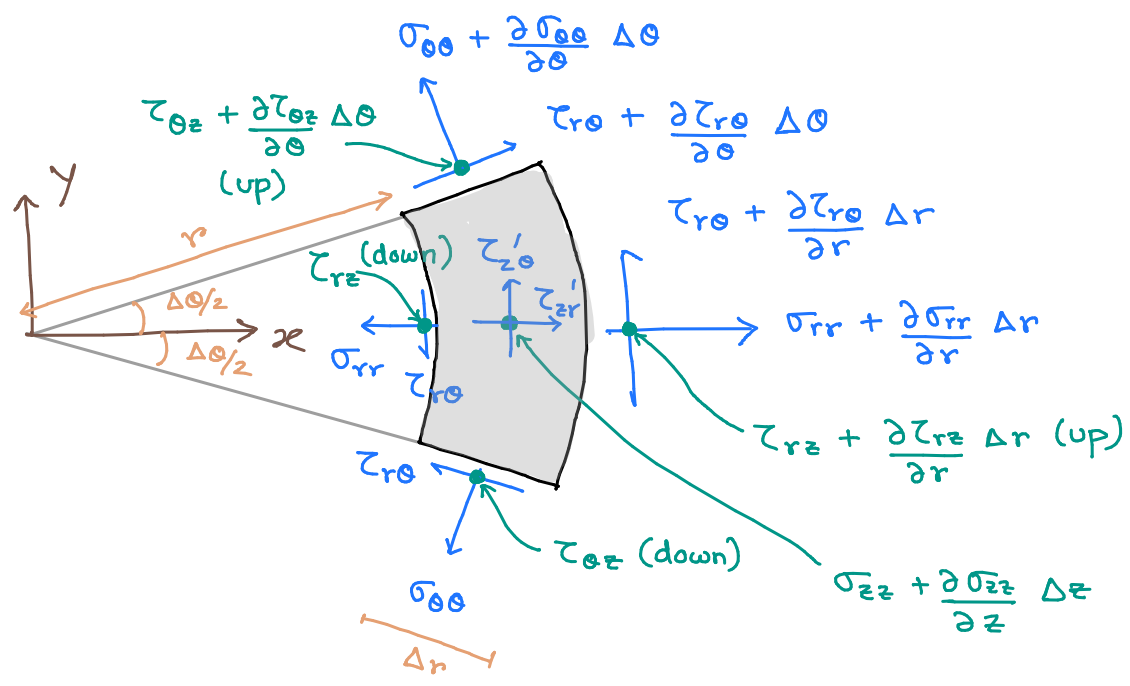
like  $(\Delta r)^2$ ,  $(\Delta\theta)^2$

Neglecting the higher order terms, and dividing by  $r \Delta r \Delta\theta \Delta z$

$$\Rightarrow \frac{\partial \sigma_{rr}}{\partial r} + \frac{1}{r} \frac{\partial \tau_{r\theta}}{\partial r} + \frac{\partial \tau_{zr}}{\partial z} + \frac{\sigma_{rr} - \sigma_{\theta\theta}}{r} = 0$$



Thickness =  $\Delta z$



$\uparrow \sum F_y = 0$

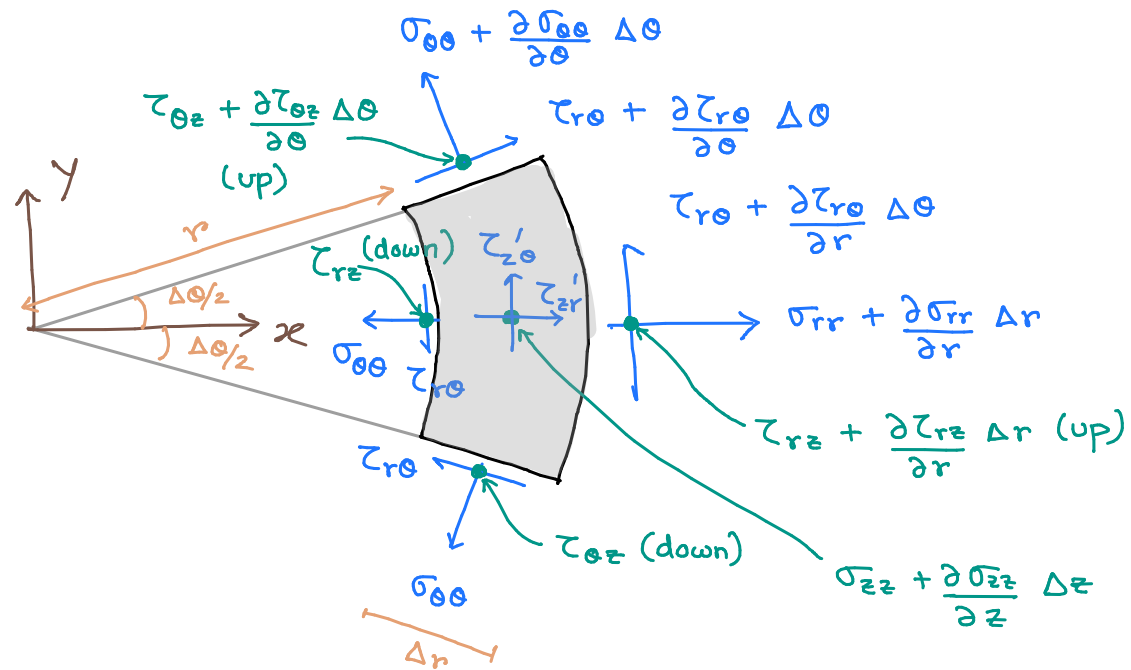
$$\Rightarrow \left[ \left( \cancel{\sigma_{\theta\theta}} + \frac{\partial \sigma_{\theta\theta}}{\partial \theta} \Delta \theta \right) \cancel{\cos\left(\frac{\Delta \theta}{2}\right)} \Delta r \Delta z - \cancel{\sigma_{\theta\theta} \cos\left(\frac{\Delta \theta}{2}\right)} \Delta r \Delta z \right. \\ + \left( \tau_{r\theta} + \frac{\partial \tau_{r\theta}}{\partial \theta} \Delta \theta \right) \cancel{\sin\left(\frac{\Delta \theta}{2}\right)} \Delta r \Delta z + \tau_{r\theta} \cancel{\sin\left(\frac{\Delta \theta}{2}\right)} \Delta r \Delta z \\ + \left( \tau_{r\theta} + \frac{\partial \tau_{r\theta}}{\partial r} \Delta r \right) (r + \Delta r) \Delta \theta \Delta z - \tau_{r\theta} r \Delta \theta \Delta z \\ \left. + \left( \tau_{\theta z} + \frac{\partial \tau_{\theta z}}{\partial z} \Delta z \right) r \Delta r \Delta \theta - \tau_{\theta z} r \Delta r \Delta \theta \right] = 0$$

$$\Rightarrow \frac{\partial \sigma_{\theta\theta}}{\partial \theta} \Delta r \Delta \theta \Delta z + r \frac{\partial \tau_{r\theta}}{\partial r} \Delta r \Delta \theta \Delta z + \\ + \tau_{r\theta} \Delta r \Delta \theta \Delta z + r \frac{\partial \tau_{r\theta}}{\partial r} \Delta r \Delta \theta \Delta z + \frac{\partial \tau_{r\theta}}{\partial \theta} \Delta r \left(\frac{\Delta \theta}{2}\right)^2 \Delta z \\ + \tau_{r\theta} \Delta r \Delta \theta \Delta z + r \frac{\partial \tau_{\theta z}}{\partial z} \Delta r \Delta \theta \Delta z + \frac{\partial \tau_{r\theta}}{\partial r} (\Delta r)^2 \Delta \theta \Delta z \\ + \frac{\partial \tau_{\theta z}}{\partial z} r \Delta r \Delta \theta \Delta z = 0$$

Dividing by  $r \Delta r \Delta \theta \Delta z$

$$\Rightarrow \frac{\partial \tau_{r\theta}}{\partial r} + \frac{1}{r} \frac{\partial \sigma_{\theta\theta}}{\partial \theta} + \frac{\partial \tau_{\theta z}}{\partial z} + \frac{\partial \tau_{r\theta}}{\partial \theta} = 0$$

Thickness =  $\Delta z$



$$\sum F_z = 0$$

$$\Rightarrow \left[ \left( \cancel{\sigma_{zz}} + \frac{\partial \sigma_{zz}}{\partial z} \Delta z \right) r \Delta r \Delta \theta - \cancel{\sigma_{zz}} r \Delta r \Delta \theta \right] + \left( \cancel{\tau_{\theta z}} + \frac{\partial \tau_{\theta z}}{\partial \theta} \Delta \theta \right) \Delta r \Delta z - \cancel{\tau_{\theta z}} \Delta r \Delta z + \left( \tau_{rz} + \frac{\partial \tau_{rz}}{\partial r} \Delta r \right) (r + \Delta r) \Delta \theta \Delta z - \cancel{\tau_{rz}} r \Delta \theta \Delta z$$

$$\Rightarrow r \frac{\partial \sigma_{zz}}{\partial z} \Delta r \Delta \theta \Delta z + \frac{\partial \tau_{\theta z}}{\partial \theta} \Delta r \Delta \theta \Delta z + \tau_{zr} \Delta r \Delta \theta \Delta z$$

$$+ r \frac{\partial \tau_{rz}}{\partial r} \Delta r \Delta \theta \Delta z + \frac{\partial \tau_{rz}}{\partial r} (\Delta r)^2 \Delta \theta \Delta z = 0$$

Dividing by  $r \Delta r \Delta \theta \Delta z$

$$\Rightarrow \boxed{\frac{\partial \tau_{rz}}{\partial r} + \frac{1}{r} \frac{\partial \tau_{\theta z}}{\partial \theta} + \frac{\partial \sigma_{zz}}{\partial z} + \frac{\tau_{zr}}{r} = 0}$$