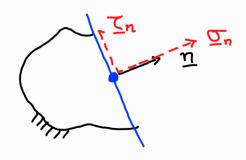


decompose In into normal & shear components



From failure considerations of materials, it is of interest to know the following:

- (a) If there are any planes passing through a given point on which traction vector is wholly normal?

 (i.e. traction vector has zero shear component & non-zero normal component)
- (b) On which plane does the normal stress become maximum? Lohat will be its magnitude?
- (c) On which plane does the shear stress become maximum? What will be its magnitude?

Consider a plane with normal n s.t. the traction vector is oriented along the normal vector

$$\frac{e_2}{n}$$

$$\left[\underline{T}^{n}\right] = \lambda \left[\underline{n}\right] - 0$$

$$\begin{bmatrix} I_n \end{bmatrix} = \begin{bmatrix} \overline{0} \end{bmatrix} \begin{bmatrix} \overline{1} \end{bmatrix} - \underline{0}$$

$$\Rightarrow \left[\overline{c} - y \overline{\mp} \right] \left[\overline{n} \right] = \overline{c}$$

$$\Rightarrow \begin{bmatrix} \sigma_{11} - \lambda & C_{21} & C_{31} \\ C_{21} & \sigma_{22} - \lambda & C_{32} \\ C_{31} & C_{32} & \sigma_{33} - \lambda \end{bmatrix} \begin{bmatrix} \eta_1 \\ \eta_2 \\ \eta_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

A brivial solu is going to be $n_1 = n_2 = n_3 = 0$ For non-trivial solu, determinant must vanish

$$\lambda^{3} - (\sigma_{11} + \sigma_{22} + \sigma_{33}) \lambda^{2} + (\sigma_{11} \sigma_{22} + \sigma_{22} \sigma_{33} + \sigma_{11} \sigma_{33} - \tau_{21}^{2} - \tau_{31}^{2} - \tau_{32}^{2}) \lambda$$

$$-\left(\sqrt{11022033} + 2\sqrt{21022031} - \sqrt{110320202031} - \sqrt{2102033} - \sqrt{21020202020} \right)$$

Cubic equ. -> three roots

$$\lambda_1$$
, λ_2 , λ_3 3 eigenvalues

Substitute
$$\lambda = \lambda_1$$
 \Rightarrow $[\underline{M}] = [\underline{n}_1] = [\underline{n}_{11}]$ \leftarrow eigenvector lst Principal stress
$$\begin{bmatrix} \sigma_{11} - \lambda_1 & \tau_{21} & \tau_{32} \\ \sigma_{22} - \lambda_1 & \tau_{32} \\ \text{sym} & \sigma_{33} - \lambda_1 \end{bmatrix} \begin{bmatrix} \eta_{11} \\ \eta_{21} \\ \eta_{31} \end{bmatrix} = \begin{bmatrix} \sigma \\ 0 \\ 0 \end{bmatrix}$$

 $n_{11}^{2} + n_{21}^{2} + n_{31}^{2} = 1$ — the magnitude of the eigenvector is taken as 1

 $[n_1] \rightarrow$ is the outward normal of the 1st principal plane

Substitute
$$\lambda = \lambda_2$$
 \Rightarrow $\underline{N} = \underline{N}_2 = \begin{bmatrix} n_{12} \\ n_{22} \end{bmatrix} \leftarrow \text{eigenvector } 2$

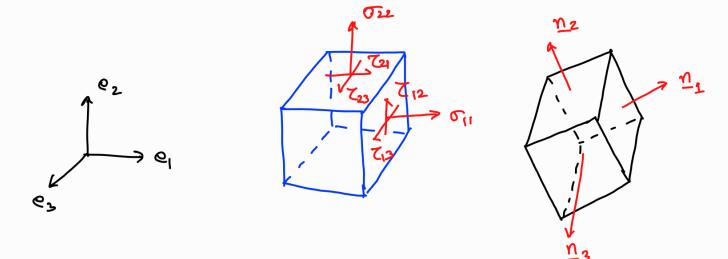
1st Principal stress
$$\begin{bmatrix} \sigma_{11} - \lambda_2 & \tau_{21} & \tau_{31} \\ \sigma_{22} - \lambda_2 & \tau_{32} \end{bmatrix} \begin{bmatrix} n_{12} \\ n_{22} \\ n_{22} \end{bmatrix} = \begin{bmatrix} \sigma \\ 0 \\ 0 \end{bmatrix}$$

Sym $\sigma_{33} - \lambda_2 = \begin{bmatrix} n_{12} \\ n_{22} \\ n_{22} \end{bmatrix} = \begin{bmatrix} \sigma \\ 0 \\ 0 \end{bmatrix}$

 $n_{12}^2 + n_{22}^2 + n_{32}^2 = 1$ — the magnitude of the eigenvector is taken as 1

[n2] -> is the outward normal of the 2nd principal plane

Proposties of principal planes at a point



I) If eigenvalues $\lambda_1 \neq \lambda_2 \neq \lambda_3$ (distinct) $\underline{n}_1 \quad \underline{h} \quad \underline{n}_2 \quad \underline{h} \quad \underline{n}_3$

 $\lambda_1 = \lambda_2 \neq \lambda_3$ (two eigenvalues repeated) $\lambda_1 = \lambda_2 \neq \lambda_3$ (two eigenvalues repeated) $\lambda_1 = \lambda_2 \neq \lambda_3$ (two eigenvalues repeated) $\lambda_1 = \lambda_2 \neq \lambda_3$ (two eigenvalues repeated)

3) $\lambda_1 = \lambda_2 = \lambda_3$ (all eigenvalues repeated)

Every direction is a principal direction

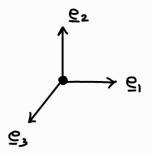
Representation of stress tensor in the coordinate system of its eigenvectors

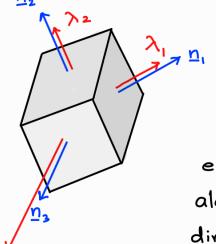
If you choose three mutually perpendicular eigenvectors to be the basis vectors of a coordinate system and then represent the stress tensor in the coordinate system

By definition, the traction on the principal planes will be $\lambda \, \underline{n}$ (no shear components would be present)

The stress matrix will be diagonal when expressed in the coordinate system spanned by principal directions

$$\begin{bmatrix} \underline{G} \\ \underline{G} \\ \underline{G} \\ \underline{G} \\ \underline{G} \end{bmatrix} \begin{pmatrix} \underline{G} \\ \underline{G} \\ \underline{G} \\ \underline{G} \end{pmatrix} = \begin{bmatrix} \underline{\lambda}_1 & 0 & 0 \\ 0 & \underline{\lambda}_2 & 0 \\ 0 & 0 & \underline{\lambda}_3 \end{bmatrix}$$





With a cuboid element's faces along the principal directions, there will be no shear components